



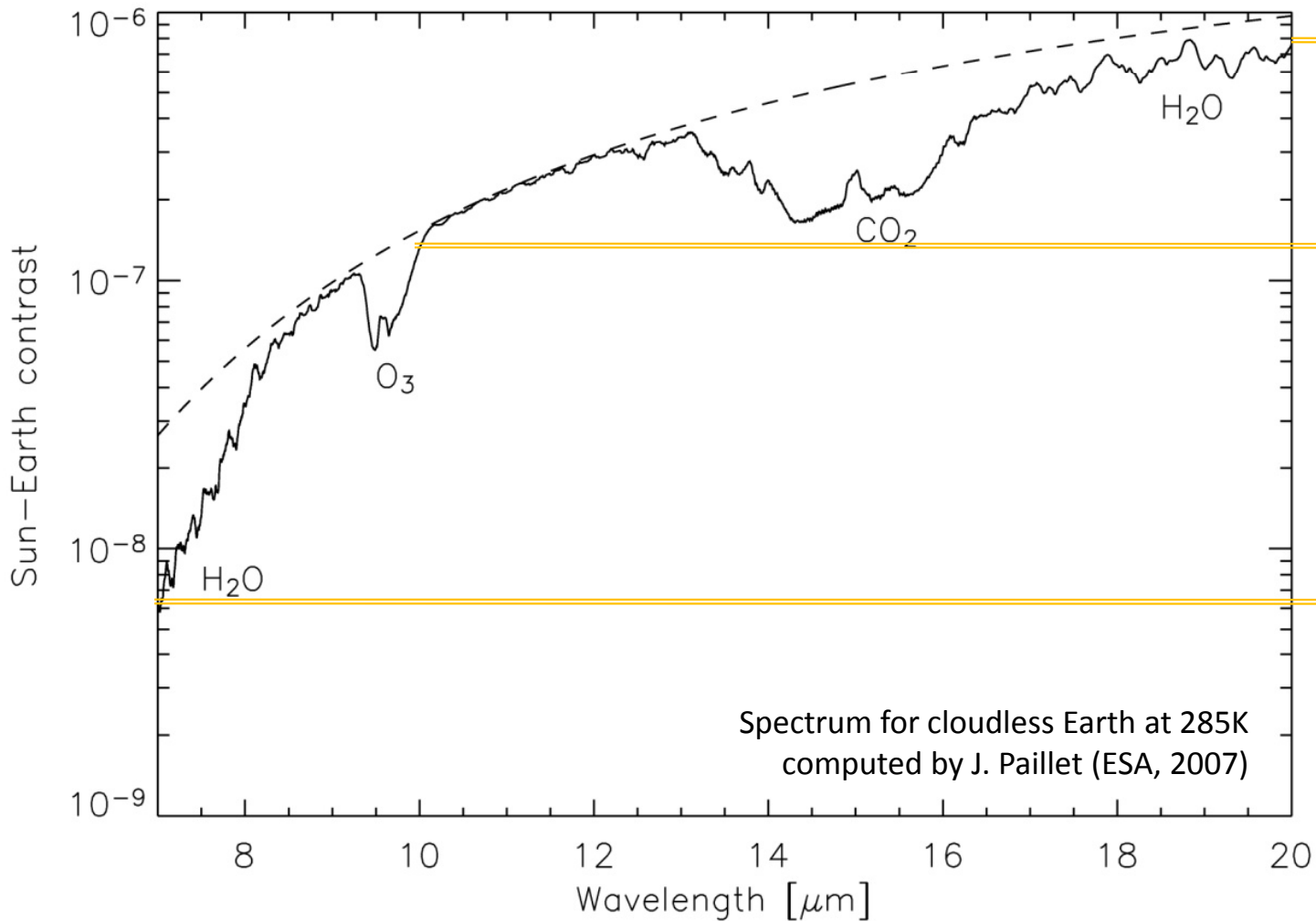
Darwin: required performance

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The Sun-Earth contrast



At 20 μm :
 7.8×10^{-7}
(1.3×10^6)

At 10 μm :
 1.3×10^{-7}
(7.6×10^6)

At 7 μm :
 6.2×10^{-9}
(1.6×10^8)

Required SNR

- During the detection phase
 - SNR of 5 on the integrated waveband
- During the spectroscopic phase ($\lambda/\Delta\lambda=20$)
 - O₃ [9.2 μm -10 μm]: SNR of 5
 - CO₂ [13 μm -16 μm]: SNR of 5
 - H₂O: most critical
 - [6.0 μm -7.2 μm]: SNR of 5 (too difficult \rightarrow discarded)
 - [7.2 μm -8.5 μm]: SNR of 10
- Goal for this study
 - SNR=10 at 7 μm with $\lambda/\Delta\lambda=20$

Geometric nulling: integration times

- Assume Bracewell with minimum baseline = 7m
 - 2 × 2m telescopes and 10% throughput
 - Rotation modulation efficiency ~ 50%
- Put bright fringe on planet (middle of HZ)
- Earth flux: 0.3 ph/m²/s for [7.0μm-7.35μm] at 10pc
- Compute integration time for SNR = 10
 - Closer targets (forced b=7m): integration time does not change
 - Nulling and planetary flux ∝ distance⁻²

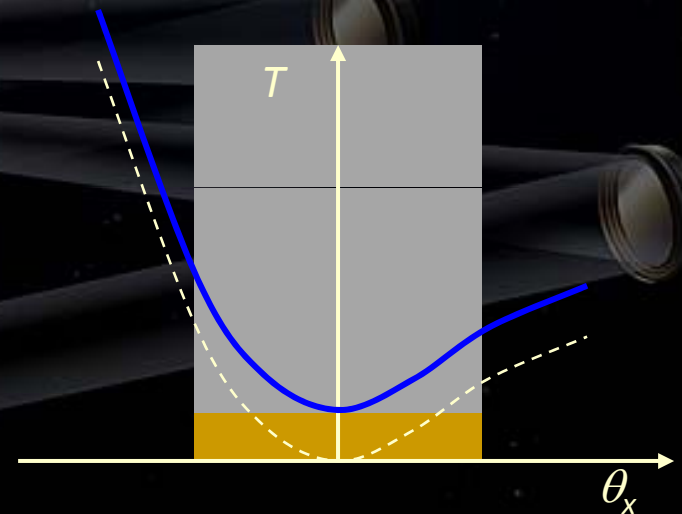
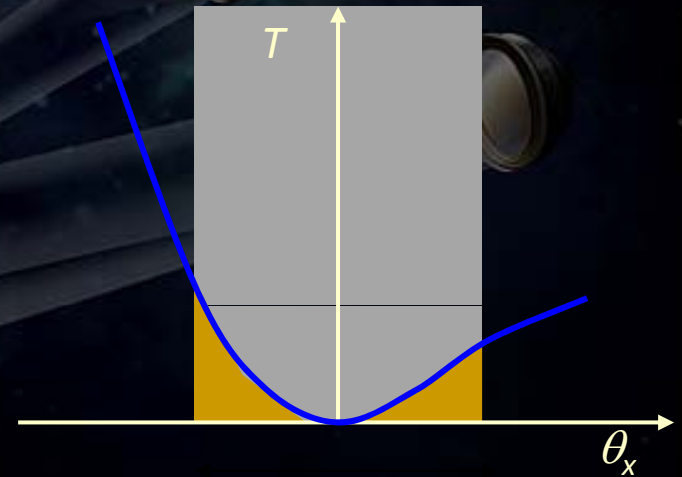
At λ = 7μm	F0V	G0V	K0V	M0V	M5V
Middle of HZ	2.4 AU	1.16 AU	0.68 AU	0.27 AU	0.08 AU
Dist. for b=7m	23 pc	11 pc	6.5 pc	2.6 pc	0.8 pc
Star diameter	0.61 mas	0.93 mas	1.22 mas	2.15 mas	3.14 mas
Nulling ratio	5.2e-6	1.2e-5	2.1e-5	6.8e-5	1.5e-4
Contrast	2.1e-9	5.0e-9	1.0e-8	2.8e-8	1.8e-7
Integration time	57 days	13 days	3.9 days	0.7 days	0.02 days

CONCLUSION #1

- No fundamental show-stopper to H₂O spectroscopy around Sun-like stars with θ^2 configurations
- Warning: availability of short baselines is crucial
 - A minimum baseline of 20m would ruin the performance
- We will assume a K0V star in the following study

The various flavours of stellar leakage

- Geometric stellar leakage
→ set by target
- Instrumental stellar leakage
 - Avg removed by rotation
 - Shot noise remains
 - Requirement: smaller than geometric leakage
 - Fluctuations: instability noise
 - Instrumental imperfections
 - Amplitude and phase of beams
 - Polarisation errors
 - Collector position
 - Requirement: SNR of 10 →
 $\sigma(\text{null}) < \text{flux ratio}/10$



CONCLUSION #2

- Requirements on
 - Mean instrumental leakage: $\langle \text{null} \rangle < 2 \times 10^{-5}$
 - Instability noise: $\sigma_{\text{null}} < 10^{-9}$ on 60 days
- The latter is (almost) always dominant

“Naive” stability requirements

- Separating each individual contribution
- Assuming that $\sigma_{\text{null}} \approx \langle \text{null} \rangle$

	Phase	Intensity	Polarisation
Analytical null	$\Delta\phi^2/4$	$\Delta I^2/16$	$\Delta\theta^2/4$
Result at 7 μm for null = 10^{-9}	$\Delta\text{OPD} <$ 0.07 nm rms	$\Delta I < 0.01\%$ rms	Diff. rotation < 13'' rms

- Does not seem within reach
 - But note: to measure them is to correct them!

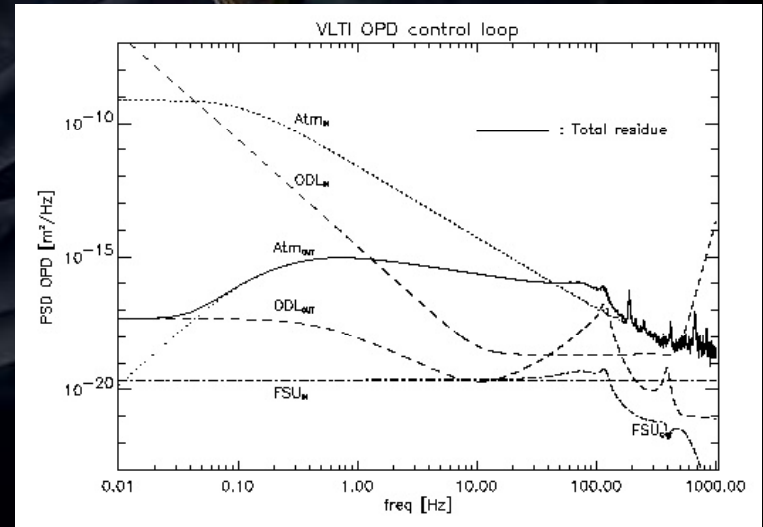
Relaxing the requirements with time

- Back to definition: $\sigma_{\text{null}} = \sigma_{\text{leakage}} / F_{\star}$
- Time behaviour depends on power spectra of all instrumental perturbations
- Naive assumption: white noise
 - $\sigma_{\text{leakage}}(t) \propto t^{1/2}$, while $F_{\star}(t) \propto t$
 - $\sigma_{\text{null}} \propto t^{-1/2} \rightarrow \sigma_{\text{null}} = 2.3 \times 10^{-6}$ in 1 sec
- Revised requirements on a 1 sec integration time

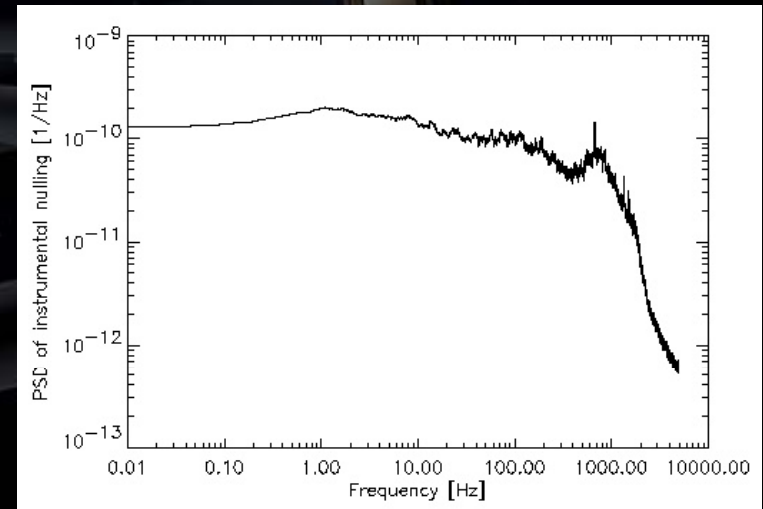
	Phase	Intensity	Polarisation
Result at $7\mu\text{m}$ for 1 sec integration	$\Delta\text{OPD} <$ 3.4nm rms	$\Delta I <$ 0.6% rms	Diff. rotation < 10' rms

Is white noise realistic?

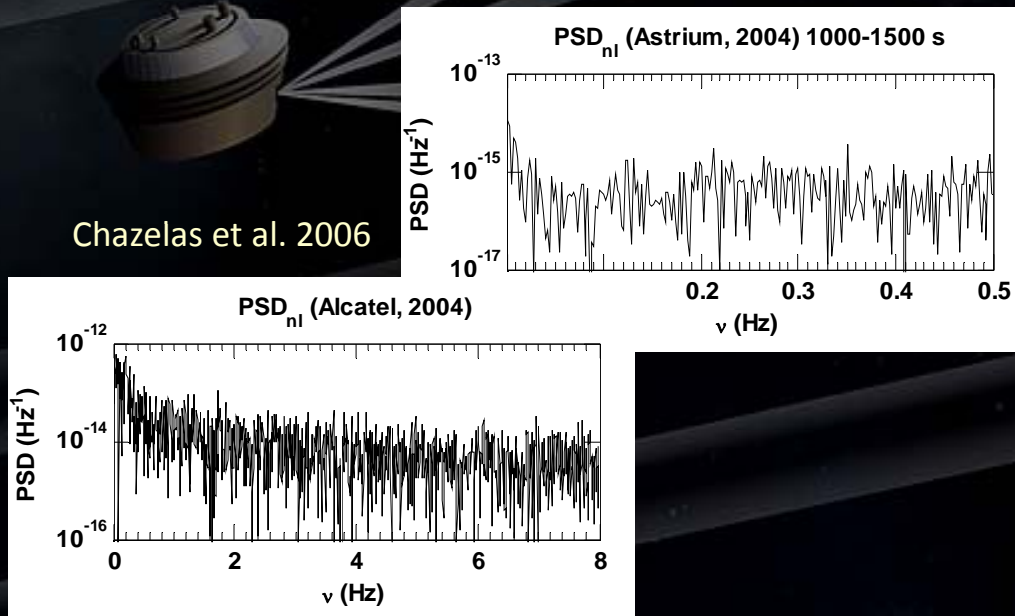
- Control loops simulations
 - Power reduced at low frequencies
- Tests in laboratory
 - White noise within reach
 - Control loop drifts?



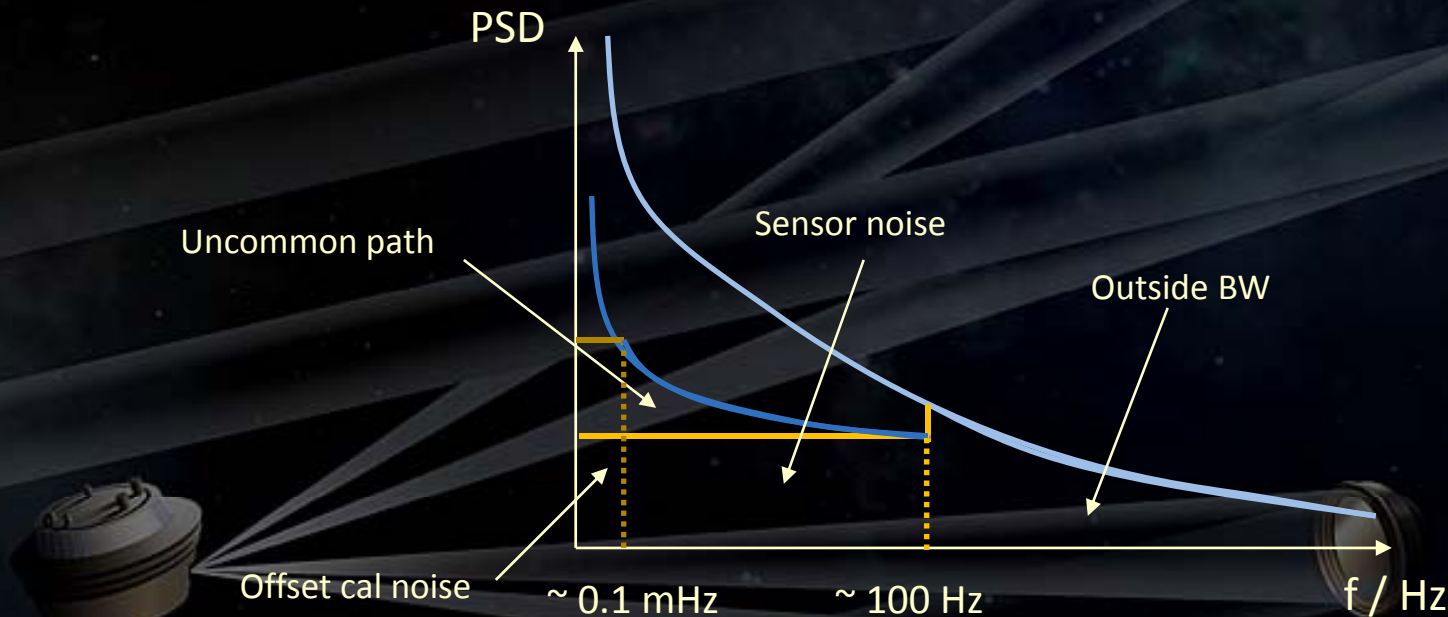
Absil et al. 2006 (GENIEsim)



Chazelas et al. 2006



Fighting long-term drifts



- Control can be based on the nulled output
 - Produce offsets in phase and amplitude to re-centre the null with a low frequency

CONCLUSION #3

- Stability requirements in 1 sec
 - OPD $< 3.4\text{nm rms}$
 - Intensity mismatch $< 0.6\% \text{ rms}$
- Requires white noise for frequencies $< 1\text{Hz}$
 - Control loops + correction of long-term drifts

Instability noise: advanced description

- Expansion of instrumental null (Lay 2004)
- If $\eta =$ template with odd harmonics, the demodulated output:

$$\begin{aligned}
 \delta N_* &\approx \sum_j \left[\frac{\partial N_*}{\partial A_j} A_j \delta a_j + \frac{\partial N_*}{\partial \phi_j} \delta \phi_j + \frac{\partial N_*}{\partial x_j} \delta x_j \right. \\
 &\quad \left. + \frac{\partial N_*}{\partial y_j} \delta y_j \right] + \sum_j \sum_k \left[\frac{1}{2} \frac{\partial^2 N_*}{\partial A_j \partial A_k} A_j A_k \delta a_j \delta a_k \right. \\
 &\quad \left. + \frac{\partial^2 N_*}{\partial A_j \partial \phi_k} A_j \delta a_j \delta \phi_k + \frac{1}{2} \frac{\partial^2 N_*}{\partial \phi_j \partial \phi_k} \delta \phi_j \delta \phi_k \right] \\
 &\approx \sum_j C_{A_j}^* \delta a_j + C_{\phi_j}^* \delta \phi_j + C_{x_j}^* \delta x_j + C_{y_j}^* \delta y_j \\
 &\quad + \sum_j \sum_k [C_{AA_{jk}}^* \delta a_j \delta a_k + C_{A\phi_{jk}}^* \delta a_j \delta \phi_k \\
 &\quad + C_{\phi\phi_{jk}}^* \delta \phi_j \delta \phi_k]. \tag{14}
 \end{aligned}$$

$$O = O_{\text{planet}} + O_{\text{ran}} + O_{\text{sys}}$$

$$O_{\text{planet}} = \frac{1}{T} \int_0^T N_{\text{planet}} \eta dt = \widehat{N_{\text{planet}}}$$

$$\begin{aligned}
 O_{\text{sys}} &= \sum_j C_{A_j} \widehat{\delta a_j} + C_{\phi_j} \widehat{\delta \phi_j} + C_{x_j} \widehat{\delta x_j} + C_{y_j} \widehat{\delta y_j} \\
 &\quad + \sum_j \sum_k [C_{AA_{jk}} \widehat{\delta a_j \delta a_k} + C_{A\phi_{jk}} \widehat{\delta a_j \delta \phi_k} \\
 &\quad + C_{\phi\phi_{jk}} \widehat{\delta \phi_j \delta \phi_k}], \tag{38}
 \end{aligned}$$

- 1st order terms close to zero \rightarrow 2nd order not negligible

- Variance:

$$\begin{aligned}
 \langle O_{\text{sys}}^2 \rangle &= \sum_j C_{A_j}^2 \langle \widehat{\delta a_j}^2 \rangle + \sum_j C_{\phi_j}^2 \langle \widehat{\delta \phi_j}^2 \rangle + \sum_j C_{x_j}^2 \langle \widehat{\delta x_j}^2 \rangle \\
 &\quad + \sum_j C_{y_j}^2 \langle \widehat{\delta y_j}^2 \rangle + \sum_j \sum_k C_{AA_{jk}}^2 \langle \widehat{\delta a_j \delta a_k}^2 \rangle \\
 &\quad + \sum_j \sum_k C_{A\phi_{jk}}^2 \langle \widehat{\delta a_j \delta \phi_k}^2 \rangle \\
 &\quad + \sum_j \sum_k C_{\phi\phi_{jk}}^2 \langle \widehat{\delta \phi_j \delta \phi_k}^2 \rangle. \tag{39}
 \end{aligned}$$

Influence on power spectra

- Expansion in Fourier series
($T = \text{rot. period}$)

$$\delta a_j = \sum_{p=-\infty}^{\infty} \beta_p \exp(i2\pi p t/T).$$

$$\langle |\beta_p|^2 \rangle \approx \frac{1}{2T} \text{PSD}_e\left(\frac{p}{T}\right),$$

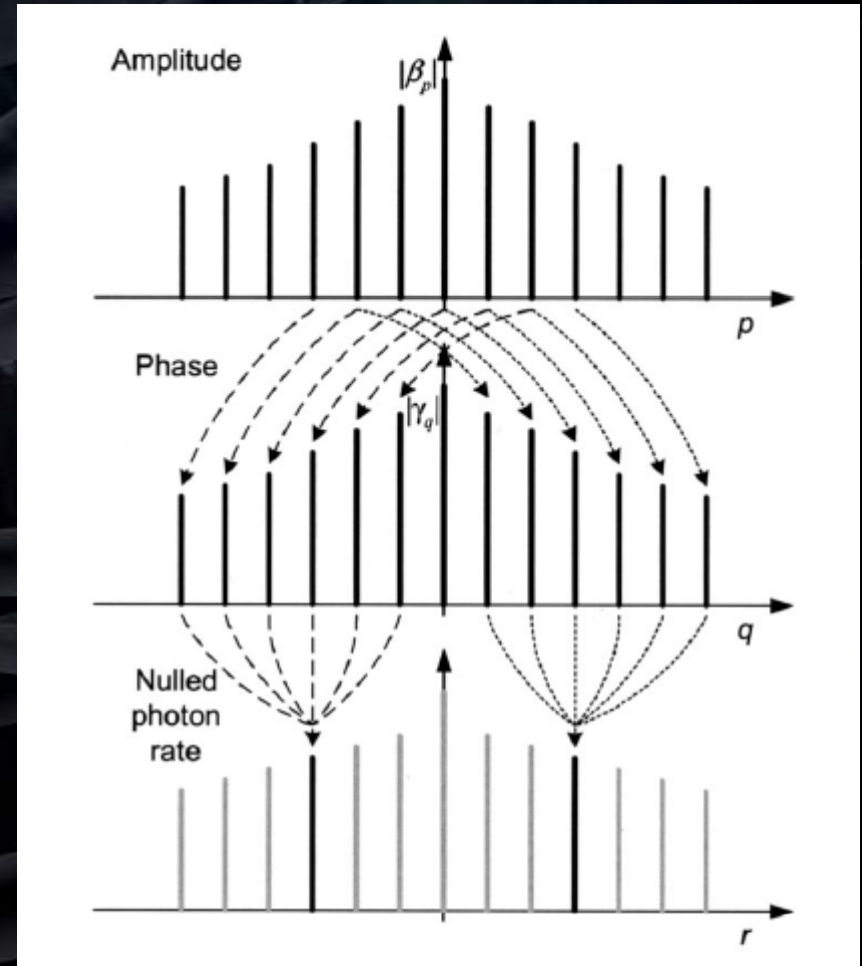
$$\eta = \sum_{r=-\infty}^{\infty} \varepsilon_r \exp(i2\pi r t/T).$$

- Linear terms
 - Only at planet frequency

$$\langle \widehat{\delta a_j}^2 \rangle = \left\langle \left[\int_0^T \delta a_j \eta dt \right]^2 \right\rangle = \sum_{r=-\infty}^{\infty} |\varepsilon_r|^2 \langle |\beta_r|^2 \rangle.$$

- Bilinear/quadratic terms
 - At all frequencies

$$\begin{aligned} \langle \widehat{\delta a_j \delta \phi_k}^2 \rangle &= \left\langle \left[\int_0^T \delta a_j \delta \phi_k \eta dt \right]^2 \right\rangle \\ &= \sum_{r=-\infty}^{\infty} |\varepsilon_r|^2 \sum_{p=-\infty}^{\infty} \langle |\beta_p|^2 \rangle \langle |\gamma_{p-r}|^2 \rangle. \end{aligned}$$

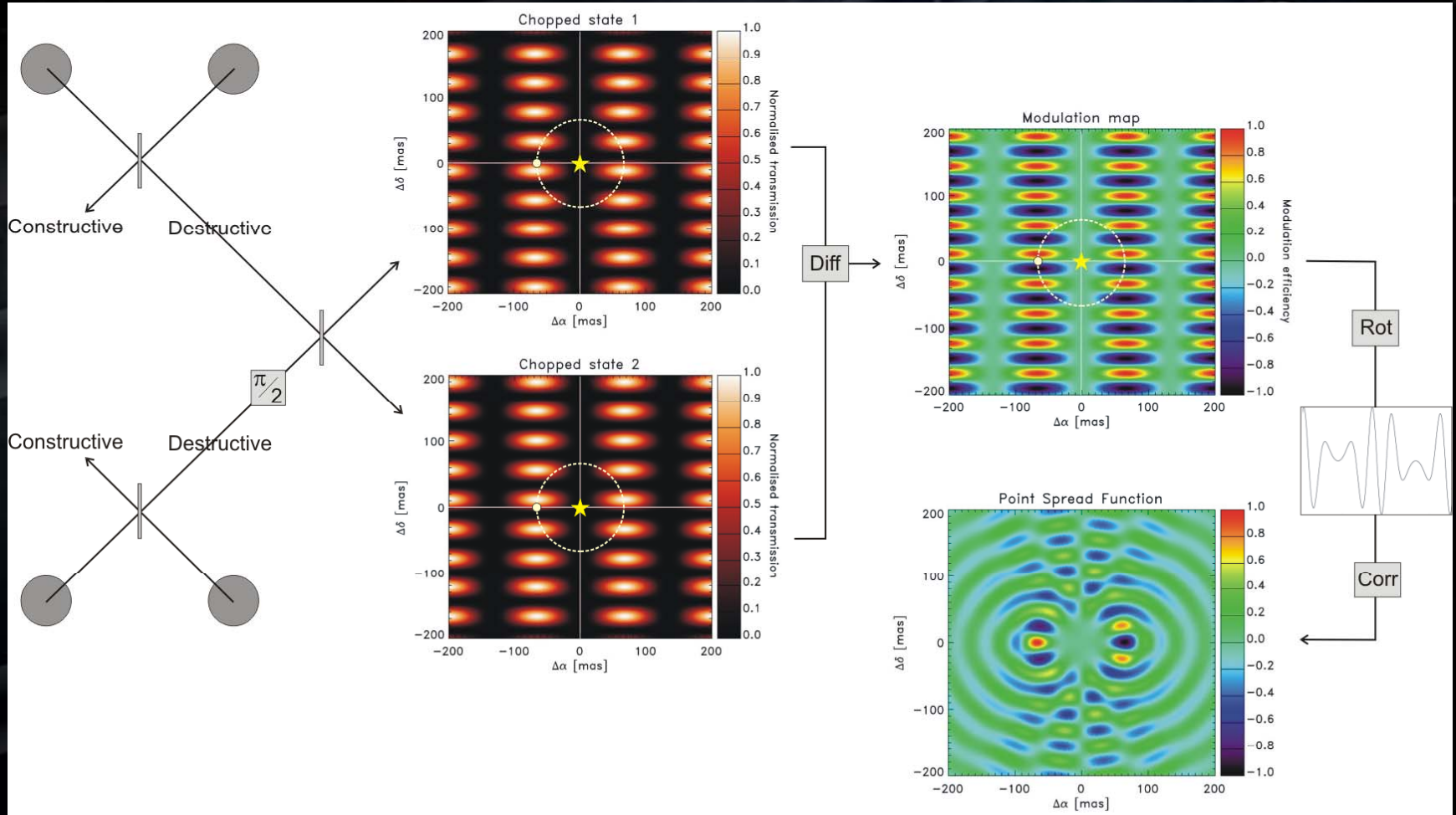


Ex: phase at 100Hz, amplitude at 101Hz \rightarrow beating at 1Hz

CONCLUSION #4

- Bilinear/quadratic terms in phase and amplitude
 - Dominant contribution in instability noise
 - Convolution of power spectra (~~a posteriori correction~~)
- Naive approach is simply not valid
 - $\sigma_{\text{null}} \neq \langle \text{null} \rangle$
 - All frequencies do not contribute in the same way

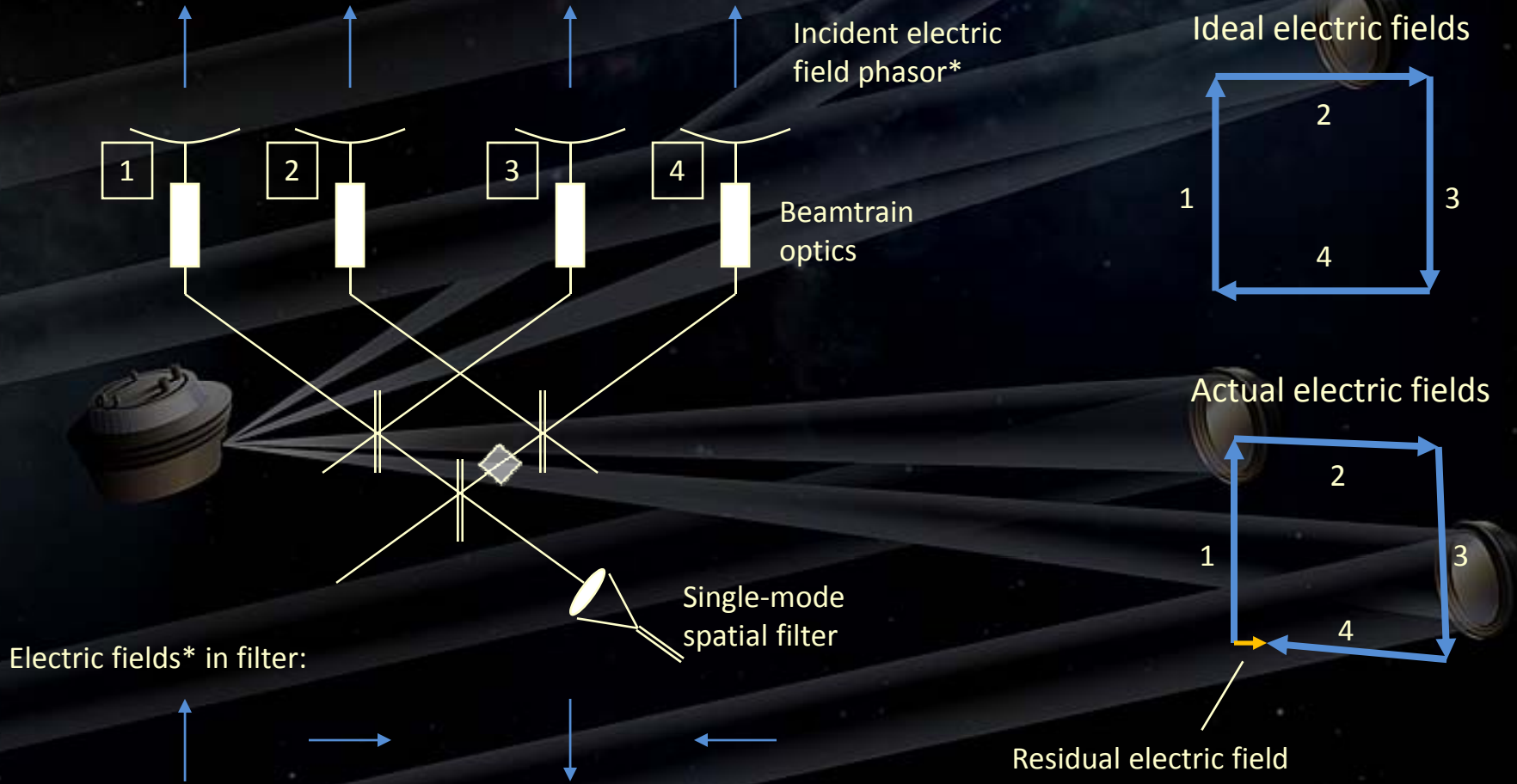
Introducing phase chopping



A different view: electric fields



Plane wavefront from star

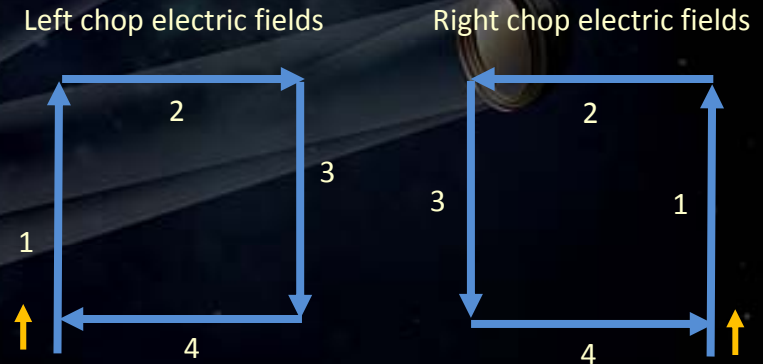


* Phasor angle represents electric field phase, not polarization

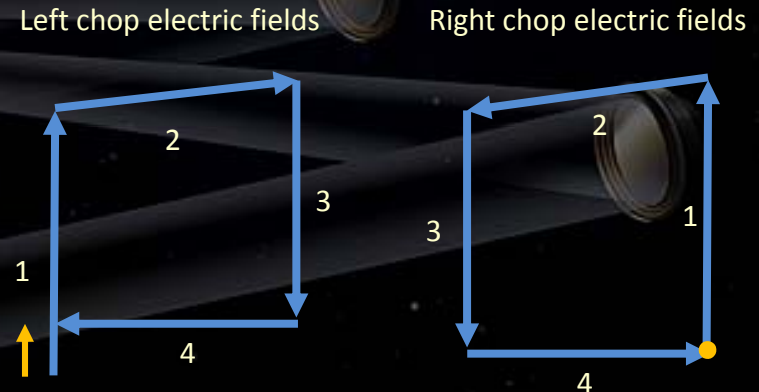
Influence of phase chopping (Lay '04)

- Removes the “symmetric part” of instability noise
 - Pure amplitude errors and pure quadratic phase errors
 - Polarisation errors
 - Collector position errors
- 1st order phase errors and bilinear phase-amplitude errors remain
 - Most important contributors
 - PSDs mix together as in rotational case
- Other “instrumental” contributions
 - Stray light, thermal emission, detector drifts
 - Mean value cancelled by phase chopping
 - Low-frequency drifts also cancelled
 - Beware of chop asymmetry

(a) Pure amplitude errors

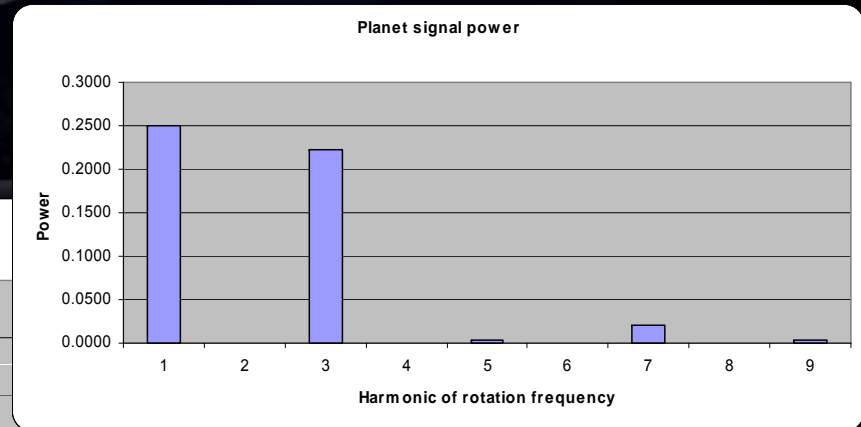
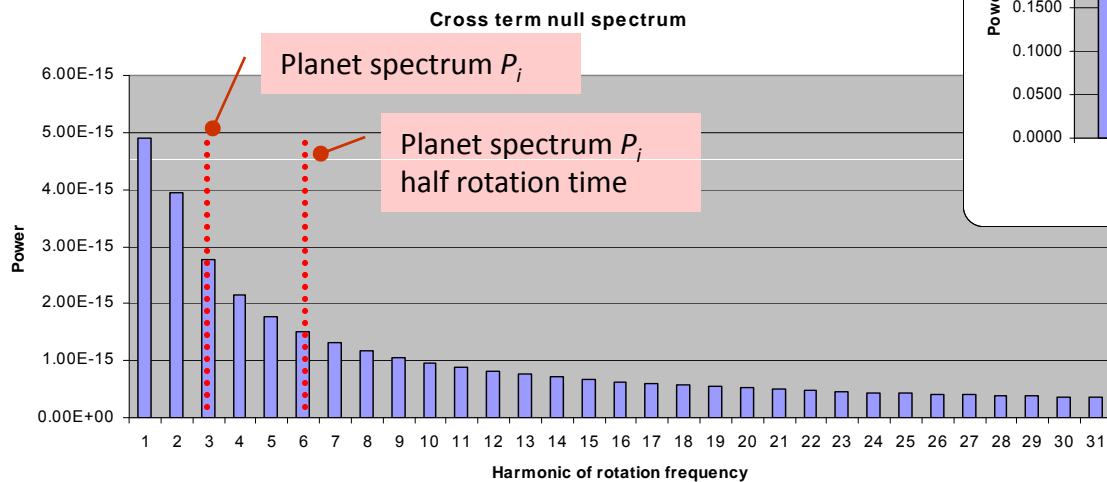


(b) Phase-amplitude cross term



Effect of rotation on a chopped array

- If systematic noise not correlated to rotation
 - $\text{SNR} \propto n_{\text{rot}}^{1/2}$ (optimistic)
- Higher rotation speed shifts the planet signal to higher frequencies
 - (Small) gain if noise $\propto 1/f$



Revised stability requirements

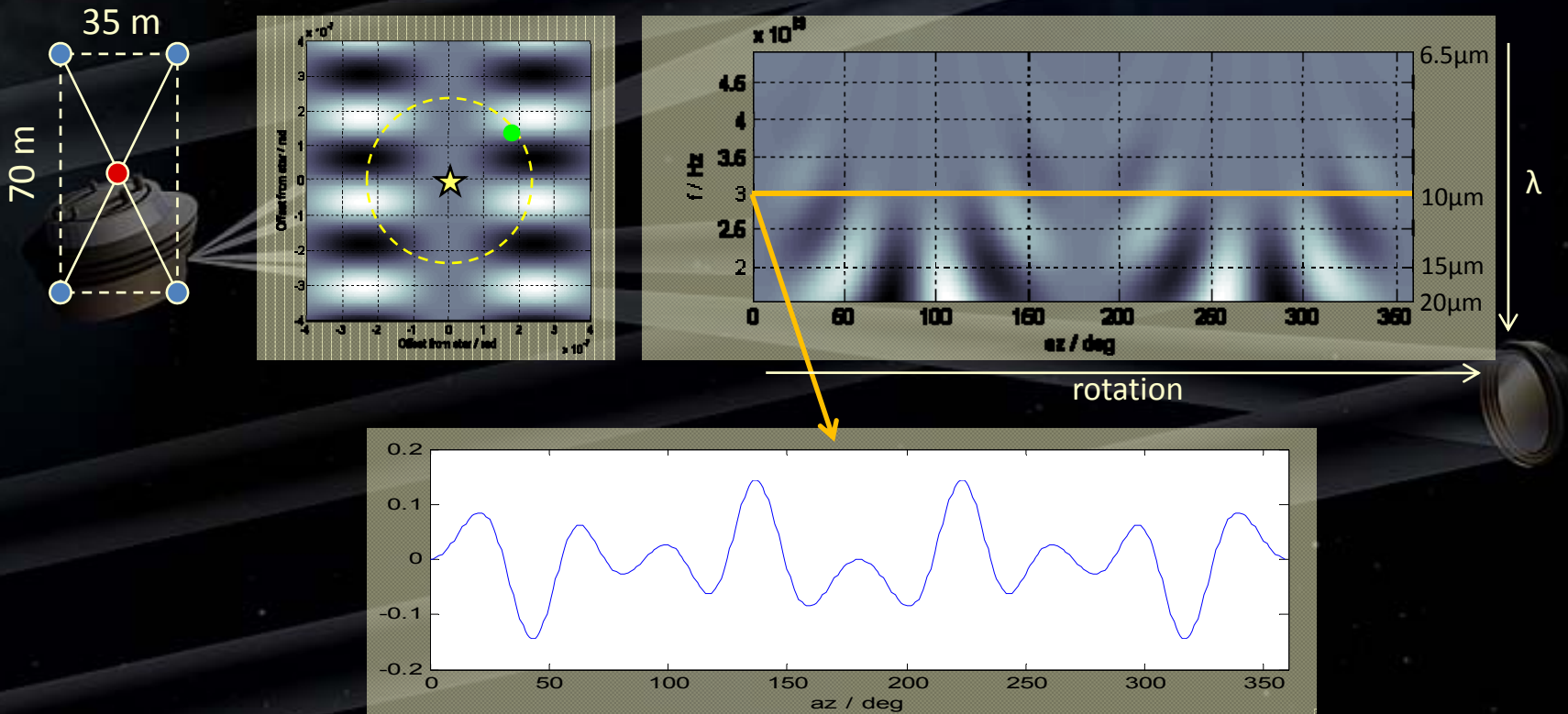
- Analytical approach becomes complicated
 - Computation of sensitivity coefficients
 - Analytical or tabulated description of input power spectra across “infinite” frequency domain
- Lay 2004 (Applied Optics)
 - Sun-Earth at 15pc, $\lambda=10\mu\text{m}$, $R=20$
 - Dual Bracewell, 4m diameter, 0.5 day integration
 - Assumes $1/f$ power spectra with no DC
 - Requirements for O_3 spectroscopy
 - OPD: 1.5nm rms
 - Intensity: 0.1% rms

CONCLUSION #5

- Revised requirements: 1.5nm, 0.1% (eq. null = 5×10^{-7})
 - Challenging at $10\mu\text{m}$ \rightarrow unrealistic at $7\mu\text{m}$?
- Need to be revisited
 - Configuration and target parameters
 - Realistic power spectra (1/f is pessimistic)
- Noise reduction techniques should be investigated

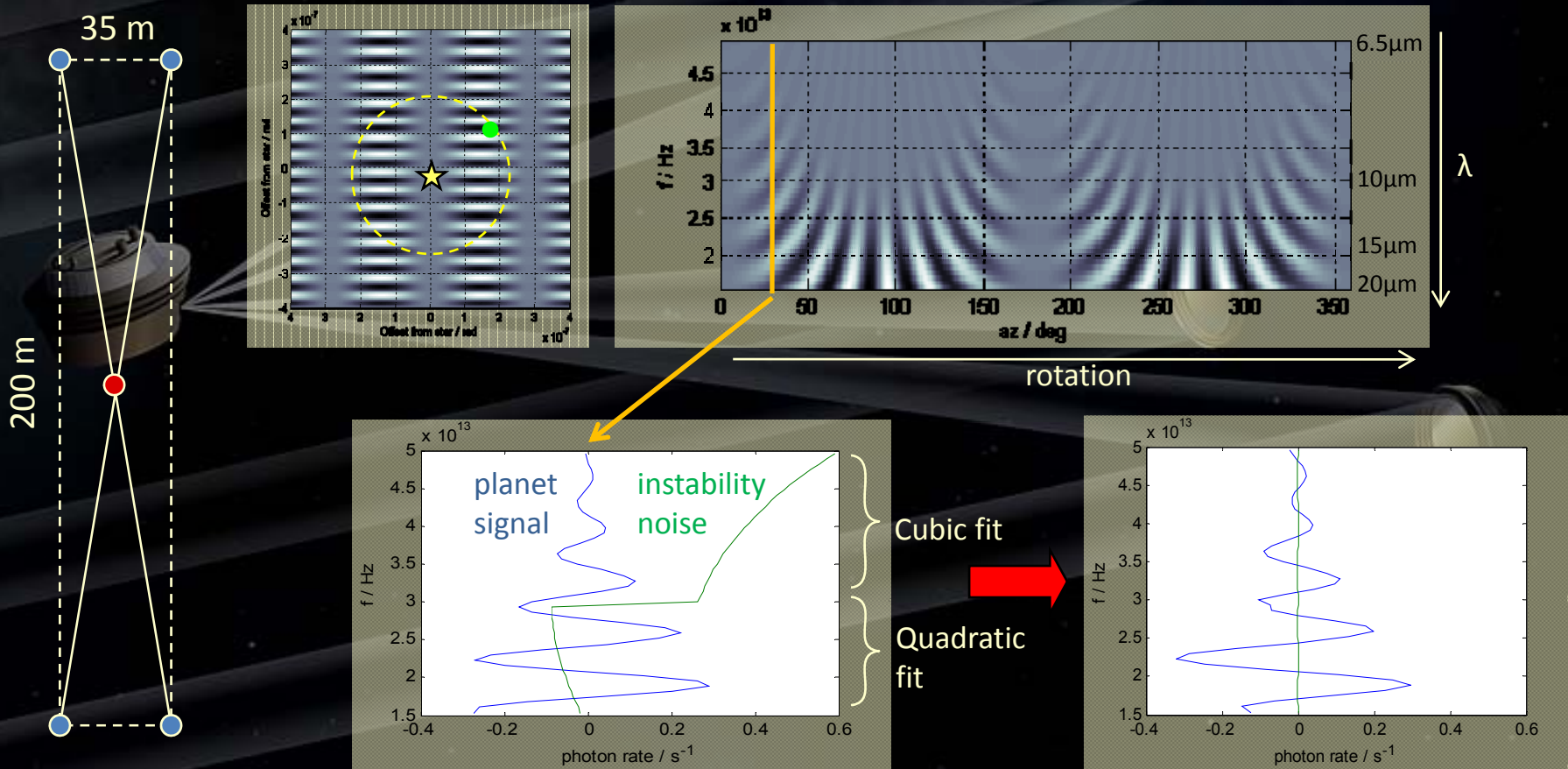
Spectral fitting (Lay 2006)

- Separating signal and noise in time domain is challenging
 - Noise contributions at all frequencies



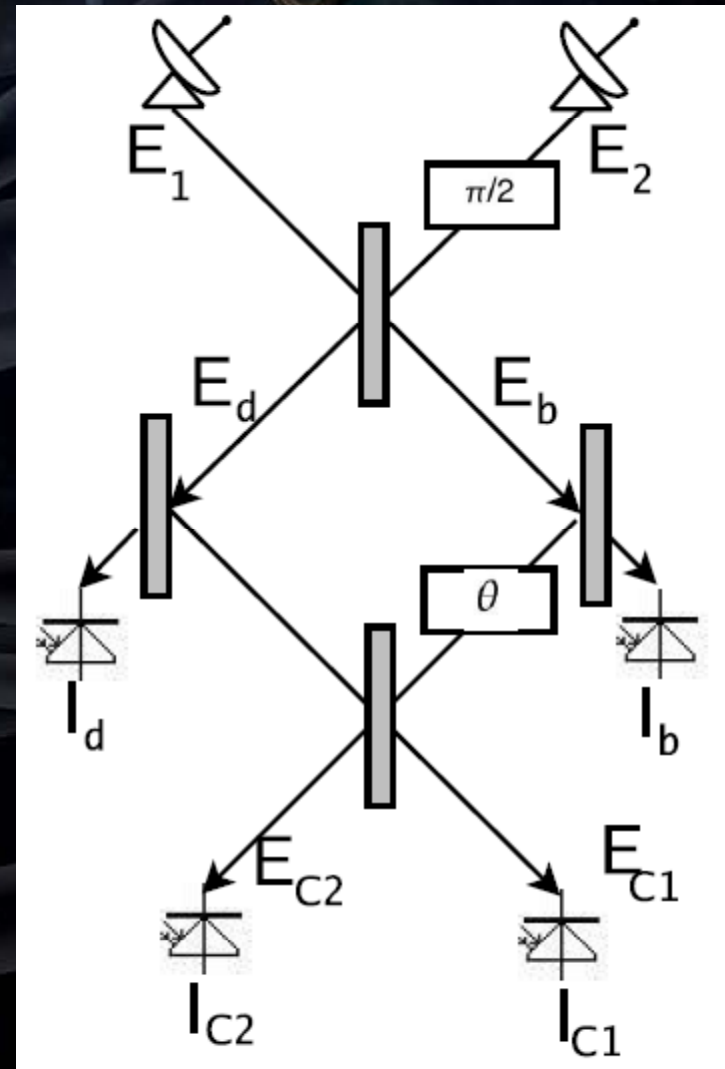
Spectral fitting (Lay 2006)

- Separation in wavelength domain easier
 - Instability noise is a slow function of λ
 - Need to stretch the array and to fit the noise



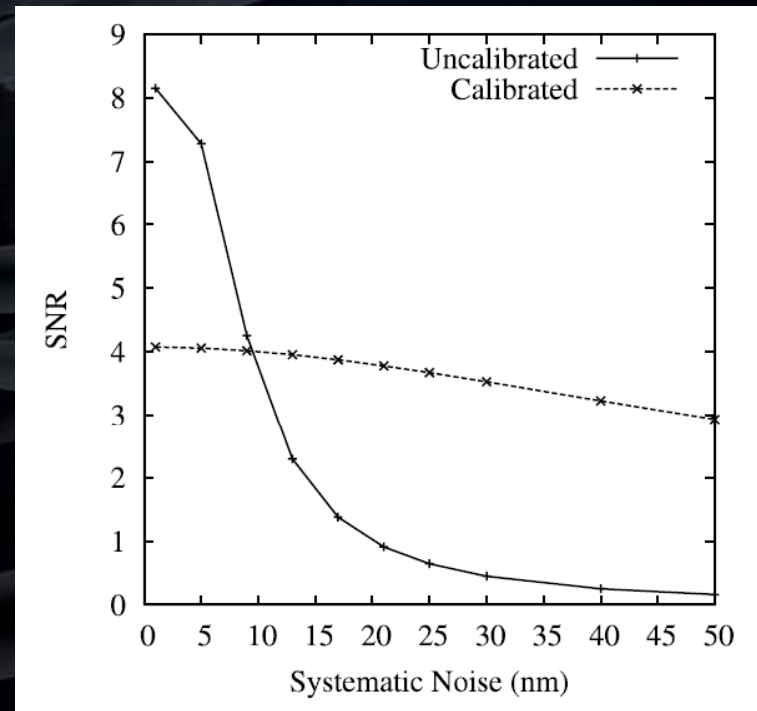
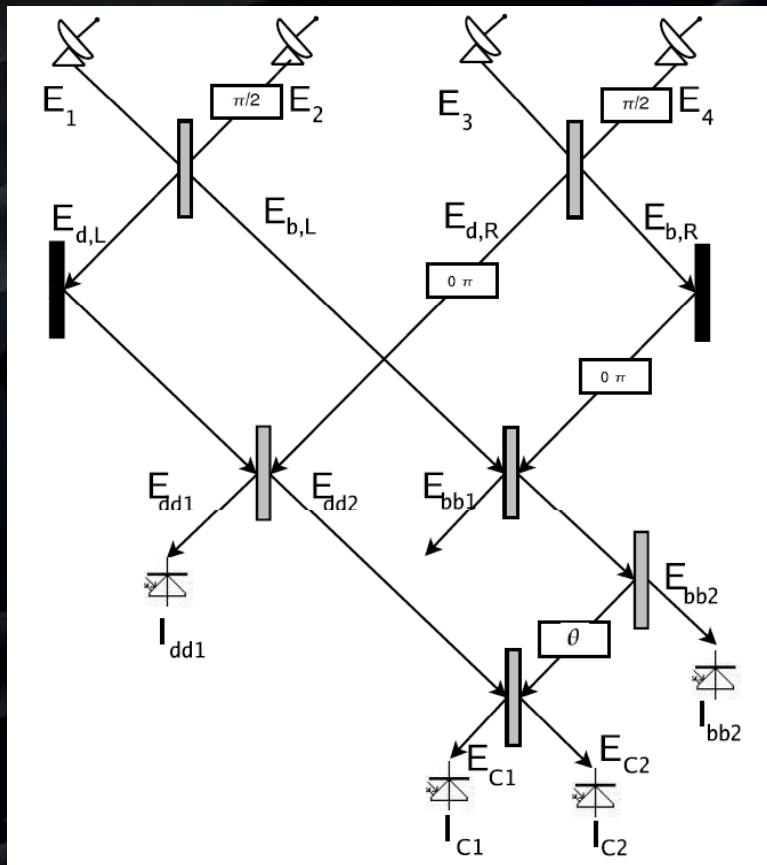
Post-nulling calibration (Lane 2006)

- Based on coherence properties of stellar light
 - Calibration interferometer with the two outputs
 - Modulation of θ
 - Fringe pattern forms
 - Star and planet separately
 - Fringes ratio: $\langle \text{null} \rangle^{0.5} F_{\star} / F_p$
 - Estimation of stellar leakage is possible
 - Can be subtracted from destructive output a posteriori



Post-nulling calibration (Lane 2006)

- Straightforward adaptation to the X-array
- May not be appropriate for low perturbations



CONCLUSION #6

- Instability noise reduction techniques
 - Stability requirement could be driven by $\langle \text{null} \rangle$ instead of σ_{null}
 - New requirements about 5nm rms and 0.5% rms (?)
 - Part of the planetary signal is lost
 - Further testing required (simulations and lab)

What needs to be done?

- Make sure that H₂O at 7μm is really needed
 - Dropping it would relax the stability requirements
- Update the Lay 2004 analysis at 7μm
 - Seems easy with Oliver's spreadsheets
- Validation with numerical simulations
 - DarwinSim: the machinery is already available!
 - Control loops properly described
 - Need accurate modelling of input power spectra
 - May require FEM study of Darwin spacecrafts
 - Include the effect of noise reduction techniques
- Validation on test benches (PRIORITY!)
 - Under "space-like" conditions
 - Star/planet simulator and proper data reduction