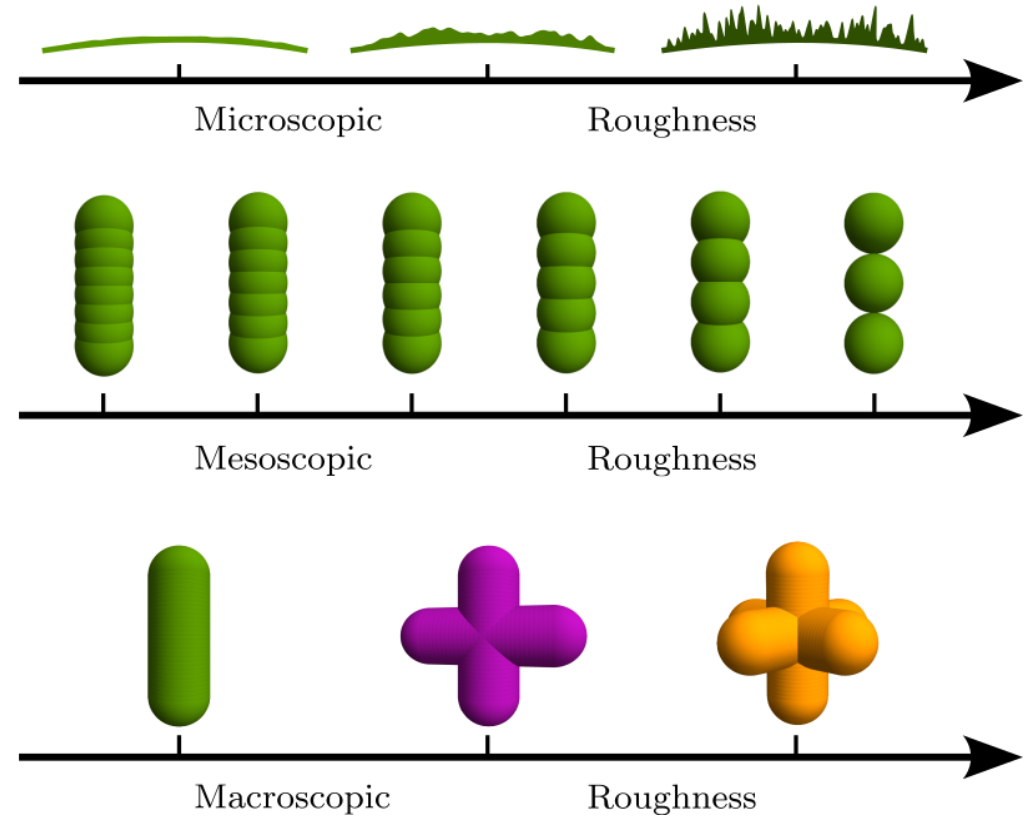


Impact of Particle Roughness on Packing

Adrien Luyckx, Eric Opsomer

10 March 2026, DPG Dresden 2026

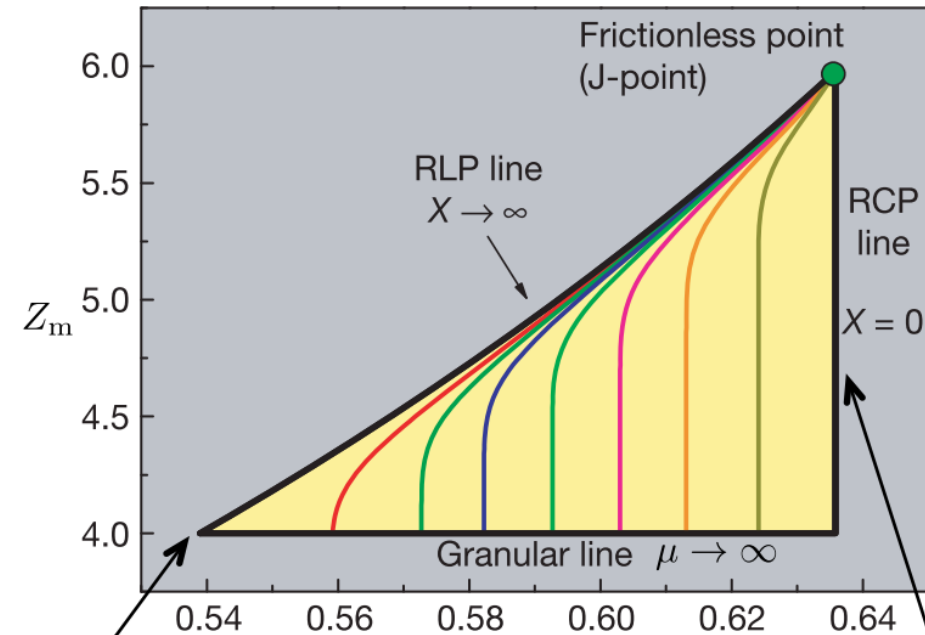


Historical context



- Z_m : Number of contacts
- X : Compactivity (large $X \sim$ loose configuration)
- μ : Friction coefficient

- Friction affects packing fraction
 - RLP : high friction
 - RCP : low friction

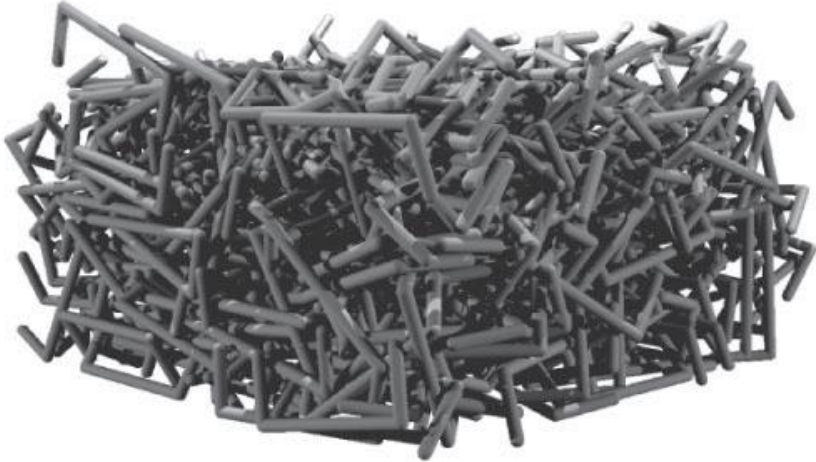


$$\phi_{rlp} = \frac{1}{1 + \sqrt{3}/2} \approx 0.536$$

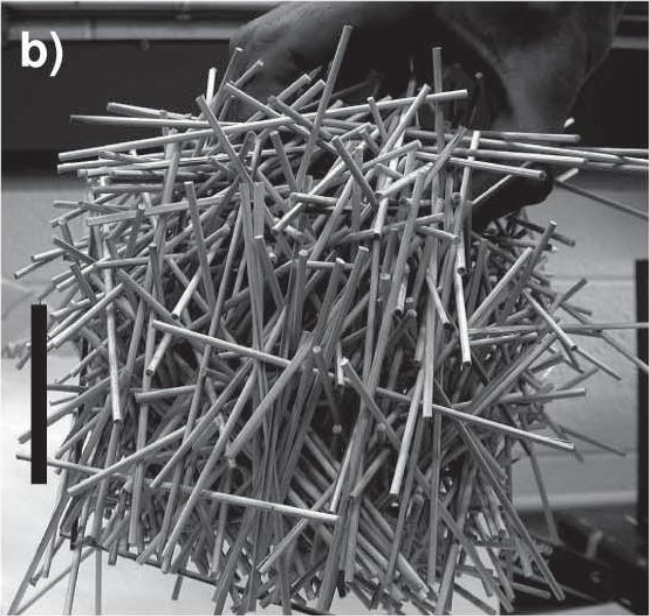
$$\phi_{rcp} = \frac{1}{1 + \sqrt{3}/3} \approx 0.634$$

Baule, A. et al. (2018). Edwards statistical mechanics for jammed granular matter. Reviews of Modern Physics

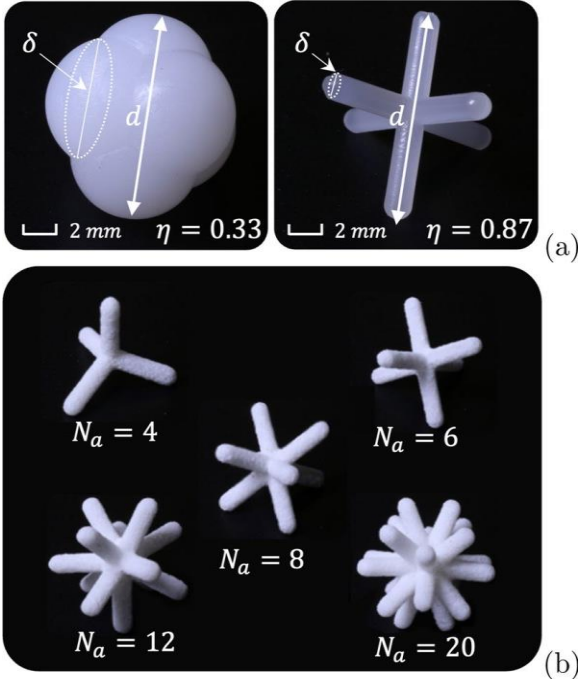
Historical context



Gravish, N. et al. (2012). Entangled Granular Media. Physical Review Letters

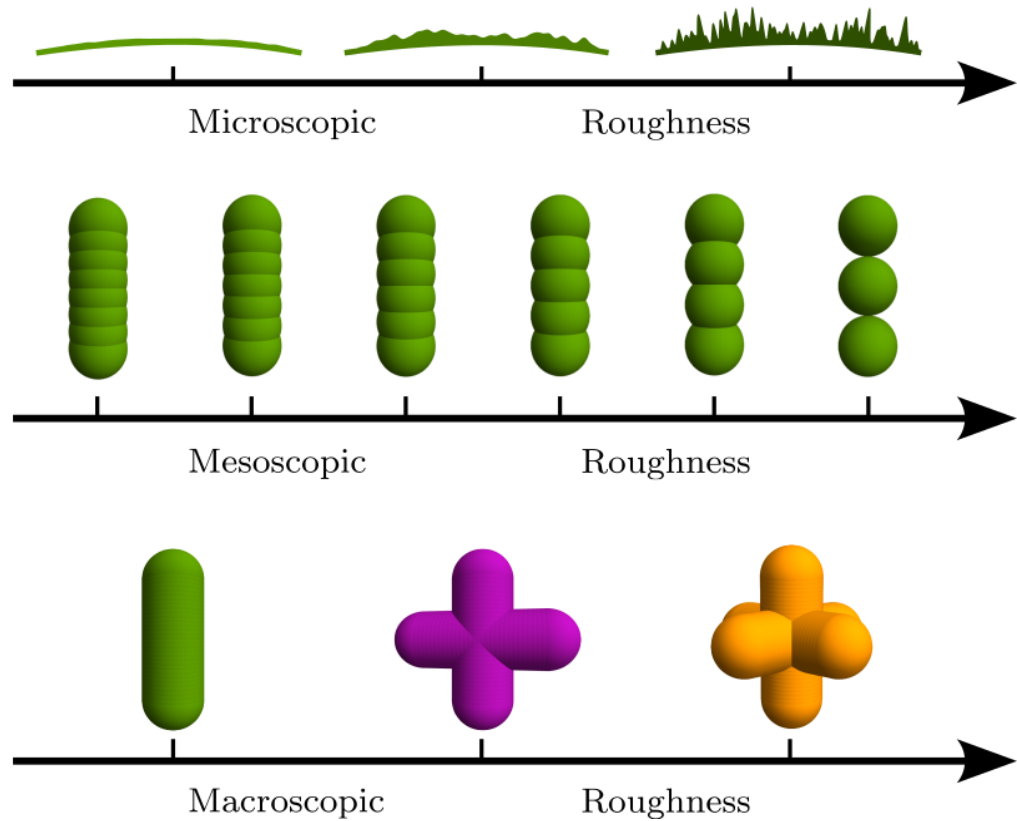


Blouwolff, J. et al. (2006). The coordination number of granular cylinders. Europhysics Letters

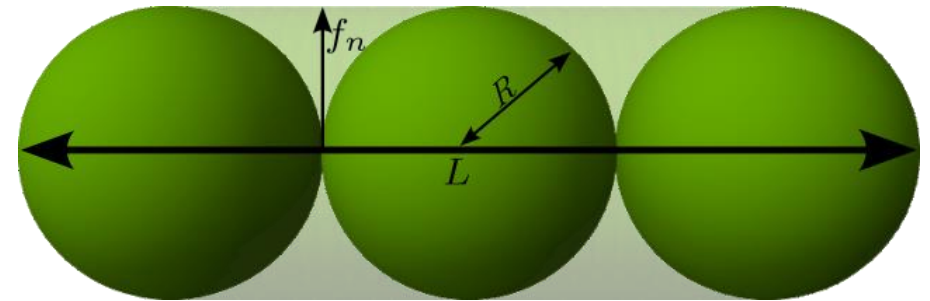


Aponte, D. et al. (2025). Experimental exploration of geometric cohesion and solid fraction in columns of highly non-convex Platonic polytops. Granular Matter

Roughness



Simple parameter



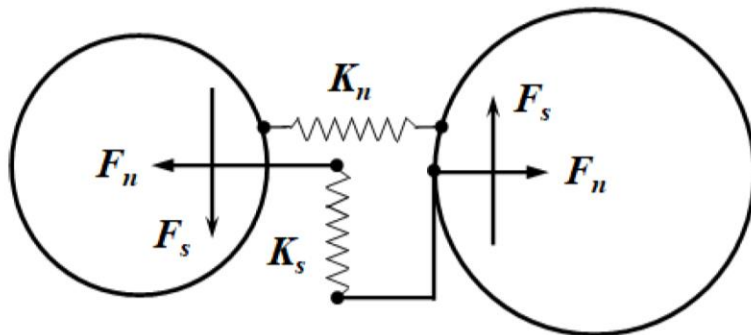
$$\mu_{\text{meso}} = 1 - \frac{f_n}{R}$$

Discrete Element Modeling

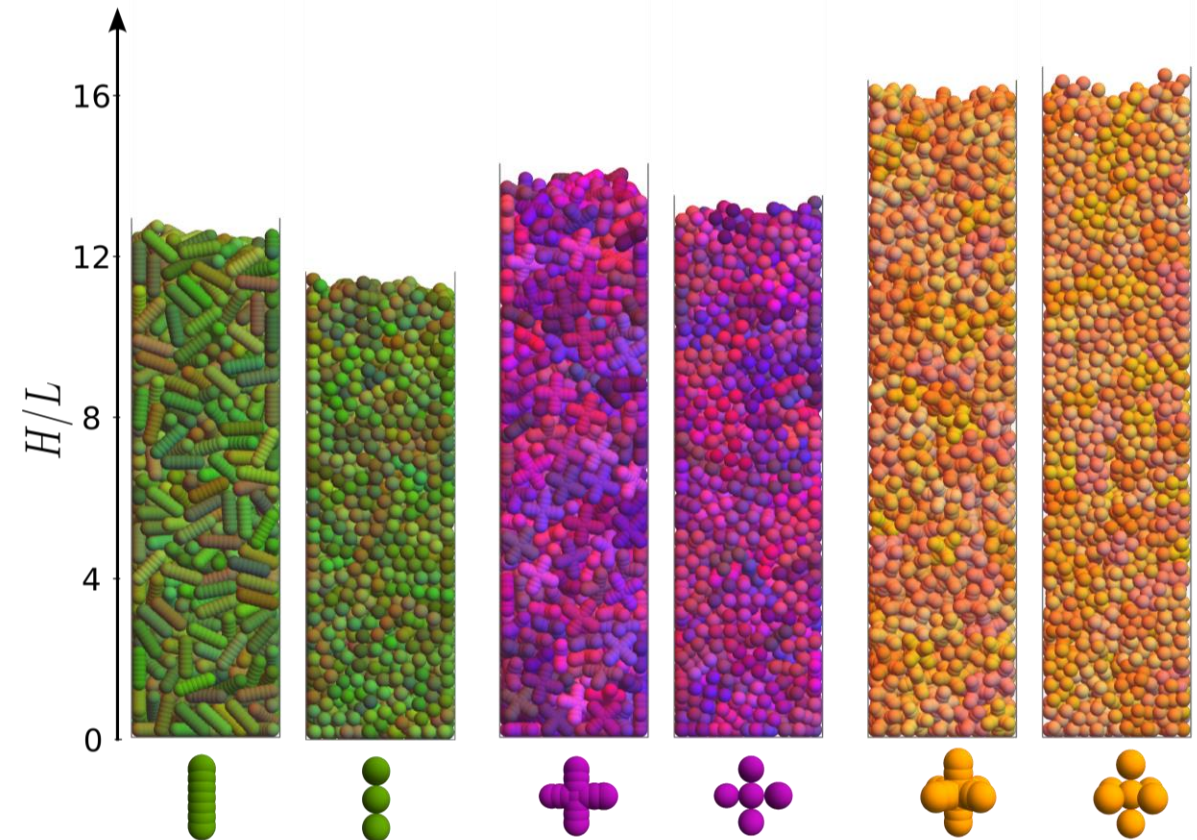


- Random placing
- Gravity deposition
- Hertzian contact

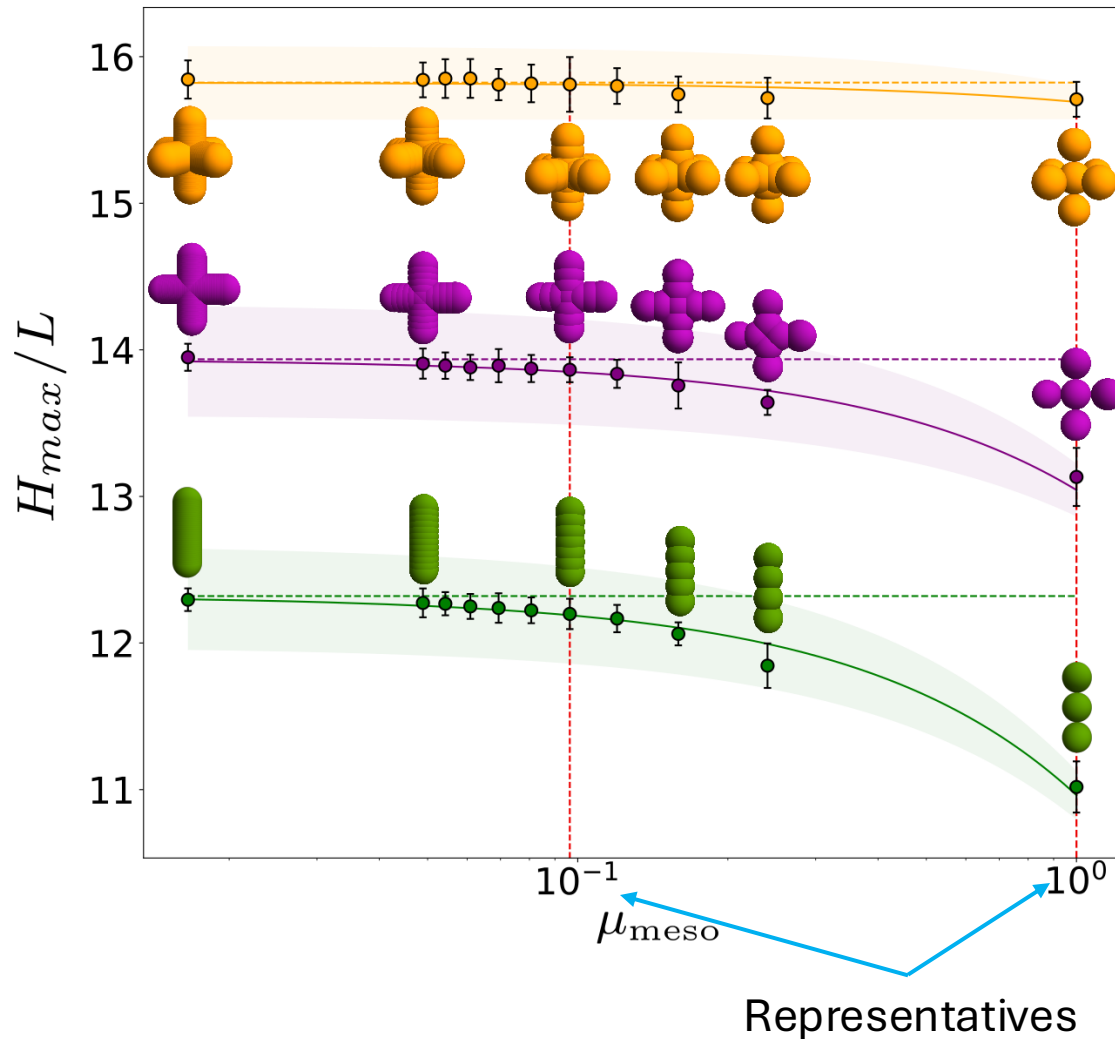
Contact Model



Zhu, R., Gao, H., Zhan, Y., & Wu, Z.-X. (2022). Construction of Discrete Element Constitutive Relationship and Simulation of Fracture Performance of Quasi-Brittle Materials. Materials



Maximum Height



Model

$$H_{max}(n) = H_1 + H_{\Delta}(1 - \mu_{meso})$$

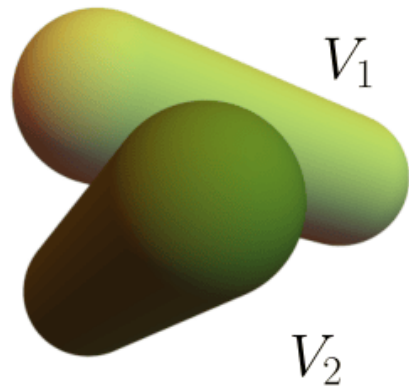
New parameter

$$\mu_{macro} = 1 - \frac{H_{\Delta}}{H_1}$$

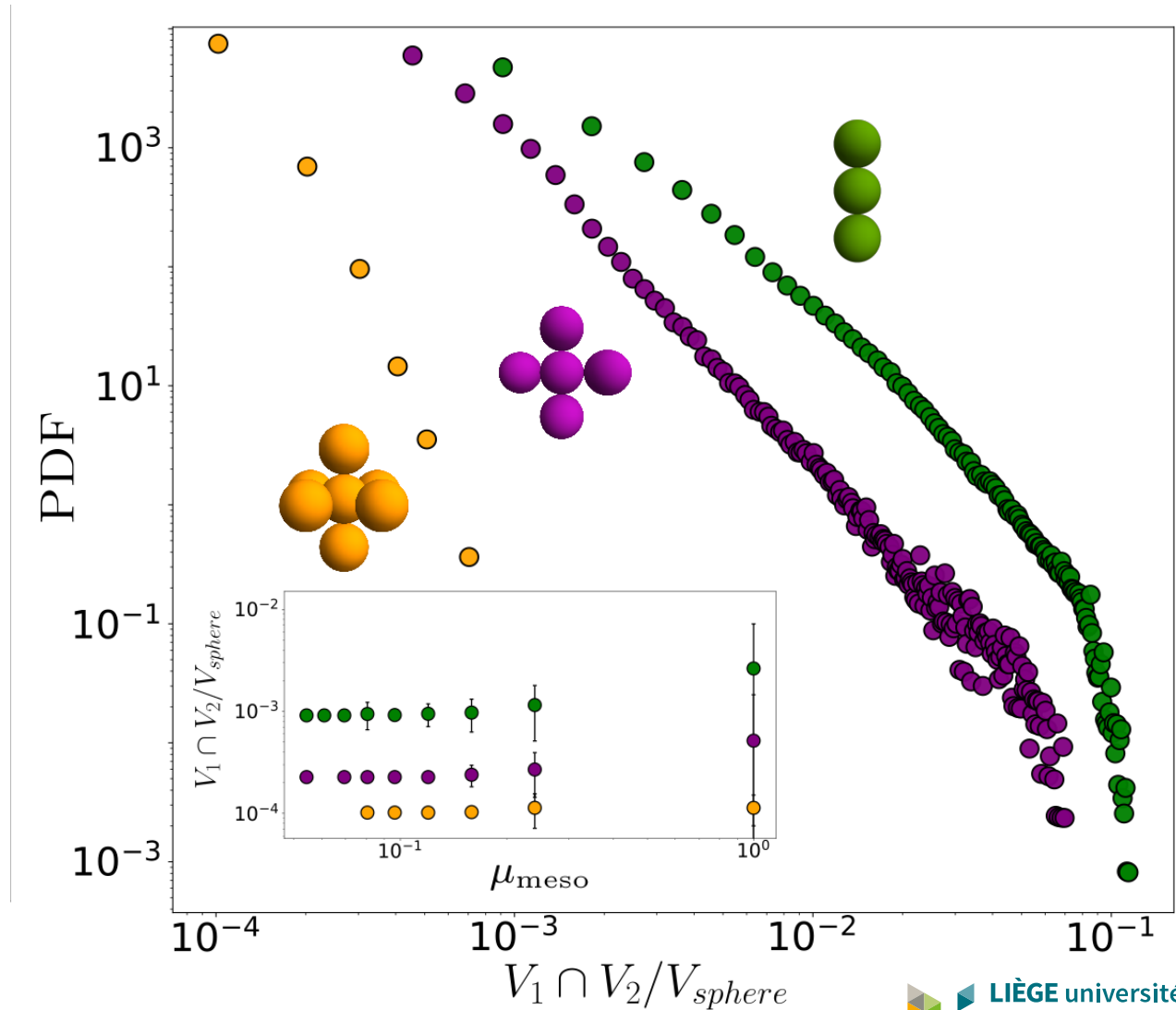
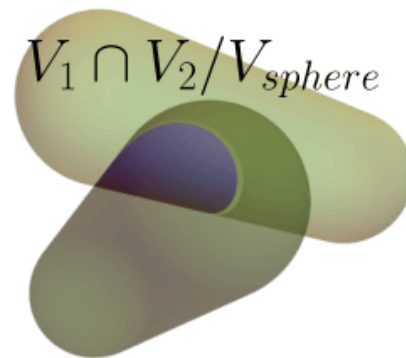
Convex-Hull Overlap



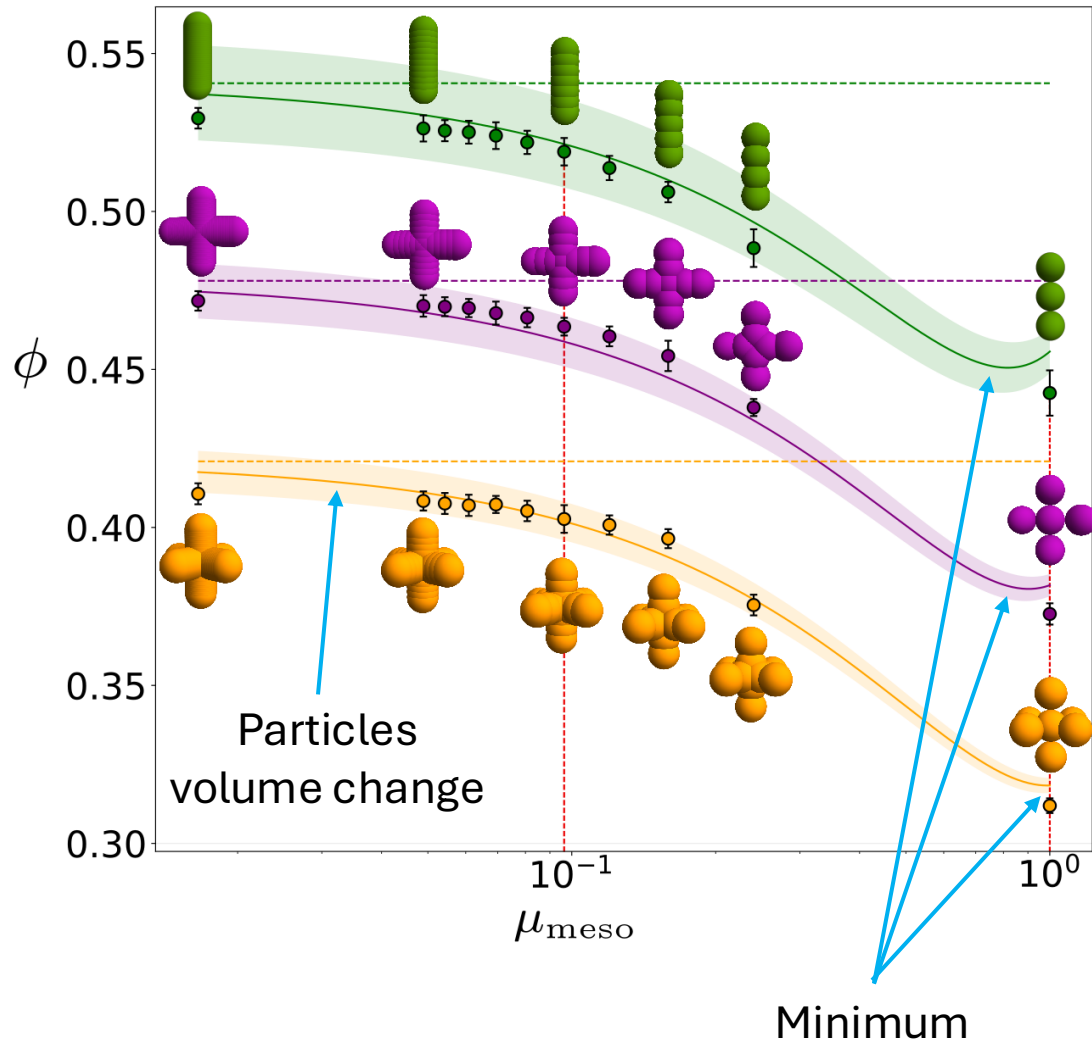
Convex-Hull



Overlap



Packing fraction



Semi-empirical Model

$$\phi(\mu, \mu_{\text{meso}}, \mu_{\text{macro}}) \approx \frac{Nv_n}{V_{\text{max}}}$$

$$= \phi_1 \frac{(1 - \mu_{\text{meso}})^2 + 3}{3(1 - \mu_{\text{macro}})(1 - \mu_{\text{meso}}) + 3}$$

Linear modulation

Minimum ?

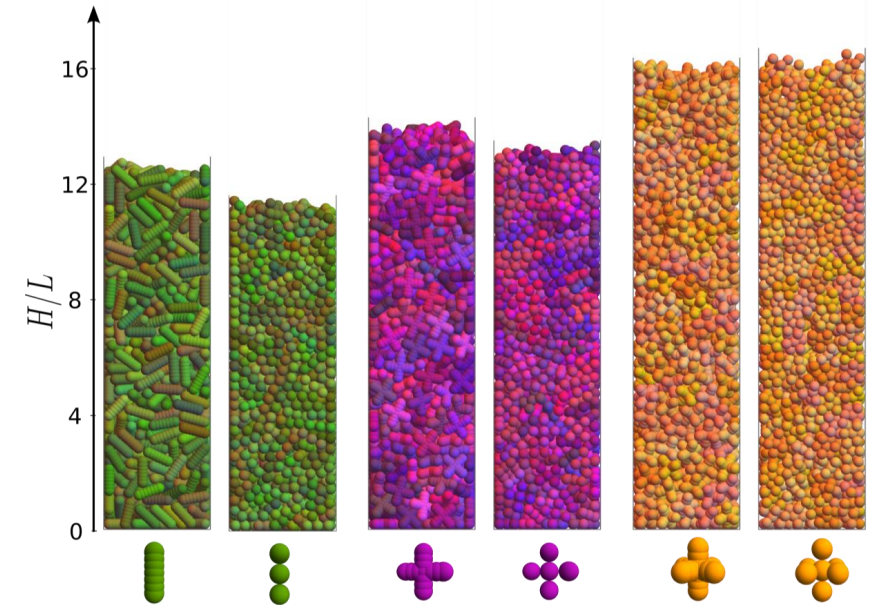
$$\mu_{\text{meso}} = \frac{2 - \mu_{\text{macro}} - \sqrt{1 + 3(1 - \mu_{\text{macro}})^2}}{1 - \mu_{\text{macro}}}$$

Take-home message



- Bumpiness of particles μ_{meso} impact:

- Packing fraction through interlocking



- Effect modulated linearly by the shapes of particles μ_{macro}

Perspectives



Extent this study to a wide range of macroscopic roughness

Study other observables (e.g. Angle of repose)

Use Edwards theory to check our semi-empirical modelling

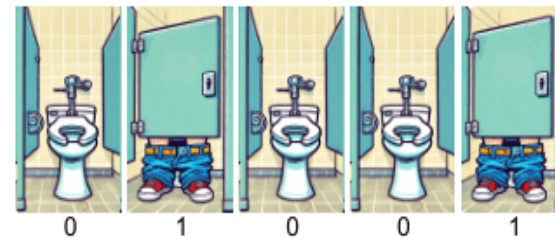
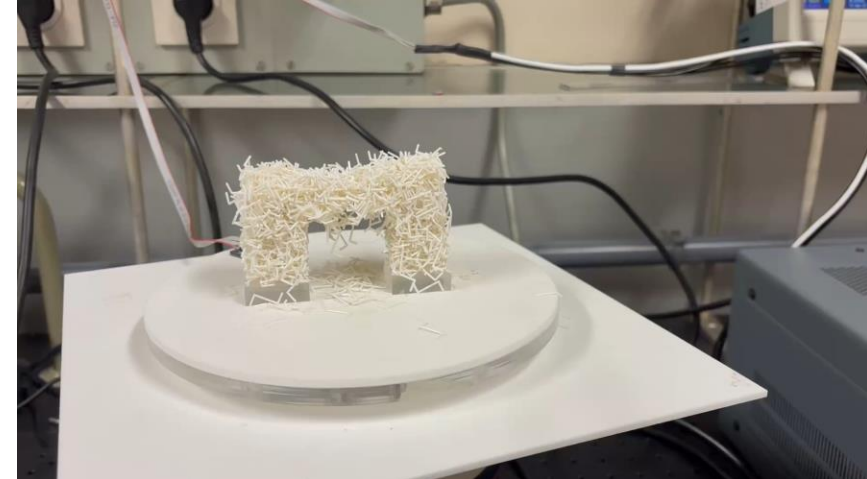
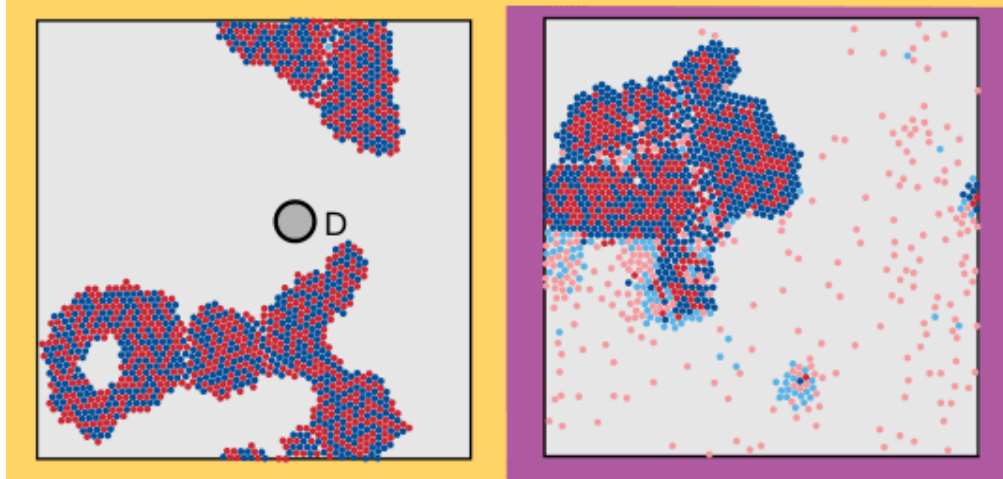
Shape manufacturing with less materials

Model through DEM with less spheres

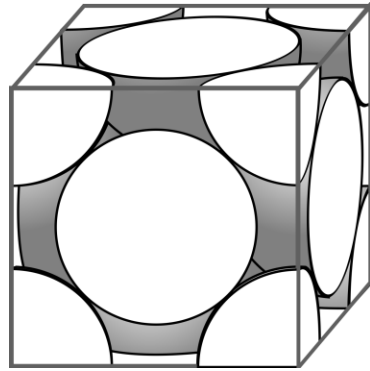


Question

Others



Historical context



$$\phi = \frac{\pi}{3\sqrt{2}} \approx 0.74$$

1611 Kepler Conjecture: Maximal close packing for spheres

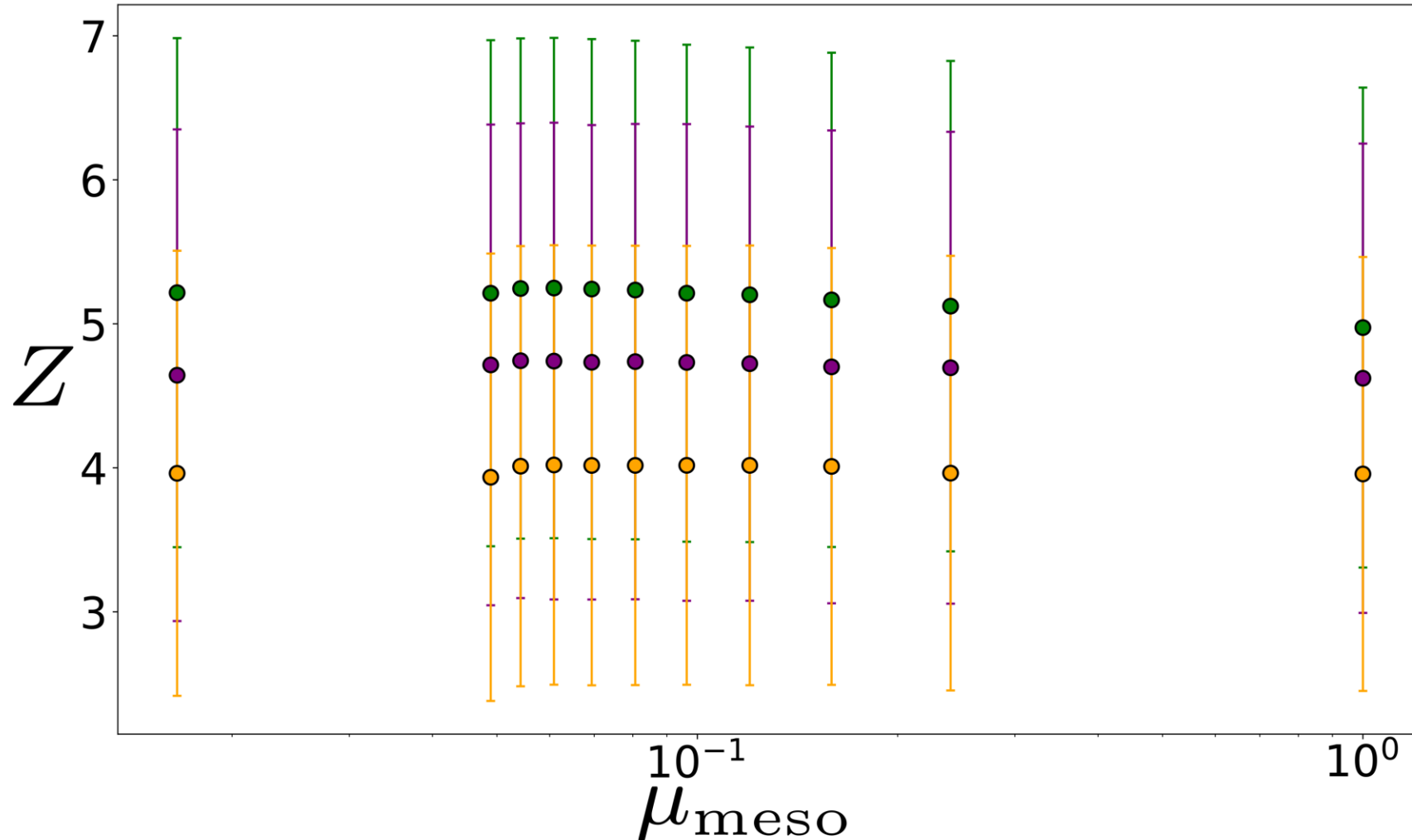
1831 Gauss proof in case of lattice arrangement

1900 Included as part of the 23 unsolved problem of Hilbert



2017 Formal proof by Thomas Hales et al.

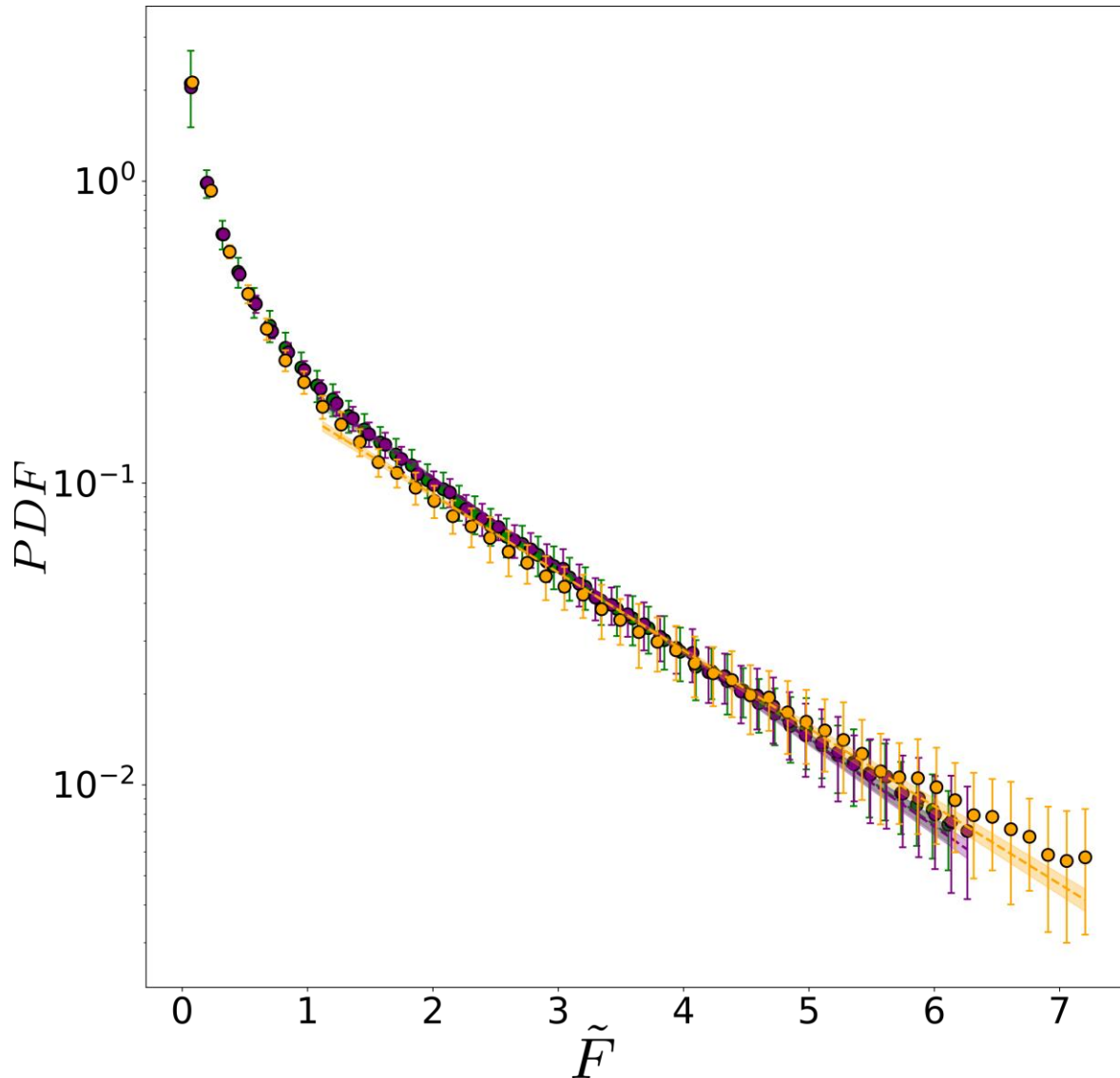
Coordination number



Constant with meso

Vary with macro

Forces distribution

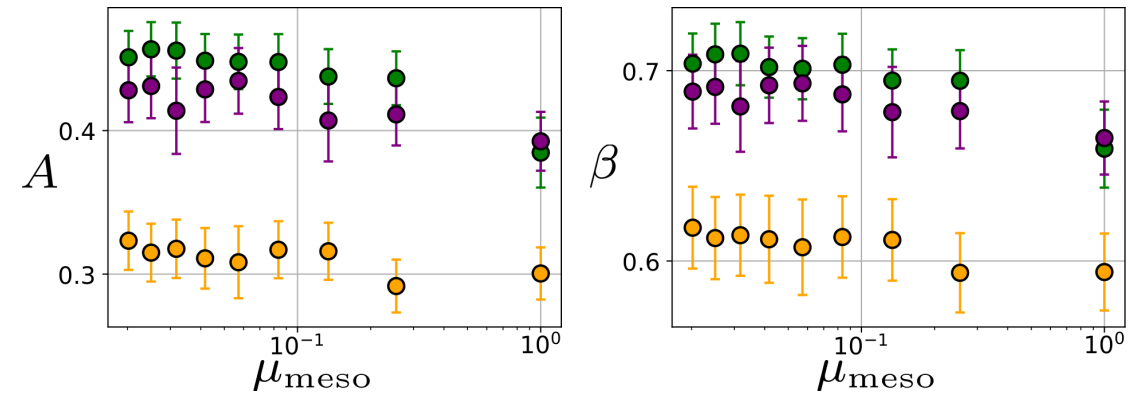


15

Model

$$A \exp\left(-\beta \tilde{F}\right) \text{ for } \tilde{F} > 1$$

Fitting parameters



Constant with meso

Vary with macro



$$\mathbf{F} = m\mathbf{a} \quad \mathbf{I}\dot{\boldsymbol{\omega}} + \boldsymbol{\omega} \times (\mathbf{I}\boldsymbol{\omega}) = \mathbf{M}$$

$$F_n = K_n \delta_n^{3/2} + \eta_n v_n \quad F_t = K_t \delta_t^{3/2} + \eta_t v_t$$

$$\mu_{\text{macro}} \approx \{0.88, 0.94, 0.99\}$$

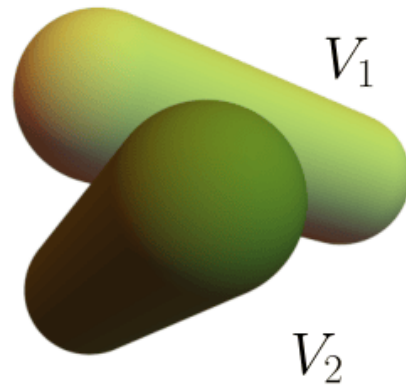
Table 1 Simulation parameters

Property	Ranges of values
Density, ρ	$1.2 \times 10^3 \text{ kg m}^{-3}$
Young's Modulus, E	2.5 GPa
Poisson's Ratio, ν	0.35
Coefficient of Restitution, e	0.3
Coefficient of Friction, μ	0.4
Box Dimension, $l_x \times l_y \times l_z$	$0.1 \times 0.1 \times 0.5 \text{ m}^3$
Maximum Simulation Time, t_{max}	15 s
Time Step, dt	$1 \times 10^{-6} \text{ s}$
Shapes	Rod,Cross,Star
Number of Particles, N	3780,2268,1620
Mass, m	0.3139,0.5277,0.7301 g
Moment of inertia along x, I_{xx}	5.2, 5.8, 10.7 $\mu\text{g m}^2$
Moment of inertia along y, I_{yy}	5.2, 10.1, 10.7 $\mu\text{g m}^2$
Moment of inertia along z, I_{zz}	5.2, 5.8, 10.7 $\mu\text{g m}^2$
Sphere radius, R	2.5 mm
Rod Length, L	$6R$
Gravity, g	9.81 kg m s^{-2}

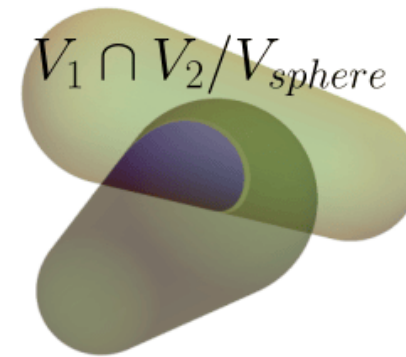
Slide Remove overlap



Convex-Hull



Overlap



$$F_n = mg$$

$$\hat{\delta}_n = \left(\frac{16m_{\text{star}}g}{K_n} \right)^{\frac{1}{2}} \approx 5 \cdot 10^{-4} R$$

$$10\hat{\delta}_n^2 R / R^3 \approx 10^{-6}$$

Slide Model packing fraction

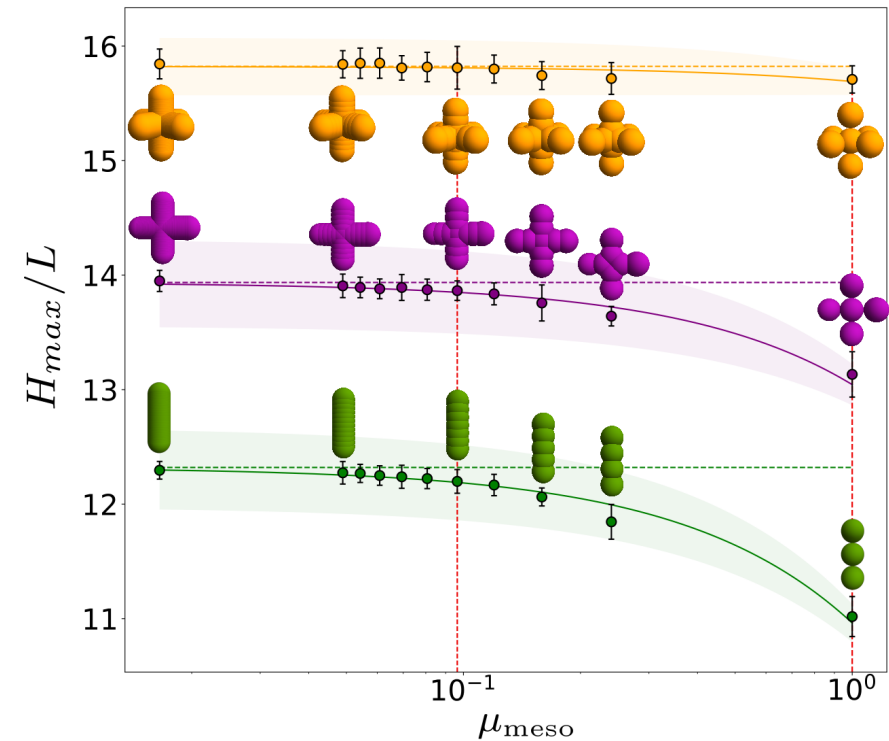


$$\phi(\mu_{\text{meso}}, \mu_{\text{macro}}) \approx \frac{Nv_n}{V_{\text{max}}} = \frac{N}{l_x l_y} \frac{v_n}{H_{\text{max}}}$$

$$v_n = \frac{(1 - \mu_{\text{meso}})^2 + 3}{4} v_{\infty}$$

$$= \frac{Nv_{\infty}}{4l_x l_y} \frac{(1 - \mu_{\text{meso}})^2 + 3}{H_{\Delta}(1 - \mu_{\text{meso}}) + H_1}$$

$$= \phi_1 \frac{(1 - \mu_{\text{meso}})^2 + 3}{3(1 - \mu_{\text{macro}})(1 - \mu_{\text{meso}}) + 3}$$



Edwards thermodynamics



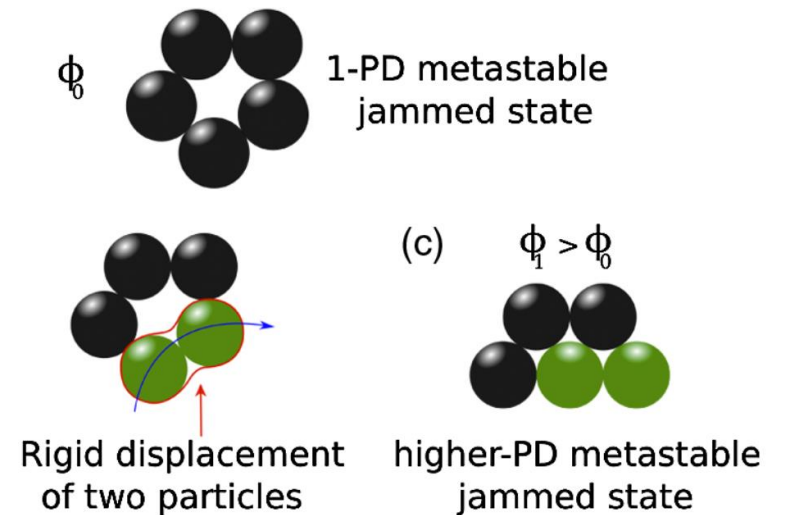
- A.K.A granular statistical mechanics
- Key idea 1989-1994:
 - State variable = Volume $\mathcal{W}(\{\mathbf{r}_i, \hat{\mathbf{t}}_i\})$
 - Proper definition for *jammed* configurations
 - Ergodicity & Equiprobability of micro-states

Usual statistical mechanics	Edwards statistical mechanics
Energy (conserved)	Volume (variable)
Metastable state	<i>Jammed</i> state
Temperature	Compactivity
Hamiltonian	Stress-moment

Jamming



- *Jamming*: Metastability w.r.t. Displacements
 - Packing Fraction do not increase
 - k-Particle-Displacement (k-PD), other fixed
 - Ground state for $k \rightarrow \infty$
 - Ground state allows for 2-5% of particle displacement



Concept	Typical case
Excluded Volume Constraints	No Overlap
Mechanicals Constraints	Forces & Torques balance

Typical Observable



$$S(V) = \lambda \log \Omega(V) \quad \Omega(V) = \int d\mathbf{q} \delta(V - \mathcal{W}(\mathbf{q})) \Theta_{\text{jam}} \quad X^{-1} = \frac{\partial S(V)}{\partial V}$$

- Compactivity X
- Granular material undergoing vertical tapping
- Application to spherical shapes
- Application to nonspherical shapes

Shape modeling

