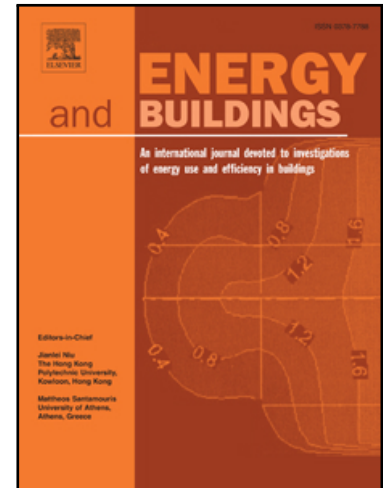


Journal Pre-proof

Reducing urban heat stress through green roofs: a modeling-based performance analysis across green roof types and urban morphologies

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Reducing urban heat stress through green roofs: a modeling-based performance analysis across green roof types and urban morphologies

Thaïs Keravec-Balbot^a, Mitali Yeshwant Joshi^b, Srinidhi Gadde^c, Auline Rodler^d, Marjorie Musy^d, Rémy Claverie^e, Jacques Teller^a

^aUniversity of Liège, Urban & Environmental Engineering Department, LEMA Research Group, Allée de la Découverte 9, B52, Sart-Tilman, Liège, 4000, Belgium

^bCopernicus Institute of Sustainable Development, Utrecht University, Princetonlaan 8a, Utrecht, 3584 CB, The Netherlands

^cWater Resources Department, Faculty ITC, University of Twente, P.O. Box 217, Enschede, 7500 AE, The Netherlands

^dCEREMA Equipe BPE, Nantes, F-44000, France

^eCEREMA Est, TEAM Research Group, Tomblaine, 71 rue de la grande haie, F-54510, France

Abstract

Rising temperatures driven by climate change and rapid urbanization have heightened the need for effective urban cooling strategies. Green roofs, as nature-based solutions, can offer a practical alternative contribution in dense urban areas by improving thermal comfort. However, accurately modeling their microclimatic impact remains difficult due to a large variety in green roof design parameters and limited validation of available tools. In addition, few green roof modeling studies account for urban morphology at the block scale. This study addresses these gaps by validating the green roof module of the Solene-microclimat urban microclimate model with a comparison against measurements and by conducting a local sensitivity analysis of the green roof parameters. The green roof model outcomes were compared to measurements and found to depict physical processes correctly. A local sensitivity analysis investigates how substrate and vegetation parameters as well as irrigation factors affect pedestrian level thermal comfort across nine representative urban morphological archetypes in Liège, Belgium, during a hot summer day. Results show that while irrigation and vegetation characteristics influence outdoor thermal comfort, substrate properties have minimal impact. Well-irrigated, tall, and dense green roofs were found to reduce average pedestrian air temperature by up to 1.4 °C, compared to average scenario green roof. Additionally, green roofs are most effective in improving pedestrian comfort when green roofs are clustered and located near walkable pedestrian areas. The compact mid-rise + low-rise archetype is found to maximize the benefits of green roofs.

Keywords:

Green roof modeling, Urban microclimate, Thermal comfort, Sensitivity analysis

1 INTRODUCTION

1. Introduction

In recent years, cities are experiencing a severe rise in temperatures due to a combination of unprecedented urbanisation and global climate change [1]. This is intensifying the urban heat island (UHI) effect, where the urban temperatures are higher compared to the rural counterparts [2]. Frequent extreme heat events such as heatwaves are intensifying the UHI effect increasing human-health risks [3]. Urban green infrastructure like green roofs is a suitable nature-based solution for urban areas as they can be seamlessly integrated into existing buildings especially where space for trees and parks is limited. Moreover, they offer multiple benefits, including strong building cooling potential [4, 5, 6] and improvement of outdoor thermal comfort [7, 8, 9]. Given these multiple advantages, it is important to study green roofs with accuracy and detail.

Green roof studies can be mainly classified based on their investigated benefit: microclimate regulation or thermal comfort improvement [10, 11] or reduction of building energy consumption [12]. Whatever the scale and objective, assessing these benefits at the project stage requires models that accurately represent green roofs. Vera et al. (2018) [13] performed a review of heat and mass transfer in green roof models used in building energy and urban environment simulation tools. They found that very few green roof models are used in urban-scale research [14, 15, 16, 17] and the majority of the examined models concentrate on building energy analysis for energy consumption reduction [13, 18, 19, 20].

Solene-microclimat is a microclimate model dedicated to modeling urban microclimate and building thermal behavior for the assessment of indoor and outdoor comfort. It relies on a three-dimensional tetrahedral mesh with a spatial resolution down to 1 m, allowing an accurate representation of complex urban morphologies and making it a reliable tool for assessing adaptation strategies at the district scale [21]. Its 3D capabilities are based on integrating radiative, thermal, and computational fluid dynamics (CFD) models [21]. Solene-microclimat has been used in multiple studies for investigating different nature-based solutions like trees, lawns, green walls and green roofs [22, 23, 24, 25]. Although different modules of Solene-microclimat have been validated against experimental measurements, including the green wall module [22], the green roof model has not yet been validated [25], which is necessary to conduct further research.

Recently, Joshi et al. (2024) [25] used Solene-microclimat to study the impact of green roofs on microclimate across different urban morphological block archetypes in Liège, Belgium. Their results highlighted that green roofs can reduce surface and air temperature in large low-rise archetypes. However, the study focused on extensive green roofs with fixed properties, without addressing the sensitivity of results to vari-

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32 ations in parameters such as LAI, foliage height, substrate water content, and albedo, which have been
33 shown to strongly influence green roof performance [11, 26]. Since the Solene-microclimat green roof
34 model relies on input parameters related to substrate and foliage properties which are often uncertain or
35 unknown, sensitivity analysis offers a systematic way to evaluate how variations in these inputs affect
36 outdoor microclimate regulation. Previous applications of the model [24, 25] analyzed green roof im-
37 pacts, but the influence of parameter uncertainty across different urban morphologies remains unexplored.
38 Sensitivity analysis, defined as the study of how input variations influence model outputs [27], can there-
39 fore help identify the most influential design elements, improve model performance, and guide green roof
40 implementation strategies.

41 The methods for sensitivity analysis can be classified into two categories: local and global approaches.
42 Local approaches (also called one-at-time (OAT) methods), quantify the impact on the model output when
43 one factor is changed and all the others are fixed. They require fewer computations but are less effective for
44 complex systems. Global approaches (also called all-at-a-time (AAT) methods), are related to the influence
45 of uncertain inputs over the whole input space, by considering multiple variables simultaneously. They
46 have been largely used in building thermal simulations but rarely with a large multiplicity of factors [28],
47 and rarely in green roof studies.

48 Table 1 provides a summary of the sensitivity analyses conducted on green roof models. Both local
49 and global sensitivity analysis studies specifically addressing green roof temperature models are relatively
50 limited. Most of the studies widely apply sensitivity analysis in thermal building simulations focusing on
51 thermal fluxes through the roof or energy consumption. Nevertheless, most of the green roof parameters
52 in Solene-microclimat are also used in other models, and their impact on various results has been explored
53 in Table 1. Few studies [29, 30] have examined a broad range of parameters, and none have accounted
54 for all relevant factors. All studies agree on the important influence of LAI and substrate thickness. While
55 some have conducted rigorous sensitivity and uncertainty analyses, they highlight the need for a systematic
56 evaluation of how green roof performance depends on various parameters.

57 Moreover, the lack of a comprehensive and accurate database of green roof properties poses a challenge
58 for researchers and practitioners, as it limits the ability to simulate green roofs realistically and may lead
59 to inaccurate estimations of the thermal loads in buildings incorporating such systems [31, 32].

60 Building on above literature survey, four research gaps are identified:

- 61 1. While the Solene-microclimat green roof model has been used, it has not yet been validated against
62 experimental measurements.

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63 2. Existing studies have been conducted with a fixed urban morphology, making their results highly
64 dependent on specific urban contexts. There is no study that investigates the green roof parameters
65 along with urban morphological characteristics for microclimate regulation.

66 3. There is a significant gap in the literature regarding a rigorous, comprehensive evaluation of green
67 roof parameters from a thermal outdoor environment perspective, as well as a lack of proper assess-
68 ment of the influence of all parameters and their possible interactions.

69 4. There is no established database of vegetation and soil parameters for scientists and practitioners to
70 reference when field data is unavailable for green roof models [31, 32]. This lack of reference values
71 introduces uncertainty and hinders reliable simulations.

72 Sensitivity analysis can offer valuable insights by identifying the most influential parameters, guiding
73 data collection efforts, and optimizing calibration strategies [33]. Therefore, this study aims to address
74 the above research gaps by identifying the green roof parameters that most significantly contribute to mit-
75 igating pedestrian outdoor thermal stress during hot days for the urban morphological block archetypes
76 in Liege, Belgium using sensitivity analysis. The analysis starts with the green roof model implemented in
77 Solene-microclimat, identifying the key input parameters and defining their value ranges based on existing
78 literature. An experimental validation of the green roof model is performed to show that the model rep-
79 resents green roof temperatures correctly. A sensitivity analysis is then performed, testing each parameter
80 at three levels (minimum, baseline, and maximum), to evaluate their impact on pedestrian thermal stress
81 reduction across the nine distinct urban block archetypes identified in Liège.

82 This study aims to address the aforementioned research gaps by identifying the green roof parameters
83 that most strongly contribute to reducing pedestrian outdoor thermal stress during hot days across repre-
84 sentative urban block archetypes in Liège, Belgium, using sensitivity analysis. First, the Solene-microclimat
85 green roof model is introduced, and its thirteen key input parameters are identified. Their value ranges
86 are defined based on a review of the existing literature, thereby investigating gap 4. An experimental val-
87 idation of the green roof model is then conducted to demonstrate its ability to accurately reproduce green
88 roof temperatures, examining gap 1. Subsequently, a local sensitivity analysis is then performed, testing
89 each parameter at three levels (minimum, baseline, and maximum), to evaluate their impact on pedes-
90 trian thermal stress reduction across the nine distinct urban block archetypes identified in Liège, thereby
91 addressing gaps 2 and 3.

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Reference	Model	Outcome	Parameter	Method	Result
[34]	Energy balance model	TF	Water availability of the soil and convection coefficient	OAT (2 values per parameter)	Convection coefficient and water availability are the factors that regulate heat storage
[35]	Energy balance model	TF	Foliage height, LAI, soil and insulation thickness, roof type, humidity, and wind speed	OAT (3 values per parameter)	The vegetation most important parameter is LAI as it influences transpiration and shading
[36]	Heat/moisture model	TF	Thickness of soil layer and LAI	AAT (18 cases)	Soil thickness drives year-round performance; LAI matters in summer
[37]	Heat/moisture model	TF	Dry thermal conductivity, water content, density, thickness of substrate and drainage layers	OAT and AAT	The dry conductivity and thickness of layers are more influential parameters
[38]	EnergyPlus	BEC	Thickness of soil and plant density	OAT (2 values per parameter)	Thicker soil and denser plants in summer enhance green roof performance
[39]	EnergyPlus	BEC	Irrigation schedules, plant height, substrate type and LAI	OAT and some combinations	LAI most influences the energy use, while plant height has no effect
[40]	EnergyPlus	BEC	The type of substrate, LAI, the roof structure material and the insulation levels	OAT and some combinations	Vegetation reduces cooling loads more than insulation, while insulation impacts heating more
[30]	EnergyPlus	BEC	16 parameters	AAT (4 values per parameter)	The key factors reducing cooling demand are construction R-value, LAI, substrate thickness and conductivity
[41]	EnergyPlus	BEC	Growing media depth, plant canopy density, climate and building use	AAT	In cooling-dominated buildings, LAI has a greater impact
[42]	Energy Plus	Building thermal gain	LAI, plant height, dry soil conductivity	OAT (20 values per parameter)	LAI has the most impact on building thermal gain
[29]	Urban hydrological model	TF and temperatures	15 parameters	OAT (2 values per parameter)	Only four parameters significantly affected thermal gain: LAI, plant height, dry soil conductivity, and minimum stomatal resistance
[43]	Heat/moisture model	Vegetation and indoor temperatures	Incident solar radiation, ambient temperature, evapotranspiration rate, wind speed	AAT (Monte Carlo)	Green roof performance is sensitive to aerodynamic resistance, soil hydrodynamics, and thermal properties
[31]	Envi-met	Pedestrian comfort indices	LAI, leaf angle distribution, substrate emissivity and water coefficient, air gap behind the substrate	AAT (Monte Carlo)	Indoor temperature is most affected by ambient temperature and solar radiation, and least by wind speed
[44]	Energy-Plus	BEC	Stomatal resistance, soil surface roughness, plant height and substrate thickness	OAT (3 values per parameter)	LAI is the most significant parameter. Remark: Green roof and facade models are the same but the study is on green facades
[45]	Energy-Plus	BEC and TF	Vegetation height, LAI, stomatal resistance, substrate thickness, conductivity, density and heat	OAT (1944 combinations)	Substrate height and plant height have the most significant impact on energy savings

2 METHODOLOGY

2. Methodology

2.1. Solene-microclimat model

Solene-microclimat is dedicated to modeling urban microclimate and building thermal behavior for the assessment of comfort. It is used to assess climate adaptation measures at the district scale [21]. Its 3D capabilities are based on integrating radiative, thermal, and computational fluid dynamics (CFD) models [21]. Unlike other urban microclimate models, Solene also has the advantage of representing urban blocks faithfully due to tetrahedral meshing with spatial resolution of the model depending on the meshes and up to 1 m. The simulation can be launched for hourly or sub-hourly time steps. Different kinds of nature-based solutions can be considered: trees [46], green areas [47], green roofs and green walls [22, 23, 24] as well as lawn surfaces [48]. The Solene-microclimat green roof model includes numerous parameters. A full description of the physical processes and thermal balances is available in Malys et al. (2014) [23].

2.2. Sensitivity analysis

The objective of this study is to analyse the influence of green roof parameters on the outdoor thermal comfort in summer conditions, using Solene-microclimat. The Solene-microclimat green roof model uses 12 parameters, listed in Sec. 2.3. A one-day simulation for a neighborhood sized mock-up takes several hours to complete on a supercomputer. However, performing a global sensitivity analysis requires lots of runs to investigate the interactions between parameters. Therefore, performing a global sensitivity analysis over 12 parameters was not possible. A local screening approach to identify the most influential variables is performed. This sensitivity analysis can screen dominant first-order parameter effects already and determine which parameters have a significant influence on the effect of green roofs on pedestrian thermal comfort.

In this study, multiple simulations were run for various morphological block archetypes and green roof parameters to analyse the influence of green roof parameters on the outdoor thermal comfort in summer conditions. The simulations were performed on supercomputers for multiple morphological block archetypes in the city of Liège, Belgium [49]. This work uses the block archetypes from Joshi et. al. (2024) [25], described in Section 2.5. In this paper, the authors investigated the impact of green roofs on microclimate in Liège, Belgium, using Solene-microclimat model. They identified 27 July 2018, the hottest day of an intense heatwave, as the reference for their simulations. The same day is adopted for our sensitivity analysis (see [25] for detailed meteorological conditions), simulating the microclimate between 7 AM and 9 PM, focusing on daytime variation.

To assess the impact of green roof parameters on outdoor thermal comfort, the analysis focuses on walkable surfaces (lawns and impervious areas) within urban block archetypes. Given that air temperature alone is insufficient for evaluating comfort, a thermal comfort index is needed. In this study the Rothfus (1990) [50] equation, commonly used by the American National Oceanic and Atmospheric Administration (NOAA), is adopted to account for the combined effect of temperature and humidity on perceived heat.

The heat index is calculated as the output of the sensitivity analysis, considering 12 green roof parameters across nine urban morphologies. Since this involves a large number of simulations, the code was parallelized and executed on high-performance computing systems: the NIC5 supercomputer (Université de Liège) and the Dutch national supercomputer, Snellius.

For the local sensitivity screening, each parameter is assigned a low, baseline, and high value. Varying one parameter at a time, the selected day (7 AM–9 PM) is simulated across the nine block archetypes. Outputs (air temperature, humidity, and heat index) are computed over the mesh and compared to the baseline simulation to assess the parameter's influence. The workflow is summarized in Fig. 1, with parameter ranges listed in Table 2. In total, 225 simulations are performed.

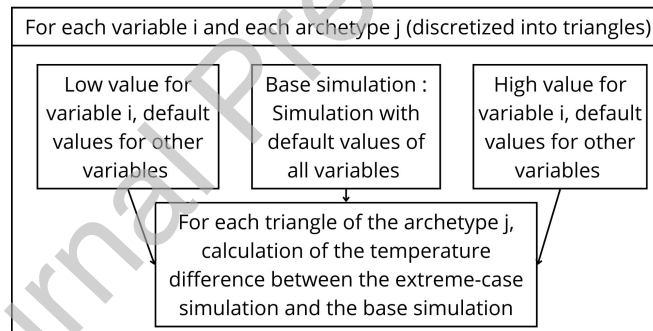


Figure 1: Simulation method: Simulation workflow for the local sensitivity screening. Each variable is tested at its minimum and maximum values while keeping the others at default settings. Results (temperature, humidity, heat index) are compared against the baseline simulation.

2.3. Green roof parameters

2.3.1. Structural parameters

The green roof vegetation in Solene-microclimat is represented by five parameters : Leaf Area Index (LAI), which is the total surface area of leaf compared to the total surface area of ground, foliage height, extinction coefficient used to calculate the transmission of solar radiation through foliage, emissivity, and albedo. For LAI, foliage height, emissivity and albedo, Table 12 in Appendix A presents the ranges of values

used in green roof parametric studies or sensitivity analysis, which serve for selecting the low, default, and high values used in our analysis.

LAI is a key vegetation variable widely studied [51] and measurable through harvesting, light interception [52], or satellite data [53, 54]. Together with foliage height, it is commonly used in green roof models due to data accessibility and their role in energy and mass exchanges [13]. While several studies have shown correlations between LAI and foliage height depending on vegetation type [55, 56, 57], there is no consensus on a universal relationship, particularly in the context of green roofs. As a result, LAI and the foliage height are treated as independent parameters in this study.

The extinction coefficient is used to account for shading in most green roof models [13]. The extinction coefficient is calculated from the leaf angle and solar orientation [58, 59]. Based on extinction coefficient considered in several studies [60, 61, 62, 63, 64], the extinction coefficient is taken between 0.5 and 0.9.

The substrate is described by several parameters : its thickness, conductivity, density and specific heat. There is a strong relationship between substrate conductivity and its mass [65] and material conductivity, density, and capacity are generally interrelated [66]. However, to avoid introducing additional errors, the substrate properties are considered independent. Table 13 in Appendix A highlights the substrate properties taken in green roof studies on which the choice of low, default and high values for the analysis is based.

2.3.2. Process-related parameters

Evapotranspiration is the dominant physical heat transfer process in green roofs. In Solene-microclimat, it is estimated based on the FAO guidelines [57]. The model incorporates adjustment coefficients that distinguish soil evaporation and plant transpiration (the foliage transpiration coefficient, α_{lat} , that quantifies the part of transpiration in evapotranspiration) and water disposability (the irrigation coefficient f , that quantifies the magnitude of evapotranspiration) to calculate a suitable evapotranspiration. The derivation of these coefficients and its values are presented in Appendix A.

Another coefficient, the canopy air rate coefficient α_R , is used to calculate the air exchange rate in the canopy according to Eq. 2.3.2:

$$R(v) = R_{min} + (R_{max} - R_{min}) \times \alpha_R \times \frac{v}{v_{max}} \quad (1)$$

R represents the air exchange rate in the canopy, depending on v the wind speed, taken as maximum value $v_{max} = 10m.s^{-1}$. It is usually between 125 and 1000 h^{-1} [58]. Therefore, the maximum and minimum

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2.4 Experimental validation of green roof model

of the value, R_{min} and R_{max} are taken as $R_{min} = 125 h^{-1}$ and $R_{max} = 1000 h^{-1}$. Most generally, α_R is taken equal to 1. α_R is the only one of the considered parameters that isn't related to a real physical parameter but more a calculation parameter. To investigate the impact of the dependency of R to the wind on the green roof performance, the wind speed coefficient will be taken between 0.8 and 1.2.

Table 2 presents the final variation range for the parameters, as well as the low, default and high values.

Parameter	Low	Default	High
Foliage transpiration coefficient α_{lat} [-]	0.5	0.75	1
Irrigation coefficient f [-]	0.1	0.75	1.5
Wind speed coefficient α_R [-]	0.8	1	1.2
Extinction coefficient k_s [-]	0.5	0.7	0.9
Foliage height [m]	0.05	0.25	0.5
LAI [-]	1	2.5	5
Substrate heat capacity [$J.kg^{-1}.K^{-1}$]	700	950	1200
Substrate conductivity [$W.m^{-1}.K^{-1}$]	0.2	0.6	1
Substrate density [$kg.m^{-3}$]	600	950	1300
Substrate thickness [m]	0.1	0.2	0.3
Foliage albedo [-]	0.2	0.3	0.4
Foliage emissivity [-]	0.85	0.9	0.95
Urban morphology	9 block archetypes (A → I)		

Table 2: Final values for the 13 green roof parameters

2.4. Experimental validation of green roof model

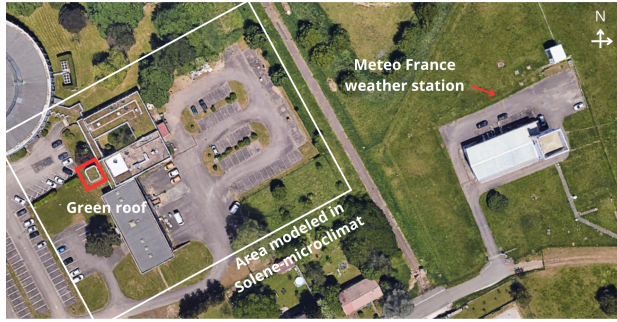
Before conducting the sensitivity analysis, the green roof model in Solene-microclimat is validated. Experimental data collected in Nancy, France by the CEREMA (coordinates : 48° 41' 13.457"N, 6° 13'8.444" E) is used. Nancy is a medium-size city, located in the East of France with a Köppen classification Cfb (temperate, no dry season, warm summer), the same as Liège. The set up is presented in Fig. 2a. The isolated green roof is used to perform the validation.

The 5 m² studied green roof is composed of (Fig 5 (b)): (1) a vegetation layer, whose composition has been studied by [67] (mostly sedum), (2) a 10 cm substrate layer (pouzzolana, recycled terracotta, terracotta sand, coal slag and compost in unknown proportions), (3) a 5 cm drainage layer (composed of expanded clay beads), (4) a 17.5 cm concrete layer and (5) a 10 cm false ceiling.

This study focuses on the green roof and its surrounding environment, the scale at which observations are available. Consequently, simulations are carried out at a 1 m resolution. To simulate atmospheric conditions to which the green roof is exposed, a series of locally observed meteorological fields are prescribed hourly: atmospheric pressure, shortwave incoming solar radiation (direct and diffuse), longwave incoming radiation, air temperature, relative humidity and average wind speed. These meteorological data

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2.4 Experimental validation of green roof model



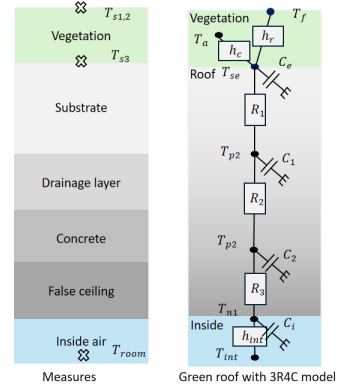
(a) Experimental set-up

Measures :

$T_{s1,2}$ Top of vegetation surface temperature
 T_{s3} Top of substrate surface temperature
 T_{room} Inside air temperature

Thermal model :

T_f Top of vegetation surface temperature
 T_a Vegetation canopy air temperature
 T_{se} Top of substrate surface temperature
 T_{p2} Roof first thermal node
 T_{p1} Roof second thermal node
 T_{int} Inside air temperature



(b) Thermal nodes in Solene-microclimat (right) and experimental measurements (left)

Figure 2: Experimental set-up and thermal model

190 are obtained from a nearby Meteo France weather station (coordinates : 48° 41' 17.267"N, 6° 13' 16.943"
 191 E). The model is assessed under meteorological conditions consistent with those applied during the local
 192 sensitivity analysis, therefore for a hot summer day. Comparing the measurements available to the mete-
 193 orological conditions forced for the 27th July 2018 in Liège, the closest days found are the 19 to 23 June
 194 2023. Meteorological hourly forcing is based on Meteo France weather station data and depicted in Fig. 3.

195 Based on plans, construction information and Google Maps data, a geometry is created in Solene-
 196 microclimat to represent the studied green roof and its surroundings. The whole CEREMA building is
 197 represented, with its green roofs, with the surrounding parking lot and urban vegetation.

198 Typically, Solene-microclimat uses a 3R4C green roof model, inspired by the model of Fraisse (2002)
 199 [68], in which two thermal nodes are placed within the building layer to accurately calculate conductive
 200 fluxes (see Fig. 2b). Soil temperatures are recorded using PT100 sensors at different depths, including two
 201 measuring foliage surface temperature, one measuring the substrate surface temperature and one measur-
 202 ing the inside temperature. This last value is used in Solene-microclimat to set the indoor temperature as
 203 a boundary condition.

204 Based on the literature and construction data, the type of building and the construction year, the wall
 205 and roof composition will be taken as displayed in Table 10 in Appendix A. The characteristics of the
 206 materials are presented in Table 11 in Appendix A.

207 The remaining green roof parameters, such as albedo and LAI, need to be defined, and various com-
 208 binations are explored to identify the most suitable configuration. Multiple simulations were performed
 209 and the best one was for a LAI of 2, a foliage height of 0.25 m and an extinction coefficient of 0.9. Hydro-

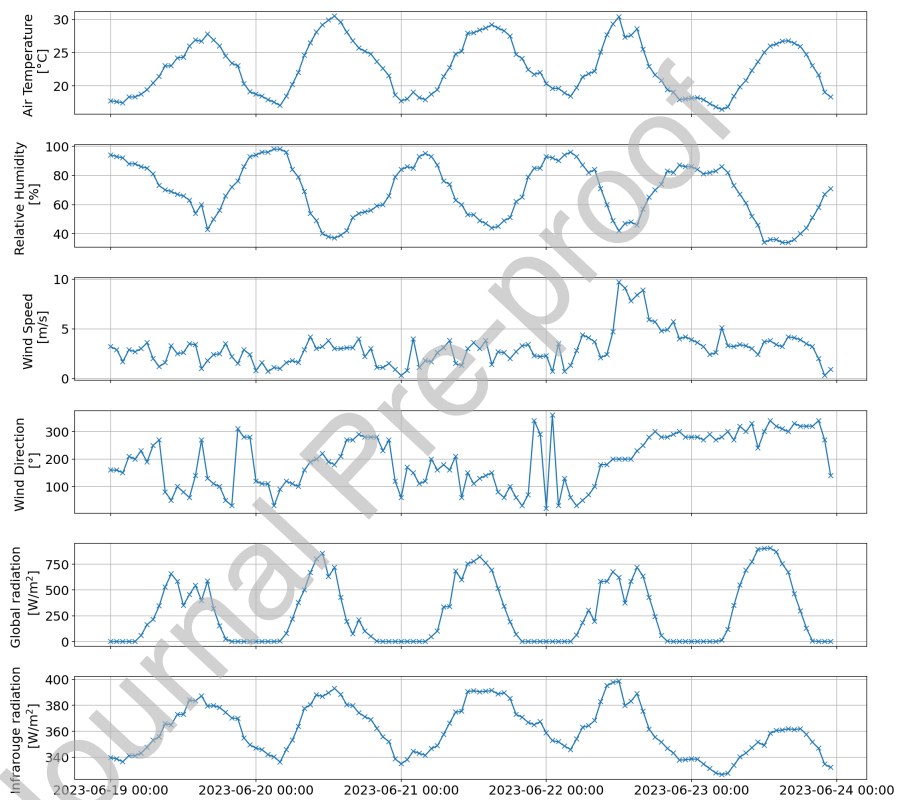


Figure 3: Meteorological conditions used for the experimental validation

logical parameters were derived from substrate moisture measurements and hydrological determination of the substrate, which gives $\theta_{WP} = 5 \text{ m}^3 \cdot \text{m}^{-3}$ and $\theta_{FC} = 24 \text{ m}^3 \cdot \text{m}^{-3}$ for the substrate under study. The dry conductivity of the substrate was determined by De Munck et al. [16] and combined with the substrate water content to obtain the substrate conductivity.

The validation focused on comparing simulated and measured green roof 2m air temperature, foliage, and substrate surface temperature.

2.5. Urban block archetypes

This study aims to determine which parameters have the greatest impact on green roof performance with respect to thermal comfort, by systematically evaluating all relevant factors. One parameter that has received limited attention in the literature is the type of building supporting the green roof and the surrounding urban morphology. Urban morphology is defined as a range of spatial and structural characteristics that shape the physical form of urban areas. To account for this, the present study incorporates the urban block classifications developed by Joshi et al. [49] for the city of Liège, using them as a proxy for urban morphology in the sensitivity analysis. This classification identifies nine distinct urban block typologies, derived through a PCA-based k-means clustering applied to 17 urban morphological parameters (Fig. 4).

The spatial resolution is set to 2 meters, as the Solene-microclimat model has been previously validated for urban mitigation strategies at similar grid resolution [69]. At this resolution, running all simulation cases required approximately 500000 core-hours on the Snellius supercomputer of the Netherlands Organization for Scientific Research, using 16 cores per case. Tab. 8 and 9 in Appendix A highlight the properties of urban surfaces taken for the modeling. The roofs are composed of a concrete layer, with additional foliage and substrate for the green roofs. For the lawns, properties were taken similarly from previous studies [22, 69]: $\text{LAI} = 2$, $k_s = 0.75$, $f = 1$, $\alpha_{lat} = 0.75$.

The meteorological data, namely air temperature, wind velocity, wind direction, global radiation, direct and diffused radiation, infrared radiation, relative humidity and pressure, are obtained from the observations of the Royal Meteorological Institute, Belgium (RMI).

3. Results

3.1. Experimental validation

A validation was conducted to support the main objective of this study, which is to investigate outdoor thermal stress.

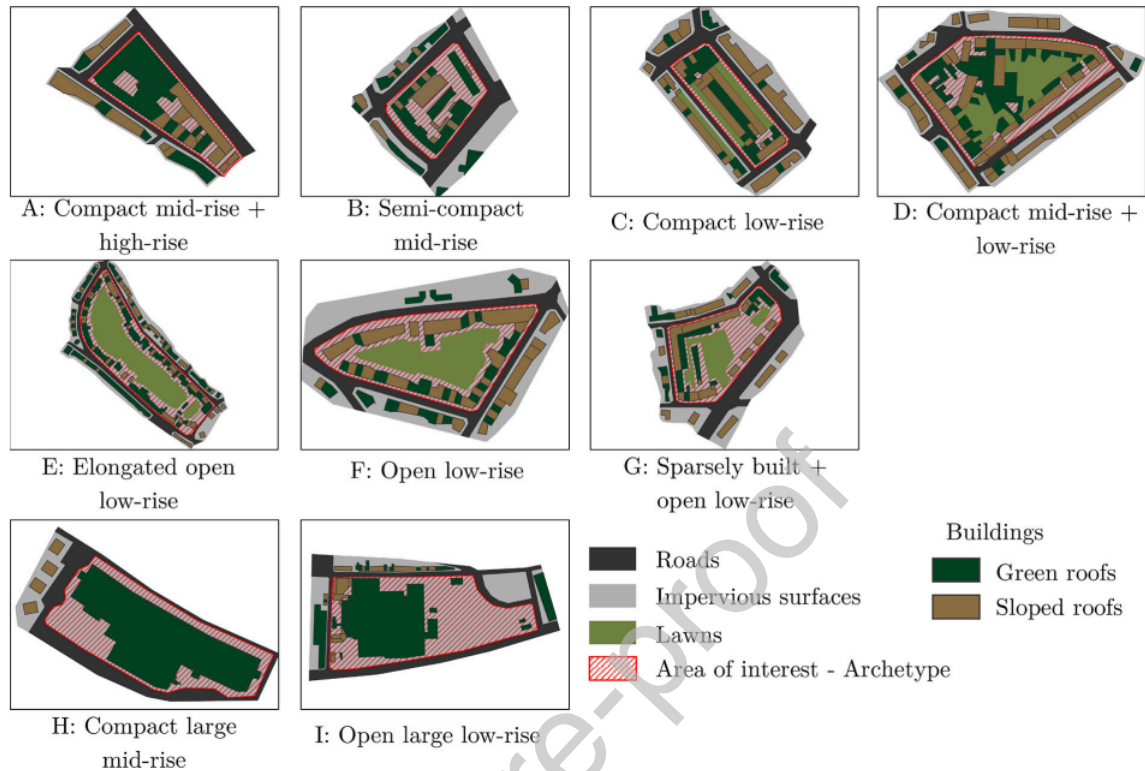


Figure 4: Detailed geometries based on urban morphological block archetypes for the Liege city (from [25])

240 Fig. 5a and 5b show the comparison of the model outputs and the measurements. The surface tem-
 241 perature results show that the RMSE is 2.70 °C for the substrate temperature and 4.4 °C for the foliage
 242 temperature. According to Vera et al. [13]'s review of green roof models, most models are generally more
 243 accurate in predicting surface substrate temperature (within 1–3.5 °C) compared to leaf surface temper-
 244 ature (within 1.9–3.9 °C). The results here are consistent with this review, as the substrate temperatures
 245 were also better predicted than foliage temperatures.

246 The main discrepancy in foliage temperature lies in nighttime values, which the model tends to over-
 247 estimate. For instance, the average minimum model vegetation temperature for the last 3 days is 24.35 °C
 248 while for the measurements it is 17.3 °C. The vegetation evening and nighttime cooling is largely under-
 249 estimated. This could be due to underestimated nighttime convection or long-wave radiation. In contrast,
 250 the substrate temperature at night aligns more closely with measurements. Since the analysis will focus on
 251 daytime and early evening periods, this limitation is not critical for the following sensitivity analysis.

252 The validation statistics were calculated over the entire simulation period to maximize the amount of

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3.2 Sensitivity analysis

253 data, which includes both the initial spin-up phase and nighttime intervals previously shown to be less
254 accurately represented. Consequently, model performance during daytime conditions is likely better than
255 these overall metrics suggest.

256 It is also worth noting that Ts1 and Ts2, both foliage temperature measurements, show noticeable
257 differences. This can be attributed vegetation species heterogeneity or uneven plant health. These factors
258 add bias to the validation and should be taken into account when interpreting the results.

259 The air temperature results indicate a strong similarity between the meteorological data from the Météo-
260 France station (used as boundary conditions in the simulation), the experimental measurements taken
261 above the green roof, and the outputs of the Solene-microclimat model. This agreement is expected, given
262 that the large-scale air temperature, which is relatively homogeneous, was directly imposed as a boundary
263 condition in the model.

264 However, the validation was performed at the building scale. Results indicate that the Solene-microclimat
265 model satisfactorily reproduces green roof temperatures at this scale. However, in the subsequent analysis,
266 the model will be applied at the urban block scale.

3.2. Sensitivity analysis

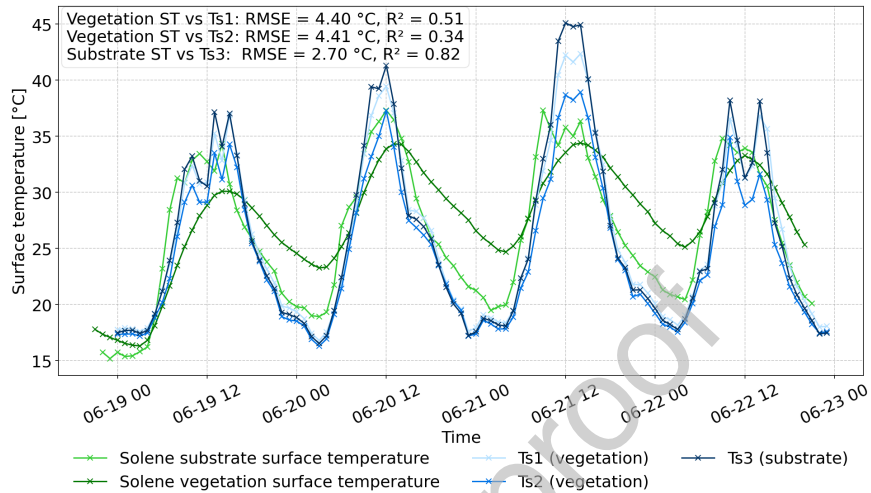
268 Temperatures were computed for July 27, 2018, from 7 AM to 9 PM. The results are depicted for 4
269 PM as it represents the daily temperature peak where differences are most important. Additionally, 8 PM
270 results are shown to capture evening effects.

271 How each parameter influences the outcomes of green roofs is examined, specifically focusing on air
272 temperature 2 meters above the roof, pedestrian air temperature, humidity and heat index.

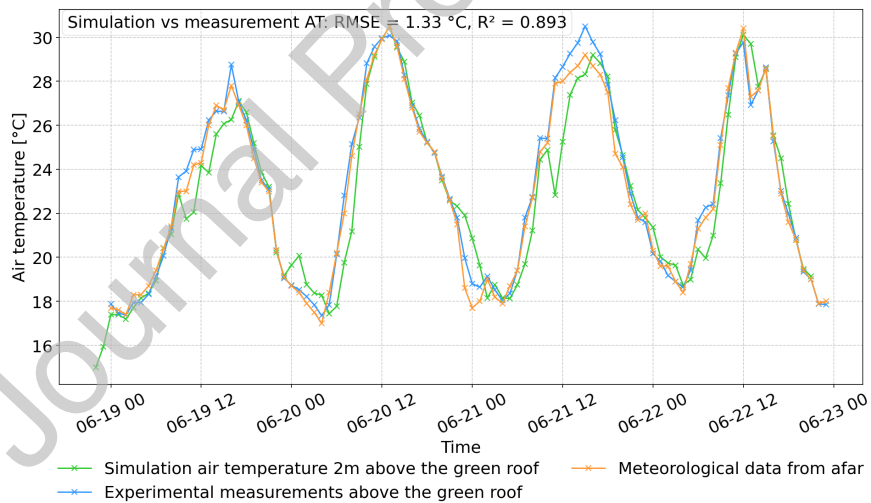
273 For each tetrahedron of the mesh of the urban morphologies, temperatures from low and high scenarios
274 simulations are compared to the base scenario. The differences ($T_{air}(\text{scenario}) - T_{air}(\text{base scenario})$ for
275 example) are shown using violin plots with the median marked by a black dot. A positive difference
276 indicates a cooling effect compared to base scenario. These plots represent all mesh elements without loss
277 of information.

3.2.1. Green roof air temperature

279 Fig 6 depicts the comparison of the 12 parameters to the base scenario for air temperature 2m above
280 the green roof and Tab 3 presents the parameter influence on green roof air temperature, averaged across
281 all archetypes.



(a) Surface temperatures. The statistical indicators are computed model and measurements, for vegetation and substrate surface temperatures and for the whole period.



(b) Air temperatures. The statistical indicators are computed from simulation air temperature 2m above the green roof and experimental measurements above the green roof and for the whole period.

Figure 5: Validation results : Solene and measurements temperatures.

3 RESULTS

3.2 Sensitivity analysis

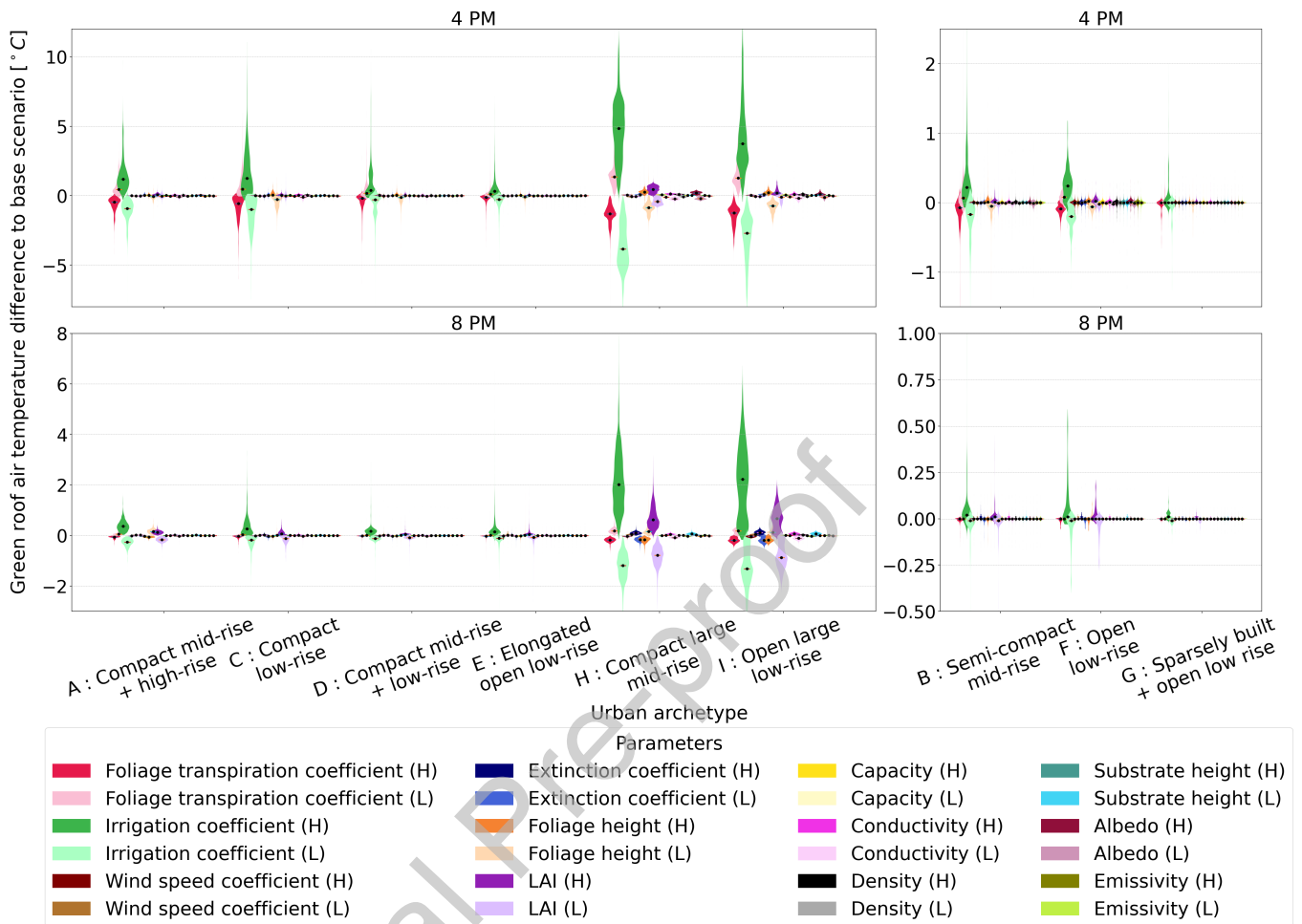


Figure 6: Above green roof air temperature reduction (compared to base scenario) for 4 PM (top) and 8 PM (bottom). H = high and L = low specify the parameter value that was modified compared to base scenario.

282 Across all urban block archetypes and at both 4 PM and 8 PM, the irrigation coefficient stands out as the
 283 most influential parameter affecting green roof air temperature (1.4 and 0.5 °C influence on average for low
 284 and high values at 4 PM and 8 PM). This is consistent with the fact that evapotranspiration is the primary
 285 cooling mechanism on green roofs [70]. Since the irrigation coefficient reflects the vegetation's moisture
 286 availability, it directly controls evapotranspiration rates and thus significantly impacts air temperature. A
 287 high irrigation coefficient promotes greater evaporative cooling by diverting more solar energy towards
 288 water evaporation rather than heat storage. The foliage transpiration coefficient, which determines the
 289 partitioning of evapotranspiration between plant transpiration and soil evaporation, is the second influ-
 290 ential parameter at 4 PM (0.6 °C influence). At 4 PM, foliage height emerges as the third most influential
 291 parameter (0.15 °C influence). Notably, decreasing foliage height below the base level significantly warms

Parameter	Average parameter influence on green roof air temperature [°C]			
	Low - 4 PM	High - 4 PM	Low - 8 PM	High - 8 PM
Foliage transpiration coefficient	0.573	-0.564	0.063	-0.063
Irrigation coefficient	-1.207	1.623	-0.396	0.647
Wind speed coefficient	-0.024	0.018	0.019	-0.017
Extinction coefficient	0.037	-0.023	-0.053	0.033
Foliage height	-0.300	0.091	0.070	-0.055
LAI	-0.076	0.109	-0.254	0.204
Capacity	-0.036	0.023	0.000	0.004
Conductivity	-0.085	0.043	-0.034	0.021
Density	-0.027	0.032	-0.001	0.007
Substrate height	0.012	0.013	0.022	-0.008
Albedo	-0.049	0.047	-0.002	0.002
Emissivity	-0.007	0.005	-0.003	0.003

Table 3: Parameter influence on green roof air temperature, averaged across all archetypes. A positive sign means the parameter change raises air temperature 2-m above the green roof.

the air, whereas increasing it above the base provides only limited additional cooling. At 8 PM, LAI has more influence than foliage height (0.2 to 0.05 °C influence). Although the influence of parameters is similar across the block archetypes, the irrigation coefficient, LAI, foliage transpiration and foliage height have a higher impact for compact large mid-rise and open large low-rise archetypes compared to other archetypes.

Table 4 presents how the green roof air temperature varies with the 12 parameters and the physical explanations beneath these impacts. The influence of the parameters on air temperature arises from opposing effects on the foliage and substrate layers due to their distinct thermal and physical characteristics. For instance, increasing the extinction coefficient and LAI reduces the transmission of solar radiation through the foliage, thereby increasing absorption in the canopy while limiting energy reaching the substrate. However, because foliage has a low heat capacity and a large surface area (with high LAI) exposed to air, it heats up quickly but also cools efficiently via convection. The substrate, on the other hand, has a higher thermal mass and limited exposure, so it warms more slowly but retains heat longer. This can result in prolonged heating of the canopy air layer when the LAI and extinction coefficient are low.

Similarly, a higher foliage transpiration coefficient increases the proportion of evapotranspiration that comes from plant transpiration rather than soil evaporation. This leads to a cooler foliage surface temperature, but potentially a warmer substrate surface, as less water is available for evaporative cooling from the substrate. As with the extinction coefficient and LAI, this highlights the importance of concentrating energy exchange processes in the foliage, which can more efficiently regulate heat.

Finally, increasing foliage height and wind speed coefficient enhances convective exchanges between

312 the canopy air and the ambient atmosphere. During the day, this promotes the upward transfer of heat
 313 from the canopy to the atmosphere, contributing to a cooling effect. At night, when the ambient air is
 314 generally cooler, stronger convection accelerates the cooling of the canopy air. However, the net effect
 315 depends on the temperature gradient and the time of night: in the early evening, mixing may initially raise
 316 the green roof air temperature by blending warmer canopy air with cooler ambient air. This is evident in
 317 the 8 PM results, where an increase in foliage height is actually associated with a rise in air temperature. As
 318 the night progresses, this same mixing promotes faster cooling, potentially resulting in lower temperatures
 319 later in the night.

320 It is important to note that all results related to substrate properties are highly sensitive to the simula-
 321 tion setup, particularly the short (half a day) simulation period and the assumption of a fixed indoor air
 322 temperature, which together constrain the extent to which substrate heat dynamics can fully develop.

Table 4: Impact of parameters on green roof air temperature. A positive sign means an increase in the parameter raises air temperature 2-m above the green roof.

Parameter	4 PM	8 PM	Impact of increasing the parameter
Foliage transpiration coefficient	+	+	Larger plant transpiration cools foliage but reduces substrate evaporation; overall, canopy air temperature tends to rise.
Irrigation coefficient	-	-	Promotes greater evapotranspiration, reducing heat in foliage and substrate, leading to cooler green roof air.
Wind speed coefficient	-	-	Increased convection with ambient air causes cooling.
Extinction coefficient	+	+	More solar radiation absorbed by foliage reduces substrate radiation but increases substrate heating, raising air temperature.
Foliage height	-	+	Higher foliage increases convection cooling but also thermal inertia, delaying evening cooling.
LAI	-	-	Denser foliage reduces solar transmission and substrate heating, enhancing convective cooling.
Substrate height, capacity and density	-	-	Greater substrate thermal inertia slows heating, reducing heat transfer to canopy air and cooling the roof.
Conductivity	-	-	Improved heat transfer between cool indoor and outdoor layers lowers green roof temperature.
Albedo	-	-	Higher reflectivity reduces heat gain, especially during daytime.
Emissivity	-	-	Enhanced longwave emission cools surface, especially at night.

3 RESULTS

3.2 Sensitivity analysis

3.2.2. Air temperature and humidity rate at pedestrian level

Pedestrian air temperature and relative humidity are computed for each parameter variation and compared to the base scenario. Results are shown at 4 PM and 8 PM across the nine urban block archetypes (Fig. 7 and 8).

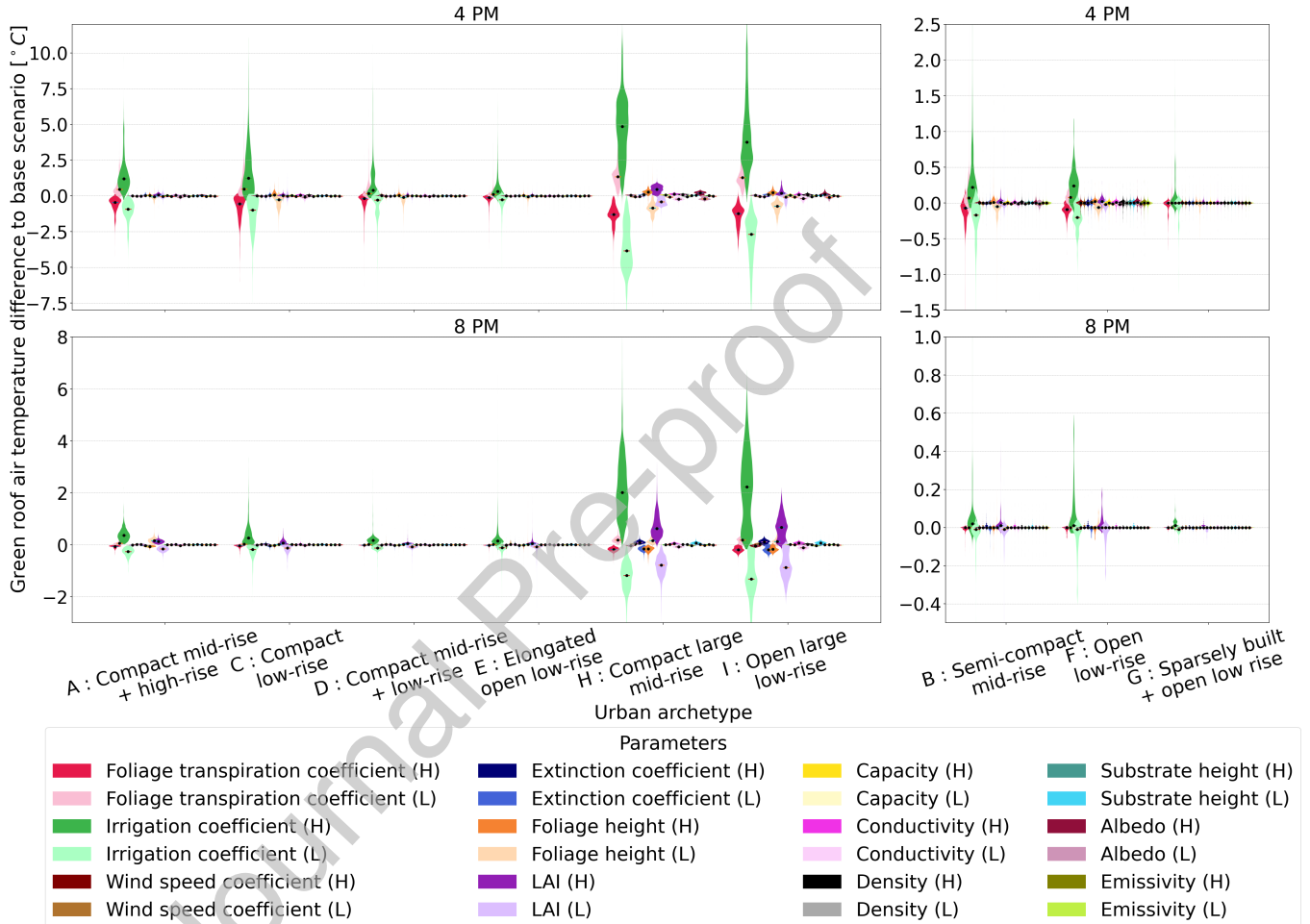


Figure 7: Pedestrian air temperature reduction (compared to base scenario) for 4 PM (top) and 8 PM (bottom). H=high and L=low specify the parameter value that was modified compared to base scenario.

Regarding pedestrian air temperature, the influence of each parameter mirrors that observed on green roof air temperature, which is expected given that the impact of green roof on pedestrian air temperature is majorly driven by convective exchanges with the air above the green roof.

Variations in mean relative humidity can reach up to 2 %, and their patterns differ from those observed for temperature. Since higher humidity tends to reduce comfort in warm conditions, some configurations that lower air temperature may actually lower comfort. For example, increasing the irrigation coefficient

3 RESULTS

3.2 Sensitivity analysis

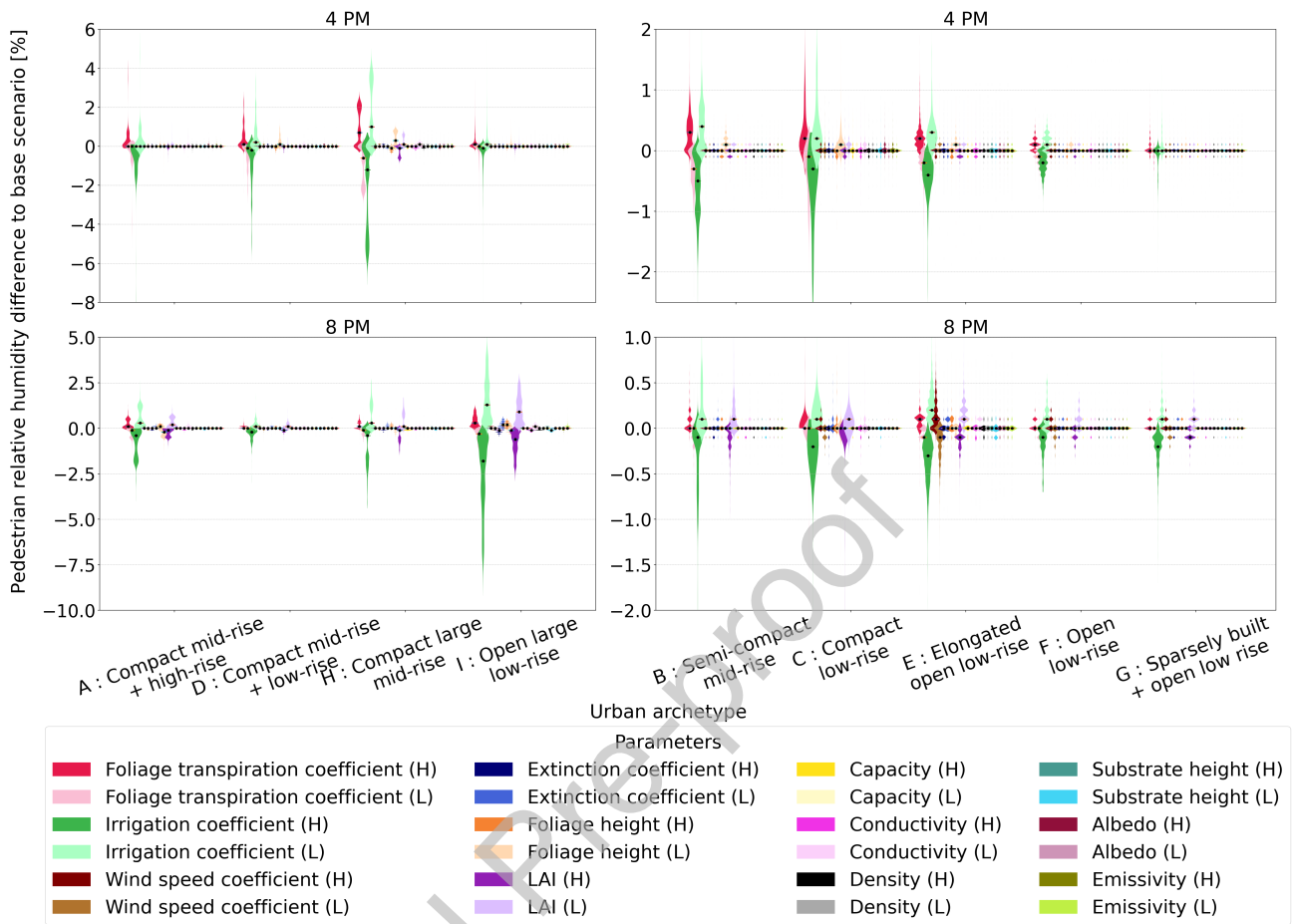


Figure 8: Pedestrian relative humidity reduction (compared to base scenario) for 4 PM (top) and 8 PM (bottom). H = high and L = low specify the parameter value that was modified compared to base scenario.

333 or LAI leads to lower pedestrian air temperatures but simultaneously results in higher humidity levels. This
 334 relationship is explained further in the next section with heat index.

3 RESULTS

3.2 Sensitivity analysis

3.2.3. Pedestrian heat index

Figure 9 shows the heat index, integrating the combined influence of pedestrian air temperature and relative humidity on perceived thermal comfort. The heat index results mimic the results of pedestrian air temperature. The similarity between the heat index graph (Fig. 9) and the pedestrian air temperature graph (Fig. 7) indicates that green roof parameters have a stronger influence on air temperature than on humidity, relative to their respective contributions to the heat index. Therefore when combining air temperature and humidity in the heat index, the parameters' influence are of the same sign as for the air temperature.

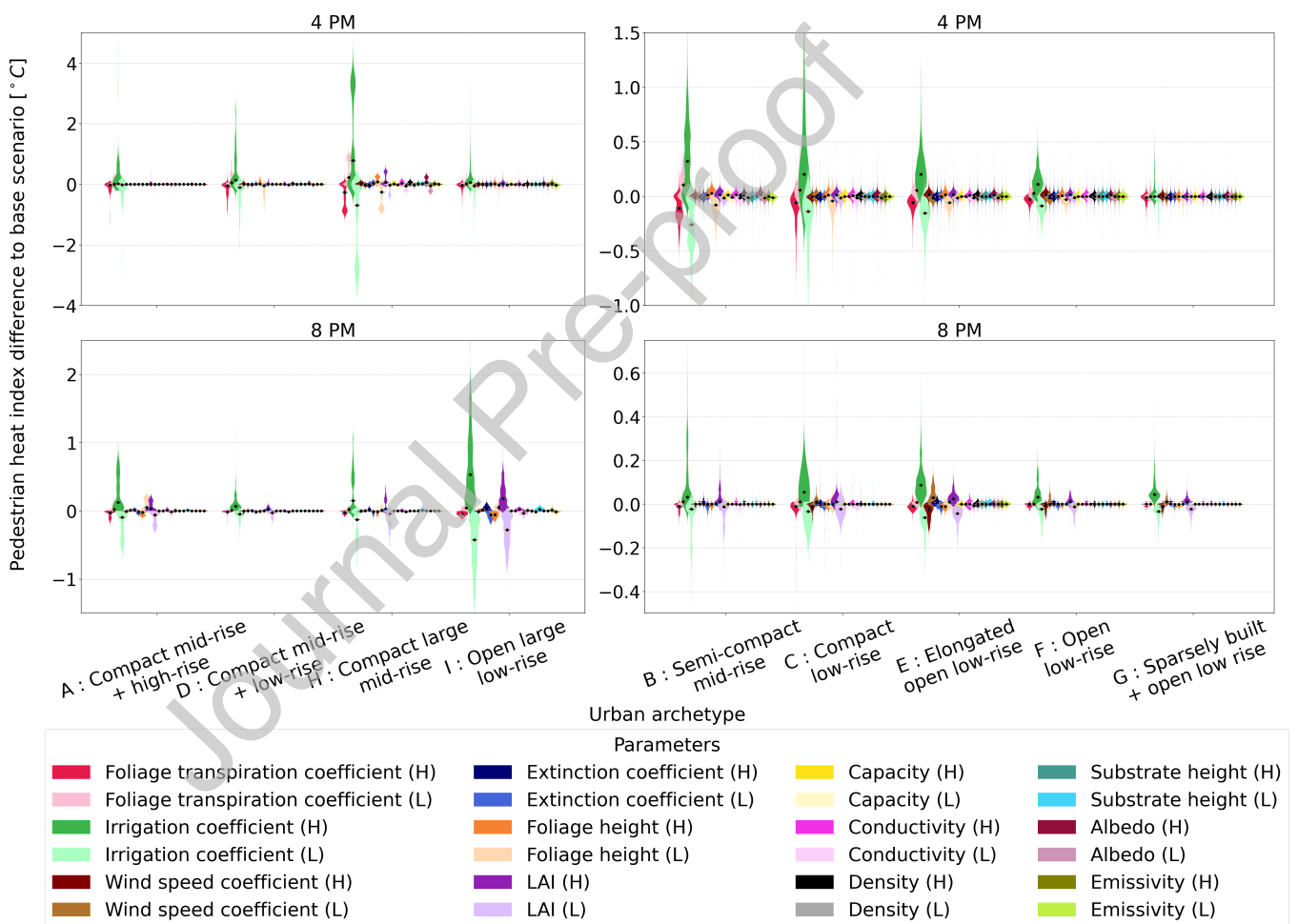


Figure 9: Pedestrian heat index reduction (compared to base scenario) for 4 PM (top) and 8 PM (bottom). H=high and L=low specify the parameter value that was modified compared to base scenario.

Overall, the heat index values range between 36 °C and 40 °C. According to the official classification by the U.S. National Weather Service, this falls within the 'Extreme Caution' category (32 – 41 °C), where pro-

3 RESULTS

3.2 Sensitivity analysis

³⁴⁵ longed exposure or physical activity could lead to heat-related illness. Even if these values are indicative,
³⁴⁶ this highlights the importance of reducing the heat index, even by a fraction of a degree.

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4 DISCUSSION

4. Discussion

4.1. Green roof parameters : influential & uncertain

Although there are noticeable differences in parameter impact across different hours, the top four most influential parameters remain consistent throughout the day. While the evapotranspiration coefficient appears to have a significantly greater influence on pedestrian temperature, it also comes with higher uncertainty compared to other parameters (see a larger variation range in Table 2). Here, a parameter's uncertainty is defined as the range of values it can take. The wider this range, the more possible values researchers must choose from, which increases uncertainty in simulations when parameters haven't been experimentally determined.

To address this issue of varying uncertainty, the influence of each parameter on pedestrian heat index is scaled by the range of its variation. This provides an estimate of the influence per unit change in the parameter, under the assumption of a linear relationship between parameter variation and pedestrian temperature response. A practical way to reveal each parameter's relative influence is to compute the average heat index difference it causes across archetypes, then divide the result by the range between its low, default, and high values. This ratio offers a more comparable metric of influence across parameters. This process is called scaling. Parameters were then ranked according to this scaled (S) influence on pedestrian heat index.

Table 5 summarizes the parameters rankings at 4 PM and 8 PM, based on both impact and uncertainty. For the influence ranking, both scaled (divided by the range of values of the parameter) and the non-scaled (straight influence on pedestrian heat index) are depicted. The uncertainty ranking is determined by calculating the percentage increase from the base value to the high value, and similarly, the percentage decrease to the low value. The six most uncertain parameters are marked with a U, and the six most influential (based on cumulative rank across both times) are marked with an I.

This scaling helps explain why parameters such as emissivity may appear to have little impact: their input ranges are small due to high certainty, not because they are inherently unimportant. At 8 PM convection takes a more important place than at 4 PM, therefore wind speed coefficient and extinction coefficient have more impact. While at 4 PM, solar radiation dominates, making albedo more influential.

Influential parameters are those for which small variations lead to significant changes in the heat index, while uncertain parameters are those with a wide possible range of values. The most critical parameters in this context are those that are both influential and uncertain. The irrigation coefficient, foliage height, and LAI fall into this category.

Parameter	Low-Default-High	Uncertainty ranking	Impact ranking at 4 PM (S)	Impact ranking at 8 PM (S)	Type
Foliage transpiration coefficient [-]	0.5 - 0.75 - 1	7	2 (2)	3 (4)	x - I
Irrigation coefficient [-]	0.1 - 0.75 - 1.5	1	1 (1)	1 (1)	U - I
Wind speed coefficient [-]	0.8 - 1 - 1.2	11	7 (5)	3 (3)	x - I
Extinction coefficient [-]	0.5 - 0.7 - 0.9	9	11 (11)	6 (5)	x - x
Foliage height [m]	0.05 - 0.25 - 0.5	2	3 (4)	4 (7)	U - I
LAI [-]	1 - 2.5 - 5	3	5 (7)	2 (2)	U - I
Substrate heat capacity [$J.kg^{-1}.K^{-1}$]	700 - 950 - 1200	10	9 (9)	11 (11)	x - x
Substrate conductivity [$W.m^{-1}.K^{-1}$]	0.2 - 0.6 - 1	4	6 (8)	7 (8)	U - x
Substrate density [$kg.m^{-3}$]	600 - 950 - 1300	6	8 (10)	10 (10)	U - x
Substrate thickness [m]	0.1 - 0.2 - 0.3	5	12 (12)	8 (9)	U - x
Foliage albedo [-]	0.2 - 0.3 - 0.4	7	4 (6)	12 (12)	x - x
Foliage emissivity [-]	0.85 - 0.9 - 0.95	12	10 (3)	9 (6)	x - I

Table 5: More uncertain parameters: U stands for uncertain, I for influential. Impact rankings with scaled values are given in parentheses.

378 Table 6 presents the average reduction in pedestrian heat index associated with selected parameters,
379 compared to base scenario. Only impacts greater than $\pm 0.1^\circ C$ (for average of all walkable surfaces) are
380 shown, as this threshold was chosen to represent a meaningful effect (as decided in [71]). Among all
381 tested parameters, only four exceed this threshold in several urban block archetypes: foliage transpira-
382 tion coefficient, irrigation coefficient, foliage height, and LAI. The parameter influence on pedestrian air
383 temperature, averaged across all archetypes, for all parameters is provided in Appendix, with Table 14.

384 The results show that to effectively reduce urban overheating through green roofs, irrigation is essential.
385 Transitioning from a medium-moisture to a well-irrigated green roof improves pedestrian temperature
386 by an average of $0.4^\circ C$ across all urban archetypes, reaching up to $1.4^\circ C$ for the compact large mid-rise
387 archetype.

388 Another key benefit of irrigation is plant survival. Without sufficient water, vegetation may die, greatly
389 reducing the effectiveness of green roofs. This study assumes healthy, living vegetation and does not
390 capture the diminished benefits of dead or poorly maintained green roofs.

391 Regarding vegetation characteristics, the effects of LAI and foliage height were assessed independently,
392 making it difficult to precisely quantify their combined impact. However, increasing both density and
393 height from medium to high is expected to slightly improve pedestrian comfort.

4 DISCUSSION

4.1 Green roof parameters : influential & uncertain

Parameters	A	B	C	D	E	F	G	H	
Foliage transpiration coefficient (high)	-0.11	-0.11	x	-0.23	x	x	x	-0.37	
Foliage transpiration coefficient (low)	x	0.11	x	0.23	x	x	x	0.35	
Irrigation factor (high)	0.31 (0.26)	0.36 (0.11)	0.28	0.69 (0.21)	0.24	0.14	0.19	1.38 (0.28)	0.27 (0)
Irrigation factor (low)	-0.22 (-0.19)	-0.27	-0.19	-0.51 (-0.15)	-0.19	-0.10	-0.14	-1.20 (-0.21)	-0.22 (-0)
Foliage height (high)	x	x	x	x	x	x	x	0.11	
Foliage height (low)	x	x	x	x	x	x	x	-0.35	
LAI (high)	x	x	x	x	x	x	x	0.16	x (0)
LAI (low)	x (-0.10)	x	x	x	x	x	x	-0.12 (-0.13)	x (-0)

Table 6: Average impact on heat index at pedestrian level [$^{\circ}\text{C}$]: temperature difference relative to the baseline scenario, per urban archetype. In parenthesis values for 8 PM that respect the threshold. Values with an absolute magnitude below 0.1 are marked with a cross. Parameters for which all values were below this threshold are omitted from the table.

394 In summary, tall, dense, irrigated green roofs offer the most effective cooling solutions. This may also
395 require deeper substrates to support such vegetation, as taller plants often need more growing medium.

396 The strong influence of irrigation parameters, LAI, and foliage height observed in this study as well
397 as the overall influence of improving the green roof parameters are consistent with findings reported in
398 the literature. First, as shown by the majority of sensitivity analysis studies summarized in Table 1, LAI
399 and soil thickness are generally identified as the most influential parameters affecting green roof cooling
400 performance; however, irrigation-related factors were not explicitly investigated in these studies.

401 Second, Wang et al. (2022) [72] compared two city-scale scenarios in Berlin (Cfb climate) assuming
402 100 %green roof implementation, with and without irrigation, using the WRF model. Averaged over urban
403 grid cells, irrigated green roofs reduced air temperature by $0.71\text{ }^{\circ}\text{C}$, compared to $0.55\text{ }^{\circ}\text{C}$ for non-irrigated
404 roofs. In the present study, there is an average temperature difference of $0.427\text{ }^{\circ}\text{C}$ (Table 14) between
405 scenarios with moderately moist substrates and well-irrigated green roofs at 4 PM, which is of comparable
406 magnitude.

407 Third, Morakinyo et al. (2017) [6] investigated green roofs under various climates, urban densities,
408 roof coverage ratios, and configurations (extensive versus intensive) using ENVI-met and EnergyPlus. Their
409 results indicate that green roofs with increased substrate depth and vegetation height achieved approxi-
410 mately twice the cooling effectiveness. Joshi et al. (2024) [25] reported an average cooling effect of about

4 DISCUSSION

4.2 Variation across urban archetypes

411 0.5 °C when comparing green roof scenarios with non-green roof cases with Solene-microclimat, while in
 412 the present study the cumulative improvement of green roof parameters at 4 PM reaches approximately
 413 0.7 °C (Table 14). Although the present study does not identify a strong individual influence of vegeta-
 414 tion height or substrate depth, the observed doubling of cooling intensity resulting from overall green roof
 415 parameter improvements remains consistent with these findings.

416 Finally, in a Dfa climate, Berardi et al. (2016) [9] showed that increasing LAI enhances daytime air
 417 temperature cooling at the pedestrian level by up to 0.4 °C. Similarly, in this study, increasing LAI led to
 418 a maximum air-temperature reduction of 0.38 °C for archetype H (Table 6), although the average effect
 419 across archetypes remained below 0.1 °C (Table 14).

420 4.2. Variation across urban archetypes

421 The aim here is to understand how the urban morphology of the archetypes explains the varying in-
 422 fluence of green roof parameters on the different metrics used. Fig. 10 displays key characteristics of the
 423 urban archetypes, helping to interpret the variations in results observed between them.

424 Archetypes H and I show the strongest parameter influences on green roof air temperature, both in terms
 425 of average effect and variability (see Fig. 7). The results are similar to what Joshi et al. (2024) observed.
 426 These archetypes also feature the largest green roof areas, both in total surface and in the size of individual
 427 roofs. Although archetype A has a similar percentage of green roof coverage as archetype I, the parameter
 428 impacts differ significantly. This could be explained by the fact that archetype A consists of smaller green
 429 roofs located at varying altitudes, leading to weaker interactions between green roofs, potentially account-
 430 ing for the observed differences. To explore this further, the analysis uses a proximity-weighted green roof
 431 density metric (PWGRD) that quantifies the local concentration of green roofs surrounding each green roof
 432 mesh element.

433 It is calculated by summing the surface areas of nearby green roofs, each weighted by the inverse of
 434 the square of its distance to the target mesh part, giving more influence to closer surfaces (see Eq. 2).

$$PWGRD_j = \sum_{i=1}^N \frac{A_i}{d_{ij}^2} \quad (2)$$

435 with $PWGRD_j$ the proximity-weighted green roof density metric of the green roof mesh j , A_i the surface
 436 area of green roof i , d_{ij} = the distance from green roof i to the target mesh part j , N the number of green
 437 roof surfaces within the considered proximity (150 m radius). This radius is considered based on the results
 438 of the cooling distance obtained in the literature. The cooling distance is the length between the center of

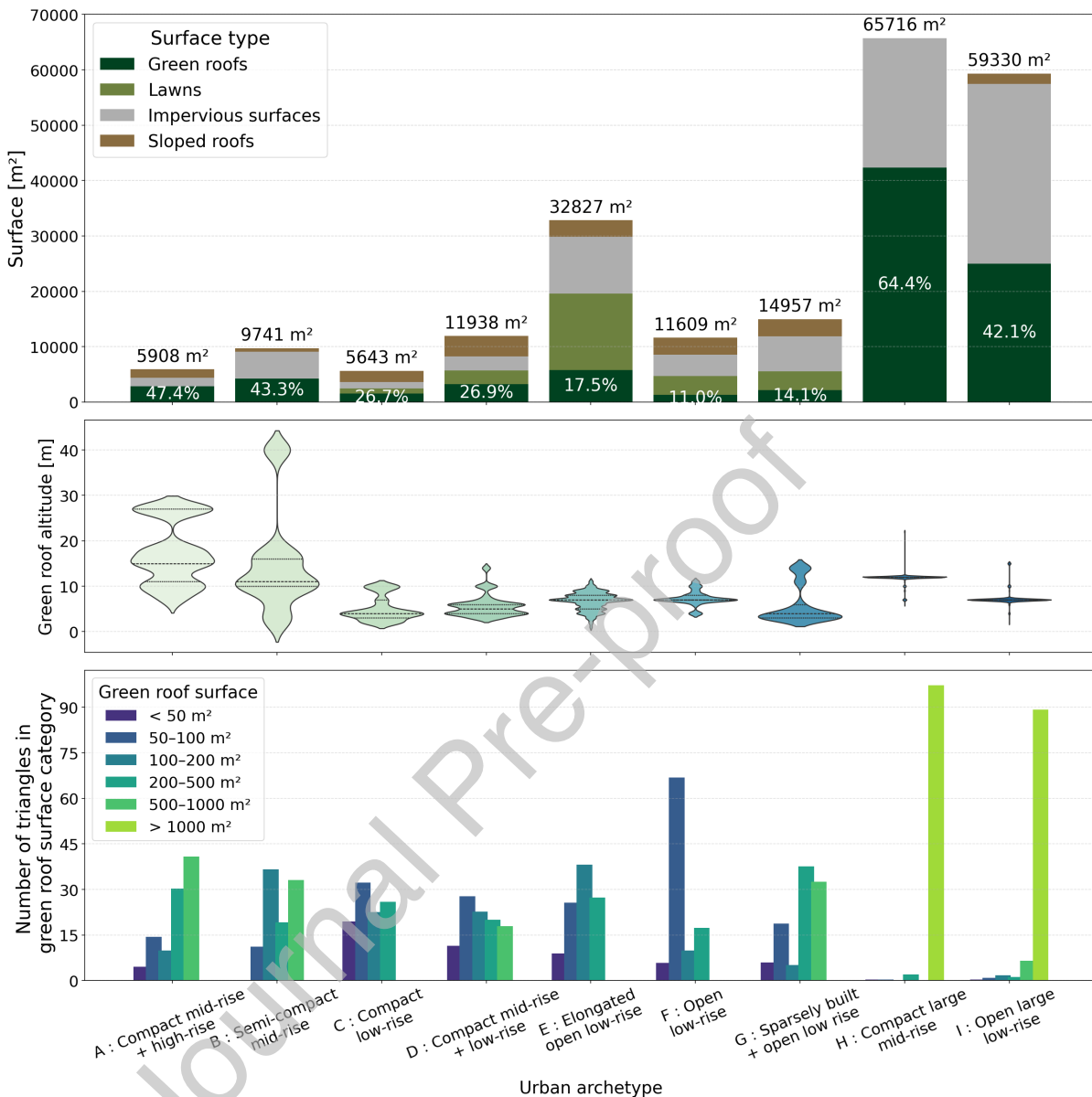


Figure 10: Urban archetypes characteristics

439 the green roof and the boundary of the cooling area. Soltanifard et al. (2025) [73] reviewed the cooling
 440 effect of urban green infrastructure and found that the cooling distance is between 120 and 300 m.

441 This approach captures not just the quantity but the spatial clustering of green roofs. A radius of 150
 442 meters is used to define the neighborhood around each mesh part, ensuring relevant local interactions are
 443 considered. The resulting values are then averaged at the block level, providing an indicator of green roof
 444 density per urban archetype. These block-level densities are compared to the high irrigation coefficient

445 results, computed as the difference from the baseline scenario. To assess the strength of this relationship,
 446 a Pearson correlation analysis was conducted. As shown in Fig. 11, the results reveal a strong correlation,
 447 suggesting that the spatial distribution of green roofs largely explains the variation in the impact of the
 448 irrigation coefficient on green roof air temperature. Indeed, more than 90% of the variance in irrigation
 449 coefficient impact is explained by the variance in the green roof proximity-weighted green roof density.
 450 The irrigation coefficient was selected for this analysis as it exhibits the most significant variation and is
 451 discussed in detail.

452 Overall, these findings suggest that green roof air temperature is sensitive to parameter changes, espe-
 453 cially when green roofs are spatially concentrated. It is important to note that in this analysis, all green
 454 roofs share the same parameter values. As a result, nearby green roofs, even if located on different build-
 455 ings, affect each other: modifying a parameter such as the irrigation coefficient simultaneously for several
 456 adjacent roofs amplifies the temperature response. However, in real-world conditions, green roofs on sep-
 457 arate buildings are likely to be managed independently. For example, if one building irrigates its green
 458 roof while a neighboring one does not, the mutual influence is reduced. This emphasizes once again that
 459 a single, large green roof tends to be more effective than multiple smaller, disconnected ones.

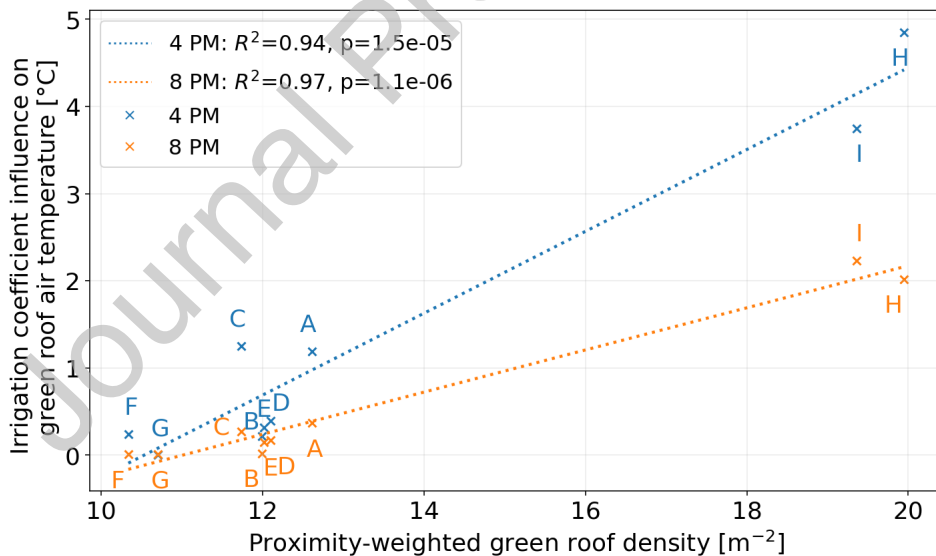


Figure 11: Irrigation coefficient impact (high to base scenarios) on green roof air temperature depending on the proximity weighted green roof density

4.3. Pedestrian values

Some of the differences in parameter impacts on green roof air temperature also help explain their influence at the pedestrian level. In particular, blocks such as F and G, which showed limited sensitivity to green roof parameters at roof level, also exhibit relatively low impacts on pedestrian air temperature and heat index. Archetypes like H and I, which displayed strong parameter influence on green roof temperature, maintain similarly high impacts at the pedestrian level. Previously, how green roof density influences the sensitivity of green roof air temperature to green roof parameters was shown. The next step is to assess how effectively each urban archetype transmits these rooftop temperature changes down to the pedestrian level.

Using the same approach as for the proximity-weighted green roof density, the ground-level green roof density, which quantifies the localized concentration of green roofs around each walkable triangle, is computed. This indicator reflects the density of green roofs as perceived from pedestrian areas. Figure 12 shows the relationship between this ground-level density and the impact of the irrigation coefficient on the heat index at 4 PM. No significant correlation is observed at 8 PM. At 4 PM, however, 63% of the variance in the irrigation coefficient impact on the heat index is explained by the ground-level green roof density. Although this is a weaker correlation than at the roof level, it remains meaningful given that at the pedestrian level, all the characteristics of the archetypes are considered.

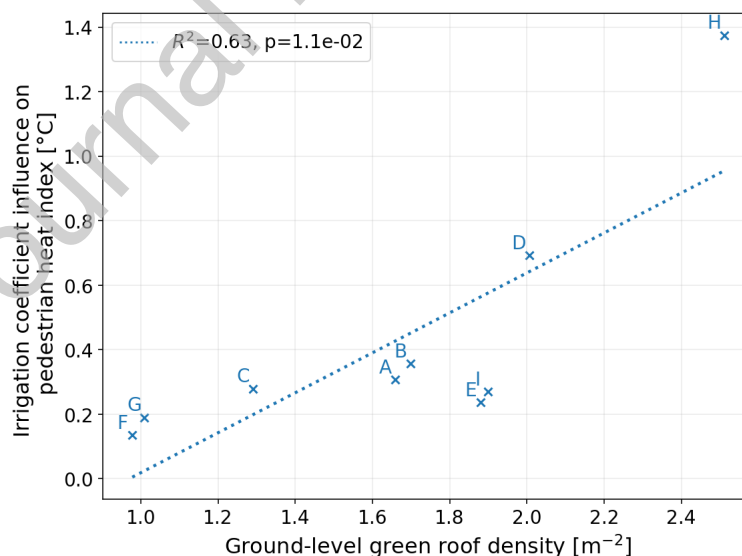


Figure 12: Irrigation coefficient impact (high-base) on the heat index depending on the ground-level green roof density

It is worth noting that H and I display similarly high proximity-weighted green roof densities, indicating

478 tightly clustered green roof triangles with strong mutual influence. However, H exhibits a much higher
 479 ground-level green roof density than I. This difference stems from the layout of walkable paths: in H,
 480 pedestrian areas are well distributed around the building and its green roofs, while in I, many walkable
 481 areas are located farther away. This spatial arrangement likely explains why, at 4 PM, parameter impacts
 482 on the heat index are considerably stronger for H than for I.

483 Similarly, A, C, and D had comparable impacts on green roof air temperature. However, D had a much
 484 greater impact at the pedestrian level, due to its higher ground-level green roof density. In both A and
 485 I, a significant portion of the green roof area is located at one corner of the urban block, which limits its
 486 influence at 4 PM to nearby zones only. However, later in the evening, air mixing through convection
 487 becomes more effective, allowing the cooling effect of the green roof to spread more widely across the
 488 block. This behavior is illustrated in Table 6, where A and I are the only two archetypes for which the
 489 average reduction in heat index at the pedestrian level at 8 PM is equal to or greater than that observed at
 490 4 PM. For all other archetypes, the cooling impact is more pronounced at 4 PM than at 8 PM. Therefore,
 491 both A and I archetypes exhibit an enhanced evening cooling effect.

492 This result aligns well with the existing literature. Previous studies have shown that temperature re-
 493 ductions associated with green roofs tend to increase with a higher roof-to-ground ratio and lower building
 494 heights [72, 6, 74, 75, 76, 25]. As the magnitude of temperature reduction grows, it is reasonable to expect
 495 that enhancements in green roof parameters will have an amplified effect. Specifically, when green roofs
 496 exert a stronger influence on near-ground air temperatures, any factor affecting roof-level thermal perfor-
 497 mance is more likely to propagate downward, impacting ground-level conditions as well. Furthermore,
 498 While the results cannot be directly generalized due to the specific urban archetypes of Liège, the observed
 499 relationship between the irrigation-related coefficient and both ground-level and proximity-weighted green
 500 roof density may be applicable to other urban contexts, as these metrics can be computed for any archetype.

501 Some urban archetypes demonstrate greater effectiveness in cooling the pedestrian level than others.
 502 However, these configurations often require extensive green roof coverage, which entails significant reno-
 503 vation efforts and associated costs. To account for both the cooling benefit and the implementation effort,
 504 a Thermal Mitigation Ratio (TMR), defined as in Eq 4.3, is introduced:

$$505 \quad \text{TMR} = \frac{A_{\text{walkable}}}{A_{\text{green_roof}}} \times I_{\text{IF}} \quad (3)$$

506 with A_{walkable} the surface area of walkable paths (the area to be cooled), $A_{\text{green_roof}}$ the surface area of

507 green roof (the area with investment) and I_{IF} the irrigation coefficient influence on heat index at 4 PM. This
 508 ratio is calculated using the irrigation coefficient influence on the heat index at 4 PM. It highlights which
 509 urban archetypes benefit most from improvements in green roof parameters, by quantifying their impact
 510 on thermal mitigation relative to the effort required to implement green roofs. This metric is computed
 511 assuming the implementation effort and the heat index reduction scale linearly with rooftop surface area,
 512 which is a simplification. Table 7 presents the results, with archetypes ranked by their thermal mitigation
 513 ratio.

Archetype	D	E	G	F	H	B	C	I	A
Thermal mitigation ratio [$^{\circ}\text{C}\cdot\text{m}^2/\text{m}^2$]	1.1	1.0	0.9	0.8	0.8	0.4	0.4	0.3	0.2

Table 7: Thermal mitigation ratio per archetype

514 Joshi et al. [25] ranked urban archetypes by their average ground air temperature under identical
 515 meteorological conditions, without green roofs. Their results show that average temperatures can differ by
 516 up to 5°C between archetypes. The ranking from highest to lowest air temperature was: H, B, I, A, G, D, C,
 517 F, E. These differences were primarily attributed to higher levels of impervious surfaces, greater building
 518 density, and increased building heights.

519 Interestingly, the ranking of archetypes by thermal mitigation ratio (Tab. 7) appears almost reversed.
 520 This suggests that the hottest archetypes, with higher levels of impervious surfaces, greater building density,
 521 and increased building heights, tend to benefit less from improving parameters. In contrast, less dense and
 522 less built-up configurations seem to be more responsive to green roof improvements, making them more
 523 favorable candidates for such strategies.

524 For archetypes D and E, for example, enhancing a green roof from medium moisture to well irrigated
 525 conditions on a 1 m^2 area results in an approximate reduction of 1°C in heat index for 1 m^2 of walkable area
 526 at pedestrian level. As previously discussed, this mitigation effect arises from complex physical interactions
 527 at the block scale and cannot be directly extrapolated to other urban configurations or to scaled-down
 528 versions of these blocks.

529 However, the effort to green the roofs and maintain them is not the same for all archetypes and build-
 530 ings. First, in certain configurations, the feasibility of installing green roofs is influenced by building
 531 ownership. For example, it is generally easier to implement green roofs on archetypes H and I, which
 532 represent commercial centers, than on archetype D, which consists primarily of individual houses. Nev-
 533 ertheless, some archetypes are more prevalent in Liège. In particular, archetype D is the most common
 534 [49]. Second, green roofs are usually feasible on flat roofs [77]. However, supporting intensive green roofs

4 DISCUSSION

4.4 Influence of meteorological conditions on the green roof parameter sensitivity

535 (dense, irrigated, with thicker substrates) add considerable weight on the buildings. Whether the buildings
536 can support such green roofs depends on the reserved structural capacity of the buildings, which needs
537 further investigation before implementation.

538 4.4. Influence of meteorological conditions on the green roof parameter sensitivity

539 It has been found that in hot-humid regions, the evaporative cooling potential of vegetation is reduced
540 compared to hot-dry regions. Furthermore, the cooling effect of green roofs is lower under conditions of
541 low solar radiation and high relative humidity [78, 11], both on specific days and, by extension, in regions
542 characterized by such conditions. For instance, Morakinyo et al. [6] investigated the performance of green
543 roofs across different climates using ENVI-met and EnergyPlus. Their results indicate that overall daytime
544 cooling effectiveness follows this order: hot-dry, hot-humid, warm-humid, and temperate.

545 It should be noted that these results are based on simulations with fixed irrigation settings that are
546 independent of local climate. Thus, they do not account for water stress in arid regions, where irrigation
547 may be limited, nor for water availability in non-irrigated green roofs, which may be less critical in humid
548 regions.

549 As a result, the sensitivity of model parameters may vary. Under more humid conditions, the influ-
550 ence of the irrigation coefficient may be reduced. Under higher solar radiation, parameters governing the
551 absorption and interception of solar fluxes, such as albedo or LAI, may become more influential. Under
552 windier conditions, sensitivity to wind speed-related parameters may decrease. A comprehensive assess-
553 ment of these interactions could be achieved in future work through a global sensitivity analysis that jointly
554 considers meteorological variables and green roof parameters.

5 CONCLUSION

5. Conclusion

Solene-microclimat results were compared to measurements in very hot summer meteorological conditions. Findings are that the model reproduces the physical processes of green roofs correctly.

The parameters used for green roof modeling in Solene-microclimat were identified, along with their plausible ranges of values. These ranges were established based on a literature review, providing useful reference values when no specific data are available. For each parameter, a baseline, high, and low value were selected to assess their individual influence on several outputs: air temperature above the green roof, pedestrian level air temperature and humidity, and the resulting heat index. This analysis was conducted across nine urban archetypes representative of the city of Liège, Belgium with realistic greening. It enables a detailed examination of how green roof properties interact with urban morphology to affect pedestrian thermal comfort.

For the parameters considered, changes that decrease air temperature at pedestrian level often result in higher relative humidity, which may in turn reduce thermal comfort. However, when combining both factors using the heat index, the cooling effect generally remains significant, although it is partially offset by the rise in humidity. Irrigation proves essential for maximizing the cooling potential of green roofs; well-irrigated systems can reduce pedestrian level temperatures by up to 1.4 °C compared to medium irrigated ones. Tall and dense vegetation further enhances cooling performance. Increasing both density and height from medium to high is expected to improve pedestrian comfort by at least 0.1°C. Modeling green roofs requires numerous parameters, each subject to varying levels of uncertainty. These parameters were classified based on their influence on cooling performance and their associated uncertainty.

Four parameters emerge as both highly influential and relatively uncertain: the two irrigation related parameters, foliage density (LAI), and foliage height. This study shows that other parameters, such as those related to substrate properties, have little to no effect on pedestrian thermal comfort. However, simulations were performed over a short period of time, and substrate parameters may become more relevant over longer simulations, with inertia effects. Overall, relative parameter rankings and trends are more reliable than absolute temperature or heat index values, as they are likely less sensitive to meteorological conditions and model parameterization.

Regarding the archetypes, the effect of green roof parameters on roof air temperature depends strongly on how green roof surfaces are spatially distributed. When green roofs are large and closely grouped, parameter adjustments yield a greater cooling impact. The influence of green roofs on the heat index along walkable paths is closely linked to the proximity of green roofs to these paths. The nearer the green roofs

5 CONCLUSION

586 are to these pedestrian areas, the stronger their effect on thermal comfort. To account for both cooling
587 effectiveness and implementation effort, a thermal mitigation ratio was introduced, ranking archetypes
588 based on the amount of walkable area cooled per unit of green roof implemented. This metric highlights
589 that while some configurations achieve good thermal outcomes, they often require disproportionately large
590 green roof areas to cool relatively small pedestrian zones. The compact mid-rise + low-rise archetype was
591 found to have the best thermal mitigation ratio.

592 However, several limitations of this study should be acknowledged. First, parameter sensitivity is
593 context-dependent. The observed impacts of each parameter are influenced by the values assigned to
594 the others. The current approach does not allow conclusions on the combined effects of interdependent
595 variables, such as LAI and foliage height, or the two irrigation parameters. A global sensitivity analysis
596 involving the most influential parameters is necessary to better understand their interactions. Given the
597 computational demands, such analyses could be focused on a limited number of configurations.

598 Furthermore, nighttime cooling was not assessed. This study focused on daytime conditions for a single
599 extreme heat day, with some results in early evening. Yet, nighttime thermal discomfort plays a critical
600 role in urban heat stress, especially during heat waves. The effects of green roofs on nocturnal cooling
601 should be explored in future research.

602 In addition, heat index was used as the sole metric for thermal comfort. While this indicator captures
603 combined effects of temperature and humidity, it does not account for radiant heat exchange and wind
604 effects. Including mean radiant temperature would provide a more comprehensive evaluation of pedestrian
605 thermal comfort. Although the Solene-microclimat tool allows such calculations, their high computational
606 cost prevented their inclusion in this study. Future work could incorporate this dimension.

607 Finally, the results depend on several hypotheses. Meteorological conditions, for instance, significantly
608 influence green roof performance. High relative humidity has been shown to suppress evapotranspiration
609 and reduce latent heat flux. As such, the outcomes presented here are highly sensitive to the weather
610 conditions. Future studies could explore how irrigation strategies affect cooling potential under more
611 humid conditions. Additionally, indoor temperature was fixed, limiting the representation of building
612 thermal dynamics. This assumption limits the analysis to buildings with cooling systems and might reduce
613 the observable influence of substrate properties on cooling performance. Furthermore, the simulations
614 covered only half a day and therefore did not capture how buildings store and release heat over longer
615 periods. Extending the analysis to multiple days would provide a better understanding of the long-term
616 cooling potential of green roofs. Lastly, a local sensitivity analysis was performed, which allowed the

5 CONCLUSION

5.1 Sensitivity analysis modeling additional information

617 identification of influential parameters but did not capture potential interaction effects between them. A
 618 global sensitivity analysis, applied to all parameters or to the four most influential ones, would be necessary
 619 to further investigate these combined effects.

620 Declaration of interests

621 The authors declare that they have no known competing financial interests or personal relationships
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629 Appendix A

630 5.1. Sensitivity analysis modeling additional information

Type of surface	Material	Height [m]	Albedo [-]	Emissivity [-]
Walls	Concrete	0.3	0.3	0.9
Impervious surfaces	Asphalt	0.1	0.2	0.9
	Concrete	1		
Lawns	Foliage	0.05	0.25	0.9
	Soil	0.15		
Roofs	Concrete	0.2	0.3	0.9

Table 8: Surfaces composition for the local sensitivity analysis

Type of material	Conductivity [$\text{W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$]	Specific heat [$\text{J}\cdot\text{kg}^{-1}\cdot\text{K}^{-1}$]	Density [$\text{kg}\cdot\text{m}^{-3}$]
Asphalte	0.75	950	2100
Concrete	1.75	1000	2300
Soil	0.70	900	1600

Table 9: Thermophysical properties of materials used

Type of building	Composition
Wall	30 cm concrete
Roof	20 cm concrete
Green roof	10 cm substrate, 5 cm drainage layer, 15.5 cm concrete, 10 cm false ceiling
Street	10 cm asphalt, 1 m concrete

Table 10: Composition of walls and roofs

Material	Conductivity [$\text{W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$]	Specific heat [$\text{J}\cdot\text{kg}^{-1}\cdot\text{K}^{-1}$]	Density [$\text{kg}\cdot\text{m}^{-3}$]
Concrete	1.75	1000	2300
Drainage layer	0.1	600	500
False ceiling	0.21	840	900
Asphalt	0.75	950	2100

Table 11: Material description for the experimental validation

631 5.2. Experimental validation modeling additional information

632 5.3. Process-related parameters derivation

633 The model incorporates adjustment coefficients that distinguish soil evaporation and plant transpiration
634 and account for both plant characteristics and water stress to calculate a more suitable evapotranspiration
635 (ET) (Eq. 4).

$$ET = (K_s K_{cb} + K_e) \times ET_0 \quad (4)$$

636 Solene-microclimat introduces two key parameters: the irrigation coefficient (f), and the foliage tran-
637 spiration coefficient (α_{lat}). These parameters are directly used in the evapotranspiration calculation to
638 approximate vegetation response under varying moisture conditions, according to Eq. 5.

$$\phi_{lat,f} = \alpha_{lat} \times f \times ET_0 \quad (5)$$

$$\phi_{lat,se} = (1 - \alpha_{lat}) \times f \times ET_0$$

639 with :

- 640 • $\phi_{lat,f}$ the latent heat flux from the foliage (crop transpiration)
- 641 • $\phi_{lat,se}$ the latent heat flux from the ground surface (soil evaporation)
- 642 • α_{lat} that quantifies the part of transpiration in evapotranspiration
- 643 • f that quantifies the magnitude of evapotranspiration
- 644 • K_s the water stress coefficient
- 645 • K_{cb} the basal crop coefficient

• K_e the soil evaporation coefficient

To approximate the crop coefficient K_{cb} , tabulated values corresponding to vegetation types typically found on green roofs are consulted. Common examples include turf grass ($K_{cb,ref} = 0.8$), mint ($K_{cb,ref} = 1.1$), and alfalfa ($K_{cb,ref} = 1.15$). For the purposes of this study, a representative value of $K_{cb} = 1$ is adopted.

Several formulations of soil moisture extractions functions (K_s) exist in the literature (e.g., [79]), many of which express the ratio of actual to potential evapotranspiration as a function of the current soil water content relative to field capacity. This study adopts the commonly used and simplest formulation given by $K_s = \frac{\theta}{\theta_{FC}}$ [80], where θ is the current volumetric water content and θ_{FC} is the water content at field capacity.

For the soil evaporation coefficient, and following the methodology outlined in [57], the expression is derived under the assumption of $K_{cb} = 1$ as in Eq. 6.

$$K_e = \min \begin{cases} 0.2 \times \frac{0.5\theta_{WP} - \theta}{0.5\theta_{WP} - \theta_{FC}} \\ 1.2 \times \exp(-k_s \times LAI) \end{cases} \quad (6)$$

with θ_{WP} the wilting point and θ_{FC} the field capacity. Finally the two coefficients are expressed as in Eq. 7.

$$\begin{aligned} f &= \frac{\theta}{\theta_{FC}} + K_e \\ \alpha_{lat} &= \frac{\frac{\theta}{\theta_{FC}}}{\frac{\theta}{\theta_{FC}} + K_e} \end{aligned} \quad (7)$$

Assuming the wilting point ranges between 0.03 and 0.15 $m^3 m^{-3}$, the field capacity between 0.2 and 0.4 $m^3 m^{-3}$, that the water stress coefficient K_s varies between 0 and 1, and taking into account the previously defined variation ranges of the LAI and extinction coefficient, the resulting variation ranges for the irrigation coefficient and the foliage transpiration coefficient are respectively 0 to 1.5 and 0.5 to 1.

5.4. Parameter ranges

Reference	LAI [-]	Foliage height [m]	Emissivity [-]	Albedo [-]
[30]	0.15 - 4.95	0.05 - 0.95	0.81 - 0.99	0.15 - 0.45
[39]	0.1 - 5	0.1 - 0.3	x	x
[35]	1 - 6	0.05 - 0.5	x	x
[41]	0.5 - 5	x	x	x
[36]	0.5 - 5	x	1	0.3
[81]	3	0.3	0.9	0.2
[82]	1-5	0.03	0.95	0.22
[83]	2.2	0.035	x	0.29
[84]	2.5	0.2	0.95	0.22
[85]	0.1-5	0.2	x	x
[6]	2	0.3-1	0.95	0.35
[40]	0.1-5	0.3	0.95	0.22
[86]	2.8-5	0.05-0.475	0.97	0.155-0.22
[33]	0.001-3.5 ^a -5	0.005-0.3 ^a -1	0.8-0.95 ^a -1	0.05-0.22 ^a -0.5
[32]	0.001-2.5 ^a -5	0.01-0.5 ^a -1	0.8-0.9 ^a -1	0.1-0.25 ^a -0.4
[42]	0.1-1 ^b -5	0.01-0.1 ^b -1	0.8-0.95 ^b -1	0.05-0.22 ^b -0.5
Values selected	1-2.5-5	0.05-0.25-0.5	0.85-0.9-0.95	0.2-0.3-0.4

Table 12: Vegetation parameters in parametric green roof studies and low, medium and high values chosen for this study. ^a Some studies assume normally distributed parameters; reported here as min–mean–max.

^b Values reported as min–default–max.

Reference	Thickness [m]	Conductivity [$W.m^{-1}.K^{-1}$]	Density [$kg.m^{-3}$]	Specific heat [$J.kg^{-1}.K^{-1}$]
[42]	0.15	0.2-0.7 ^b -1.5	300-500 ^b -2000	300-1000 ^b - 2000
[81]	0.1	0.4	x	x
[82]	0.08	0.4	641	1000
[83]	0.2	0.25	1600	890
[84]	0.1	0.35	1100	1200
[87]	0.15-0.75	0.2	1020	1093
[85]	0.1	0.35	1100	1200
[6]	0.3	0.9	1850	850
[40]	0.15	0.85	1639	1800
	0.15	0.28	730	1100
[33]	0.05-0.25 ^a -0.7	0.2-0.4 ^a -1.5	300-641 ^a -2000	500-1000 ^a -2000
[41]	0.05 - 0.3	x	x	x
[35]	0.05 - 0.5	x	x	x
[39]	0.15	0.208	1100	730
	0.15	0.85	1800	1639
[36]	0.04 - 0.15	x	x	x
[29]	x	0.15-0.85 ^a -4	x	100-720 ^a -2000
[30]	0.06 - 0.66	0.250 - 1.45	400 - 1990	520 - 1990
[65] ^c	x	0.2	873.2	788
	x	0.21	759.6	923
	x	0.284	772.7	1360
	x	0.288	748.4	546
	x	0.229	724	375
Values selected	0.1-0.2-0.3	0.2-0.6-1	600-950-1300	700-950-1200

Table 13: Substrate parameters ranges used in parametric green roof studies, and low, medium and high values chosen for this study. ^a Some studies assume normally distributed parameters; reported here as min–mean–max. ^b Values reported as min–default–max. ^c Based on experimental substrate characterization.

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Parameter	Average parameter influence on pedestrian heat index [°C]			
	Low - 4 PM	High - 4 PM	Low - 8 PM	High - 8 PM
Foliage transpiration coefficient	0.121	-0.127	0.020	-0.021
Irrigation coefficient	-0.336	0.427	-0.152	0.206
Wind speed coefficient	-0.014	0.011	0.015	-0.014
Extinction coefficient	0.009	-0.007	-0.020	0.012
Foliage height	-0.106	0.030	0.022	-0.019
LAI	-0.028	0.033	-0.092	0.063
Capacity	-0.012	0.008	-0.001	0.002
Conductivity	-0.029	0.015	-0.015	0.009
Density	-0.010	0.010	-0.001	0.003
Substrate height	0.003	0.004	0.008	-0.002
Albedo	-0.024	0.023	0.000	0.000
Emissivity	-0.009	0.004	-0.003	0.002

Table 14: Parameter influence on pedestrian heat index, averaged across all archetypes. A positive sign means the parameter change raises air temperature 2-m above the green roof.

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