

# High-order unstructured discretisations for Scale-Resolving Simulations

VKI Lecture Series on Turbomachinery Flow Simulation and Modeling 2025

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Context

Notation and nature of the Navier-Stokes equations

Mathematical entropy

Transonic CFD - challenges and physical principles

Finite Volume Method (FVM)

Discontinuous Galerkin Method (DGM)

DG shock capturing for DNS and LES



### Turbulence and transition paramount

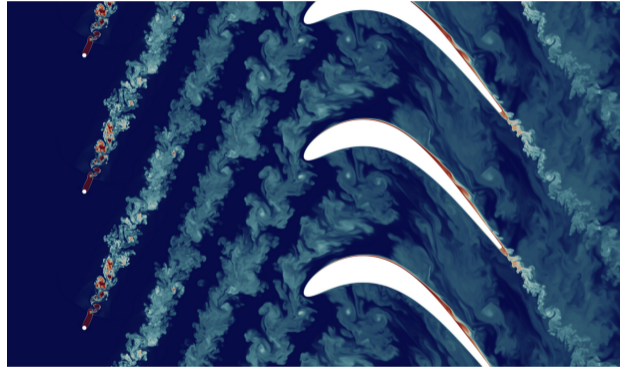
- large range of scales, smallest  $\llll$  geometry
- high loaded machinery often transonic
- conditions often between laminar and turbulent
- important source of losses/entropy
- beneficial for operational range

### RANS far from comfort zone $\rightarrow$ reference data ?

- very complex (secondary) flows
- often transition  $\sim$  low Re, high acceleration
- interaction with shocks
- vortical **and** acoustic perturbations

### Challenges for DNS / LES

- high accuracy on complex geometry/flow
- (shock) stabilisation  $\leftrightarrow$  capturing turbulence
- importance of acoustic waves / effects



DNS Spleen LPT cascade + wake generator (Courtesy VKI and Cenero)  
Entropy generation and transport through cascade



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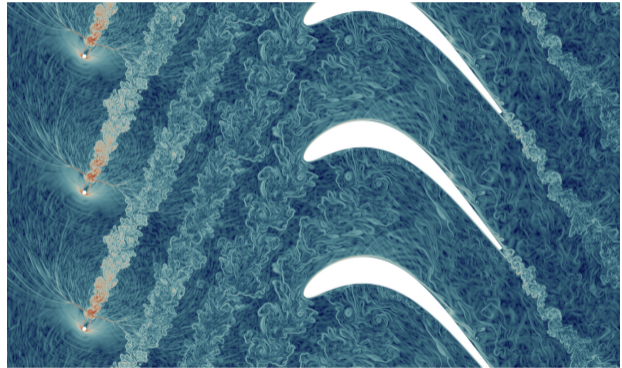
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Density gradient throughout the cascade



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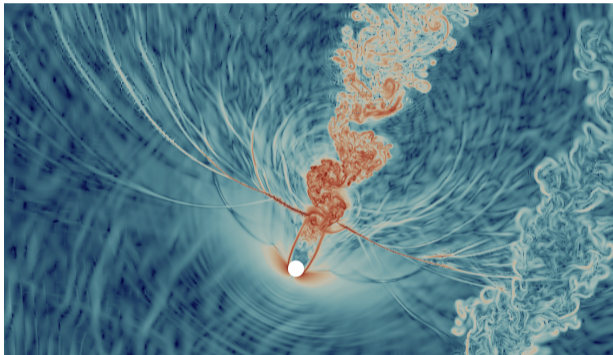
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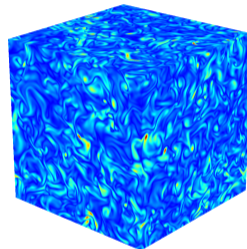
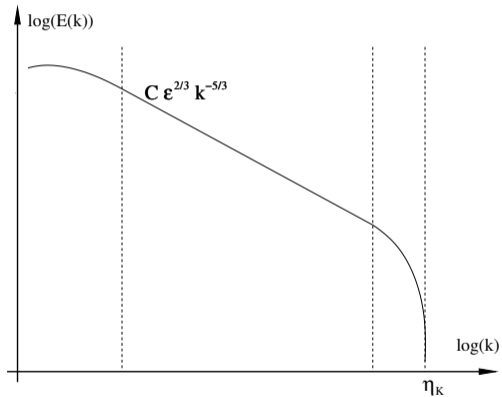
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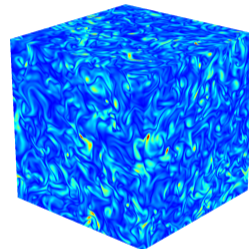
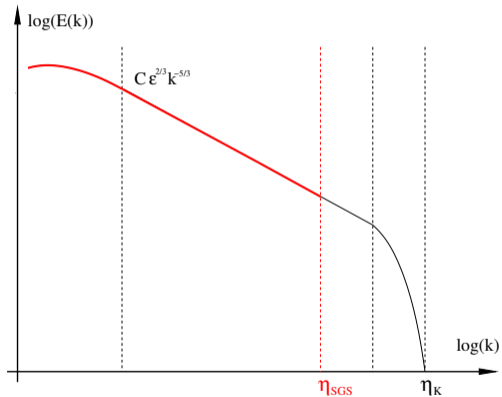
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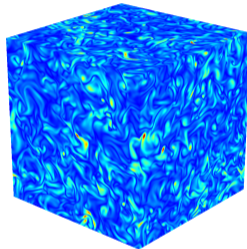
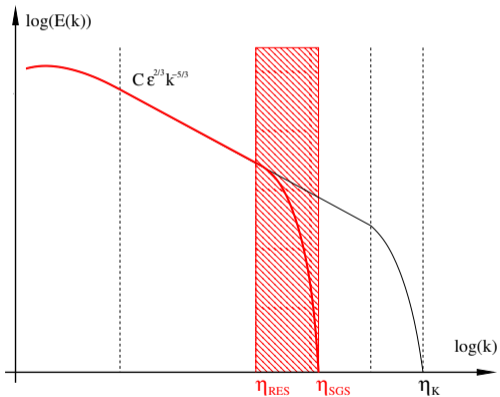


DNS Spaan LPT cascade + wake generator (Courtesy VKI and Cenero)  
Density gradient near the wake generator

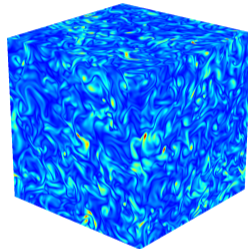
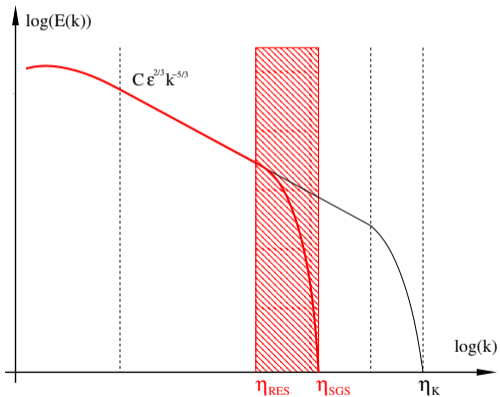




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- sacrificial range can be made smaller by using high order



- classical LES supposes sharp cut off
- near cut-off, numerical error is high  $\rightarrow$  sacrificial range
- sacrificial range can be made smaller by using high order
- global dissipation is correct if no significant error on larger scales in inertial range

# Notation and nature of the Navier-Stokes equations

## Conservative equations - integral form

Navier-Stokes equations

$$\int_V \frac{\partial \rho}{\partial t} dV + \oint_{\partial V} \rho \mathbf{v} \cdot \mathbf{n} dS = 0$$

$$\int_V \frac{\partial \rho \mathbf{v}}{\partial t} dV + \oint_{\partial V} ((\rho \mathbf{v} \cdot \mathbf{n}) \mathbf{v} + p \mathbf{n} - \boldsymbol{\tau} \cdot \mathbf{n}) dS = 0$$

$$\int_V \frac{\partial \rho E}{\partial t} dV + \oint_{\partial V} ((\rho \mathbf{v} \cdot \mathbf{n}) H - \mathbf{v} \cdot \boldsymbol{\tau} \cdot \mathbf{n} - \mathbf{q} \cdot \mathbf{n}) dS = 0$$

Generalisation to set of  $N$  convection-diffusion equations in  $\mathcal{U}^N$

$$\int_V \frac{\partial q_m}{\partial t} dV + \oint_{\partial V} (\mathbf{f}_m(q) \cdot \mathbf{n} - \mathbf{d}_m(q, \nabla q) \cdot \mathbf{n}) dS = 0$$

with

- $\mathbf{q} \in \mathcal{U}^N$  the state vector of *conserved variables*
- $\mathbf{f} \in \mathcal{U}^{N \times D}$  the *convective flux vector*
- $\mathbf{d} \in \mathcal{U}^{N \times D}$  the *diffusive flux vector*



# Notation and nature of the Navier-Stokes equations

## Conservative equations - differential form

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# Notation and nature of the Navier-Stokes equations

## Conservative equations - Convective and diffusive fluxes

- Convective fluxes correspond to *hyperbolic subsystem*: Jacobian of projected flux on any direction  $\mathbf{d}$

$$\mathcal{A}^{\mathbf{d}} \in \mathbb{R}^{N \times N} : \mathcal{A}_{mn}^{\mathbf{d}} = \frac{\partial \mathbf{f}_m}{\partial q_n} \cdot \mathbf{d}$$

has  $N$  real eigenvalues  $\lambda_j^{\mathbf{d}}$  (see [Leveque, 1992])

- Diffusive fluxes correspond to *elliptic subsystem*: Jacobian of flux wrt gradients

$$\mathcal{D} \in \mathbb{R}^{N \times D \times D \times N} : \mathcal{D}_{mn}^{kl} = \frac{\partial d_m^k}{\partial \frac{\partial q_n}{\partial x^l}}$$

is a positive semi-definite fourth order tensor (see e.g. [Chipot, 2009])

$$A_{mk} \mathcal{D}_{mn}^{kl} A_{nl} \geq 0, \forall A \in \mathbb{R}^{D \times N}$$



# Notation and nature of the Navier-Stokes equations

## Conservative equations - Change of variables

working variables  $u$  may be different from conservative variables  $q$

- express  $q$ ,  $\mathbf{f}$ ,  $\mathbf{d}$  in function of  $u$  and  $\nabla u$
- solve conservation equations for change in  $q$

$$\frac{\partial}{\partial t} q(u) + \nabla \cdot \mathbf{f}(u) - \nabla \cdot \mathbf{d}(u, \nabla u) = 0$$

- find  $u$  corresponding to the new values of  $q$



# Notation and nature of the Navier-Stokes equations

## Entropy - mechanical energy

Mechanical work along a on streamline

$$\frac{\partial \rho \mathbf{v}}{\partial t} + \nabla \cdot \rho \mathbf{v} \mathbf{v} + \nabla p = \nabla \cdot \boldsymbol{\tau}$$

$\Downarrow \cdot \mathbf{v}$

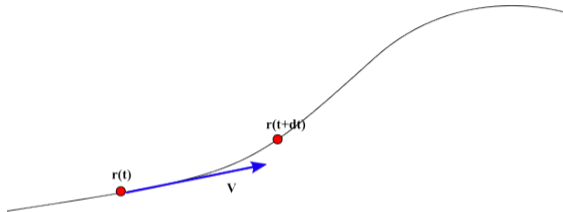
$$\frac{\partial \rho \mathcal{E}_k}{\partial t} + \nabla \cdot \rho \mathbf{v} \mathcal{E}_k = \mathbf{v} \cdot (-\nabla p + \nabla \cdot \boldsymbol{\tau})$$

$\Downarrow$

$$\frac{\partial \rho \mathcal{E}_k}{\partial t} + \nabla \cdot \rho \mathbf{v} \mathcal{E}_k = -\nabla \cdot \mathbf{v} p + \nabla \cdot \mathbf{v} \cdot \boldsymbol{\tau} + p \nabla \cdot \mathbf{v} - \boldsymbol{\tau} : \nabla \mathbf{v}$$

$\Downarrow$

$$\int_V \frac{\partial \mathcal{E}_k}{\partial t} dV + \oint_{\partial V} (\rho \mathbf{v} \cdot \mathbf{n}) \mathcal{E}_k dS = \underbrace{\oint_{\partial V} -\mathbf{v} \cdot p \mathbf{n} dS}_{\mathcal{W}_p} + \underbrace{\oint_{\partial V} \mathbf{v} \cdot \boldsymbol{\tau} \cdot \mathbf{n} dS}_{\mathcal{W}_\tau} + \underbrace{\int_V p \nabla \cdot \mathbf{v} dV}_{\mathcal{D}_p} - \underbrace{\int_V \boldsymbol{\tau} : \nabla \mathbf{v} dV}_{\epsilon > 0}$$



Subtract mechanical energy from total energy equation  $\rightarrow$  conservation of internal energy

$$\frac{\partial \rho E}{\partial t} + \nabla \cdot (\rho \mathbf{v} E + p \mathbf{v}) = \nabla \cdot \mathbf{v} \cdot \boldsymbol{\tau} + \nabla \cdot \mathbf{q}$$

$$\frac{\partial \rho \mathcal{E}_k}{\partial t} + \nabla \cdot (\rho \mathbf{v} \mathcal{E}_k + p \mathbf{v}) = \nabla \cdot \mathbf{v} \cdot \boldsymbol{\tau} + p \nabla \cdot \mathbf{v} - \boldsymbol{\tau} : \nabla \mathbf{v}$$

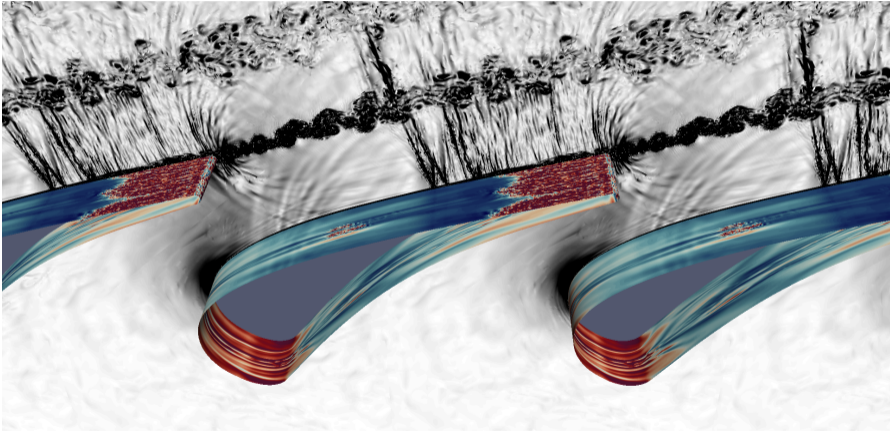
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$$\frac{\partial \rho e}{\partial t} + \nabla \cdot \rho \mathbf{v} e = -p \nabla \cdot \mathbf{v} + \boldsymbol{\tau} : \nabla \mathbf{v} + \nabla \cdot \mathbf{q}$$

Conservation equation for entropy *density*

$$\frac{\partial \rho s}{\partial t} + \nabla \cdot \rho \mathbf{v} s - \nabla \cdot \frac{\mathbf{q}}{T} = \frac{\boldsymbol{\tau} : \nabla \mathbf{v}}{T} - \frac{\nabla T \cdot \mathbf{q}}{T^2} \geq 0$$





LES of the VKI LS89 high-pressure turbine inlet guide vane, condition MUR235  
Numerical schlieren and wall heat flux (courtesy Cenaero and VKI)



# Notation and nature of the Navier-Stokes equations

## Shocks - linear effects - characteristics

Linearise

$$\frac{\partial q_m}{\partial t} + \nabla \cdot \mathbf{f}_m = 0$$

around mean solution  $q_m = \bar{q}_m + \delta q_m$

$$\frac{\partial \delta q_m}{\partial t} + \mathcal{A}_n \cdot \nabla \delta q_n = 0$$

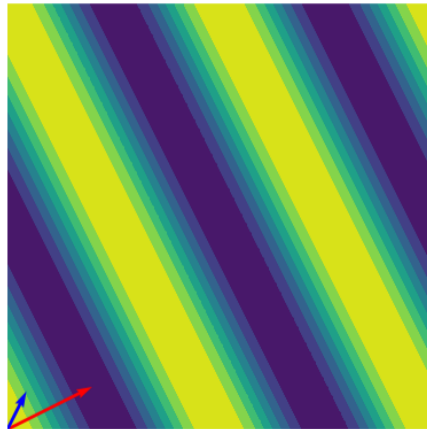
$\delta q$  consists of plane waves moving along  $\mathbf{d}$  with wave number  $k$

$$\delta q_m = \sum \widehat{\delta c}_j r_{jm} e^{ik(\mathbf{d} \cdot \mathbf{r} - \lambda_j t)}$$

since all eigenvalues  $\lambda_j$

$$(\mathcal{A} \cdot \mathbf{d}) r_j^d = \lambda_j^d r_j^d$$

are real



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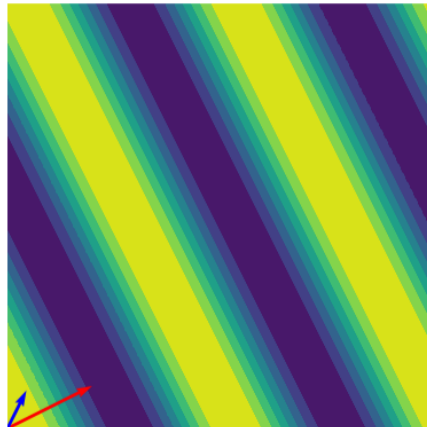
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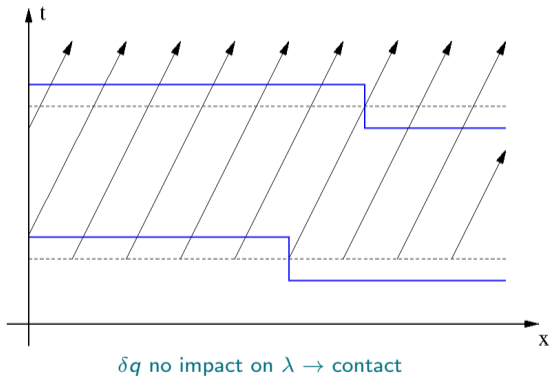
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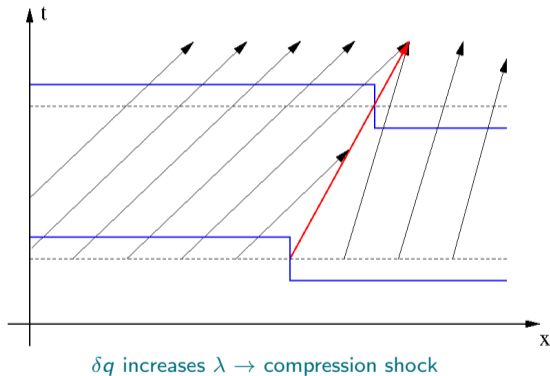
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## Shocks - non-linear propagation in 1D - scalar equation



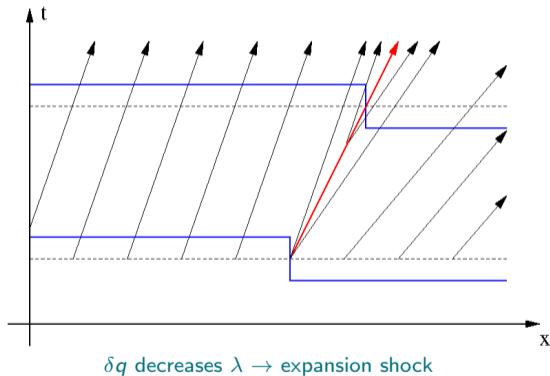
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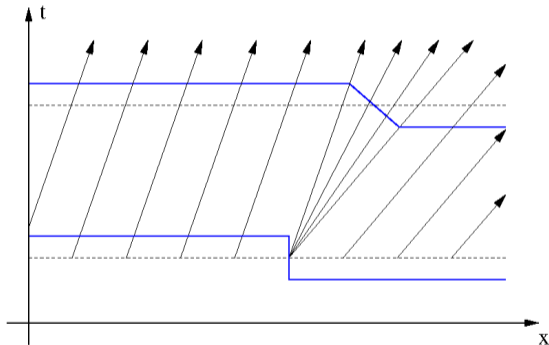
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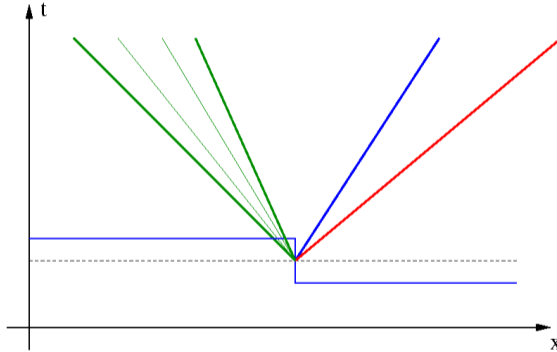
## Shocks - non-linear propagation in 1D - scalar equation



$\delta q$  decreases  $\lambda +$  vanishing viscosity / entropy consistency  $\rightarrow$  expansion fan

# Notation and nature of the Navier-Stokes equations

## Shocks - non-linear propagation in 1D - Riemann problem



$N$  characteristics containing contacts, shocks and fans



*Strong* differential form of the convection system not usable for discontinuous solutions

$$\frac{\partial q_m}{\partial t} + \nabla \cdot \mathbf{f}_m = 0$$

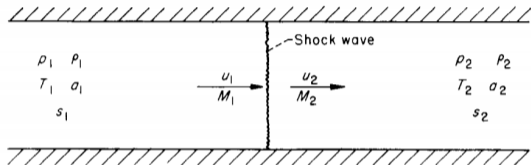
Regularity requirements lifted in *weak solution* which satisfies

$$\int_{\Omega} v \frac{\partial q}{\partial t} dV - \int_{\Omega} \nabla v \cdot \mathbf{f}(q) dV = 0, \quad \forall v \in \mathcal{V}^N$$

However

- weak solutions not necessarily unique (e.g. expansion fan and shock both possible)
- complement with entropy consistency



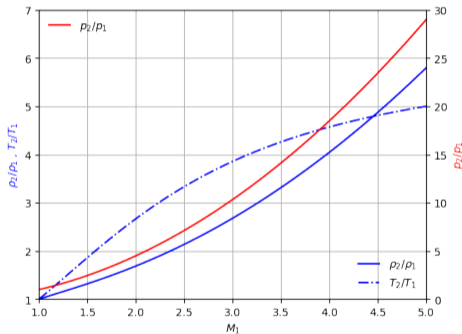


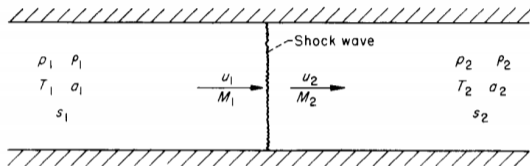
- conservation of mass, momentum and energy

$$(p_1, T_1, v_1) \leftrightarrow (p_2, T_2, v_2)$$

- second law  $s_2 > s_1$

$$(p_1, T_1, v_1) \rightarrow (p_2, T_2, v_2)$$



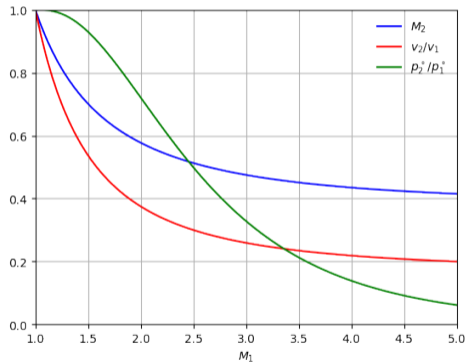


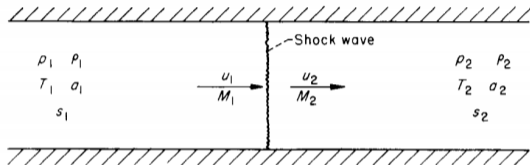
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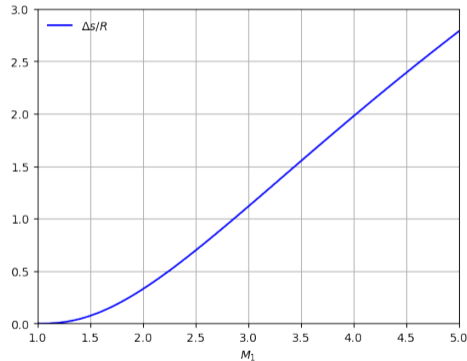


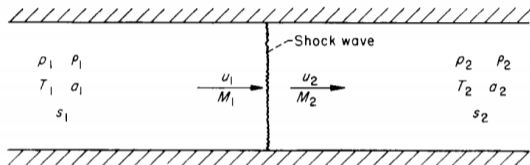
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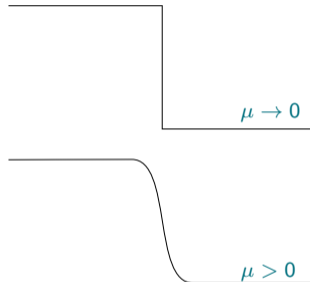


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Generation of entropy by viscous effects  $\tau : \nabla \mathbf{v}, -\nabla T \cdot \mathbf{q}$

- shock thickness depends on  $\mu$
- entropy increase  $\Delta s$  however independent
- Euler = vanishing viscosity solution



# Notation and nature of the Navier-Stokes equations

## Take-away messages

Entropy embedded equation within the Navier-Stokes equations

- ensures stability of the system
- ensures a unique weak solution

Shocks

- strength determined by conservation of mass, momentum and energy
- entropy generation - by viscous stresses - is independent of the viscosity
- **vanishing viscosity solution**: inviscid flow is limit  $\mu \rightarrow 0$



Generalisation of physical entropy to mathematical entropy  $\mathcal{S}$  and flux  $\mathcal{F}$  to study generic non-linear hyperbolic and combined hyperbolic-elliptic systems [Harten, 1983, Harten et al., 1998, Tadmor, 1987]

- conservation equation is constructed by combining  $N$  conservation equations
- can only decrease ( $\leftrightarrow$  increase) monotonically



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Mathematical entropy  $\mathcal{S}$  and entropy flux  $\mathcal{F}$

- **entropy variables**  $w$

$$w_m = \frac{\partial \mathcal{S}}{\partial q_m}$$

- existence of (scalar) **entropy flux**  $\mathcal{F}$

$$\frac{\partial \mathcal{F}}{\partial q_m} = \frac{\partial \mathcal{S}}{\partial q_n} \frac{\partial \mathbf{f}_n}{\partial q_m}$$

- **convexity**  $\nabla w_m \cdot \mathbf{d}_m \geq 0$



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Dual: potential flux  $\mathcal{Q}$  and potential flux  $\mathcal{G}$

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$$\frac{\partial \mathcal{G}}{\partial w_m} = \mathbf{f}_m$$



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Navier-Stokes equations :  $\mathcal{S} = -\rho s$  [Hughes et al., 1986]



Since

$$\frac{\partial \mathcal{S}}{\partial q_m} \frac{\partial \mathbf{f}_m}{\partial q_n} = \frac{\partial \mathcal{F}}{\partial q_n}$$

we find

$$\frac{\partial \mathcal{S}}{\partial q_m} \nabla \cdot \mathbf{f}_m = \frac{\partial \mathcal{S}}{\partial q_m} \frac{\partial f_m^k}{\partial x^k} = \frac{\partial \mathcal{S}}{\partial q_m} \frac{\partial f_m^k}{\partial q_n} \frac{\partial q_n}{\partial x^k} = \frac{\partial \mathcal{F}^k}{\partial q_n} \frac{\partial q_n}{\partial x^k} = \frac{\partial \mathcal{F}^k}{\partial x^k} = \nabla \cdot \mathcal{F}$$

and hence

$$\frac{\partial \mathcal{S}}{\partial t} + \nabla \cdot \mathcal{F} = \frac{\partial \mathcal{S}}{\partial q_m} \nabla \cdot \mathbf{d}_m = w_m \nabla \cdot \mathbf{d}_m$$



Integral form of entropy conservation

$$\begin{aligned}\int_V \frac{\partial S}{\partial t} dV + \oint_{\partial V} \mathcal{F} \cdot \mathbf{n} dA &= \int_V w_m \nabla \cdot \mathbf{d}_m dV \\ &= \oint_{\partial V} w_m \mathbf{d}_m \cdot \mathbf{n} dA - \int_V \nabla w_m \cdot \mathbf{d}_m dV\end{aligned}$$

Developing the volume production term

$$-\nabla w_m \cdot \mathbf{d}_m dV = -\frac{\partial w_m}{\partial q_n} \mathcal{D}_{mo}^{kl} \frac{\partial q_o}{\partial x^l} = -\frac{\partial q_n}{\partial x^k} \frac{\partial^2 \mathcal{S}}{\partial q_n \partial q_m} \mathcal{D}_{mo}^{kl} \frac{\partial q_o}{\partial x^l}$$

we see it is negative if  $\mathcal{S}$  is a convex function of the state vector  $q$



Existence of mathematical entropy : stability of convection/hyperbolic systems

- all conservation equations can be collapsed onto a single one
- this equation describes the convection of entropy and it's destruction
- the entropy serves as a bounded energy, providing stability
- ensures unicity of the weak solution

Consequences for numerical approximations

- entropy equation is derived from conservation equations and therefore not necessarily satisfied
- embedding *entropy-consistency* in the discretisation is desirable



## Shock position, strength and speed

- discrete exact conservation mass, momentum, energy
- generation of small yet positive amount of entropy



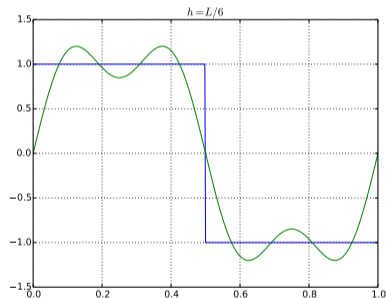
# Transonic CFD - challenges and physical principles

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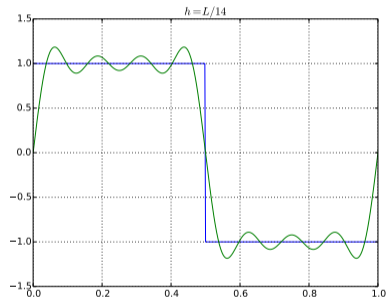
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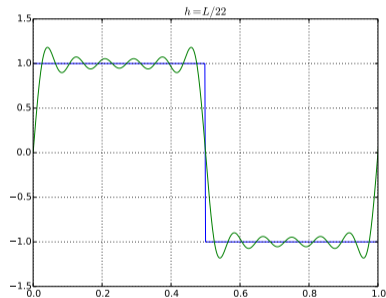
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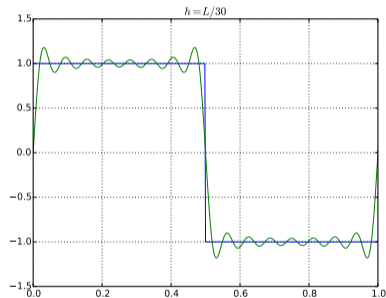


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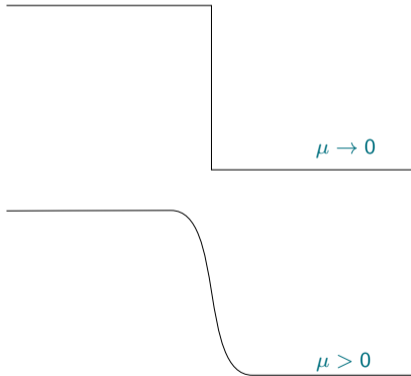
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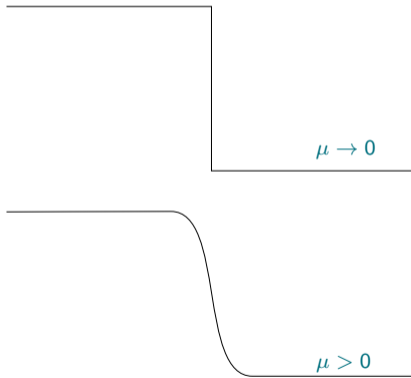
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## Non-linear stability required near shocks

- mimick physics: collapse all discrete equations onto entropy equation
- entropy generation mechanism ?
- discrete entropy variables



Vanishing diffusion conservation equation

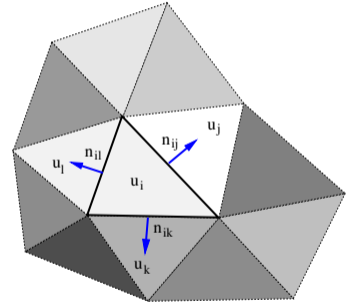
$$\int_V \frac{\partial q_m}{\partial t} dV + \oint_{\partial V} \mathbf{f}_m \cdot \mathbf{n} dS = 0$$

Solving for average  $q^i$  on control volume  $V_i$

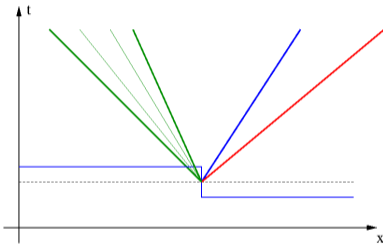
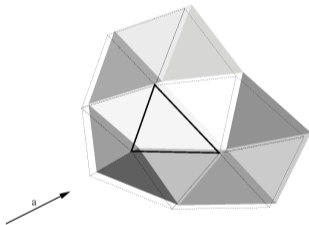
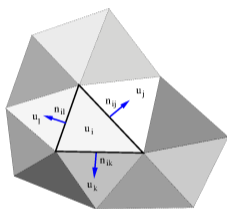
$$V_i \frac{dq_m^i}{dt} = - \sum_j \mathcal{H}_m (q^i, q^j; \mathbf{n}^{ij}) = 0$$

with the following requirements for the interface flux  $\mathcal{H}(\cdot, \cdot; \cdot)$

- conservativity  $\mathcal{H} (q^j, q^i; -\mathbf{n}^{ij}) = -\mathcal{H} (q^i, q^j; \mathbf{n}^{ij})$
- consistency  $\mathcal{H}_m (q, q; \mathbf{n}) = \mathbf{f}_m \cdot \mathbf{n}$
- stability ?



Main idea:  $\mathcal{H}(q^-, q^+; \mathbf{n}) = \lim_{dt \rightarrow 0} \mathbf{f}(\tilde{q}(t + dt)) \cdot \mathbf{n}$



- Godunov scheme:  $\tilde{q}(t + dt)$  is solution of the Riemann problem between  $q^+$  and  $q^-$
- Riemann problem is expensive to solve  $\rightarrow$  *approximate Riemann solvers* (see [Toro, 2009] for review)
- using upwind flux  $\mathcal{H}(q^+, q^*; \mathbf{n})$  on boundary ensures well-posed Dirichlet boundary conditions since coherent with characteristic propagation (see [Giles, 1988])

FVM for cell  $V_i$

$$V_i \frac{dq_m^i}{dt} = - \sum_j \mathcal{H}_m(q^i, q^j; \mathbf{n}^{ij})$$



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Evolution of cell entropy,

$$V_i w_m^i \frac{dq_m^i}{dt} = - \sum_j w_m^i \mathcal{H}_m(q^i, q^j; \mathbf{n}^{ij})$$



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Evolution of cell entropy, considering  $\sum_j \mathbf{n}^{ij}$

$$V_i w_m^i \frac{dq_m^i}{dt} = - \sum_j w_m^i \mathcal{H}_m(q^i, q^j; \mathbf{n}^{ij}) - \mathcal{G}(q^i) \cdot \sum_j \mathbf{n}^{ij}$$



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Evolution of entropy over the whole domain  $\Omega$

$$\sum_i V_i \frac{dS^i}{dt} = - \sum_{i,j} (w_m^i - w_m^j) \mathcal{H}_m(q^i, q^j; \mathbf{n}^{ij}) - (\mathcal{G}(q^i) - \mathcal{G}(q^j)) \cdot \mathbf{n}^{ij}$$



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- discontinuity  $\rightarrow$  interface fluxes  $\mathcal{H}(u^+, u^-; \mathbf{n})$ 
  - conservativity:  $\mathcal{H}(u^+, u^-; \mathbf{n}) = -\mathcal{H}(u^-, u^+; -\mathbf{n})$
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- rigorous non-linear stability: *Entropy Consistent Fluxes* “E-flux” [Oleinik]

$$(w_m^+ - w_m^-) (\mathcal{H}_m(u^+, u^-; \mathbf{n}) - \mathbf{f}_m(\tilde{u}) \cdot \mathbf{n}) \geq 0, \forall \tilde{u} \in [u^+, u^-]$$

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- E-fluxes positive dissipation  $\rightarrow$  correct shock representation
- Entropy consistent FVM
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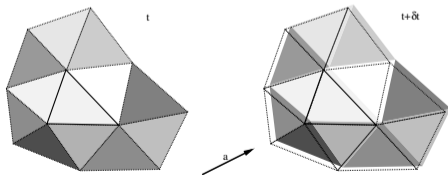
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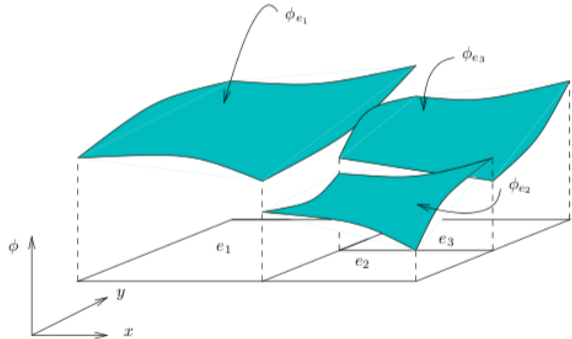
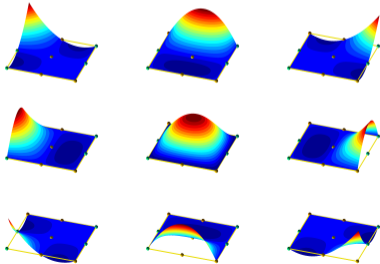


# Discontinuous Galerkin Method (DGM) Interpolation

Elementwise polynomial interpolation of  
working variables  $u$  of arbitrary order  $p$

$$u \in \mathcal{V}^N : (u_m)_e = \sum_i \mathbf{u}_{im} \phi_i^e$$

$\phi_i^e$  shape functions of order  $p = 2$  for element  
 $e$

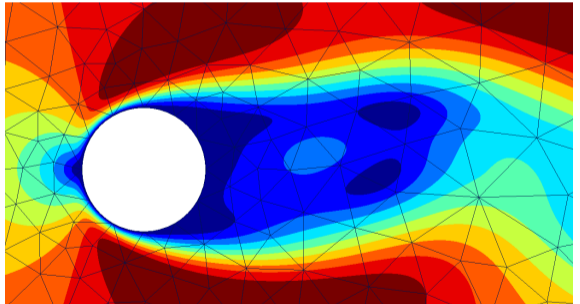
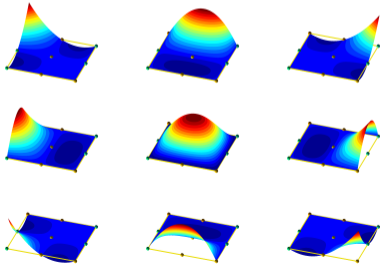


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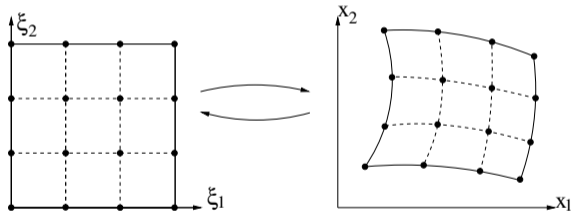
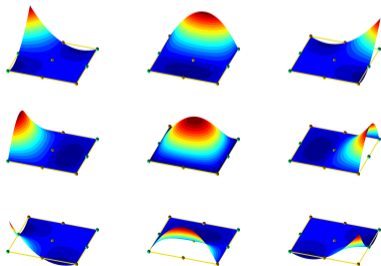


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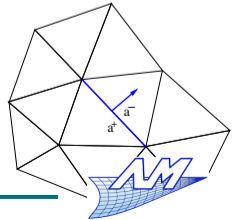
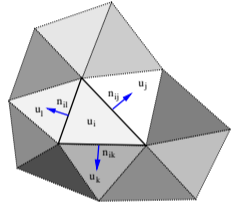


# Discontinuous Galerkin Method (DGM)

## Variational formulation

Galerkin

$$\int_{\Omega} v_m \left( \frac{\partial q_m}{\partial t} + \nabla \cdot \mathbf{f}_m \right) dV = 0, \quad \forall v_m \in \mathcal{V}$$

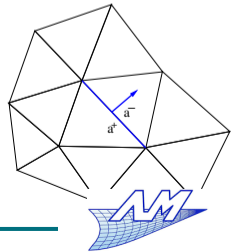
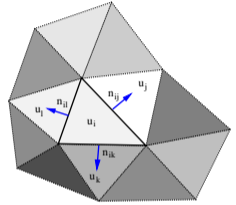


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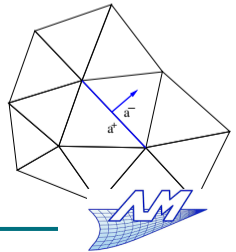
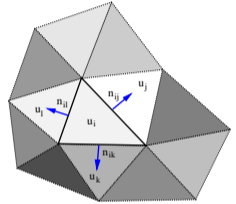
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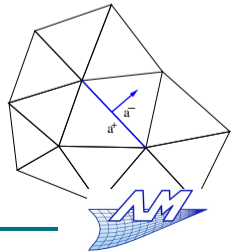
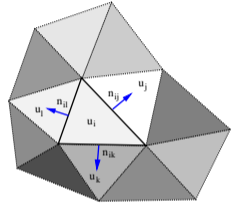
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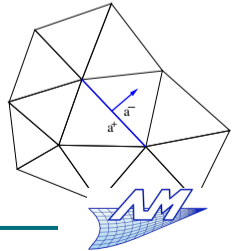
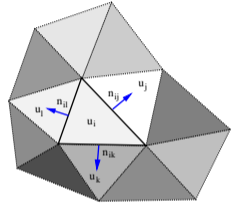
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Discretisation: choice for interface flux

$$\sum_e \int_e v \frac{\partial q}{\partial t} dV - \sum_e \int_e \nabla v_m \cdot \mathbf{f}_m dV + \sum_f \int_f \gamma(u^+, v^+, u^-, v^-, \mathbf{n}) dS = 0$$

Consistency ?

$$\gamma(u, v^+, u, v^-, \mathbf{n}) = (v^+ - v^-) \mathbf{f}(u) \cdot \mathbf{n}$$



# Discontinuous Galerkin Method (DGM)

## Variational formulation - interface flux

DGM( $p=0$ ),  $v = 1$  on  $e$  and zero elsewhere

$$\int_e \frac{\partial q}{\partial t} dV + \int_f \gamma(u^+, 1, u^-, 0, \mathbf{n}) dS = 0$$

first order FVM

$$\int_e \frac{\partial q}{\partial t} dV + \int_f \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

Both coincide if

$$\gamma(u^+, v^+, u^-, v^-, \mathbf{n}) = (v^+ - v^-) \mathcal{H}(u^+, u^-; \mathbf{n})$$

so we find a high order extension of the FVM

$$\sum_e \int_e v \frac{\partial q}{\partial t} dV - \sum_e \int_e \nabla v_m \cdot \mathbf{f}_m dV + \sum_f \int_f (v^+ - v^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

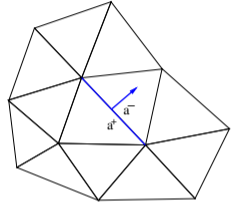


# Discontinuous Galerkin Method (DGM)

## Entropy consistency

Use entropy variables  $u = w \rightarrow$  choose  $w \in \mathcal{V}^N$

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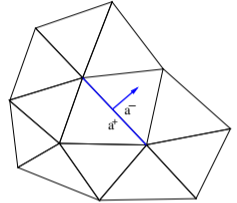
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$$\sum_e \int_e \frac{\partial \mathcal{S}}{\partial t} dV - \sum_e \int_e \nabla w_m \cdot \frac{\partial \mathcal{G}}{\partial w_m} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$



# Discontinuous Galerkin Method (DGM)

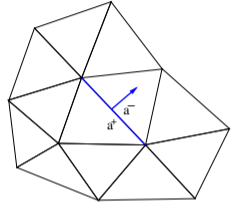
## Entropy consistency

Use entropy variables  $u = w \rightarrow$  choose  $w \in \mathcal{V}^N$

$$\sum_e \int_e w_m \frac{\partial q_m}{\partial t} dV - \int_e \nabla w_m \cdot \mathbf{f} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial S}{\partial t} dV - \sum_e \int_e \nabla w_m \cdot \frac{\partial \mathcal{G}}{\partial w_m} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial S}{\partial t} dV - \sum_e \int_e \nabla \cdot \mathcal{G} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$



# Discontinuous Galerkin Method (DGM)

## Entropy consistency

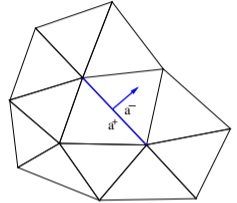
Use entropy variables  $u = w \rightarrow$  choose  $w \in \mathcal{V}^N$

$$\sum_e \int_e w_m \frac{\partial q_m}{\partial t} dV - \int_e \nabla w_m \cdot \mathbf{f} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial S}{\partial t} dV - \sum_e \int_e \nabla w_m \cdot \frac{\partial \mathcal{G}}{\partial w_m} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial S}{\partial t} dV - \sum_e \int_e \nabla \cdot \mathcal{G} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial S}{\partial t} dV + \sum_f \int_f ((w_m^+ - w_m^-) \mathcal{H}_m(u^+, u^-; \mathbf{n}) - (\mathcal{G}^+ - \mathcal{G}^-) \cdot \mathbf{n}) dS = 0$$



# Discontinuous Galerkin Method (DGM)

## Entropy consistency

Use entropy variables  $u = w \rightarrow$  choose  $w \in \mathcal{V}^N$

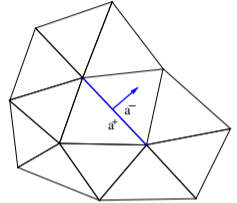
$$\sum_e \int_e w_m \frac{\partial q_m}{\partial t} dV - \int_e \nabla w_m \cdot \mathbf{f} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial S}{\partial t} dV - \sum_e \int_e \nabla w_m \cdot \frac{\partial \mathcal{G}}{\partial w_m} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial S}{\partial t} dV - \sum_e \int_e \nabla \cdot \mathcal{G} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial S}{\partial t} dV + \sum_f \int_f ((w_m^+ - w_m^-) \mathcal{H}_m(u^+, u^-; \mathbf{n}) - (\mathcal{G}^+ - \mathcal{G}^-) \cdot \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial S}{\partial t} dV = - \sum_f \int_f (w_m^+ - w_m^-) \left( \mathcal{H}_m(u^+, u^-; \mathbf{n}) - \frac{\partial \mathcal{G}}{\partial w_m}(\tilde{w}) \right) dS, \exists \tilde{w} \in [w^+, w^-]$$



# Discontinuous Galerkin Method (DGM)

## Entropy consistency

Use entropy variables  $u = w \rightarrow$  choose  $w \in \mathcal{V}^N$

$$\sum_e \int_e w_m \frac{\partial q_m}{\partial t} dV - \int_e \nabla w_m \cdot \mathbf{f} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

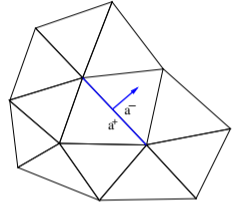
$$\sum_e \int_e \frac{\partial \mathcal{S}}{\partial t} dV - \sum_e \int_e \nabla w_m \cdot \frac{\partial \mathcal{G}}{\partial w_m} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial \mathcal{S}}{\partial t} dV - \sum_e \int_e \nabla \cdot \mathcal{G} dV + \sum_f \int_f (w_m^+ - w_m^-) \mathcal{H}(u^+, u^-; \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial \mathcal{S}}{\partial t} dV + \sum_f \int_f ((w_m^+ - w_m^-) \mathcal{H}_m(u^+, u^-; \mathbf{n}) - (\mathcal{G}^+ - \mathcal{G}^-) \cdot \mathbf{n}) dS = 0$$

$$\sum_e \int_e \frac{\partial \mathcal{S}}{\partial t} dV = - \sum_f \int_f (w_m^+ - w_m^-) \left( \mathcal{H}_m(u^+, u^-; \mathbf{n}) - \frac{\partial \mathcal{G}}{\partial w_m}(\tilde{w}) \right) dS, \exists \tilde{w} \in [w^+, w^-]$$

$$\sum_e \int_e \frac{\partial \mathcal{S}}{\partial t} dV = - \underbrace{\sum_f \int_f (w_m^+ - w_m^-) (\mathcal{H}_m(u^+, u^-; \mathbf{n}) - \mathbf{f}(\tilde{w})) dS}_{>0}$$



# Discontinuous Galerkin Method (DGM)

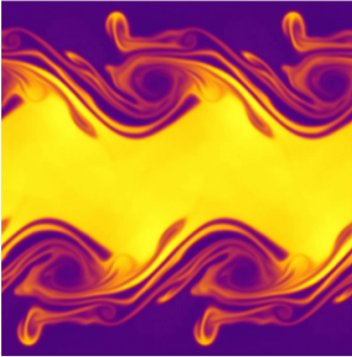
## Take-away messages

- DGM natural high order extension of first order FVM
  - inherits consistency and stability
  - arbitrary order of accuracy / interpolation
  - exact accounting for curved element shape
  - compact stencil and computational efficiency
- Using upwind fluxes, DGM can be seen as combination of small elementwise defined FEM problems, coupled by Dirichlet fluxes
- Entropy stable DG (ESDG)
  - use  $w$  as working variables  $\in \mathcal{V}$  instead of conservative  $q$
  - use of E-fluxes
  - *integration by parts* should be discretely mimicked *summation by parts*
  - quadrature error since update in conservative, not in working variables !

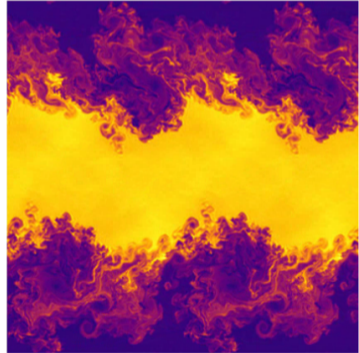


### Challenges

- robustness with respect to shocks through energy stability
- minimal impact on turbulent flow features



Artificial viscosity



Entropy stable DG



Study submitted to Journal of Computational Physics [Bilocq24\*]

- **DG**: vanilla DG without shock capturing (DG)
  - most accurate (no quadrature error)
  - no stabilisation
- **DG-AV**: DG + sensor based artificial viscosity [Persson and Peraire, 2006, Hennemann et al., 2021]
  - additional viscosity at shocks → dissipates turbulence
  - sensors to detect underresolution
- **ESDG**: Entropy stable DG [Gassner et al., 2016, Chan et al., 2019]
  - formulation in  $w$  error in update
  - full quadrature
  - expensive
- **ESDGSEM**: Spectral Element Entropy Stable DG [Gassner et al., 2016, Chan et al., 2019]
  - formulation in  $w$
  - *summation by parts* by reduced tensor-product quadrature
- **DG-SBP**: summation by parts DG
  - DG operator expressed in conserved variables
  - summation by parts operator
- **DG-ES**: sensor based switch between DG and ESGD

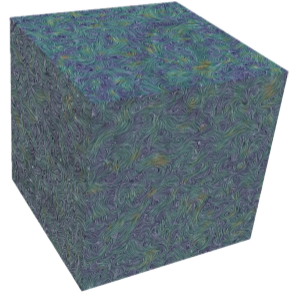


# DG shock capturing for DNS and LES

## Compressible homogeneous isotropic turbulence - test case

### Compressible homogeneous isotropic turbulence

- $M_t = 0.6$ ,  $Re_\lambda = 100$
- starting from incompressible flow field
- high vorticity  $\rightarrow \epsilon_s$
- acoustic transient  $\rightarrow \epsilonpsilon_d$  and  $\mathcal{D}_p$
- shocklets form  $M \approx 2 \rightarrow \epsilon_d$  and  $\mathcal{D}_p$
- N cells per direction, order  $p=5$ , equivalent resolution  $n = (p + 1)N = 66$



# DG shock capturing for DNS and LES

## Compressible homogeneous isotropic turbulence - convergence criterion

Kinetic energy budget on generic control volume

$$\int_V \frac{\partial \mathcal{E}_k}{\partial t} dV + \oint_{\partial V} (\rho \mathbf{v} \cdot \mathbf{n}) \mathcal{E}_k dS = \oint_{\partial V} -\mathbf{v} \cdot p \mathbf{n} dS + \oint_{\partial V} \mathbf{v} \cdot \boldsymbol{\tau} \cdot \mathbf{n} dS + \int_V p \nabla \cdot \mathbf{v} dV - \int_V \boldsymbol{\tau} : \nabla \mathbf{v} dV$$



# DG shock capturing for DNS and LES

## Compressible homogeneous isotropic turbulence - convergence criterion

Kinetic energy budget on fully periodic domain

$$\int_V \frac{\partial \mathcal{E}_k}{\partial t} dV + \cancel{\oint_{\partial V} (\rho \mathbf{v} \cdot \mathbf{n}) \mathcal{E}_k dS} = \cancel{\oint_{\partial V} -\mathbf{v} \cdot p \mathbf{n} dS} + \cancel{\oint_{\partial V} \mathbf{v} \cdot \boldsymbol{\tau} \cdot \mathbf{n} dS} + \int_V p \nabla \cdot \mathbf{v} dV - \int_V \boldsymbol{\tau} : \nabla \mathbf{v} dV$$



# DG shock capturing for DNS and LES

## Compressible homogeneous isotropic turbulence - convergence criterion

Kinetic energy budget on

$$\int_V \frac{\partial \mathcal{E}_k}{\partial t} dV + \cancel{\int_{\partial V} (\rho \mathbf{v} \cdot \mathbf{n}) \mathcal{E}_k dS} = \cancel{\int_{\partial V} -\mathbf{v} \cdot p \mathbf{n} dS} + \cancel{\int_{\partial V} \mathbf{v} \cdot \boldsymbol{\tau} \cdot \mathbf{n} dS} + \int_V p \nabla \cdot \mathbf{v} dV - \int_V \boldsymbol{\tau} : \nabla \mathbf{v} dV$$

Newtonian fluid  $\boldsymbol{\tau} = \mu (\nabla \mathbf{v} + \nabla \mathbf{v}^T - \frac{2}{3} \nabla \cdot \mathbf{v} \mathbf{I})$  Split in solenoidal (vorticity) and dilatational dissipation

$$\int_V \boldsymbol{\tau} : \nabla \mathbf{v} dV = \underbrace{2 \int_V \mu \frac{\boldsymbol{\omega} \cdot \boldsymbol{\omega}}{2} dV}_{\epsilon_s} + \underbrace{\frac{4}{3} \int_V \mu (\nabla \cdot \mathbf{v})^2 dV}_{\epsilon_d}$$



# DG shock capturing for DNS and LES

## Compressible homogeneous isotropic turbulence - convergence criterion

Kinetic energy budget on

$$\int_V \frac{\partial \mathcal{E}_k}{\partial t} dV + \cancel{\oint_{\partial V} (\rho \mathbf{v} \cdot \mathbf{n}) \mathcal{E}_k dS} = \cancel{\oint_{\partial V} -\mathbf{v} \cdot p \mathbf{n} dS} + \cancel{\oint_{\partial V} \mathbf{v} \cdot \boldsymbol{\tau} \cdot \mathbf{n} dS} + \int_V p \nabla \cdot \mathbf{v} dV - \int_V \boldsymbol{\tau} : \nabla \mathbf{v} dV$$

Newtonian fluid  $\boldsymbol{\tau} = \mu (\nabla \mathbf{v} + \nabla \mathbf{v}^T - \frac{2}{3} \nabla \cdot \mathbf{v} \mathbf{I})$  Split in solenoidal (vorticity) and dilatational dissipation

$$\int_V \boldsymbol{\tau} : \nabla \mathbf{v} dV = \underbrace{2 \int_V \mu \frac{\boldsymbol{\omega} \cdot \boldsymbol{\omega}}{2} dV}_{\epsilon_s} + \underbrace{\frac{4}{3} \int_V \mu (\nabla \cdot \mathbf{v})^2 dV}_{\epsilon_d}$$

and therefore

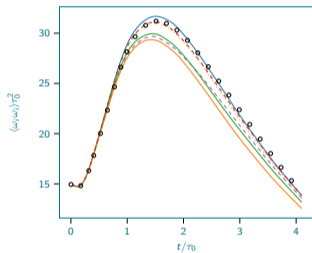
$$\underbrace{-\frac{d}{dt} \int_V \mathcal{E}_k dV}_{\epsilon_k} = \underbrace{2 \int_V \mu \frac{\boldsymbol{\omega} \cdot \boldsymbol{\omega}}{2} dV}_{\epsilon_s} + \underbrace{\frac{4}{3} \int_V \mu (\nabla \cdot \mathbf{v})^2 dV}_{\epsilon_d} - \underbrace{\int_V p \nabla \cdot \mathbf{v} dV}_{\mathcal{D}_p}$$

Kinetic energy budget  $\Delta \epsilon = \epsilon_s + \epsilon_d + \mathcal{D}_p - \epsilon_k$  is measure for instantaneous error

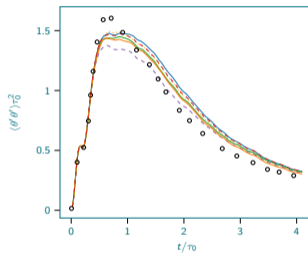


# DG shock capturing for DNS and LES

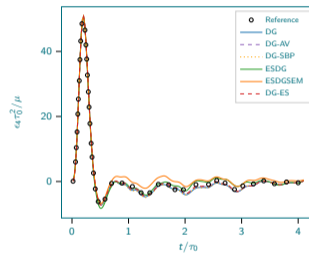
## Compressible homogeneous isotropic turbulence - contributions



Solenoidal dissipation  $\epsilon_s$



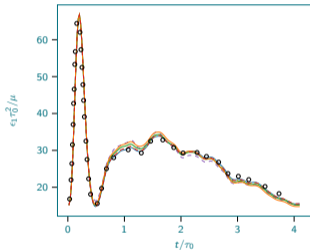
Dilatational dissipation  $\epsilon_d$



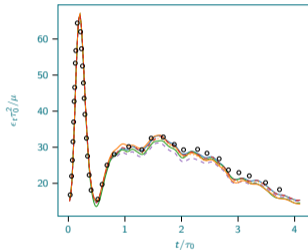
Pressure diffusion  $\mathcal{D}_p$

# DG shock capturing for DNS and LES

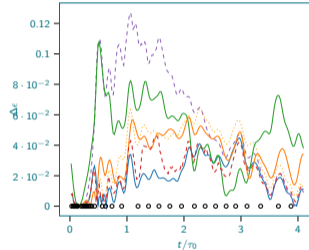
## Compressible homogeneous isotropic turbulence - budgets



Measured dissipation  $\epsilon_k$



Total dissipation  $\epsilon_s + \epsilon_d + \mathcal{D}_p$



Budget error  $\epsilon_s + \epsilon_d + \mathcal{D}_p - \epsilon_k$



# DG shock capturing for DNS and LES

## Compressible homogeneous isotropic turbulence - stability

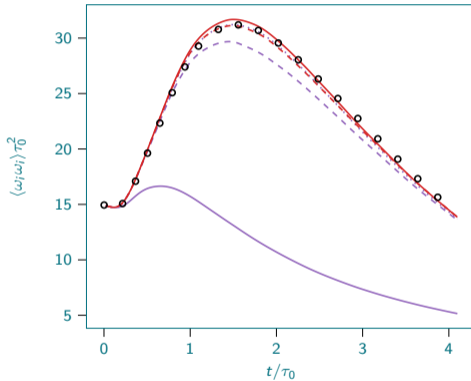
	$p = 3$			$p = 4$			$p = 5$		
	$4^3$	$8^3$	$16^3$	$3^3$	$6^3$	$13^3$	$3^3$	$5^3$	$11^3$
DG	X	X	✓	X	X	✓	X	X	✓
DG-AV	✓	✓	✓	✓	✓	✓	✓	✓	✓
DG-SBP	X	X	✓	X	X	X	X	X	✓
ESDGSEM	✓	✓	✓	✓	✓	✓	✓	✓	✓
ESDG	✓	✓	✓	✓	✓	✓	✓	✓	✓
DG-ES	✓	✓	✓	✓	✓	✓	✓	✓	✓

g

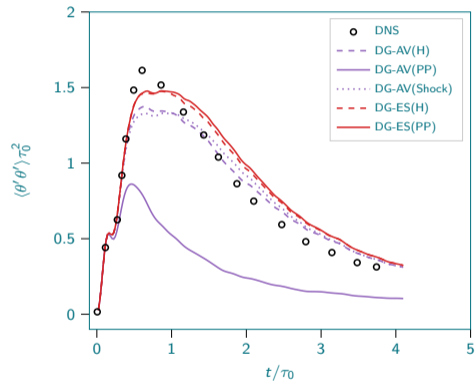


# DG shock capturing for DNS and LES

## Compressible homogeneous isotropic turbulence - sensor dependence



Solenoidal dissipation  $\epsilon_s$



Dilatational dissipation  $\epsilon_d$

### Conclusions

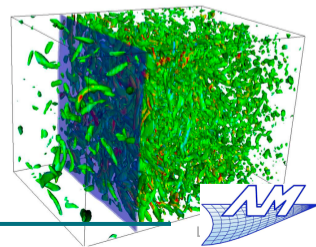
- ESDGSEM and ESDGSEM provide robustness, but not fully accurate
- DG-AV worst accuracy, high dependence on sensor
- vanilla DG, using conserved variables, most accurate
- summation by parts operator is not stabilising DG, but not jeopardizing accuracy
- best of both worlds: vanilla DG + ESDG in “troubled cells”
- DG-ES: low dependence on sensor

### Future work

- validation on shock-turbulence interaction (shock stabilisation)
- integration methods in body-fitted solver ArgoDG w/ Cenaero

### Targeted applications

- DNS and LES of high-speed turbomachinery
- hypersonic flow during atmospheric reentry



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