

## High-Fidelity Simulations of Adverse Pressure Gradient Flow over a Rounded Step for Turbulence Model Improvement via Database Generation

ETMM-15

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Michel Rasquin<sup>1</sup>, Margaux Boxho<sup>1</sup>, Thomas Toulorge<sup>1</sup>, Koen Hillewaert<sup>2,1</sup>

<sup>1</sup> Cenaero, Gosselies, Belgium <sup>2</sup> University of Liège, Liège, Belgium

Contact: [michel.rasquin@cenaero.be](mailto:michel.rasquin@cenaero.be)

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Predicting **turbulent** flows with **separation**

Remains a **major challenge** in fluid dynamics and engineering

**Industry** relies on **low-fidelity methods** (RANS, WMLES)

**Limited reliability** for **separated** or **secondary** flows

**Improved turbulence models** can strongly impact

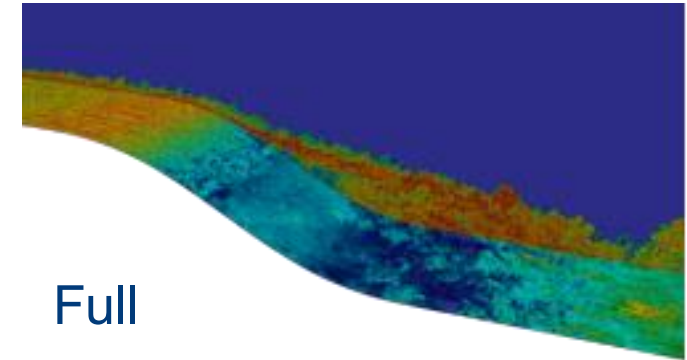
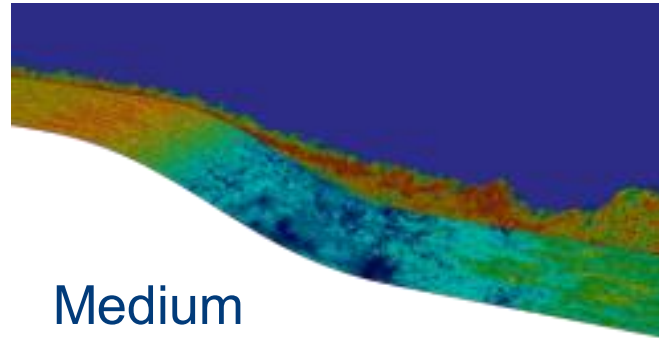
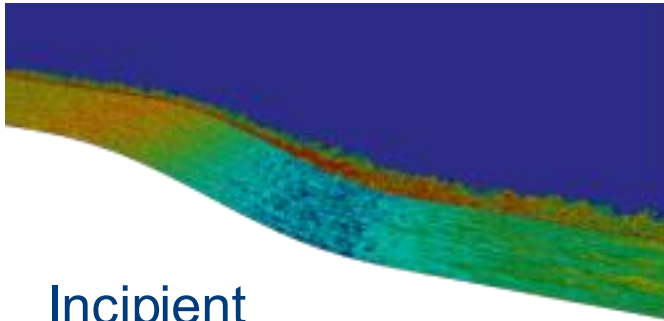
**Energy efficiency**

**Noise reduction**

**Emission**

# Approach and objectives

- **Generate a high-fidelity database** for a representative configuration
  - **HiFi-Turb DLR rounded step** (ERCOFTAC KB Wiki)



- **Gather**
  - **Statistical quantities:** Flow quantities, Favre-averaged Navier-Stokes, Reynold stress and dissipation
  - **Instantaneous fields** (solution and its gradients)



ERCOFTAC KB Wiki

- **Improve RANS and WMLES** using **data-driven** and **ML** approaches

- **Definition of common set of 180 statistics that allow reconstructing all RANS models**

- **Level 1 – Favre-averaged Navier-Stokes eq. + flow field and QoI**

- **Level 2 – Favre-averaged Reynolds stress eq.**

- Several variants considered (Gerolymos and Vallet, Knight, Grigoriev, etc)

$$\mathcal{R}_{ij,t} + (\mathcal{R}_{ij} \tilde{u}_k)_{,k} = P_{ij} + D_{ij} + \Phi_{ij} + \Phi'_{ij} - \epsilon_{ij} + K_{ij} \quad \mathcal{R}_{ij} = \overline{\rho u_i'' u_j''}$$

- **Level 3 – Solenoidal dissipation eq. (Kreuzinger et al.)**

- Includes third order derivative of velocity

$$\frac{D\epsilon_s}{Dt} = P_\epsilon^1 + P_\epsilon^2 + P_\epsilon^3 + P_\epsilon^4 + T_\epsilon + D_\epsilon - \Upsilon + F_\epsilon + T_\epsilon^C + B_\epsilon + \frac{\epsilon_s}{\tilde{\nu}} \frac{D\nu}{Dt} \quad \epsilon_s = \tilde{\nu} \overline{\omega'_k \omega'_k}$$

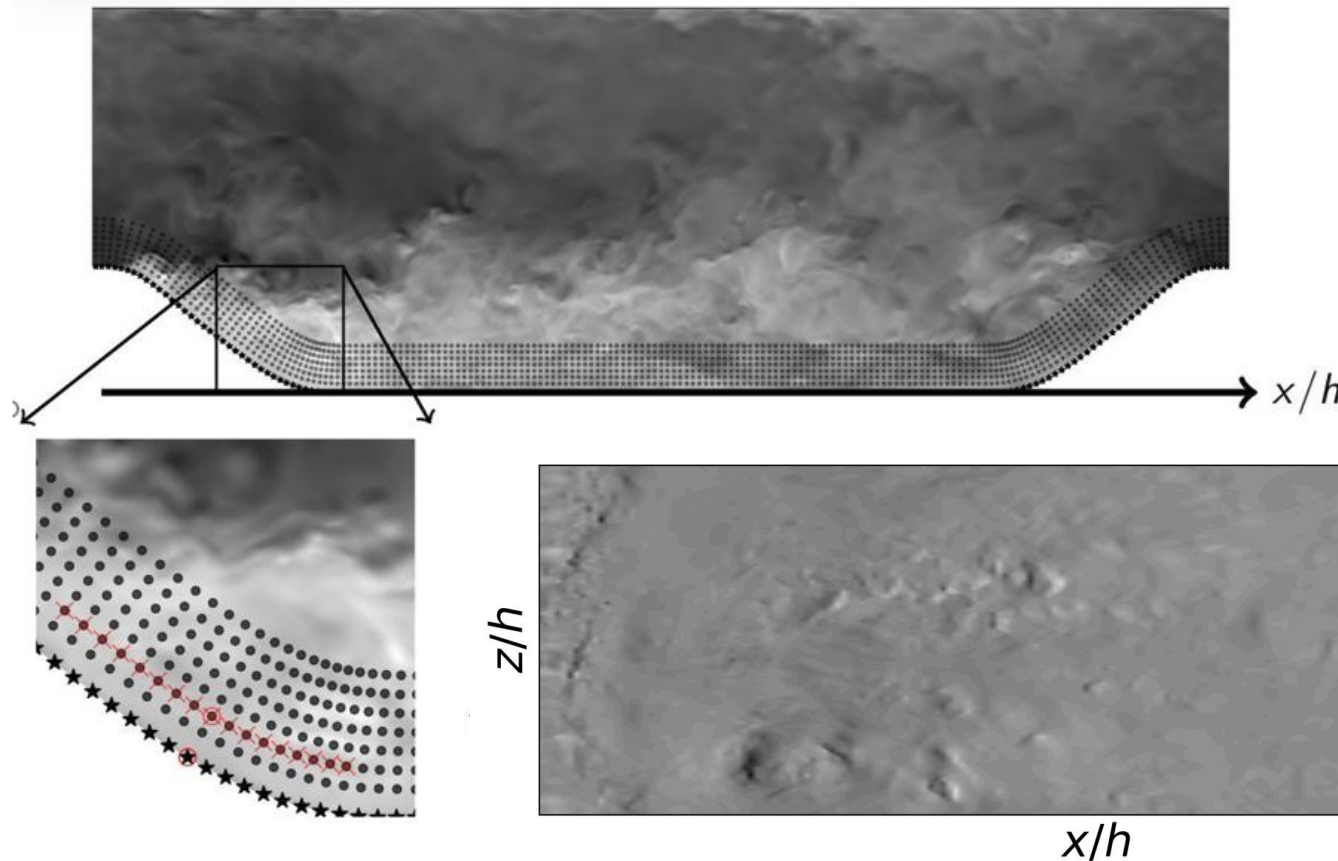
- **All intermediate terms are also stored**

- Strain rate and rotation tensors, velocity correlations, etc

- **If homogeneous direction (e.g. cascade): spanwise + temporal average**

- Resulting quantities represented by 2D polynomials functions in a plane (ParaView format)
- Low memory footprint during computation, low disk storage and reduced post-processing burden

## Instantaneous data at probes along the surface



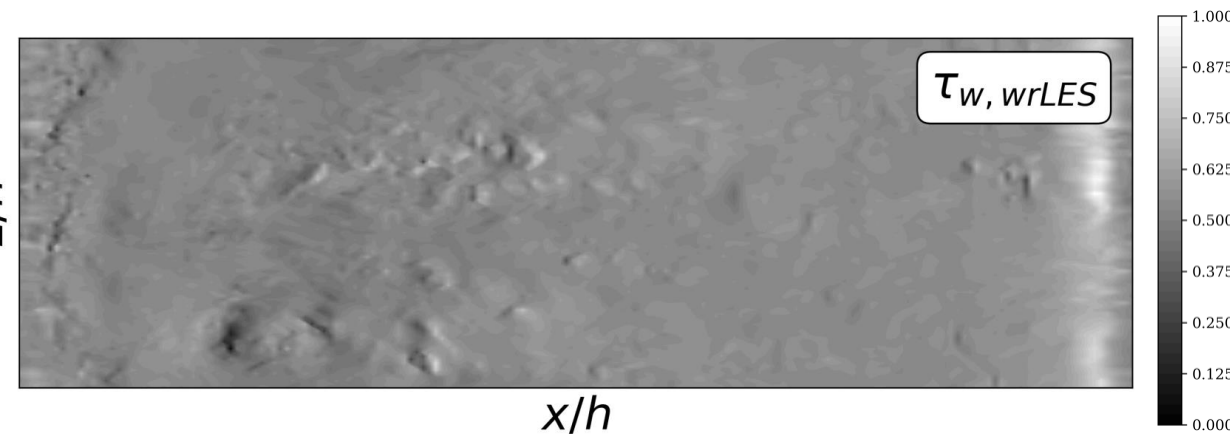
Solution and its gradients

- Boxho *et al.* (2022)

<https://doi.org/10.1007/s10494-022-00365-3>

- Boxho *et al.* (2025)

<https://doi.org/10.1007/s10494-025-00641-y>

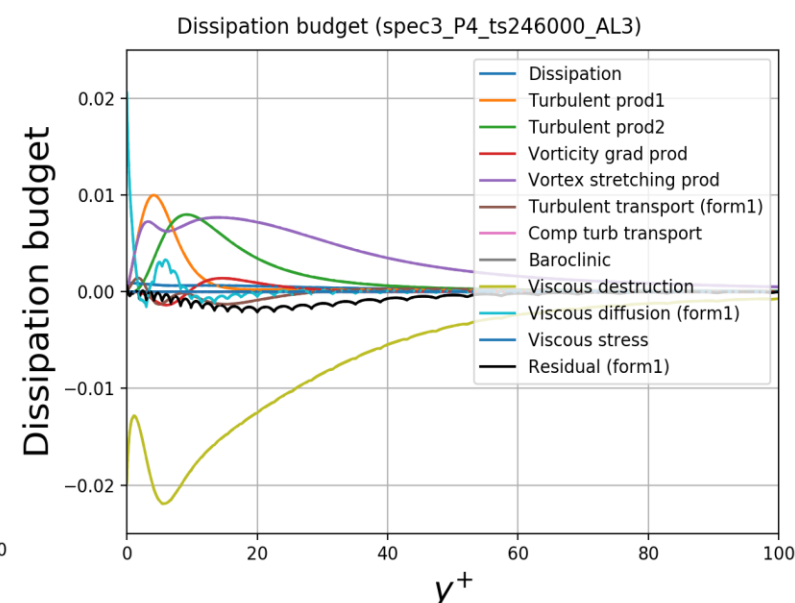
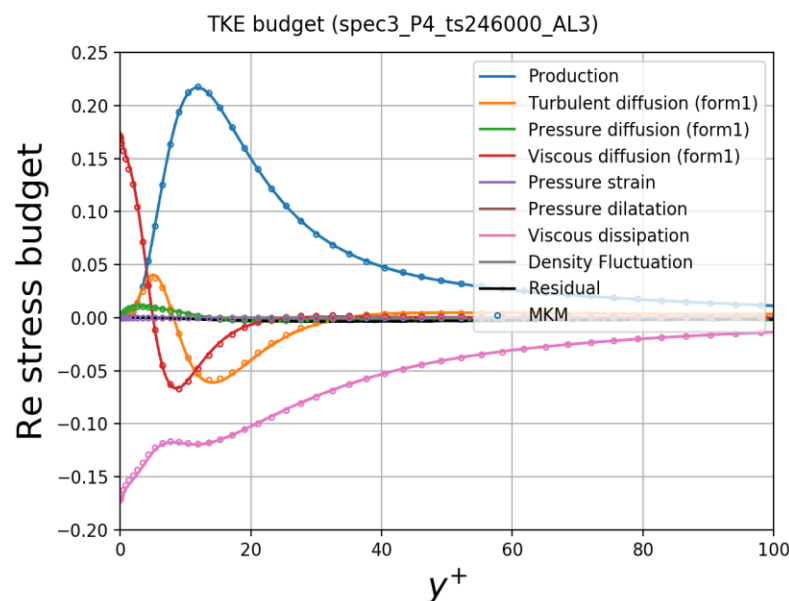


## Instantaneous wall shear stress on the surface

# TKE and dissipation budget closure

- Channel flow test case at  $Re_\tau = 180$
- TKE: validation against KMM

	$\Delta x^+$	$\Delta y_1^+$	max $\Delta y^+ = \Delta z^+$	$\Delta z^+$	DoFs (M)	$t^+$
spec1 DG-P3	10	0.5	5	5	16.8	28
spec1 DG-P4	10	0.5	5	5	14.6	22.5
spec3 DG-P4	6	0.25	4	4	39.8	28



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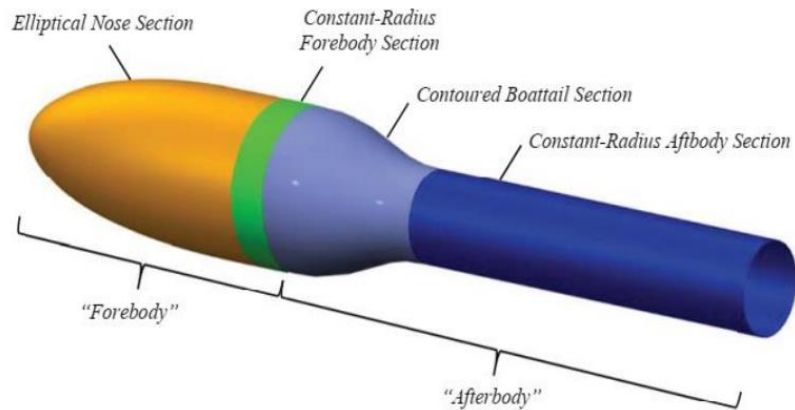
	TKE (max res/max prod)	Dissipation (max res/max viscous destruction)
spec1 DG-P3	0.051	0.208
spec1 DG-P4	0.033	0.117
spec3 DG-P4	0.015	0.078

**Budget mathematically closed** → must tend to **zero** with increased **resolution**

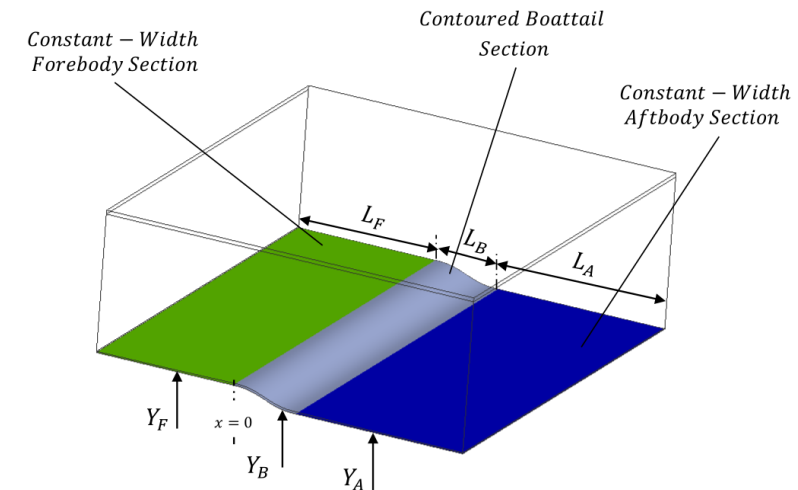
**Solenoidal assumption** → **budget mathematically not closed**

# HiFi-Turb DLR rounded step

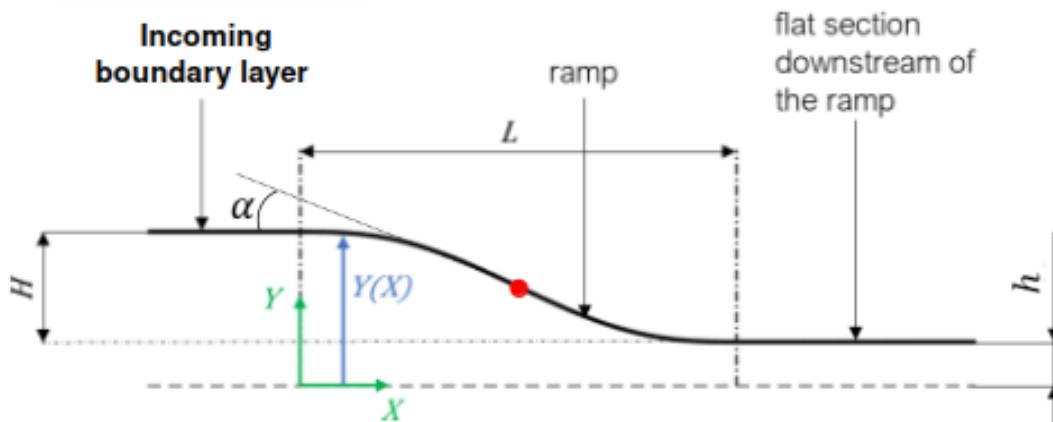
## Ercoftac KB Wiki



Disodell and Rumsey (2017)  
Simmons et al (2018)



HiFi-Turb DLR rounded step

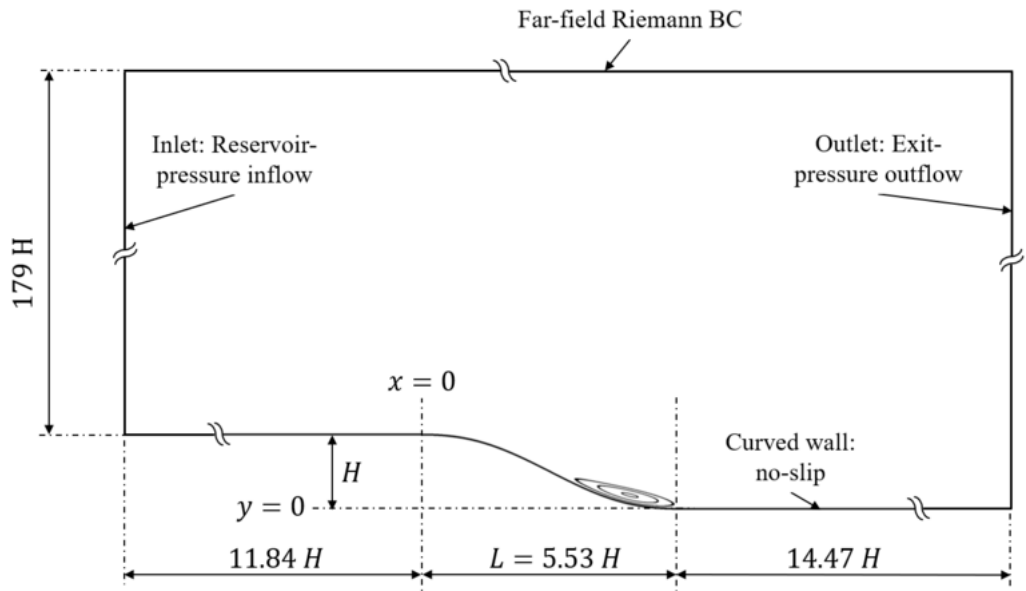
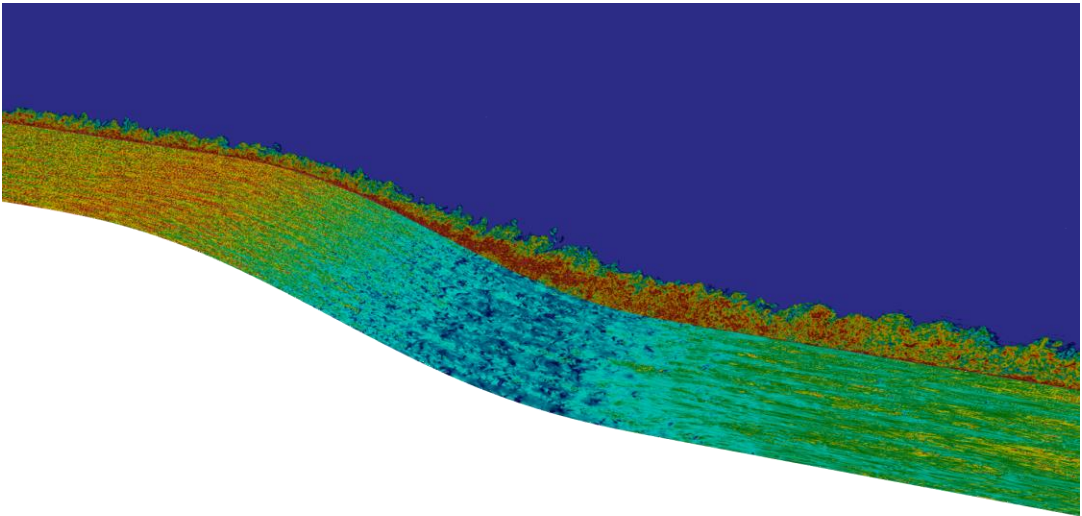


Ramp: 5th order polynomial with zero  
1st and 2nd derivatives at both ends



# HiFi-Turb DLR rounded step

Ercoftac KB Wiki

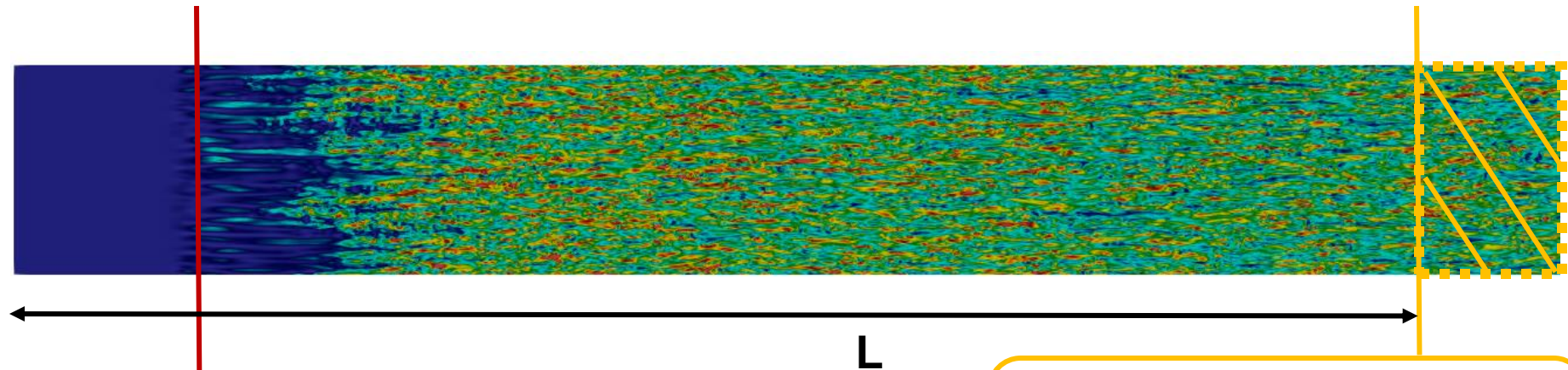
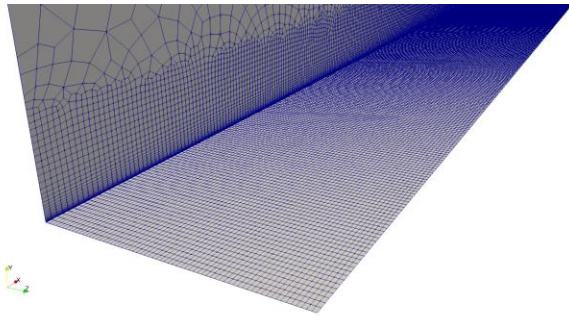
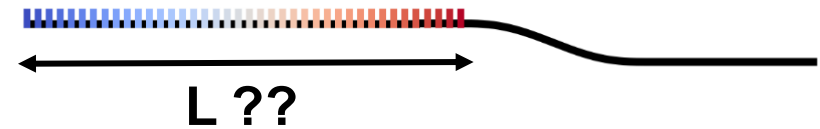


Upstream flat plate	Blasius BL profile ( $Re_{x,inlet} = 650\,000$ )
Transition	Numerical tripping based on a source term proposed by Schlatter et al. (2012) -> harmonics in time and space (span)
$Re_\tau$ at the step	$\sim 700$
Ma	$\sim 0.13$
L, H and inlet $U_\infty$	L fixed, 3 values for H, $U_\infty$ fixed
H/L	0.181 (incipient separation) 0.226 (medium separation) 0.274 (full separation)
$Re_{\infty,L}$	434k
$Re_{\infty,H}$	78k (incipient), 98k (moderate), 119k (full)
Span length / H	3

# Upstream turbulent boundary layer

Length of the **flat plate region** upstream of the step ?

Determined using a **precursor flat plate** simulation

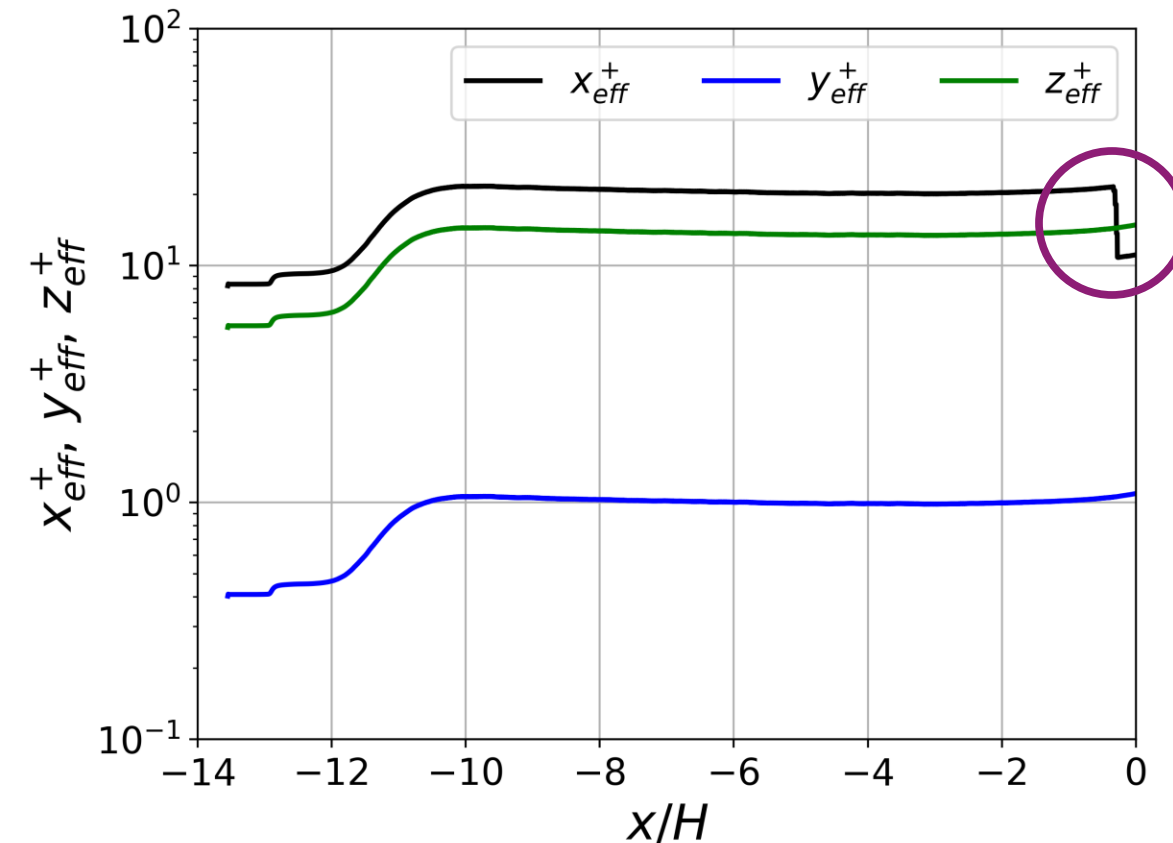
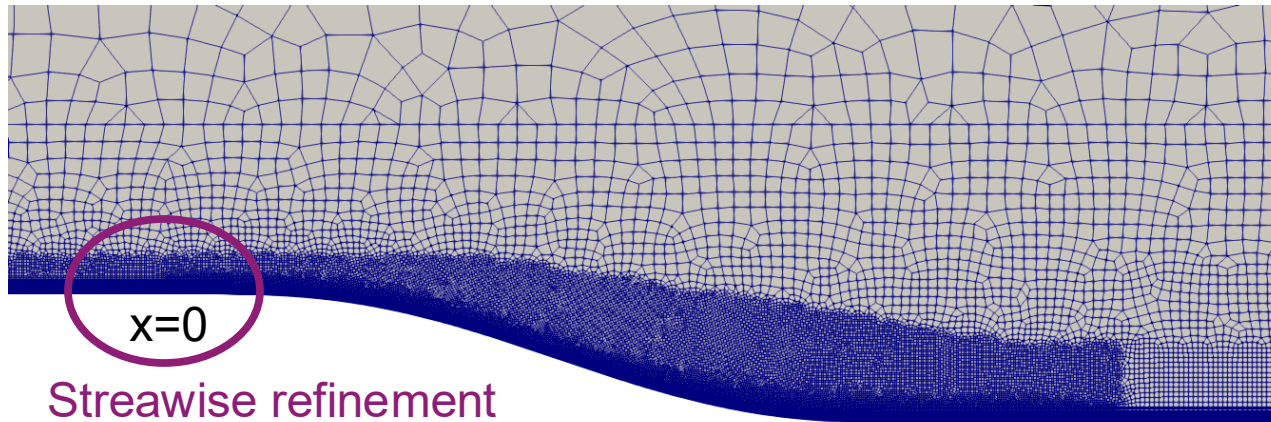


**Calibrate** the **tripping** source term to achieve the **target  $Re_\tau$**  at a reference point upstream of the step

**Cut** the flat plate domain at the **reference point** and **plug** the rounded **step**

# Simulation Methodology

## Discretization for LES

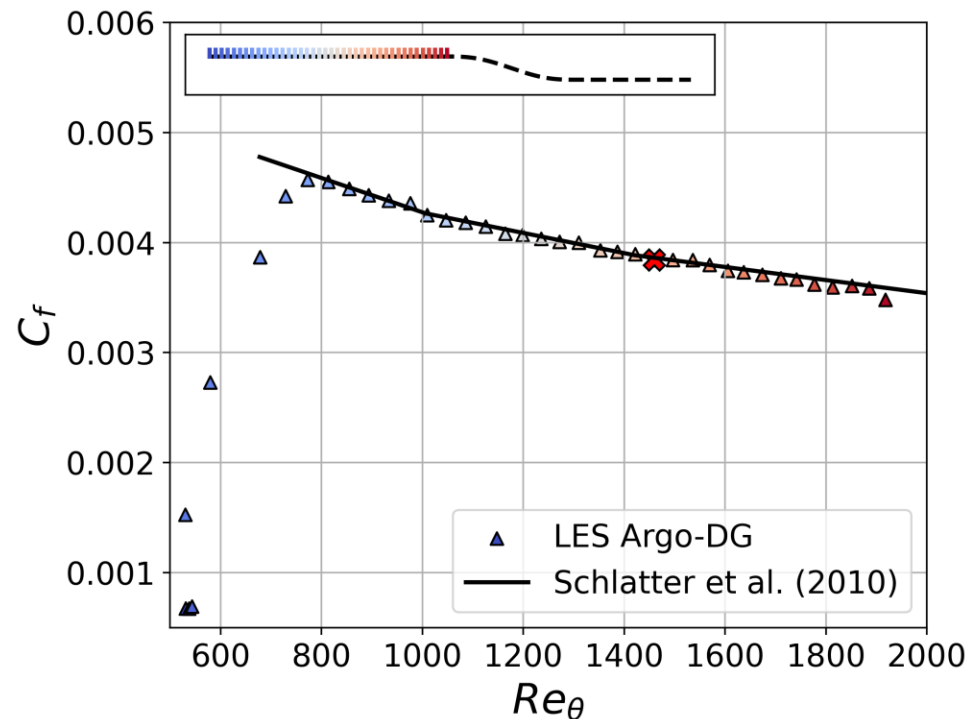


- Argo CFD solver

- Spatial discretization

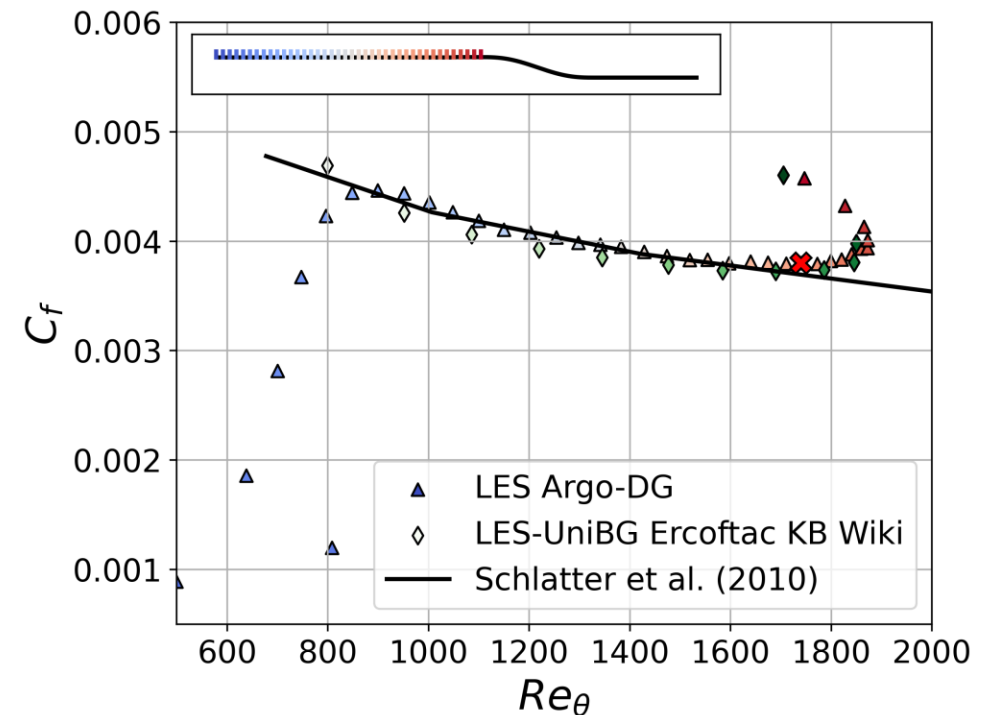
- DGM P4 (5<sup>th</sup>-order accurate)
- Hybrid hex-dominant mesh: 55k x 188 = 10M hexes
- Total: ~ 1.3B DoF/eq.
- Near-DNS resolution

- Analysis of the flat plate with and without the presence of the rounded step:  $C_f$  vs  $Re_\theta$



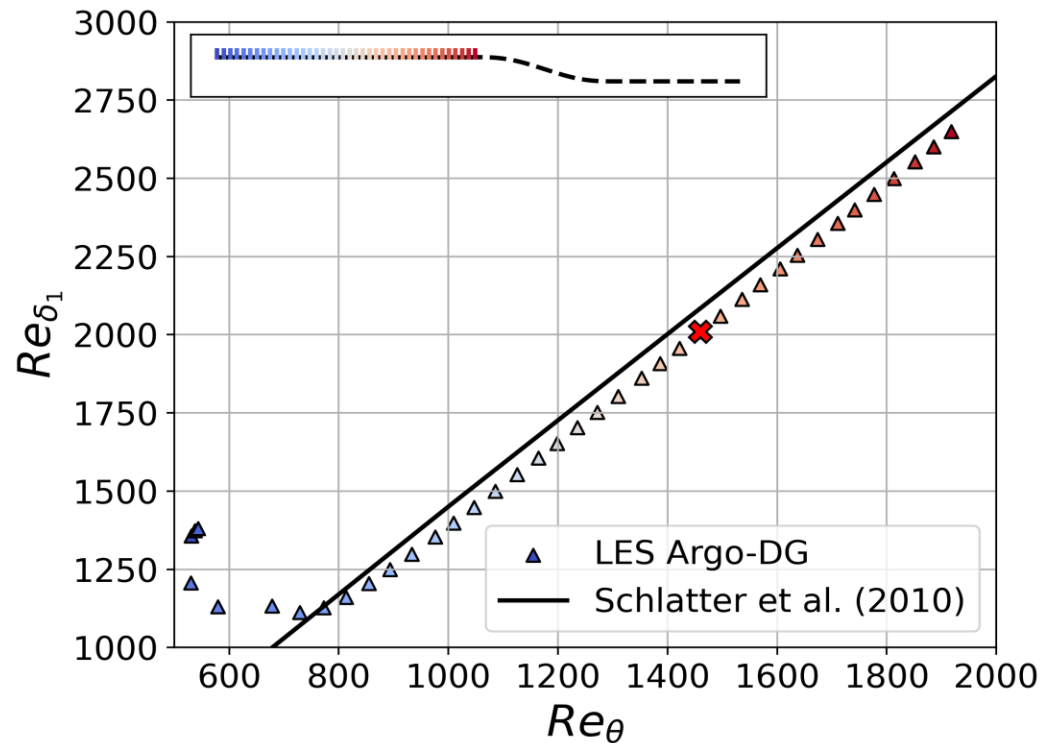
Good agreement with the DNS of Schlatter *et al.* (2010), all along the flat plate.

✗ = Reference point



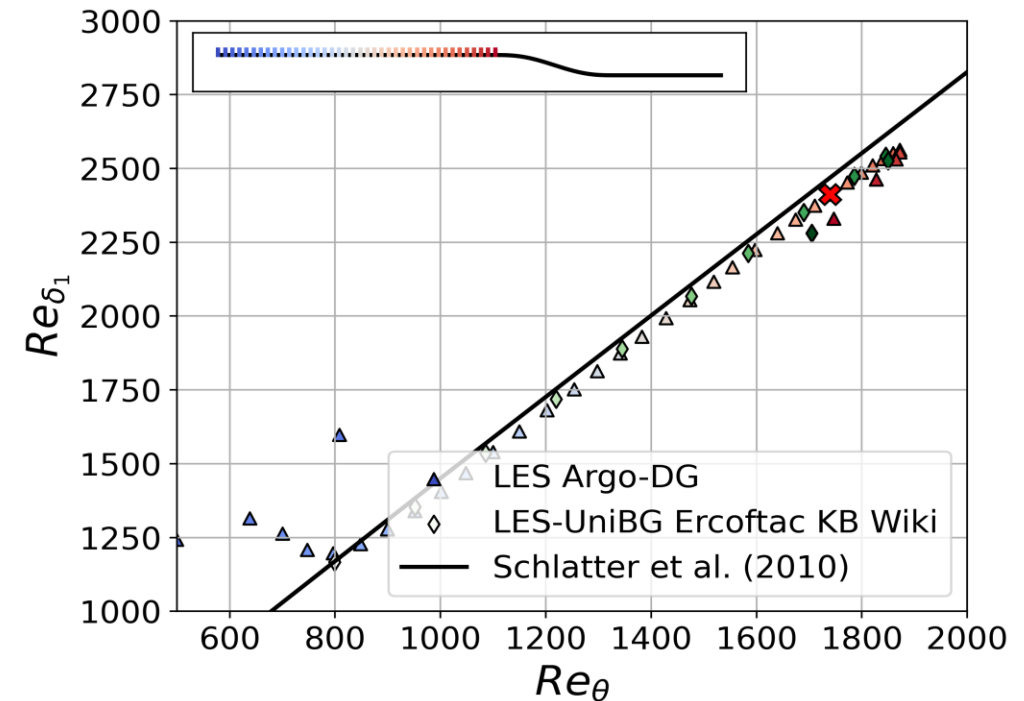
Good agreement up to the reference point (red cross), then the  $C_f$  increases indicating an **acceleration** of the TBL combined with a **reduction** in the **momentum thickness**.

- Analysis of the flat plate with and without the presence of the rounded step:  $Re_{\delta_1}$  vs  $Re_\theta$



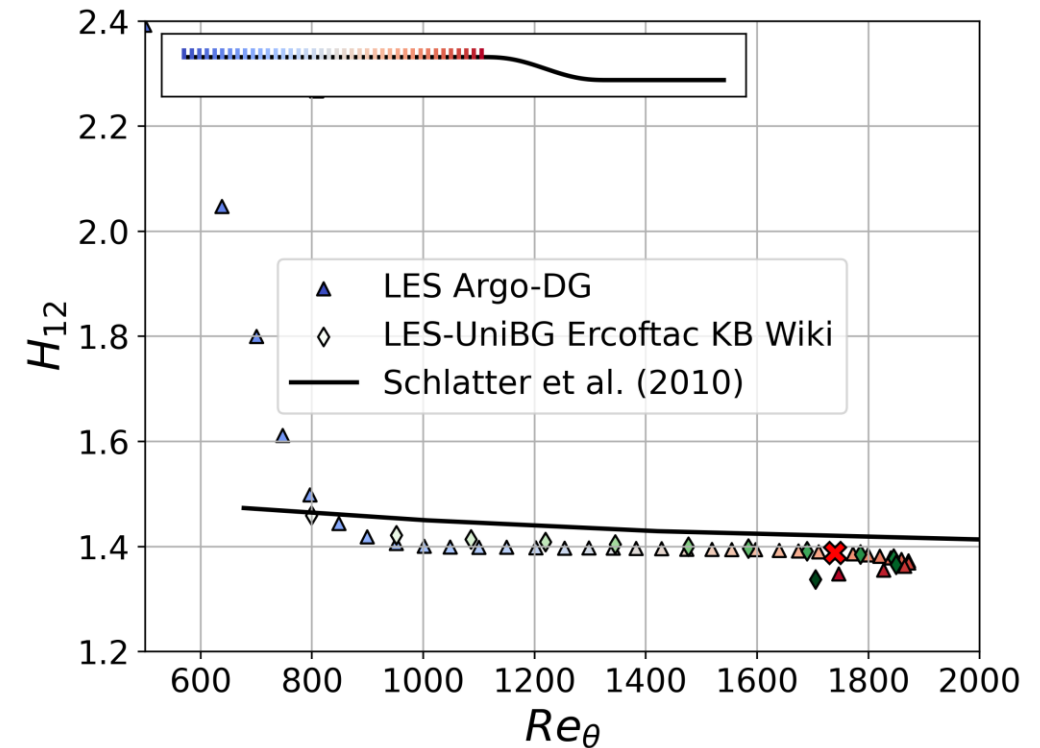
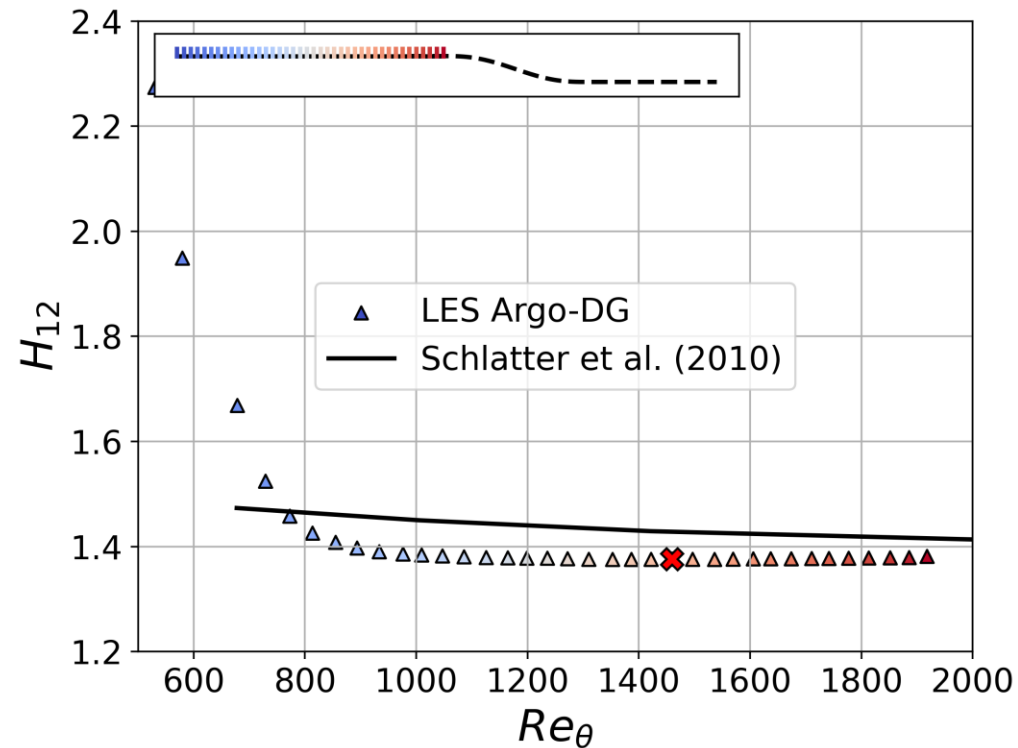
**Small offset** with the DNS of Schlatter *et al.* (2010) due to BC.

**X** = Reference point



**Good agreement** up to the **reference point** (red cross), then BL thicknesses are reduced.

- Analysis of the flat plate with and without the presence of the rounded step:  $H_{12}$  vs  $Re_\theta$



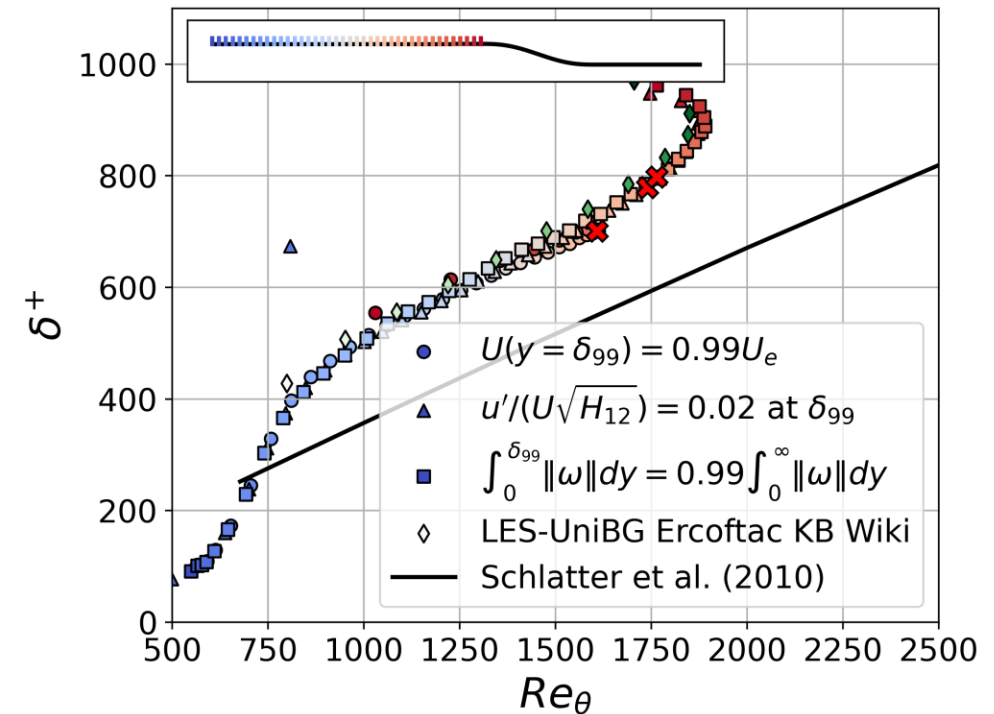
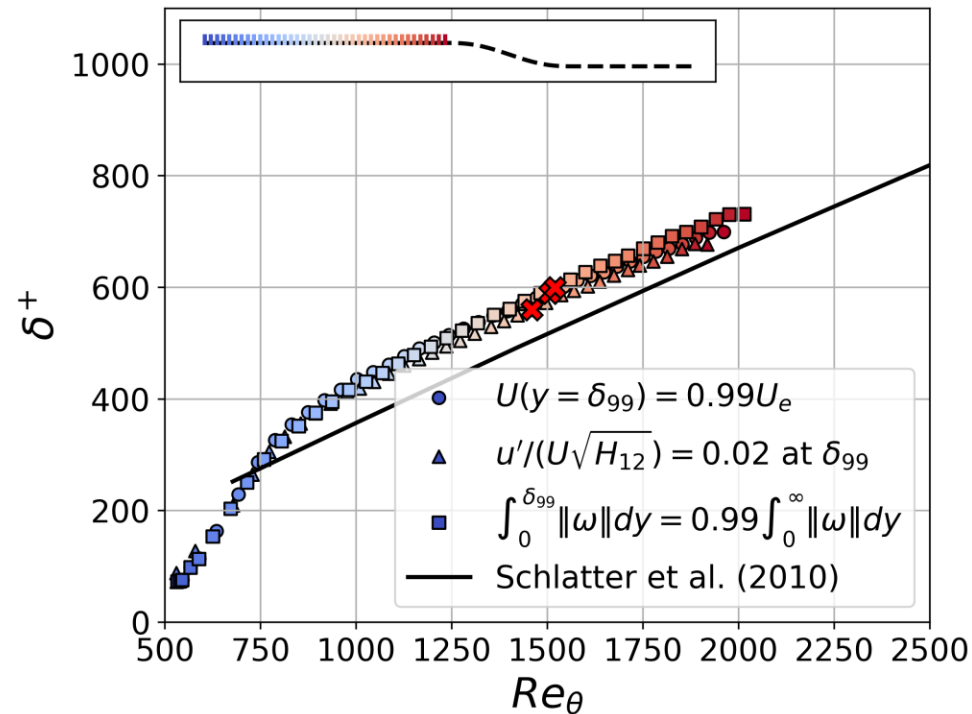
Underestimation of  $H_{12}$  compared with the DNS of Schlatter *et al.* (2010) due to BC.

Smaller  $H_{12}$  also observed in the LES from UniBG upstream the step, likely due to the pressure gradient

✗ = Reference point



- Analysis of the flat plate with and without the presence of the rounded step:  $Re_T$  vs  $Re_\theta$



The **diagnostic plot** (Vinuesa *et al.*, 2016) gives the **closest** results compared to the DNS of Schlatter *et al.* (2010), but a **small offset** is still visible (BC).

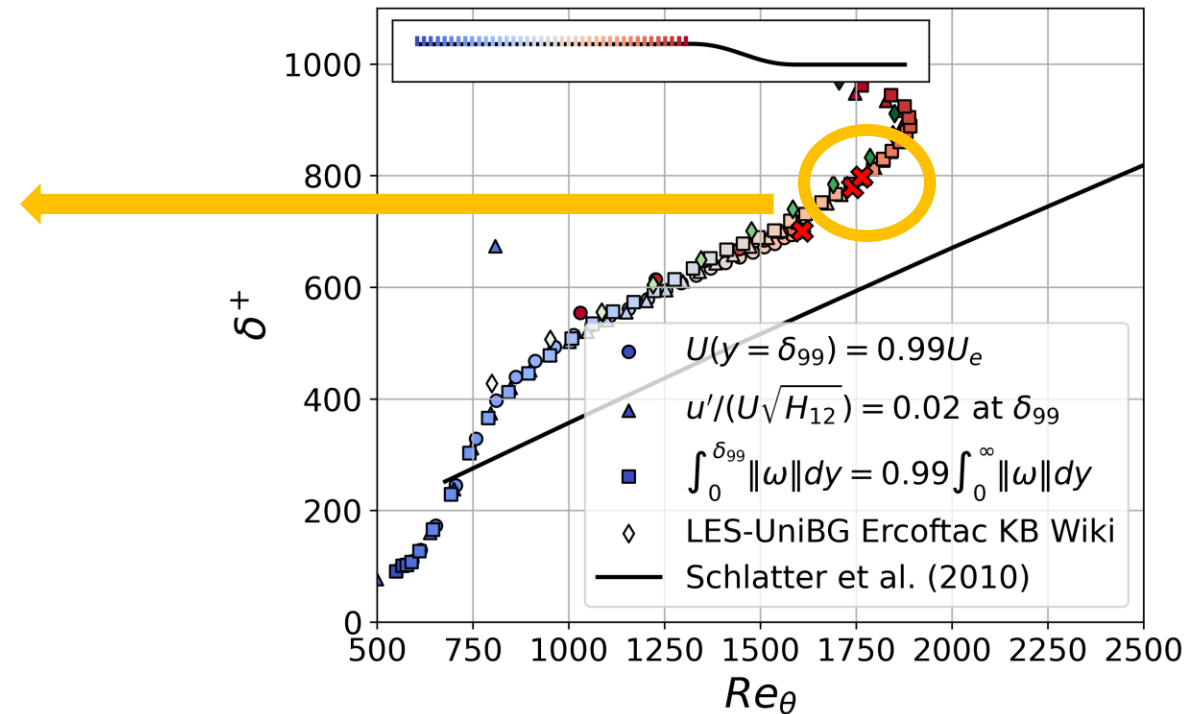
✗ = Reference point

The **diagnostic plot** and **vorticity** method produces the **correct far-field velocity** once the **rounded step effect** becomes effective.

- Analysis of the flat plate with and without the presence of the rounded step:  $Re_T$  vs  $Re_\theta$

	$x=-3.5H$ ✗	$x=0$
$Re_T$	766	947
$Re_\theta$	1711	1747
$\delta_{99} / H$	0.185	0.208

✗ = Reference point

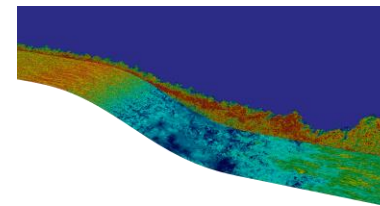
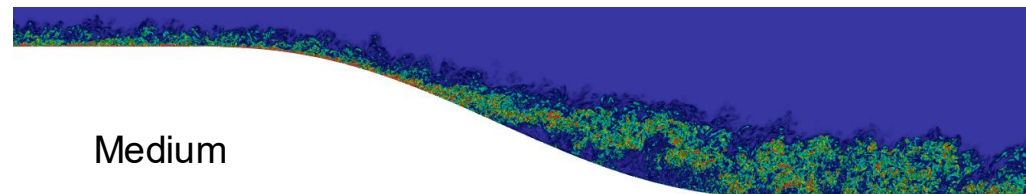
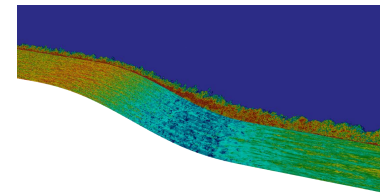
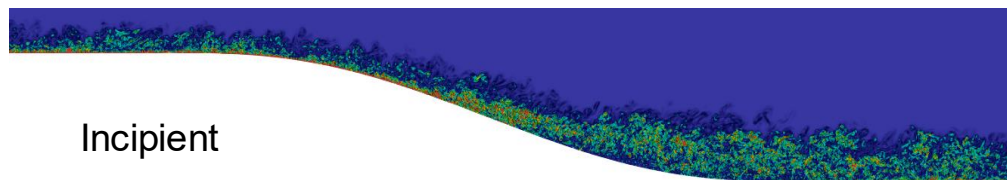


The **diagnostic plot** and **vorticity** method produces the **correct far-field velocity** once the **rounded step effect** becomes effective.



# Conclusions and Perspectives

- Assessment of the mesh requirements for budget closure on a channel
- Ongoing generation of a high-fidelity database for the HiFi-Turb DLR rounded step with adverse pressure gradient ongoing
- Analysis of the upstream boundary layer to assess inflow conditions
- Current focus on the incipient separation case; extension to medium separation planned
- Databases can serve as a reference for turbulence model improvement



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  - **EuroCC Belgium** for awarding this project access to the LUMI supercomputer, owned by the EuroHPC Joint Undertaking, hosted by CSC (Finland) and the LUMI consortium



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