



High-Fidelity Simulations of Adverse Pressure Gradient Flow over a Rounded Step for Turbulence Model Improvement via Database Generation

ETMM-15

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Predicting turbulent flows with **separation**

Remains a **major challenge** in fluid dynamics and engineering

Industry relies on **low-fidelity methods** (RANS, WMLES)

Limited reliability for separated or secondary flows

Improved turbulence models can strongly impact

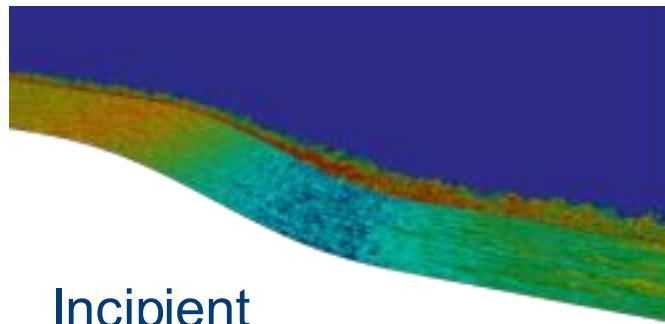
Energy efficiency

Noise reduction

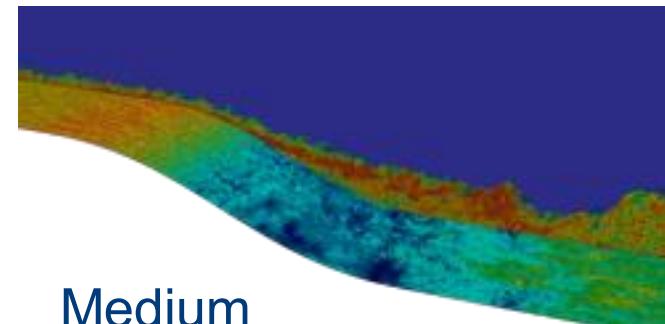
Emission

Approach and objectives

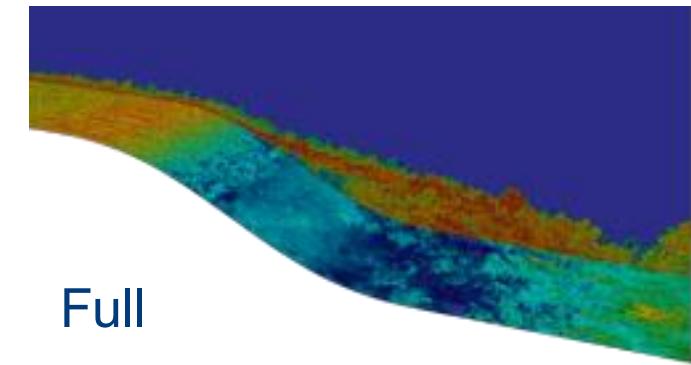
- **Generate a high-fidelity database** for a representative configuration
 - HiFi-Turb DLR rounded step (ERCOFTAC KB Wiki)



Incipient



Medium



Full

- **Gather**
 - **Statistical quantities:** Flow quantities, Favre-averaged Navier-Stokes, Reynold stress and dissipation
 - **Instantaneous fields** (solution and its gradients)
- **Improve RANS and WMLES using data-driven and ML approaches**



ERCOFTAC KB Wiki

- Definition of common set of 180 statistics that allow reconstructing all RANS models

- Level 1 – Favre-averaged Navier-Stokes eq. + flow field and QoI

- Level 2 – Favre-averaged Reynolds stress eq.

- Several variants considered (Gerolymos and Vallet, Knight, Grigoriev, etc)

$$\mathcal{R}_{ij,t} + (\mathcal{R}_{ij}\tilde{u}_k)_{,k} = P_{ij} + D_{ij} + \Phi_{ij} + \Phi'_{ij} - \epsilon_{ij} + K_{ij} \quad \mathcal{R}_{ij} = \overline{\rho u''_i u''_j}$$

- Level 3 – Solenoidal dissipation eq. (Kreuzinger et al.)

- Includes third order derivative of velocity

$$\frac{D\epsilon_s}{Dt} = P_\epsilon^1 + P_\epsilon^2 + P_\epsilon^3 + P_\epsilon^4 + T_\epsilon + D_\epsilon - \Upsilon + F_\epsilon + T_\epsilon^C + B_\epsilon + \frac{\epsilon_s}{\tilde{\nu}} \frac{D\nu}{Dt} \quad \epsilon_s = \tilde{\nu} \overline{\omega'_k \omega'_k}$$

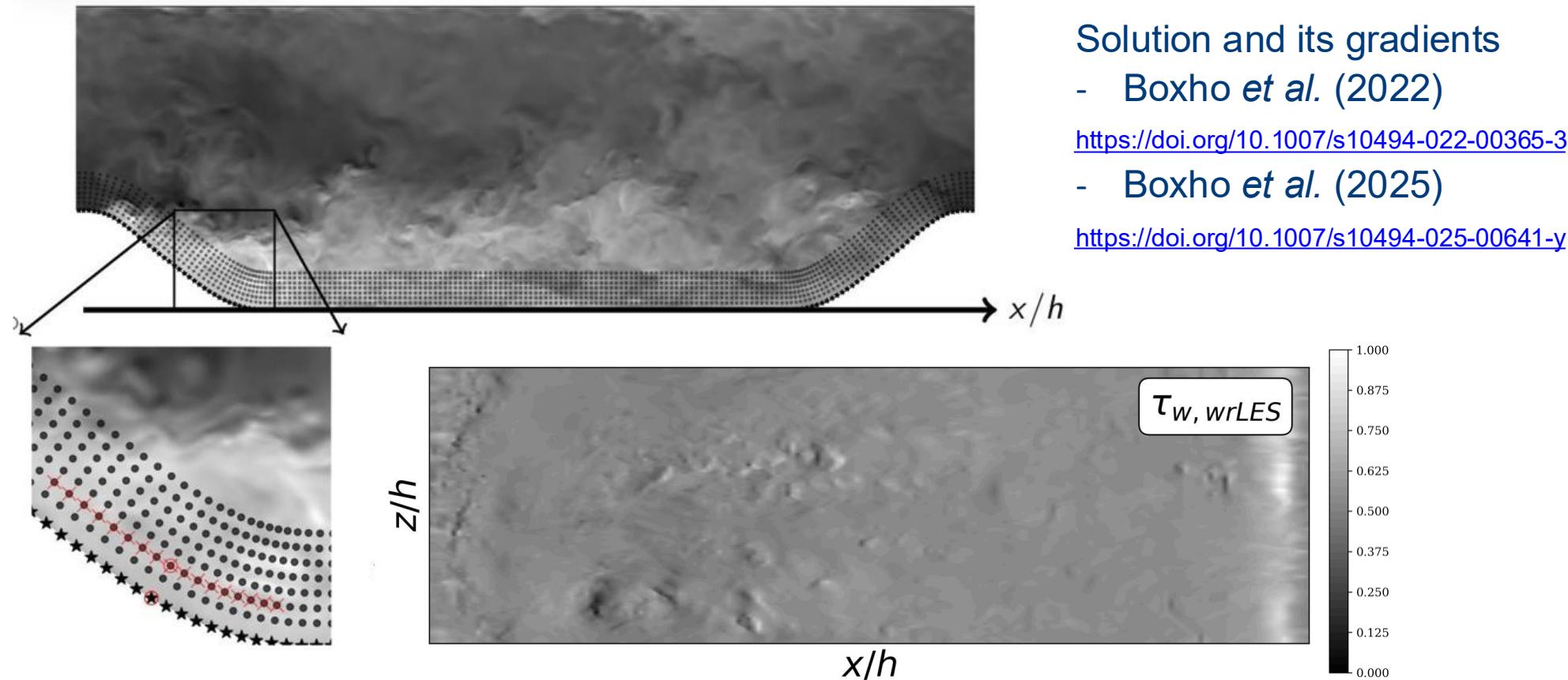
- All intermediate terms are also stored

- Strain rate and rotation tensors, velocity correlations, etc

- If homogeneous direction (e.g. cascade): spanwise + temporal average

- Resulting quantities represented by 2D polynomials functions in a plane (ParaView format)
 - Low memory footprint during computation, low disk storage and reduced post-processing burden

Instantaneous data at probes along the surface



Solution and its gradients

- Boxho *et al.* (2022)

<https://doi.org/10.1007/s10494-022-00365-3>

- Boxho *et al.* (2025)

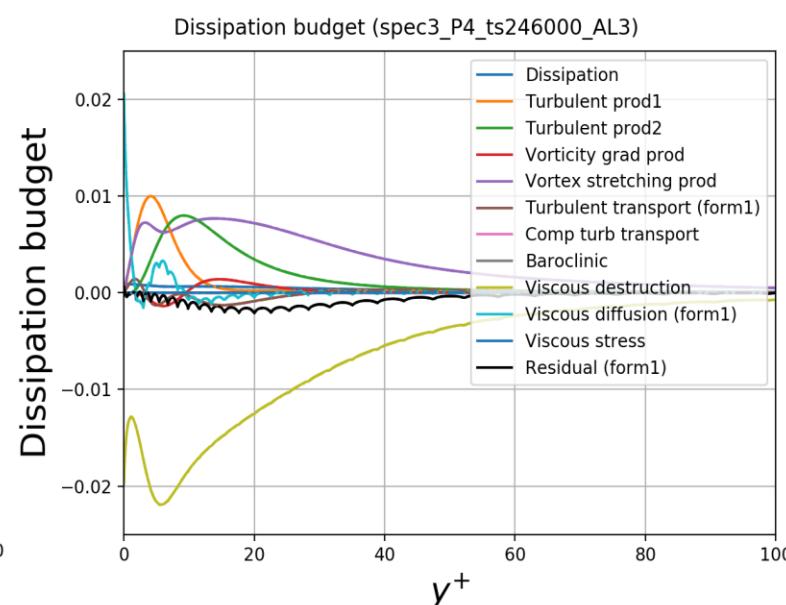
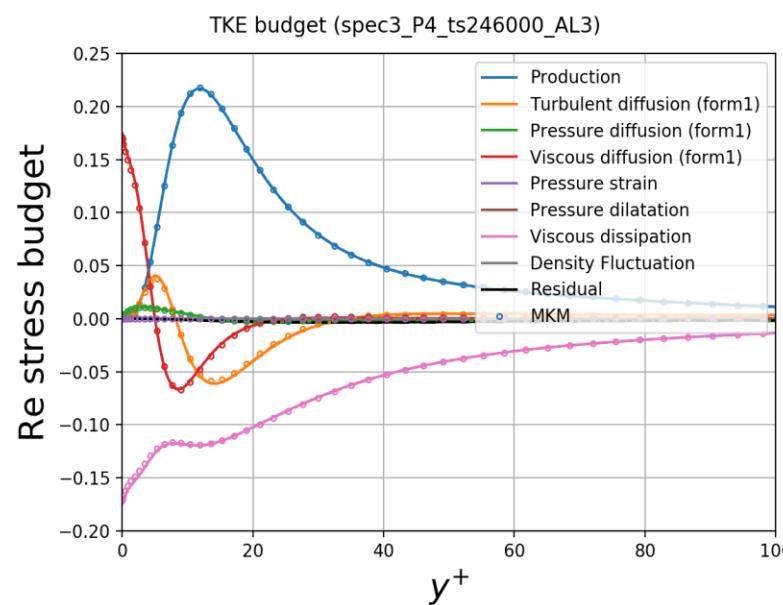
<https://doi.org/10.1007/s10494-025-00641-y>

Instantaneous wall shear stress on the surface

TKE and dissipation budget closure

- Channel flow test case at $Re_\tau = 180$
- TKE: validation against KMM

	Δx^+	Δy_1^+	$\max_{\Delta y^+ = \Delta z^+}$	Δz^+	DoFs (M)	t^+
spec1 DG-P3	10	0.5	5	5	16.8	28
spec1 DG-P4	10	0.5	5	5	14.6	22.5
spec3 DG-P4	6	0.25	4	4	39.8	28



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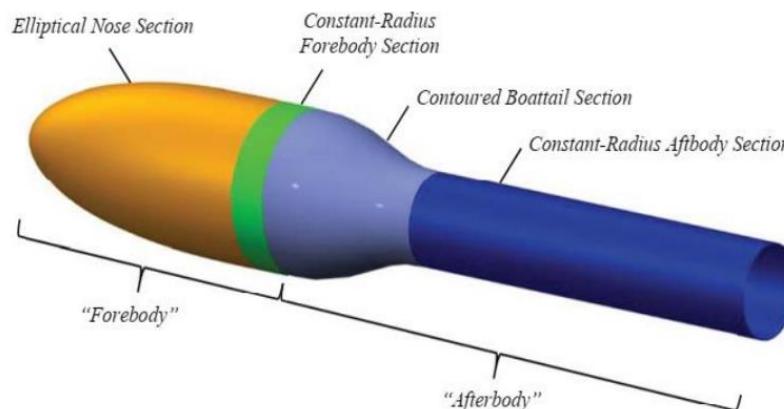
	TKE (max res/max prod)	Dissipation (max res/max viscous destruction)
spec1 DG-P3	0.051	0.208
spec1 DG-P4	0.033	0.117
spec3 DG-P4	0.015	0.078

Budget mathematically closed → must tend to **zero** with increased **resolution**

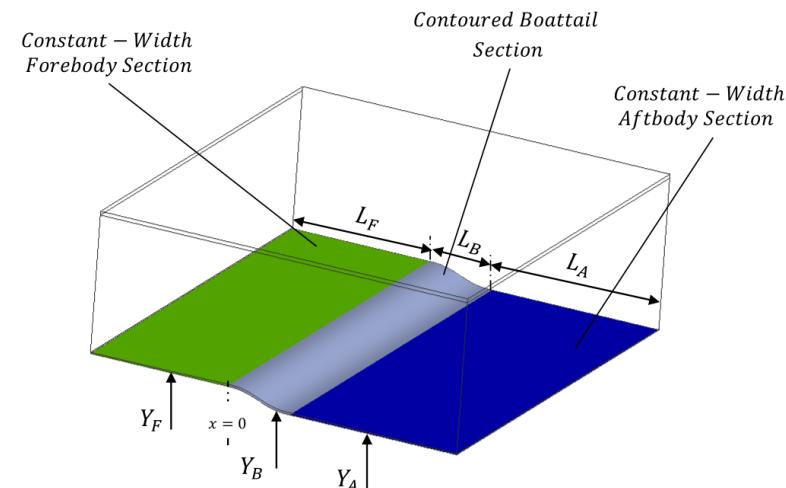
Solenoidal assumption → budget mathematically **not closed**

HiFi-Turb DLR rounded step

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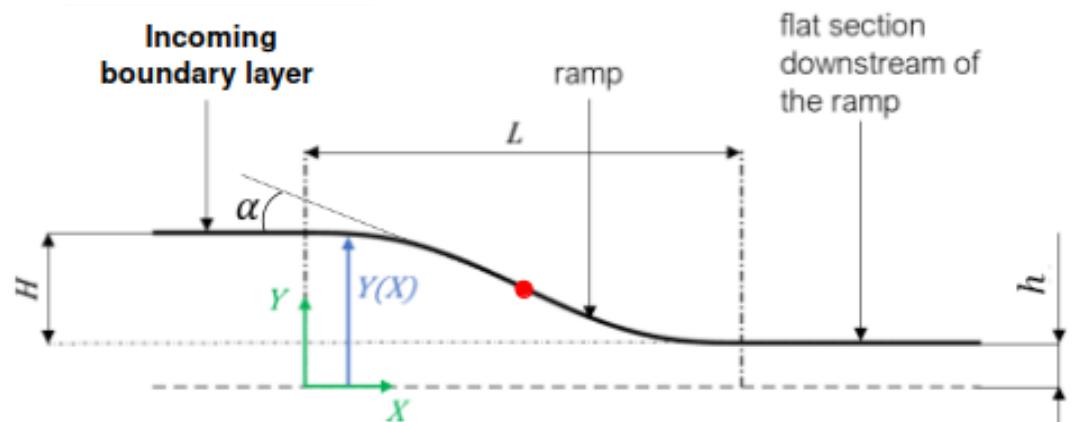
Disodell and Rumsey (2017)
Simmons et al (2018)



ERCOFTAC
European Research Community On
Flow, Turbulence And Combustion

HiFi-TURB

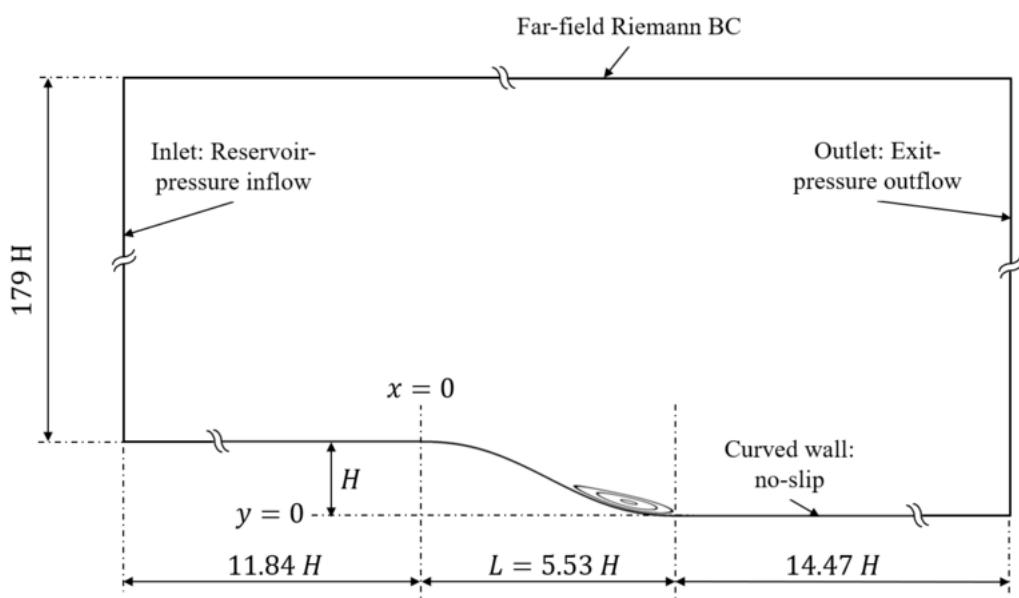
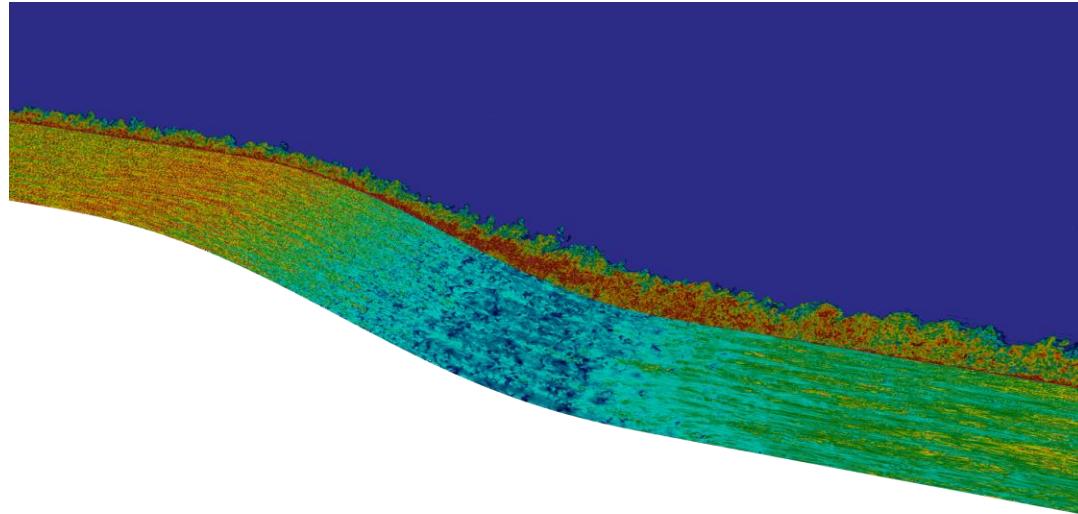
HiFi-Turb DLR rounded step



Ramp: 5th order polynomial with zero
1st and 2nd derivatives at both ends

HiFi-Turb DLR rounded step

Ercoftac KB Wiki

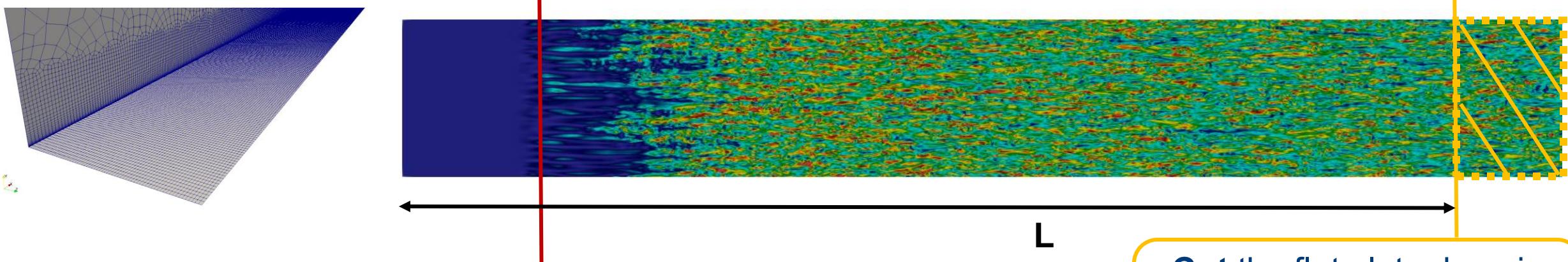
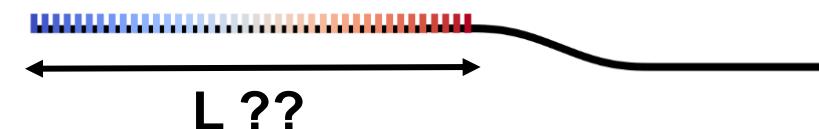


Upstream flat plate	Blasius BL profile ($Re_{x,\text{inlet}} = 650\,000$)
Transition	Numerical tripping based on a source term proposed by Schlatter et al. (2012) → harmonics in time and space (span)
Re_t at the step	~700
Ma	~0.13
L , H and inlet U_∞	L fixed, 3 values for H , U_∞ fixed
H/L	0.181 (incipient separation) 0.226 (medium separation) 0.274 (full separation)
$Re_{\infty,L}$	434k
$Re_{\infty,H}$	78k (incipient), 98k (moderate), 119k (full)
Span length / H	3

Upstream turbulent boundary layer

Length of the **flat plate region** upstream of the step ?

Determined using a **precursor flat plate** simulation

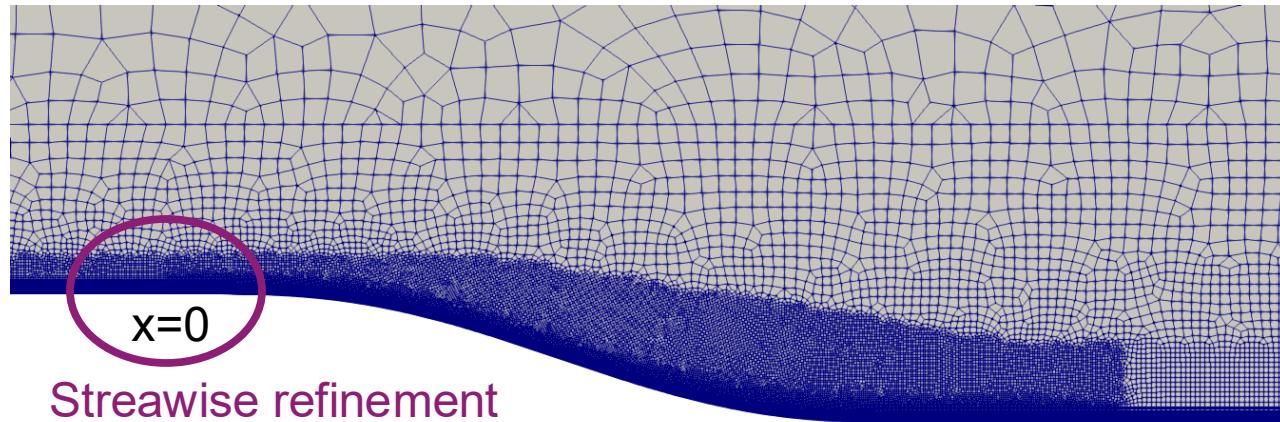


Calibrate the **tripping** source term to achieve the target Re_t at a reference point upstream of the step

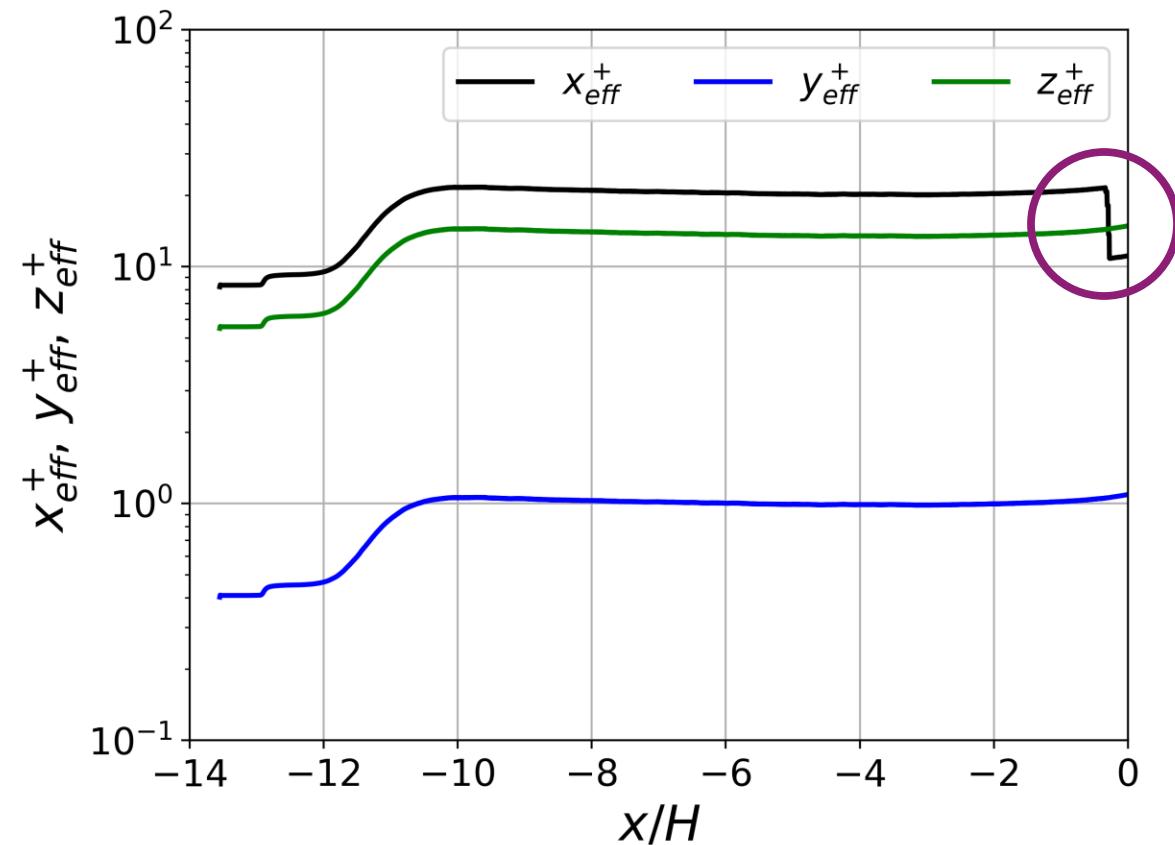
Cut the flat plate domain at the **reference point** and plug the rounded **step**

Simulation Methodology

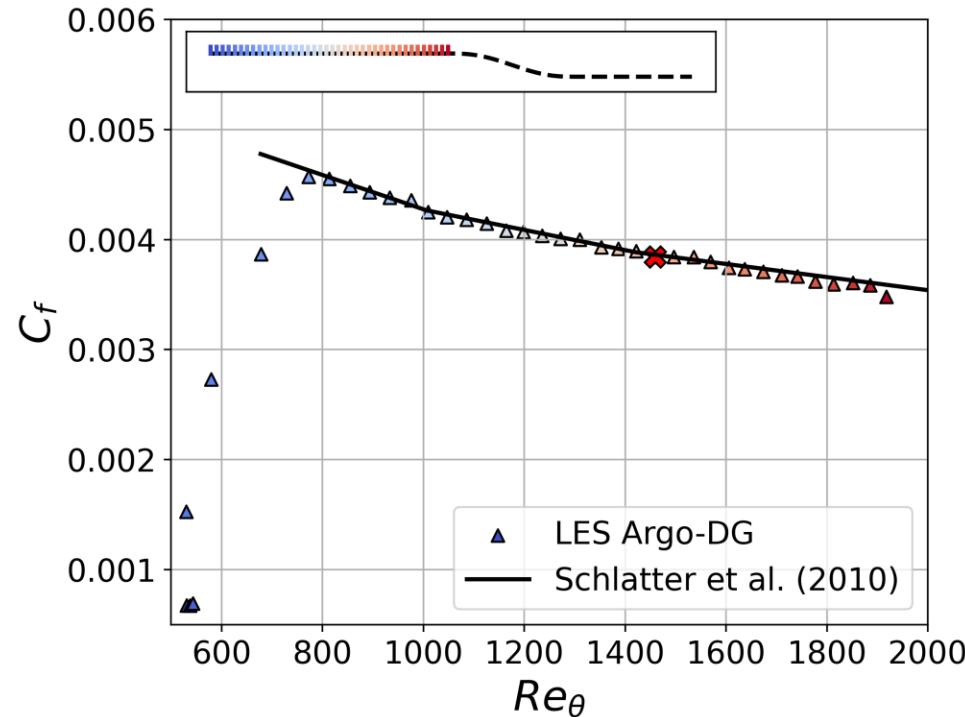
Discretization for LES



- Argo CFD solver
- Spatial discretization
 - DGM P4 (5th-order accurate)
 - Hybrid hex-dominant mesh: $55k \times 188 = 10M$ hexes
 - Total: $\sim 1.3B$ DoF/eq.
 - Near-DNS resolution

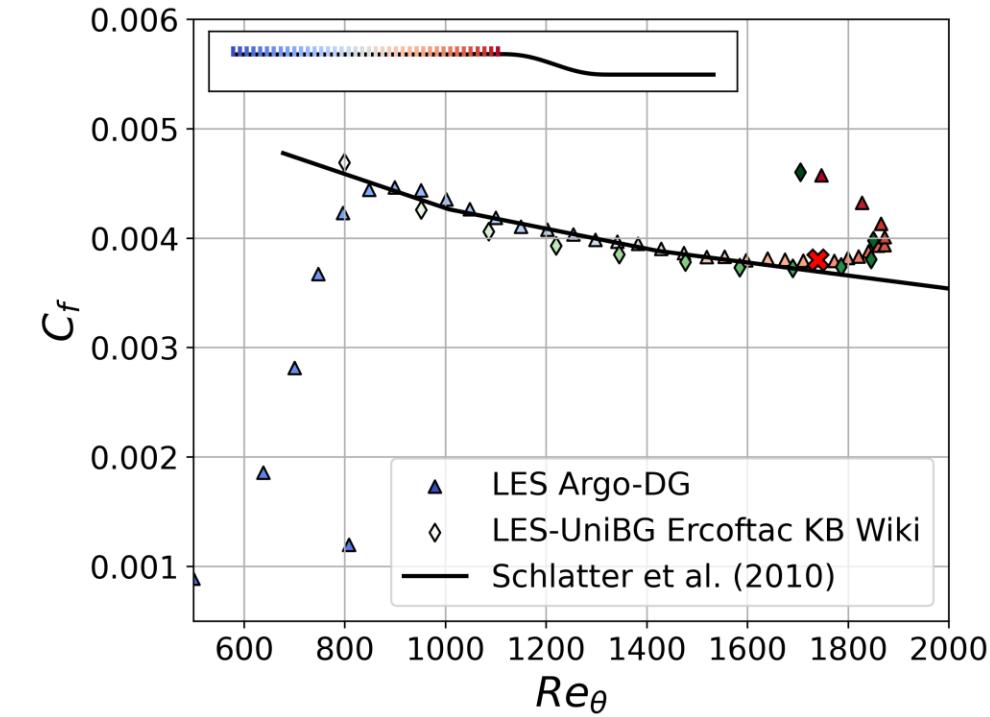


- Analysis of the flat plate with and without the presence of the rounded step: C_f vs Re_θ



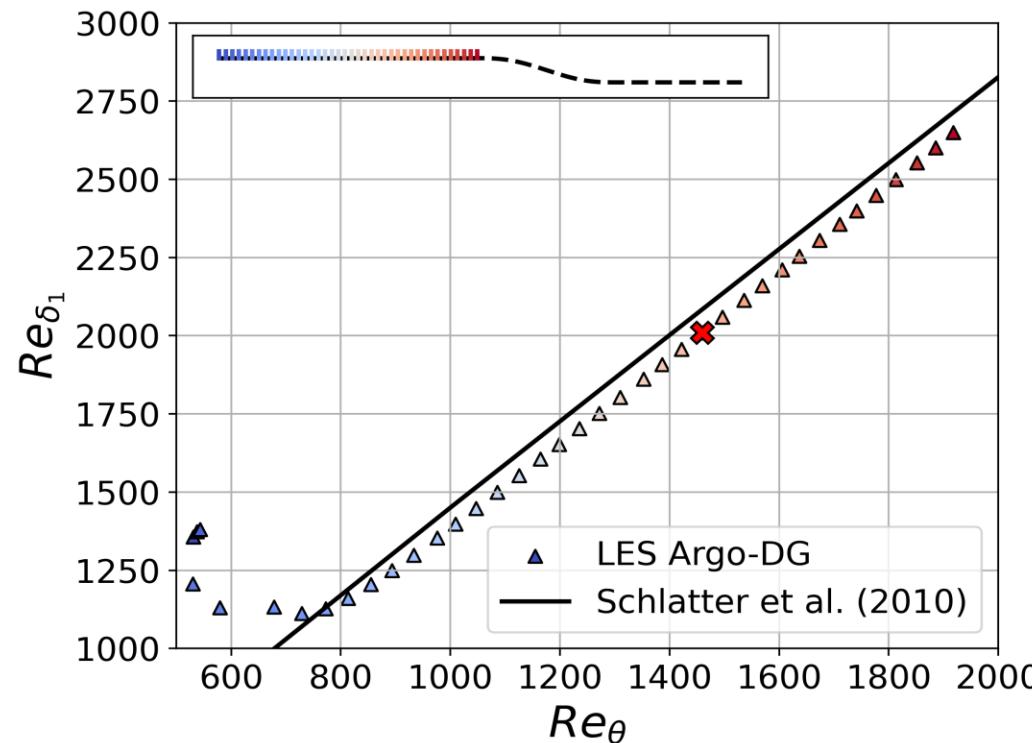
Good agreement with the DNS of Schlatter *et al.* (2010), all along the flat plate.

✗ = Reference point



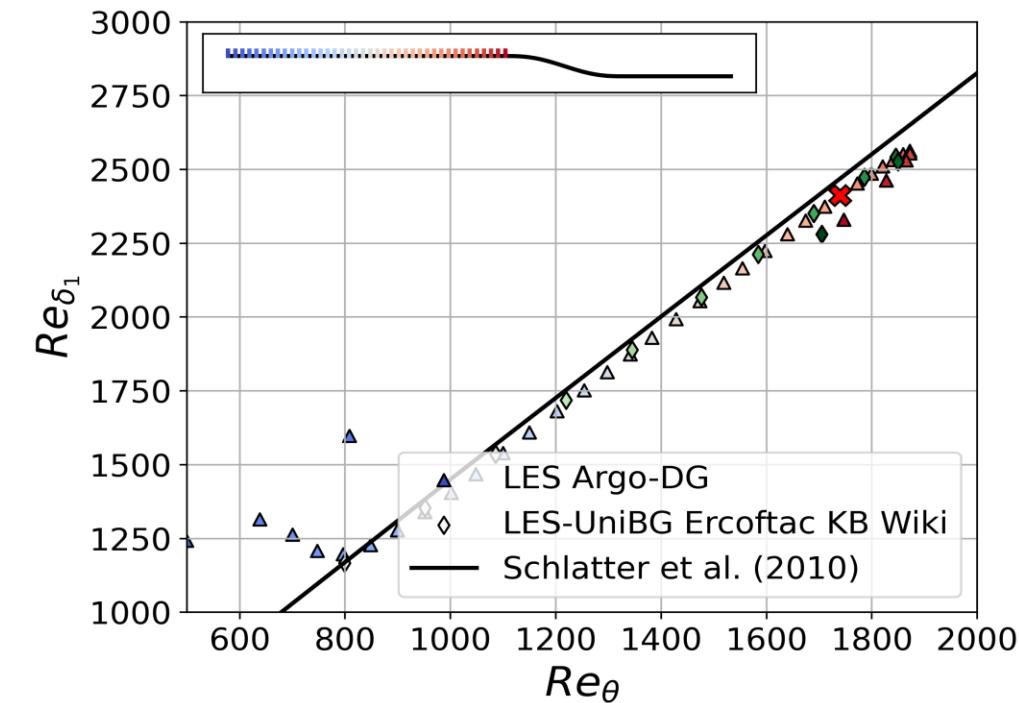
Good agreement up to the reference point (red cross), then the C_f increases indicating an acceleration of the TBL combined with a reduction in the momentum thickness.

- Analysis of the flat plate with and without the presence of the rounded step: Re_{δ_1} vs Re_{θ}



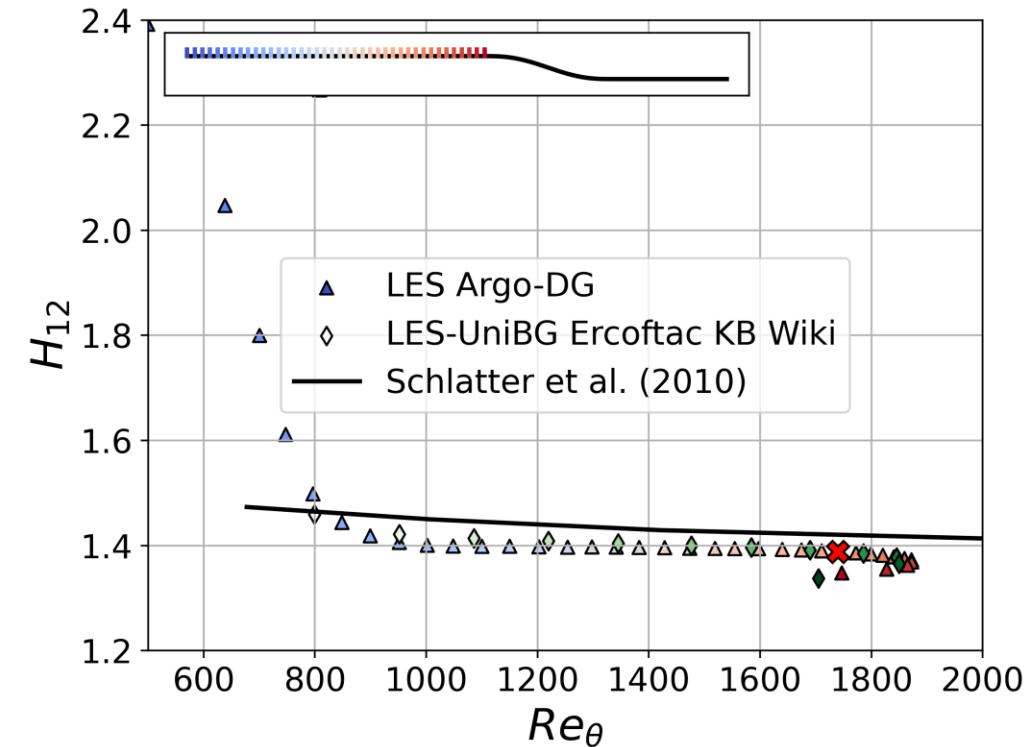
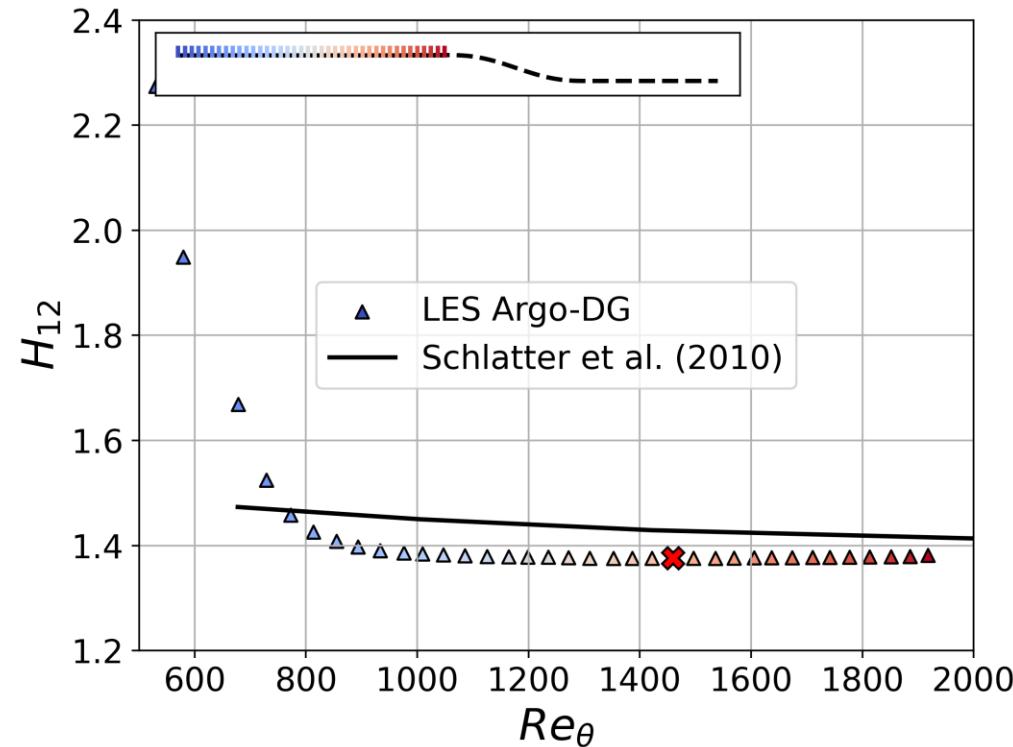
Small offset with the DNS of Schlatter *et al.* (2010) due to BC.

✗ = Reference point



Good agreement up to the reference point (red cross), then BL thicknesses are reduced.

- Analysis of the flat plate with and without the presence of the rounded step: H_{12} vs Re_θ

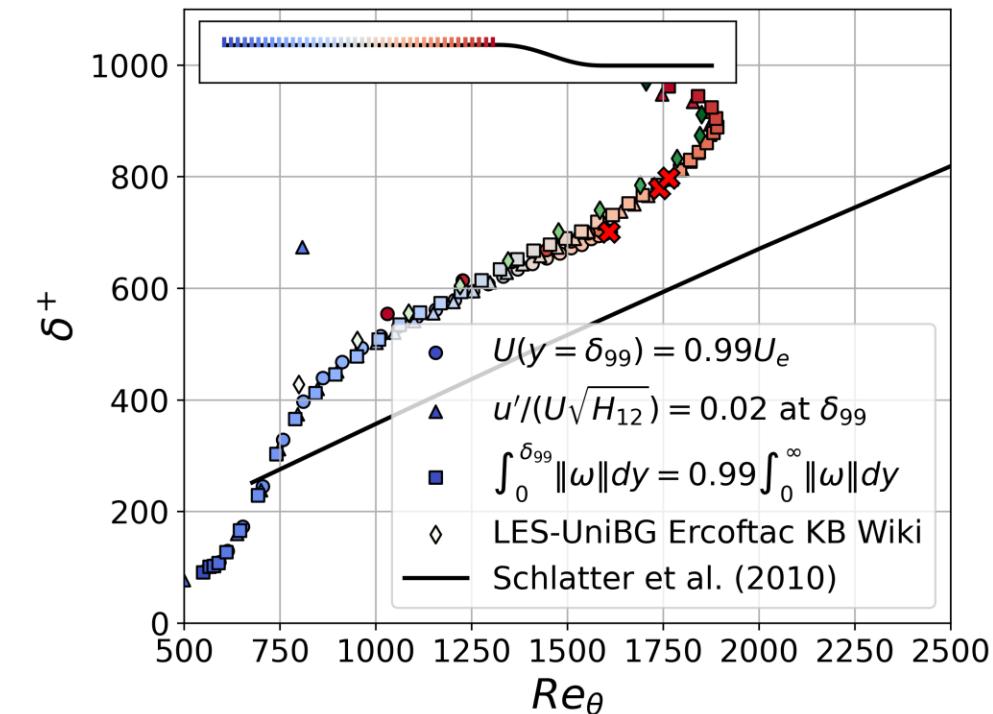
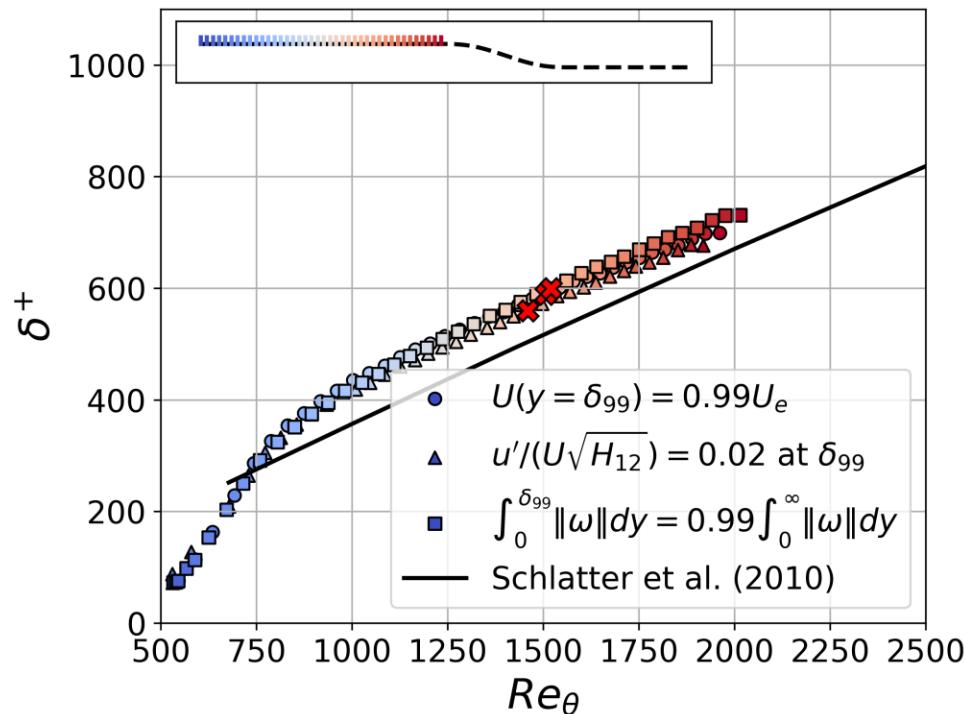


Underestimation of H_{12} compared with the DNS of Schlatter et al. (2010) due to BC.

✖ = Reference point

Smaller H_{12} also observed in the LES from UniBG upstream the step, likely due to the pressure gradient

- Analysis of the flat plate with and without the presence of the rounded step: Re_T vs Re_θ



The diagnostic plot (Vinuesa et al., 2016) gives the closest results compared to the DNS of Schlatter et al. (2010), but a small offset is still visible (BC).

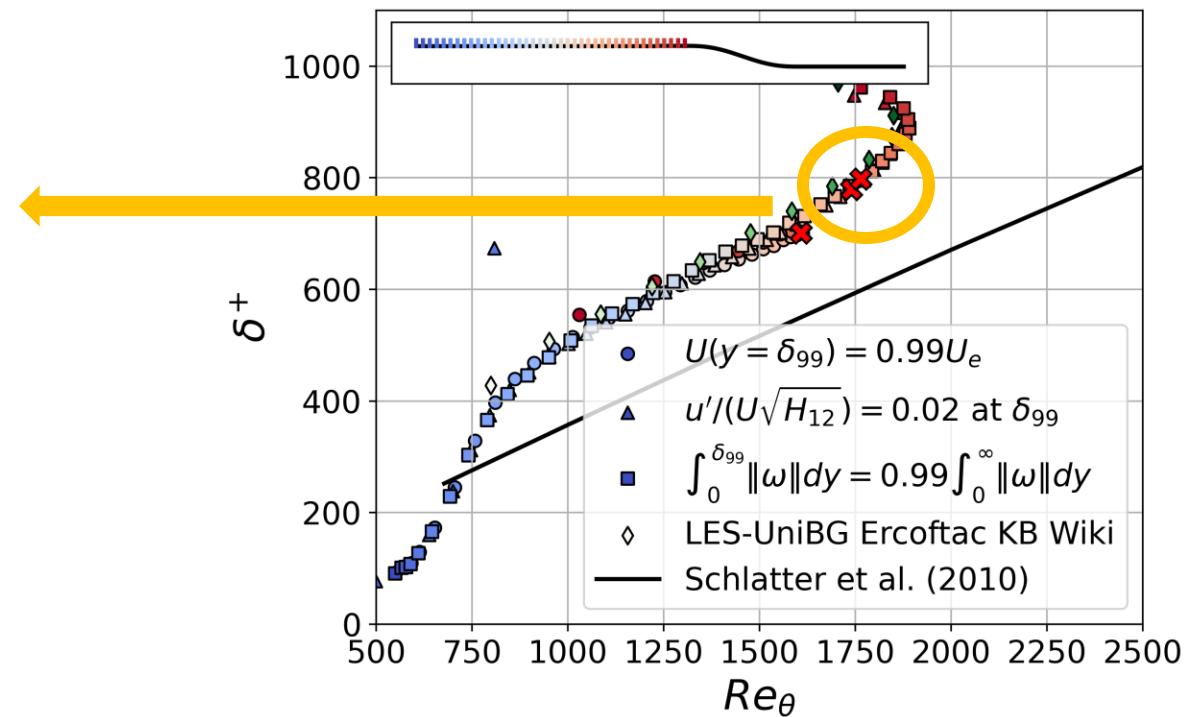
✖ = Reference point

The diagnostic plot and vorticity method produces the correct far-field velocity once the rounded step effect becomes effective.

- Analysis of the flat plate with and without the presence of the rounded step: Re_T vs Re_θ

	$x = -3.5H$	$x = 0$
Re_T	766	947
Re_θ	1711	1747
δ_{99} / H	0.185	0.208

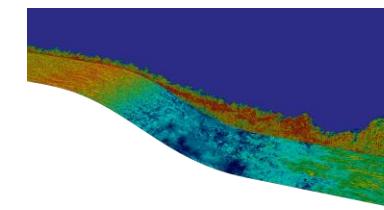
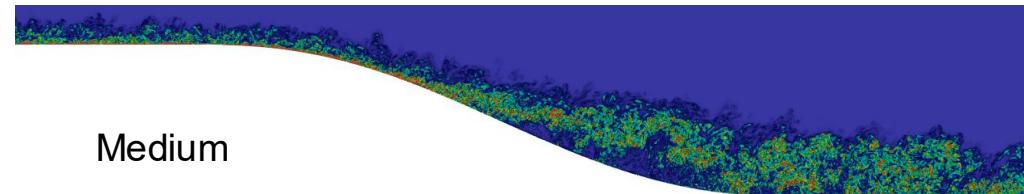
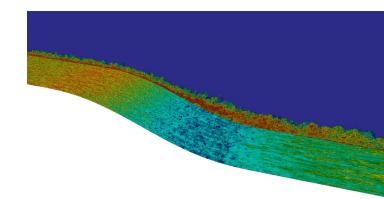
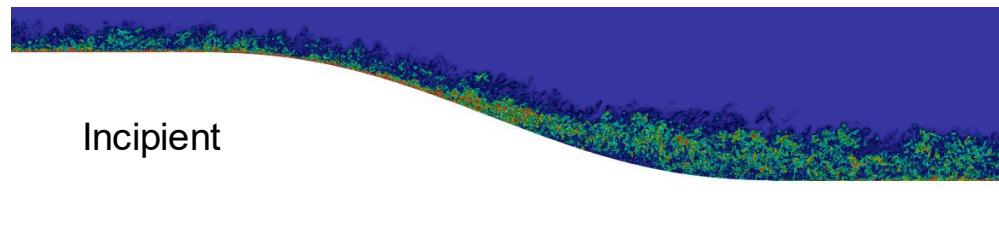
✖ = Reference point



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Conclusions and Perspectives

- **Assessment of the mesh requirements for budget closure on a channel**
- **Ongoing generation of a high-fidelity database for the HiFi-Turb DLR rounded step with adverse pressure gradient ongoing**
- **Analysis of the upstream boundary layer to assess inflow conditions**
- **Current focus on the incipient separation case; extension to medium separation planned**
- **Databases can serve as a reference for turbulence model improvement**



Acknowledgements

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 - **EuroCC Belgium** for awarding this project access to the LUMI supercomputer, owned by the EuroHPC Joint Undertaking, hosted by CSC (Finland) and the LUMI consortium



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