MODELLING
STUDY OF CO₂
SEQUESTRATION
BY MINERAL
WASTE
CARBONATION

Natalia Vidal de la Peña

PhD student from University of Liège

Promoters: Grégoire Léonard

Dominique Toye



INDEX



Introduction



CO₂ capture by mineral carbonation by using construction waste



Coupling between chemical reactions and transfer phenomena



Simulation and experimental results



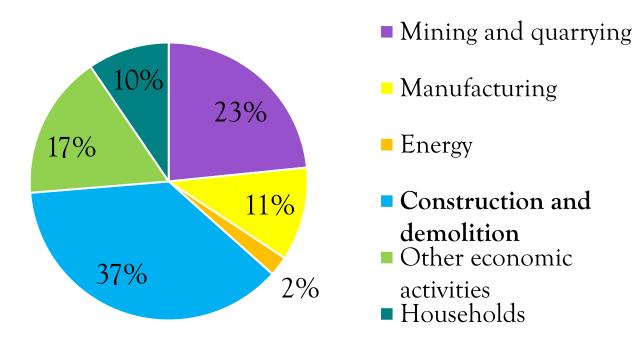
Model validation



Conclusions

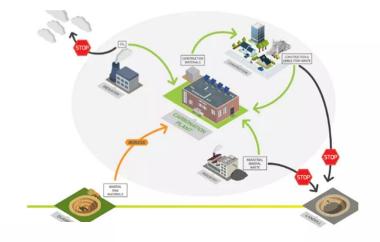
INTRODUCTION

Waste generation by economic activities and households in Europe 2020



Mineral Loop Project

- Transformation of mineral wastesby-products into higher valueadded products
- Circular economy of construction wastes











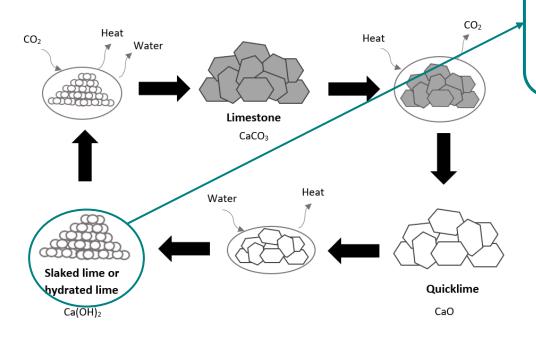






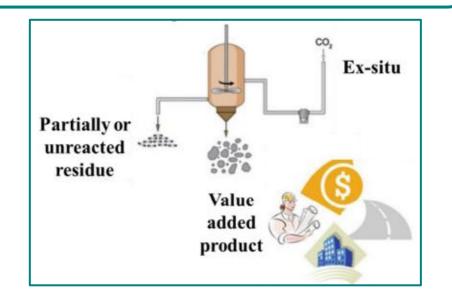
CO₂ CAPTURE BY MINERAL CARBONATION BY USING CONSTRUCTION WASTE

Lime production cycle



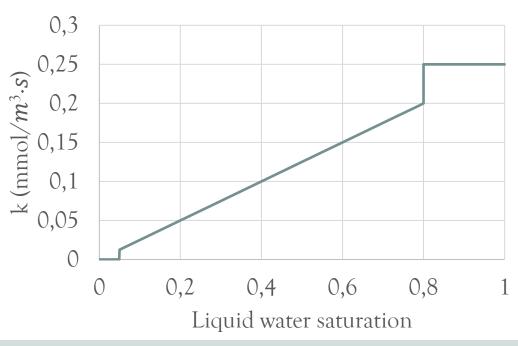
Direct carbonation

Gas-solid carbonation of hydrated lime $Ca(OH)_2+CO_2 => CaCO_3+H_2O$



• Chemical reaction: $Ca(OH)_2$ carbonation = f(liquid water saturation)

Influence of the liquid water saturation into the kinetic constant



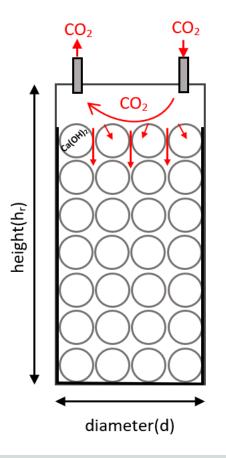
- Physical interactions: CO₂ diffusion
 between the particles and inside the
 particles = f(porosity, liquid water saturation)
 - Diffusion between the particles

$$\mathbb{D} = D_{CO_2,0} \cdot \varepsilon_{bed}^{4/3} \cdot (1 - sl_{bed})^{10/3}$$

Diffusion inside the particles

$$D_{eff} = D_{CO_{2},0} \cdot \varepsilon_{pellet}^{2,7} \cdot \left(1 - sl_{pellet}\right)^{4,2}$$

Where: $D_{CO_2,0}$ is the specific diffusion coefficient of CO_2 (1.6E-5m²/s)



Physical interactions: CO₂ diffusion

between the particles and inside the particles = f(porosity, liquid water saturation) Porosity



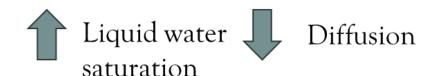


Diffusion between the particles

$$\mathbb{D} = D_{CO_2,0} \cdot \varepsilon_{bed}^{4/3} \cdot (1 - sl_{bed})^{10/3}$$

Diffusion inside the particles

$$D_{eff} = D_{CO_2,0} \cdot \varepsilon_{pellet}^{2,7} \cdot \left(1 - sl_{pellet}\right)^{4,2}$$



Where: $D_{CO_2,0}$ is the specific diffusion coefficient of CO_2 (1.6E-5m²/s)

• Variation of the liquid water saturation during the carbonation process

$$Ca(OH)_2+CO_2 => CaCO_3+H_2O$$
 Initial water-to-solid ratio ($w_{CHt,0}$)

• Variation of pellet porosity during the carbonation process = f(carbonation rate, volume change)

$$\varepsilon_{pellet}(t) = \varepsilon_{0} \cdot \left((1 - \eta) + \frac{\eta \cdot \rho_{CaCO_{3}} \cdot Mm_{Ca(OH)_{2}}}{\rho_{Ca(OH)_{2}} \cdot Mm_{CaCO_{3}}} \right) \quad \text{Volume change}$$

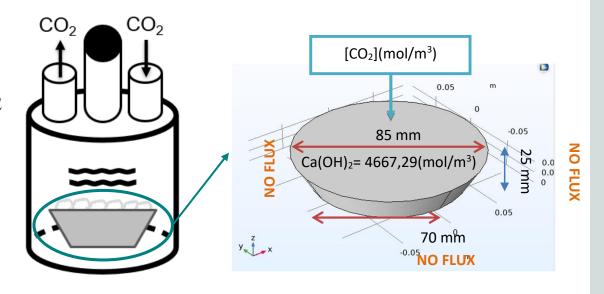
$$Carbonation \ rate \ (\eta) = \frac{[CaCO_{3}]}{[Ca(OH)_{2}]_{t0}}$$

MODEL DESCRIPTION



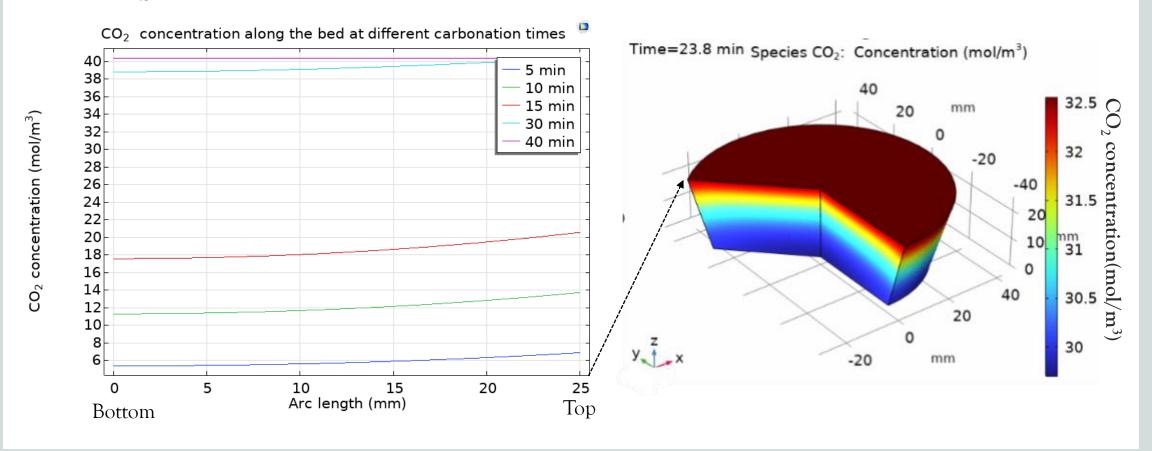
Assumptions

- Bed porosity= 0.69
- Pellet porosity= 0.12
- Temporal evolution of the CO₂ concentration in the enclosure
- CO_2 flow rate= 200 (ml/min)
- Particle radius= 1 mm
- Initial water-to-solid ratio(w_{CH})= 0.2



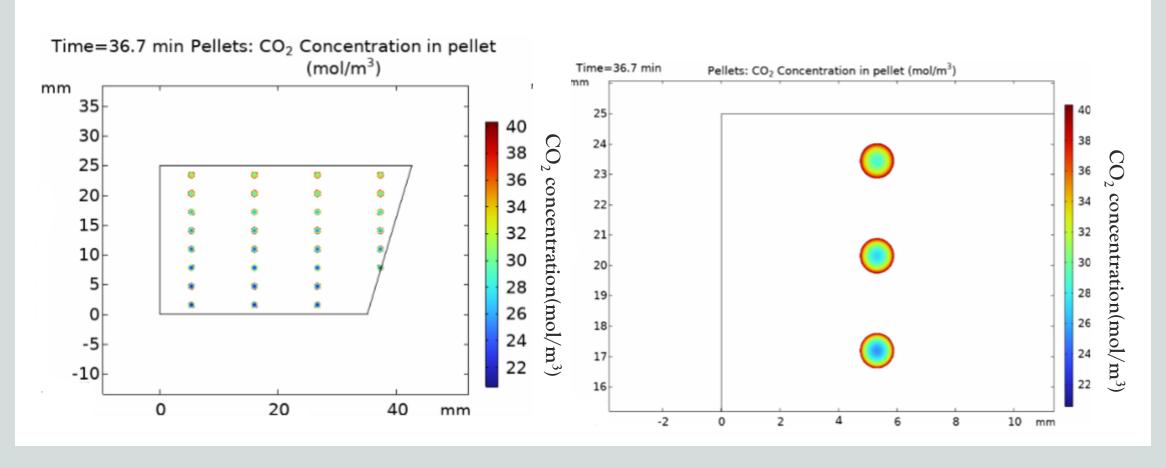
SIMULATION RESULTS

CO₂ concentration profile-Granular bed



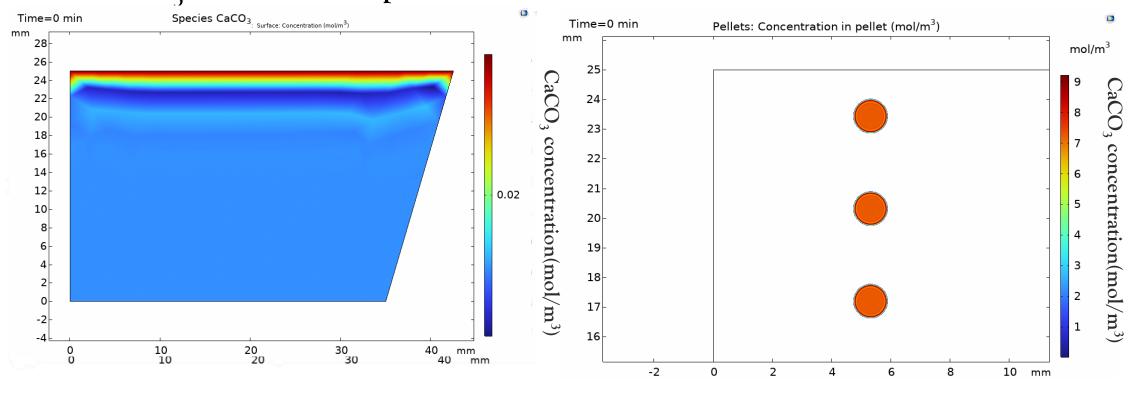
SIMULATION RESULTS

CO₂ concentration profile-Pellets



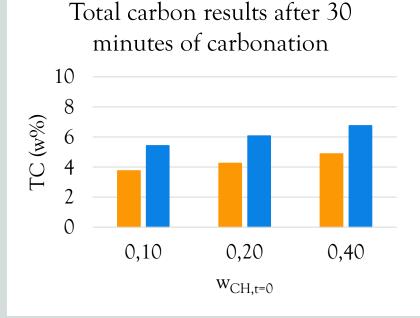
SIMULATION RESULTS

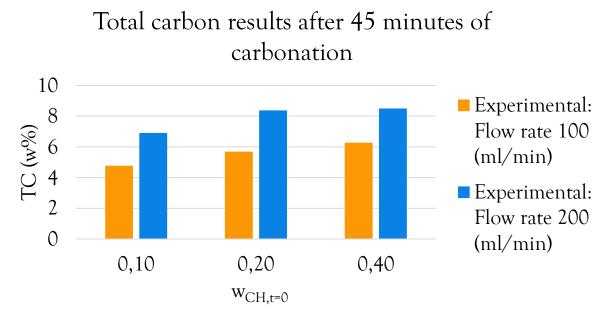




EXPERIMENTAL RESULTS

- Pellet porosity of 10% with a particle diameter of 35.5 μm
- Bed porosity equal to 68% Reaction mostly between the particles
- Parameter evaluated: total carbon (TC)





EXPERIMENTAL RESULTS

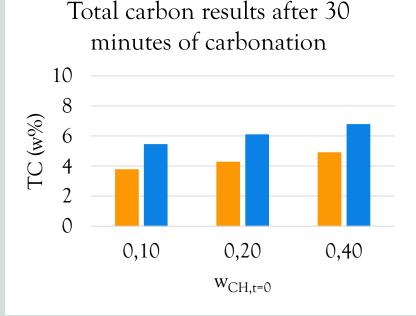
- Influence of Flow rate:

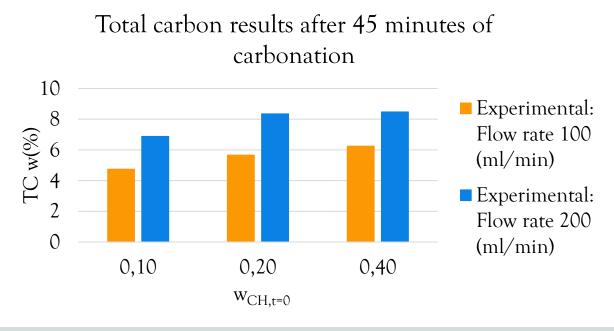
 Flow rate

 Total carbon
- Influence of initial water-to-solid ratio:



Optimal value between 0,2 and 0,4

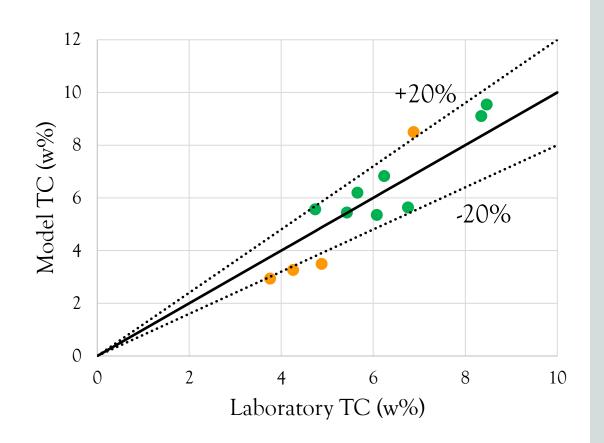




MODEL VALIDATION

- Pellet porosity of 10%
- Particle diameter of 35.5 µm
- Bed porosity of 68%

=>Successful validation



CONCLUSIONS

- Physical parameters influence the system and evolve with time
 - Porosity > Enhances the diffusion of the gas
 - Liquid water saturation \rightarrow Enhances the reaction but slows the diffusion of CO₂
- Process parameters influence the carbonation
 - Carbon dioxide flow rate \rightarrow The higher the CO₂ flow rate, the more carbonation
 - Initial water-to-solid ratio > Optimal value between 0.2 and 0.4
- COMSOL Multiphysics dual-scale model able to represent the carbonation process of hydrated lime



Contribution to the circular economy of the construction sector





Application of the model to predict the behavior of more complex materials, such as recycled concrete aggregates



Optimization of operational conditions on a larger scale



Variation of the liquid water saturation during the carbonation process

$$sl_{bed,pellet} = \frac{[H_2O]\left(\frac{mol}{m^3}\right) \cdot MM_{H_2O}\left(\frac{g}{mol}\right)}{\rho_{H_2O} \cdot \varepsilon_{bed,pellet}}$$

Variation of pellet porosity during the carbonation process

$$\varepsilon_{pellet}(t) = \varepsilon_{0} \cdot \left((1 - \eta) + \frac{\eta \cdot \rho_{CaCO_{3}} \cdot Mm_{Ca(OH)_{2}}}{\rho_{Ca(OH)_{2}} \cdot Mm_{CaCO_{3}}} \right)$$

$$Carbonation\ rate\ (\eta) = \frac{[CaCO_{3}]}{[Ca(OH)_{2}]_{t0}}$$

• Variation of bed porosity during the carbonation process

$$\varepsilon_{bed}(t) = \varepsilon_0 + 4 \cdot 10^{-6} \ (m^3/mol) * ([Ca(OH)_2]_{t,0} [Ca(OH)_2](t))$$