



Intelsig



Room-acoustics predictions using a diffusion process

-
A state of the art

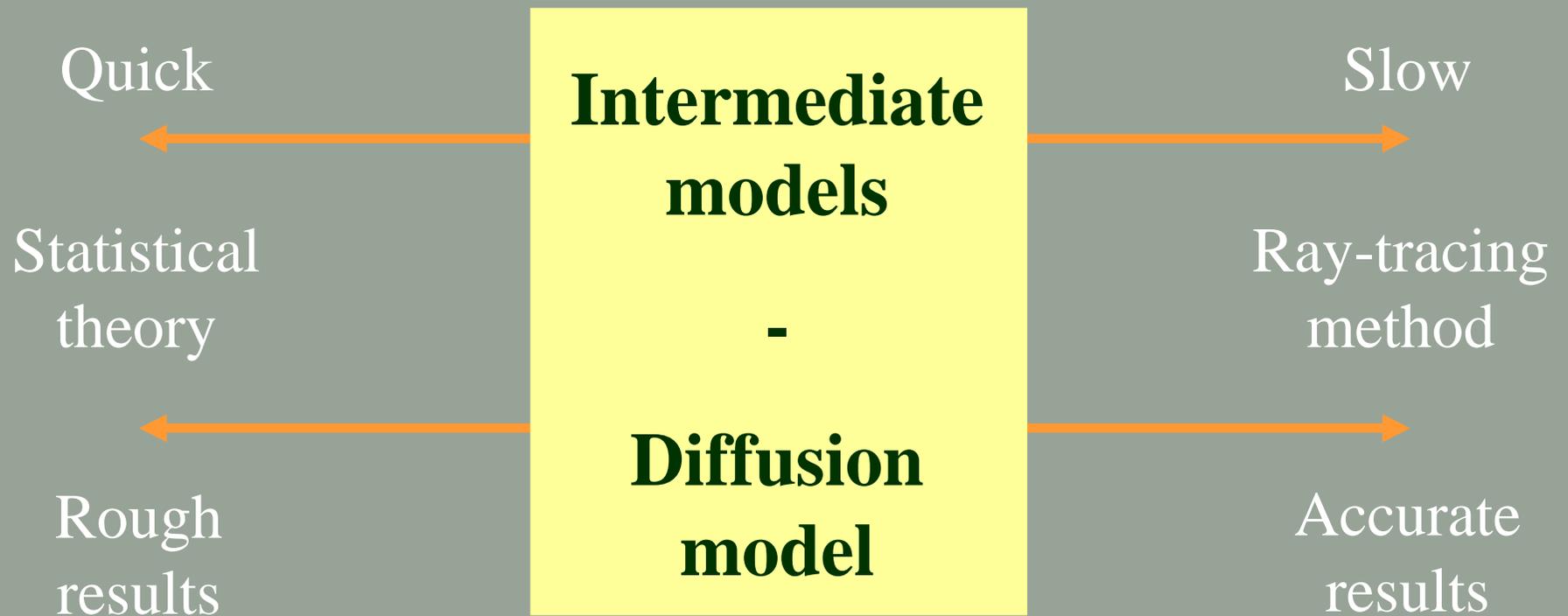
Alexis Billon

Laboratory of acoustics, University of Liège

ABAV Meeting
21 may 2008 - ULg



- Numerical tools are now widely used for buildings projects
- Most popular methods:
 - Ray-tracing method;
 - Statistical theory.



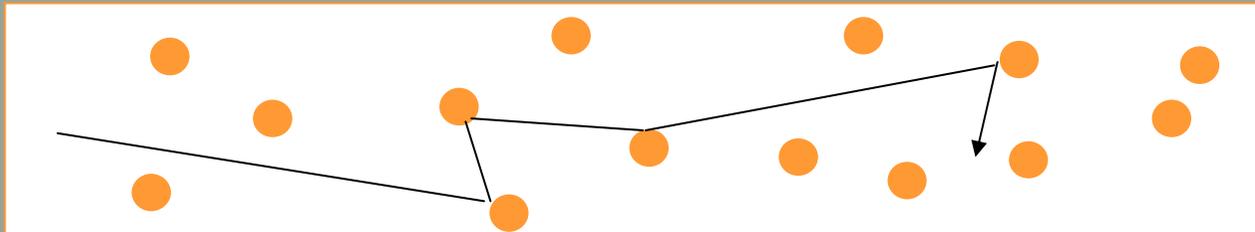
- Basic equations
- Mixed specular/diffuse reflections
- Numerical implementation
- Atmospheric attenuation
- Presence of fitting objects
- Rooms coupled through apertures
- Rooms coupled through partition walls
- Conclusions
- Application to a virtual factory

1. Basic equations

- Diffusion equation

$$\frac{\partial w(\mathbf{r}, t)}{\partial t} - D \nabla^2 w(\mathbf{r}, t) = P(\mathbf{r}, t)$$

- Propagation of sound particles in a scattering medium



- Diffusion constant

$$D = \frac{\lambda c}{3}$$

w acoustic energy density
 λ room mean free path ($4V/S$)
 c sound speed

Morse and Feshbach (1953)
 Picaut *et al.*, *Acustica* **83** (1997)
 Valeau *et al.*, *JASA* **119** (2006)

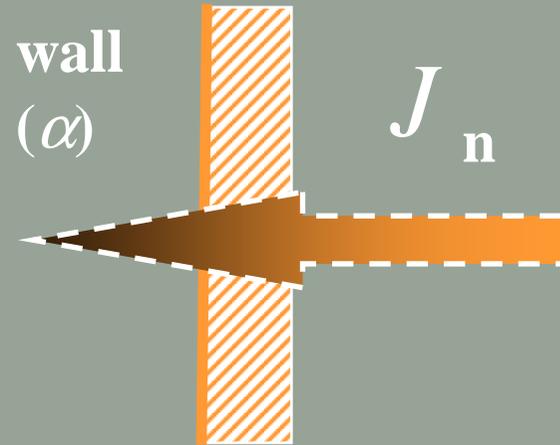
Ollendorff, *Acustica* **21** (1969)
 Picaut *et al.*, *Applied Acoustics* **56** (1999)

2. Boundary conditions

- Absorption at walls

$$J_n = -D \frac{\partial w}{\partial \mathbf{n}} = h w$$

h exchange coefficient
 \mathbf{n} wall normal



- Expressions of the exchange coefficient

$$h = \frac{c\alpha}{4}$$

Picaut *et al.*, Applied Acoustics **56** (1999)

$$h = -\frac{c \ln(1-\alpha)}{4}$$

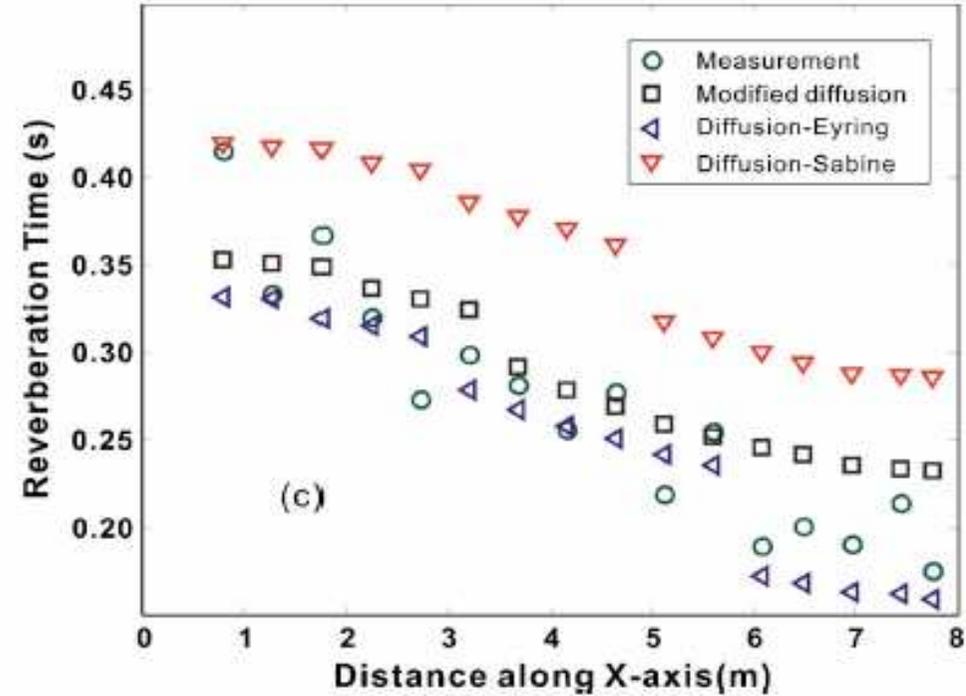
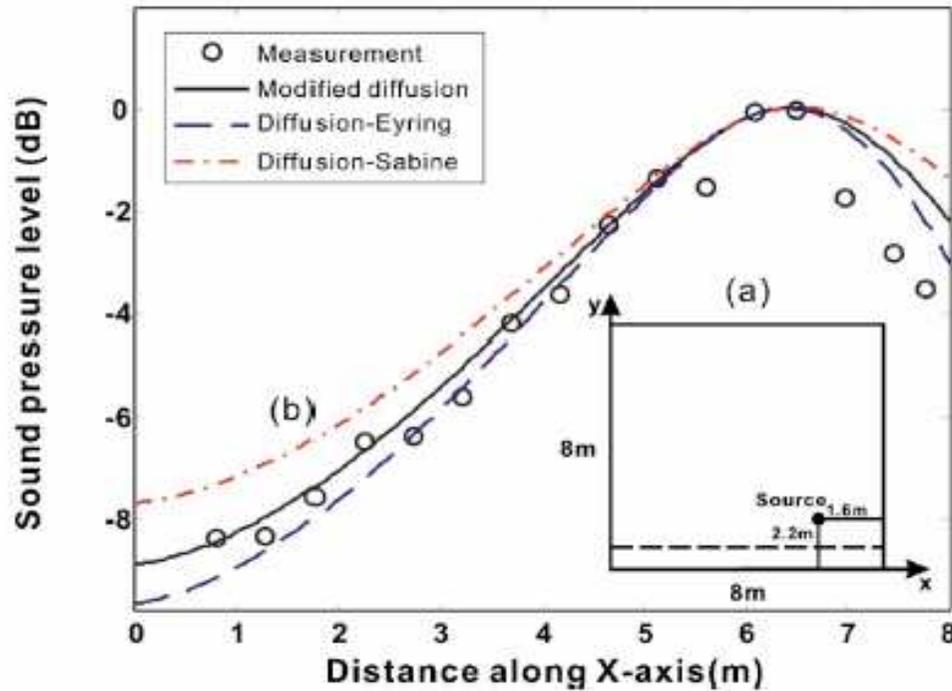
Billon *et al.*, Applied Acoustics **69** (2008)

$$h = -\frac{c\alpha}{2(2-\alpha)}$$

Jing and Xiang, JASA **123** (2008)

2. Boundary conditions

Absorption at walls



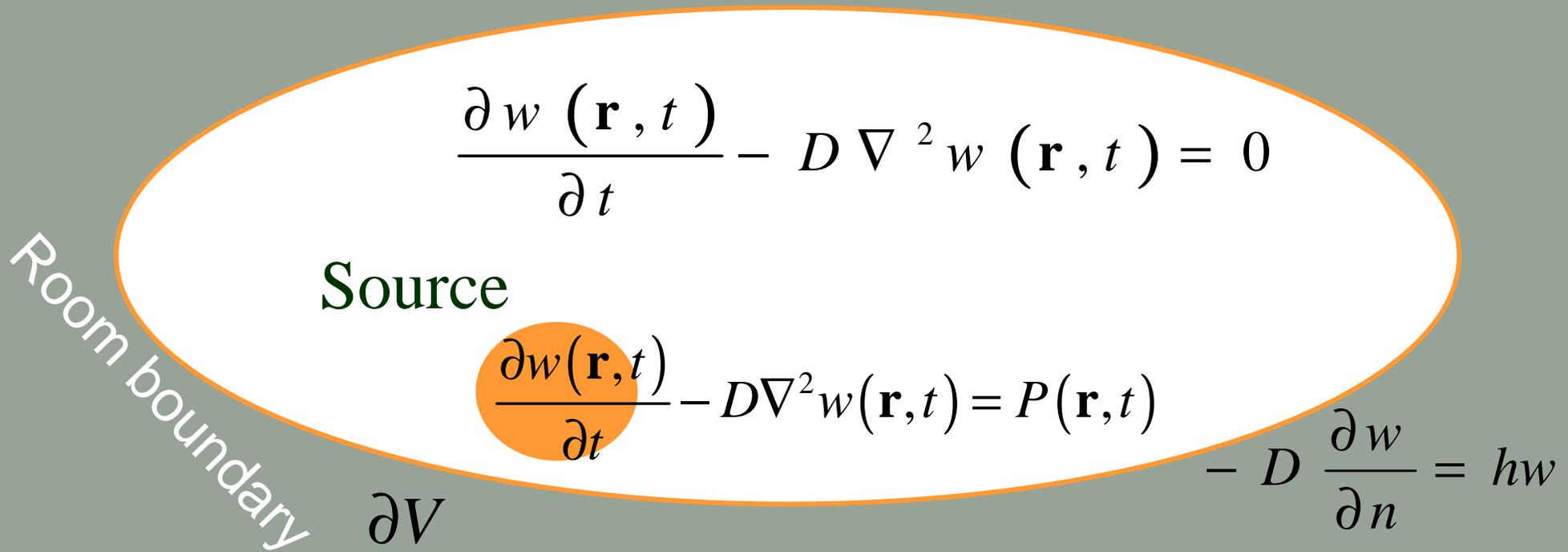
Comparison of different boundary conditions with experiments (Jing and Xiang, 2008).

Picaut *et al.*, Applied Acoustics 56 (1999)

Billon *et al.*, Applied Acoustics 69 (2008)

Jing and Xiang, JASA 123 (2008)

3. Numerical implementation



Simulations characteristics:

- Finite Element Model (FEM) solver (*Femlab*);
- Unstructured mesh;
- Stationary response  Sound Pressure Level = 10 seconds
- Impulse response  Sound decay < 1minute

4. Mixed specular/diffuse reflections

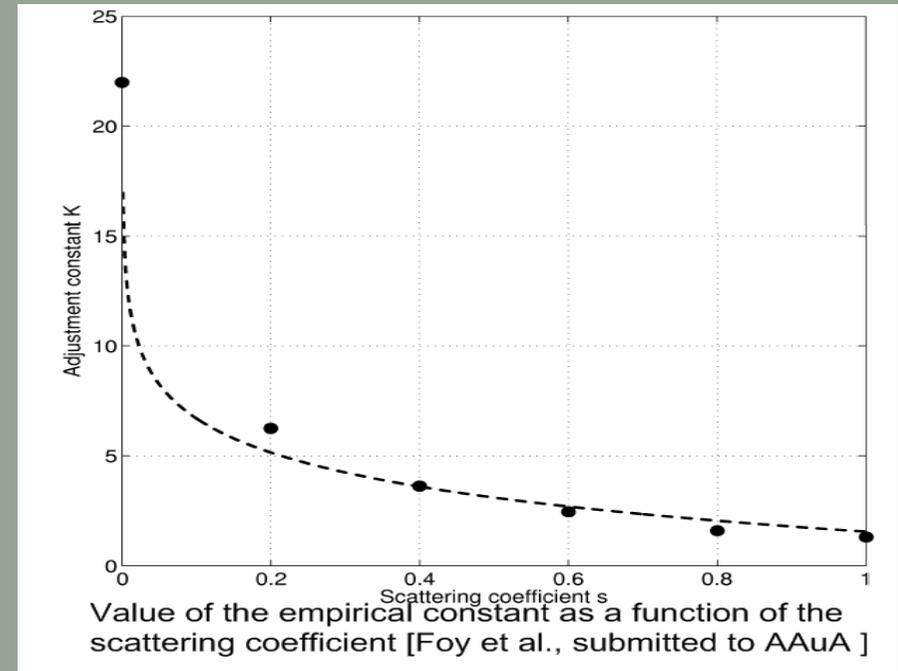
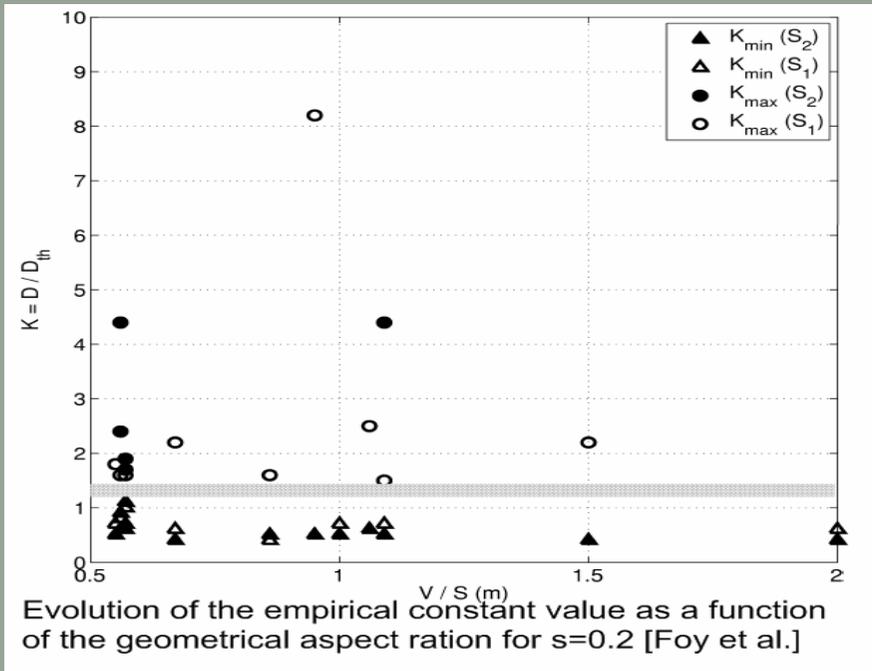
Empirical diffusion constant

Valeau *et al.*, AAuA 93 (2007)

$$D(s) = k(s) \times D_{theoretical}$$

Generalization

Foy *et al.*, submitted to AAuA



The empirical model gives good predictions in terms of SPL, but not in terms of sound decay.

4. Mixed specular/diffuse reflections

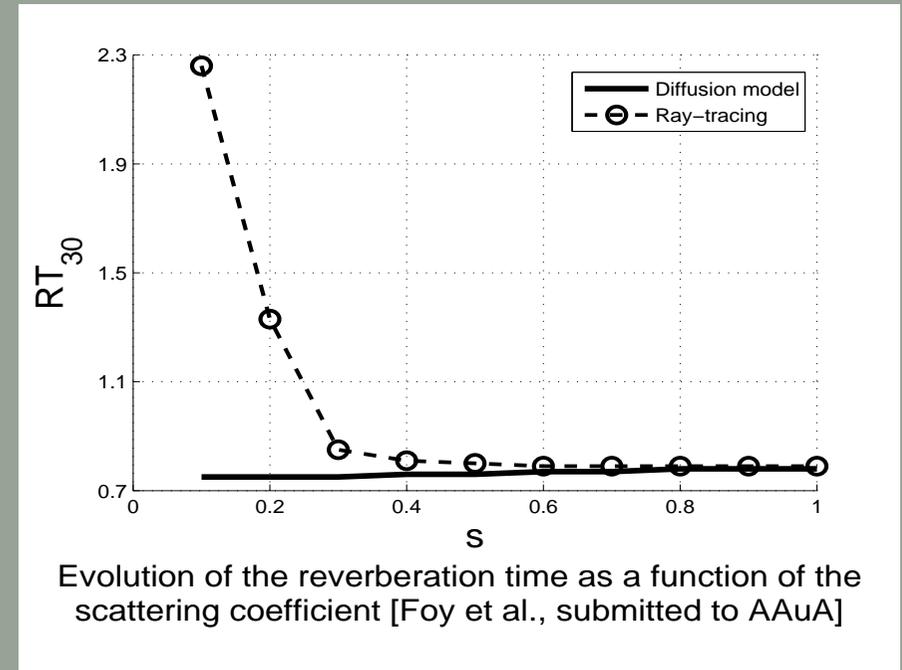
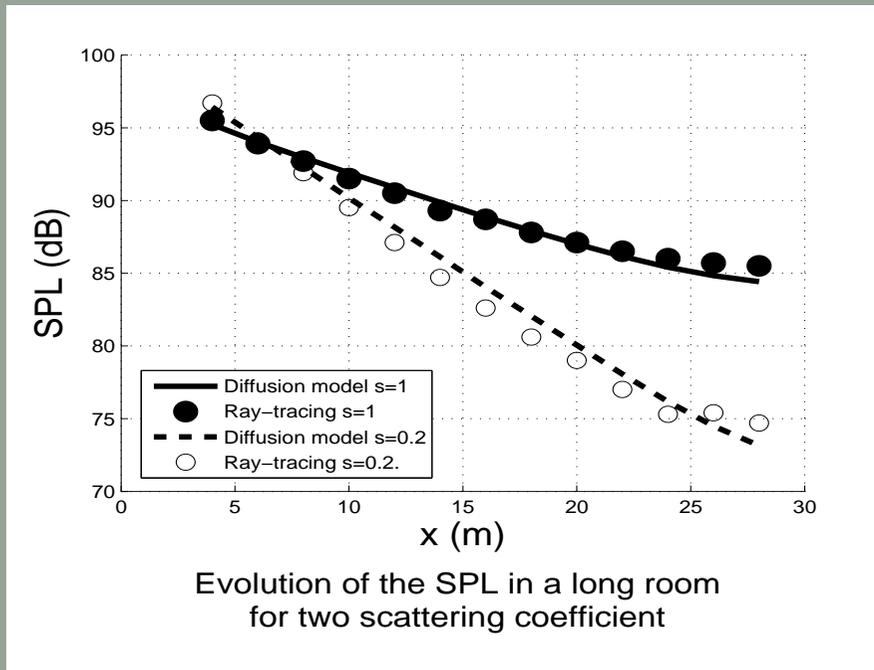
Empirical diffusion constant

Valeau *et al.*, AAcA 93 (2007)

$$D(s) = k(s) \times D_{theoretical}$$

Generalization

Foy *et al.*, submitted to AAcA



The empirical model gives good predictions in terms of SPL, but not in terms of sound decay.

5. Atmospheric attenuation

- Diffusion constant

Billon *et al.*, JASA 123 (2008)

$$D' = D \times \frac{1}{1 + m \lambda}$$

- Absorption term

$$\frac{\partial w(\mathbf{r}, t)}{\partial t} - D' \nabla^2 w(\mathbf{r}, t) + mcw(\mathbf{r}, t) = P(\mathbf{r}, t)$$

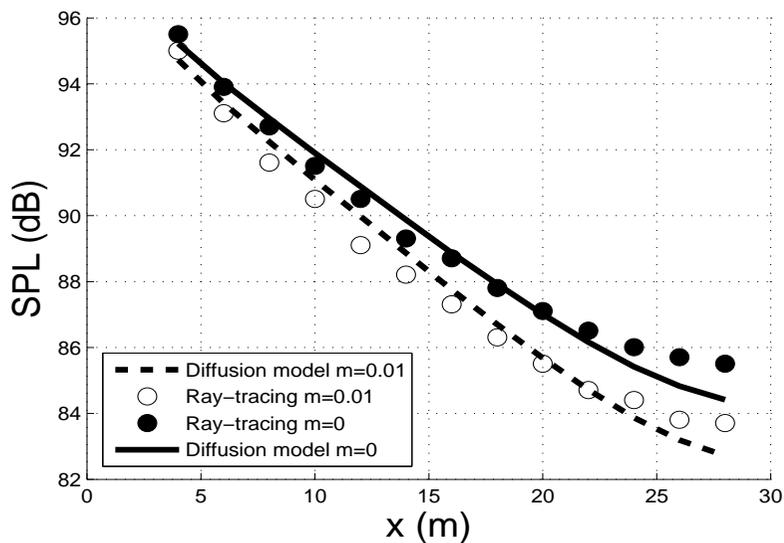
5. Atmospheric attenuation

■ Diffusion constant

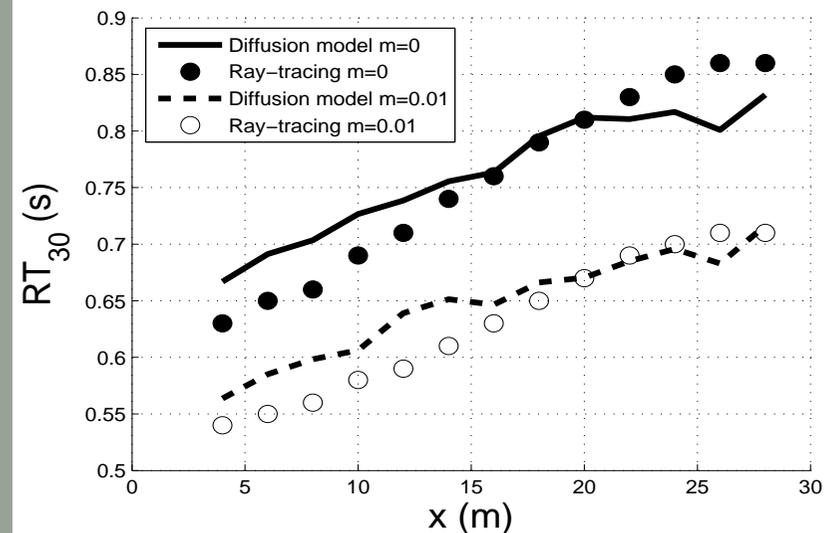
Billon *et al.*, JASA 123 (2008)

$$D' = D \times \frac{1}{1 + m \lambda}$$

■ Absorption term



Evolution of the sound pressure level in a long room with and without atmospheric attenuation $s=0.2$

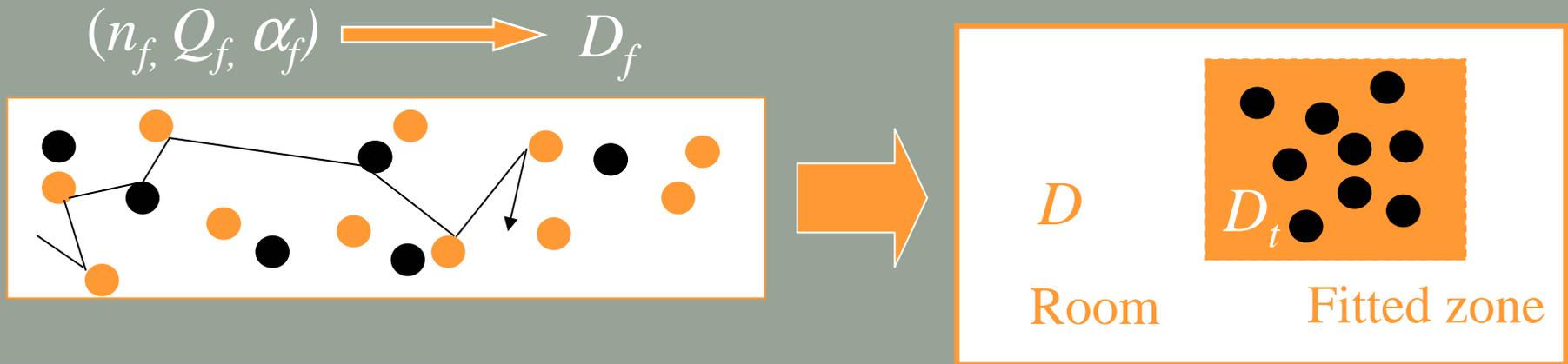


Evolution of the reverberation time in a long with and without atmospheric attenuation $s=1$

The diffusion model gives good predictions both in terms of SPL (for every s) and in terms of sound decay (for $s=1$).

6. Presence of fitting objects

- Diffusion constant



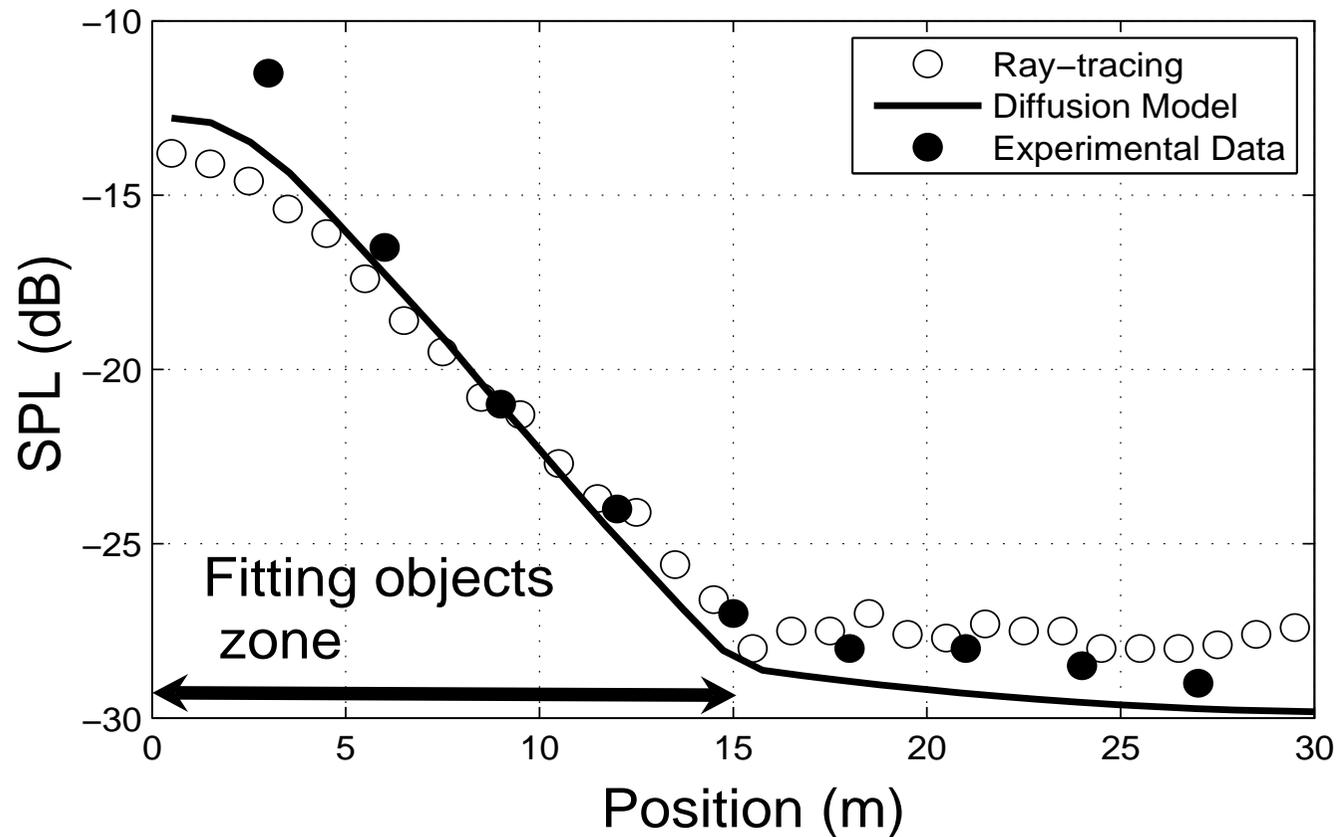
$$D_t = \frac{D_f D}{D_f + D}$$

V. Valeau et al., AAuA 93 (2007)

$$\frac{\partial w(\mathbf{r}, t)}{\partial t} - D_t \Delta w(\mathbf{r}, t) + \frac{c \alpha_f}{\lambda_f} w(\mathbf{r}, t) = P(\mathbf{r}, t)$$

6. Presence of fitting objects

- Diffusion constant



Evolution of the SPL in a fitted room
[Valeau et al. 2007]

7. Rooms coupled through apertures



Billon *et al.*, JASA 120 (2006)

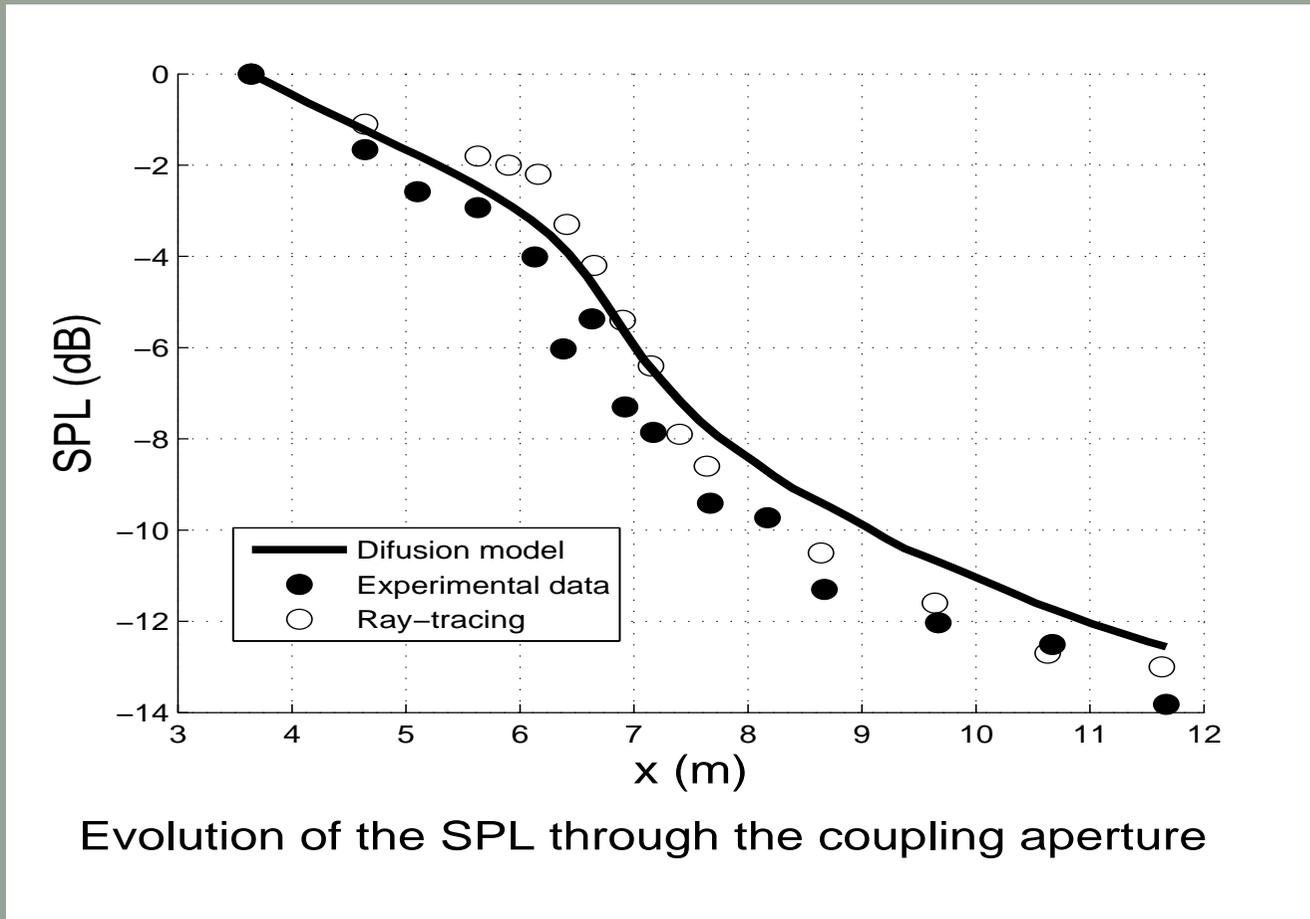
$$\frac{\partial w(\mathbf{r}, t)}{\partial t} - D_1 \nabla^2 w(\mathbf{r}, t) = 0$$

Source

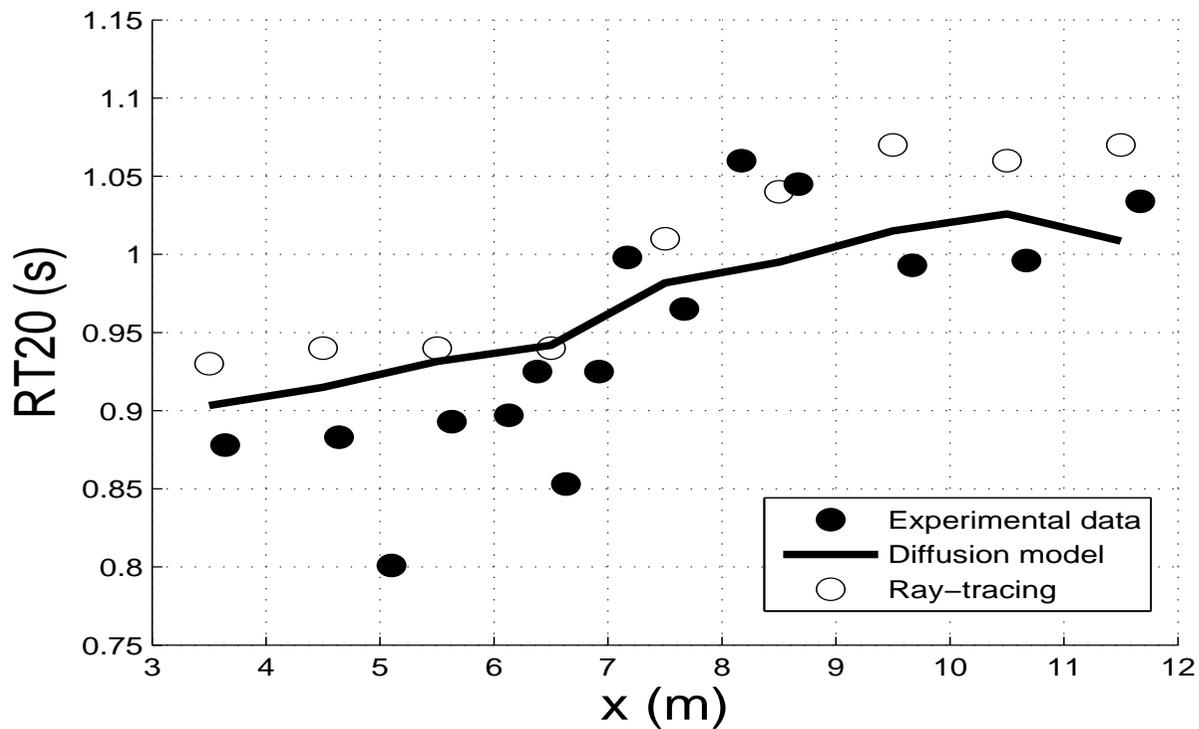
$$\frac{\partial w(\mathbf{r}, t)}{\partial t} - D_1 \nabla^2 w(\mathbf{r}, t) = P(\mathbf{r}, t)$$

$$\frac{\partial w(\mathbf{r}, t)}{\partial t} - D_2 \nabla^2 w(\mathbf{r}, t) = 0$$

8. Rooms coupled through apertures

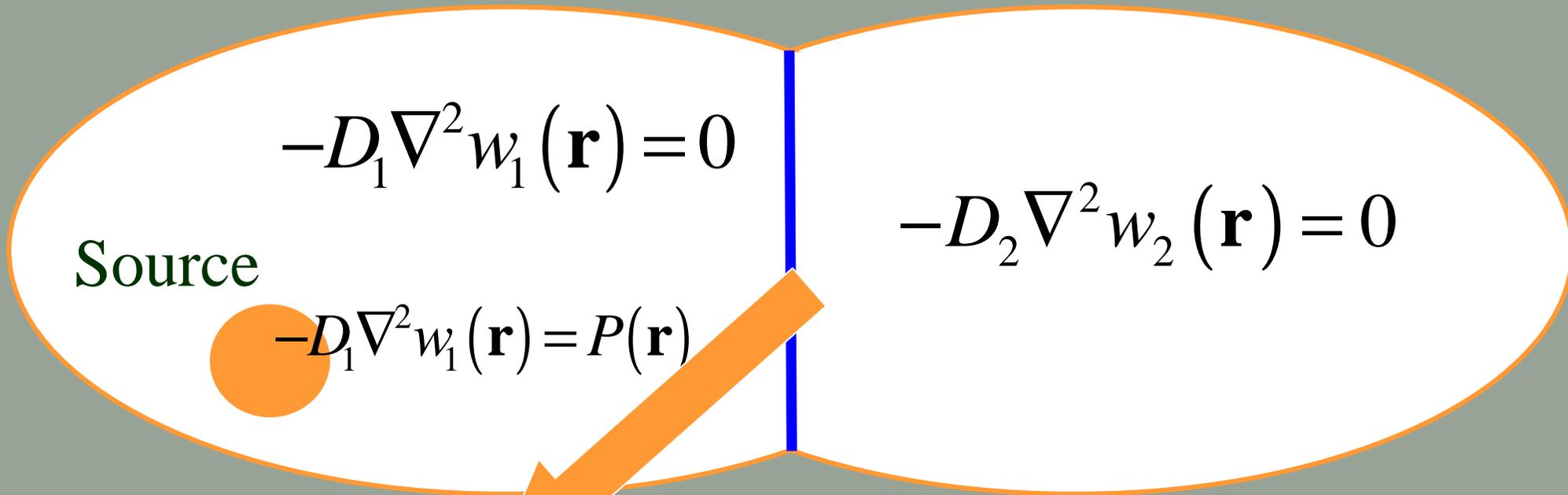


8. Rooms coupled through apertures



Evolution of the reverberation time through the coupling aperture

8. Rooms coupled through partition walls



■ Coupling equations

Side V_1

$$D_1 \frac{\partial w_1(\mathbf{r})}{\partial \mathbf{n}_1} + h_1 w_1(\mathbf{r}) = \frac{\tau c}{4} w_2$$

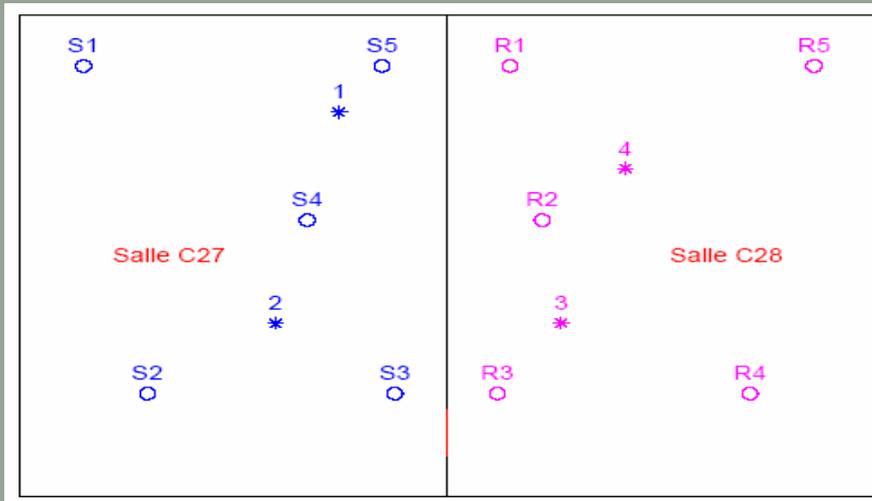
τ Transmission coefficient

Side V_2

$$D_2 \frac{\partial w_2(\mathbf{r})}{\partial \mathbf{n}_2} + h_2 w_2(\mathbf{r}) = \frac{\tau c}{4} w_1$$

Billon *et al.*, JASA 123 (2008)

8. Rooms coupled through partition walls

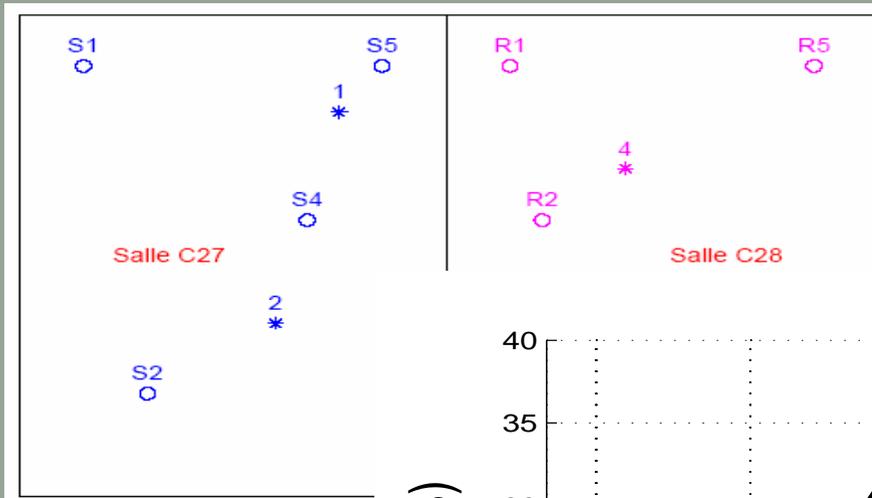


Norms 3382 and 140-4:

*: Sound source

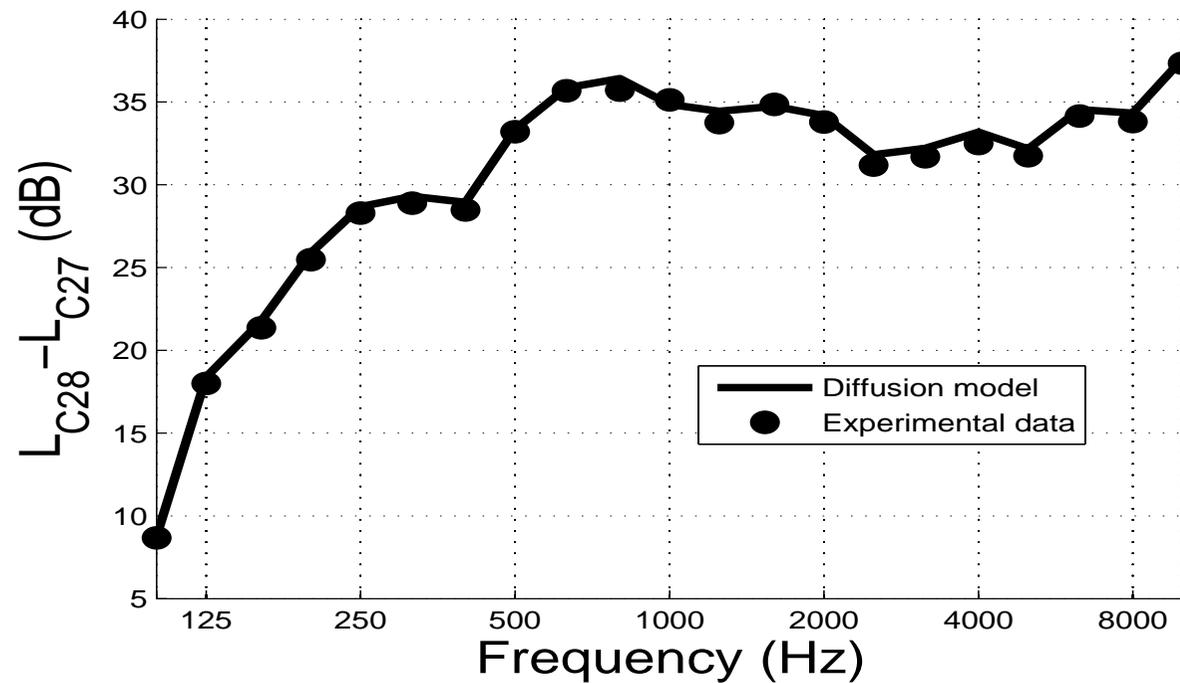
o: Microphones

8. Rooms coupled through partition walls



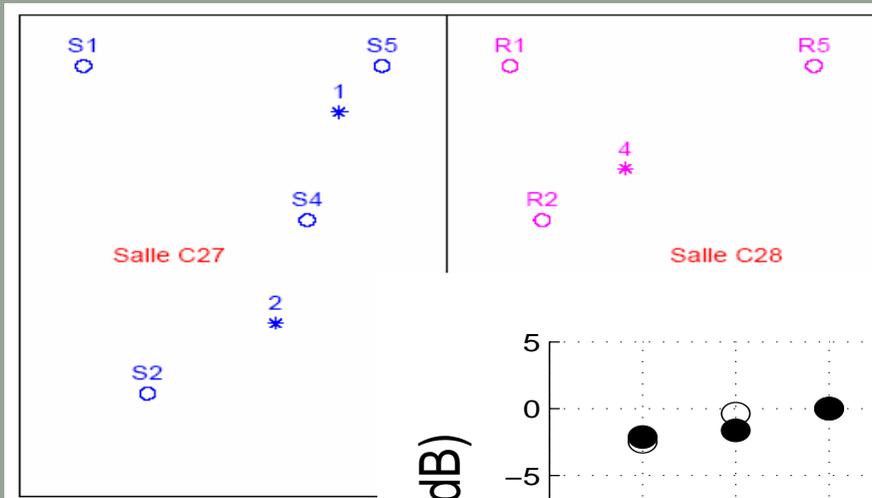
Norms 3382 and 140-4:

*: Sound source



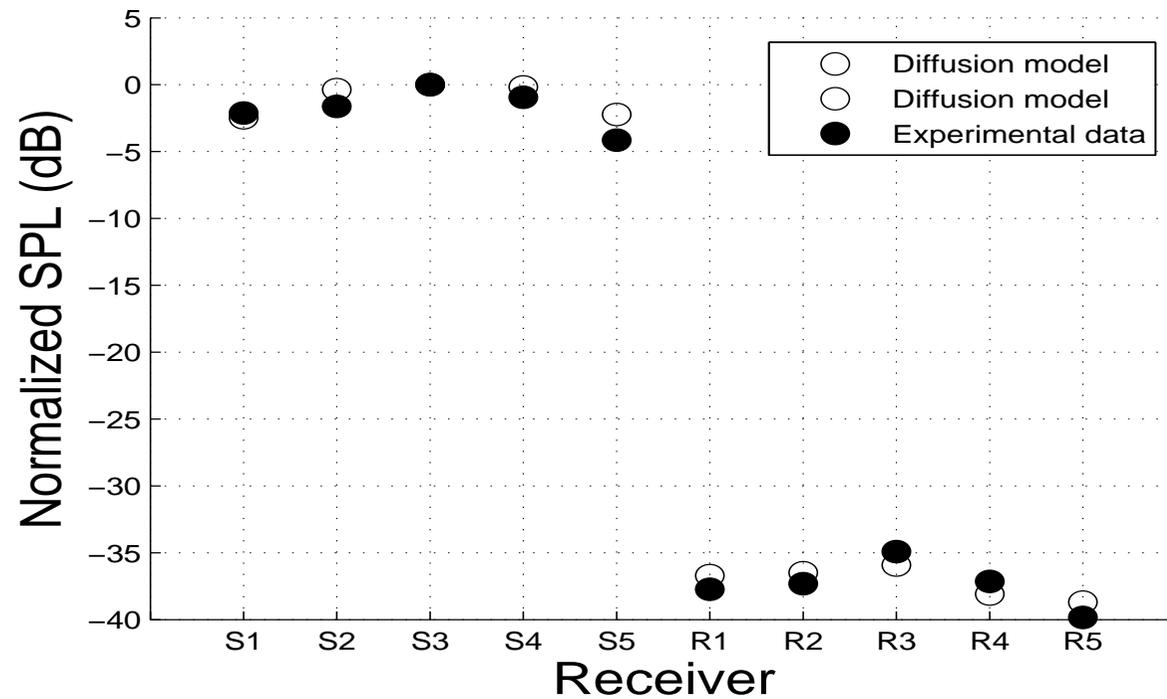
Sound level difference between the room as a function of the frequency

8. Rooms coupled through partition walls



Norms 3382 and 140-4:

*: Sound source



Normalized sound pressure level at the microphones locations

Conclusions

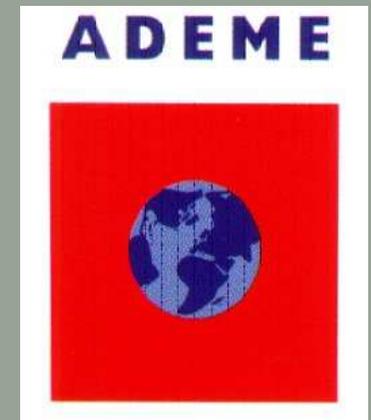
- Quick and flexible approach
- Handle main acoustic phenomena
- Adapted in networks of rooms

Future works

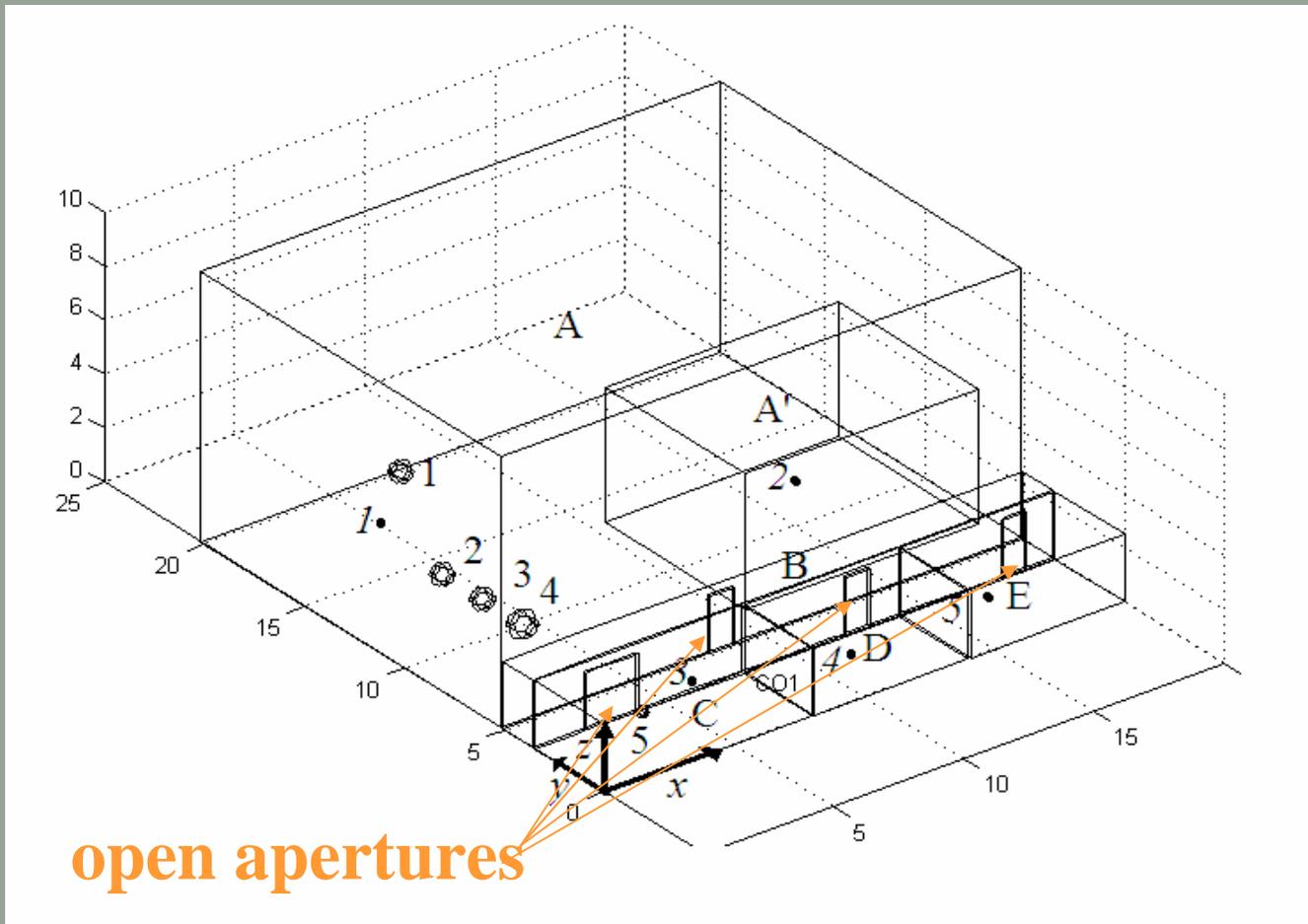
- Specular reflections in the sound decay
- Coupling with urban diffusion model

Acknowledgements:

The author would like to thank the ADEME (french agency for environmental studies) for supporting part of this work.



■ Industrial hall coupled with offices



Hall A :

- 20m x 25m x 10m
- $\alpha=0.03$
- source 1: 120dB

Fitted zone A' :

- $\alpha=0.3$
- $\lambda_f=0.25\text{m}$

Offices D, E:

- $\alpha=0.06$

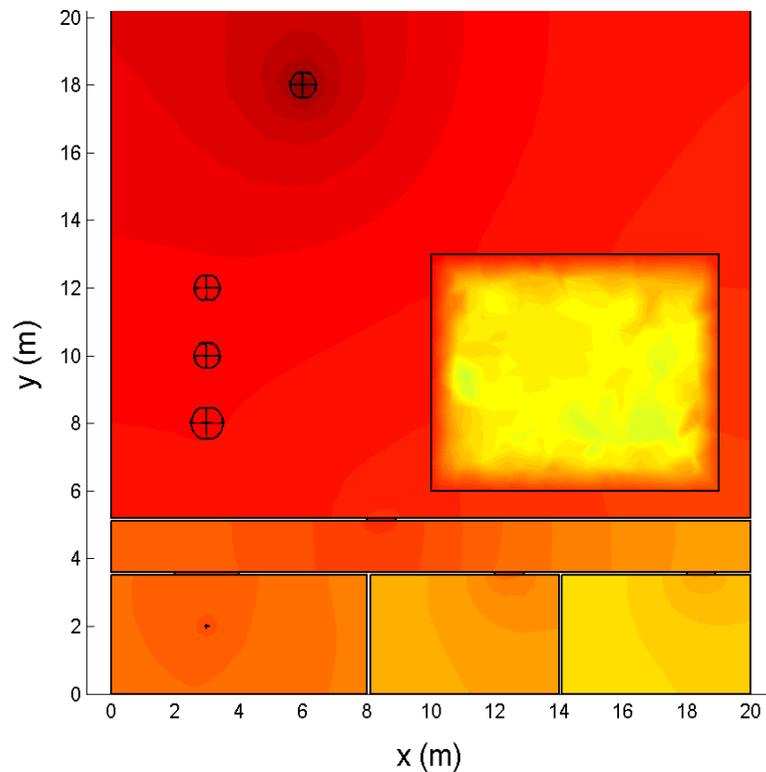
Workshop C:

- $\alpha=0.03$

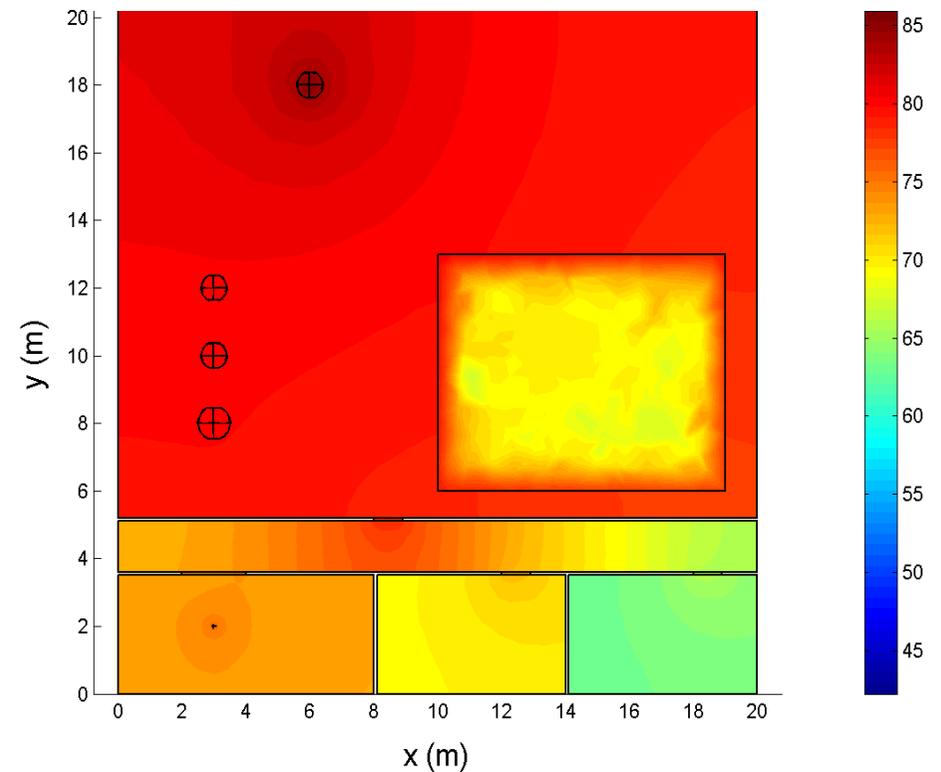
Corridor B:

- $\alpha = 0.06$ or 0.6

- Effect of the acoustic treatment



Before



After