

# Designing Custom Carnot Batteries to Suit Your Exigencies: A Near-Optimal Approach

A. Laterre<sup>1,2</sup>, D. Coppitters<sup>1</sup>, V. Lemort<sup>2</sup>, F. Contino<sup>1</sup>

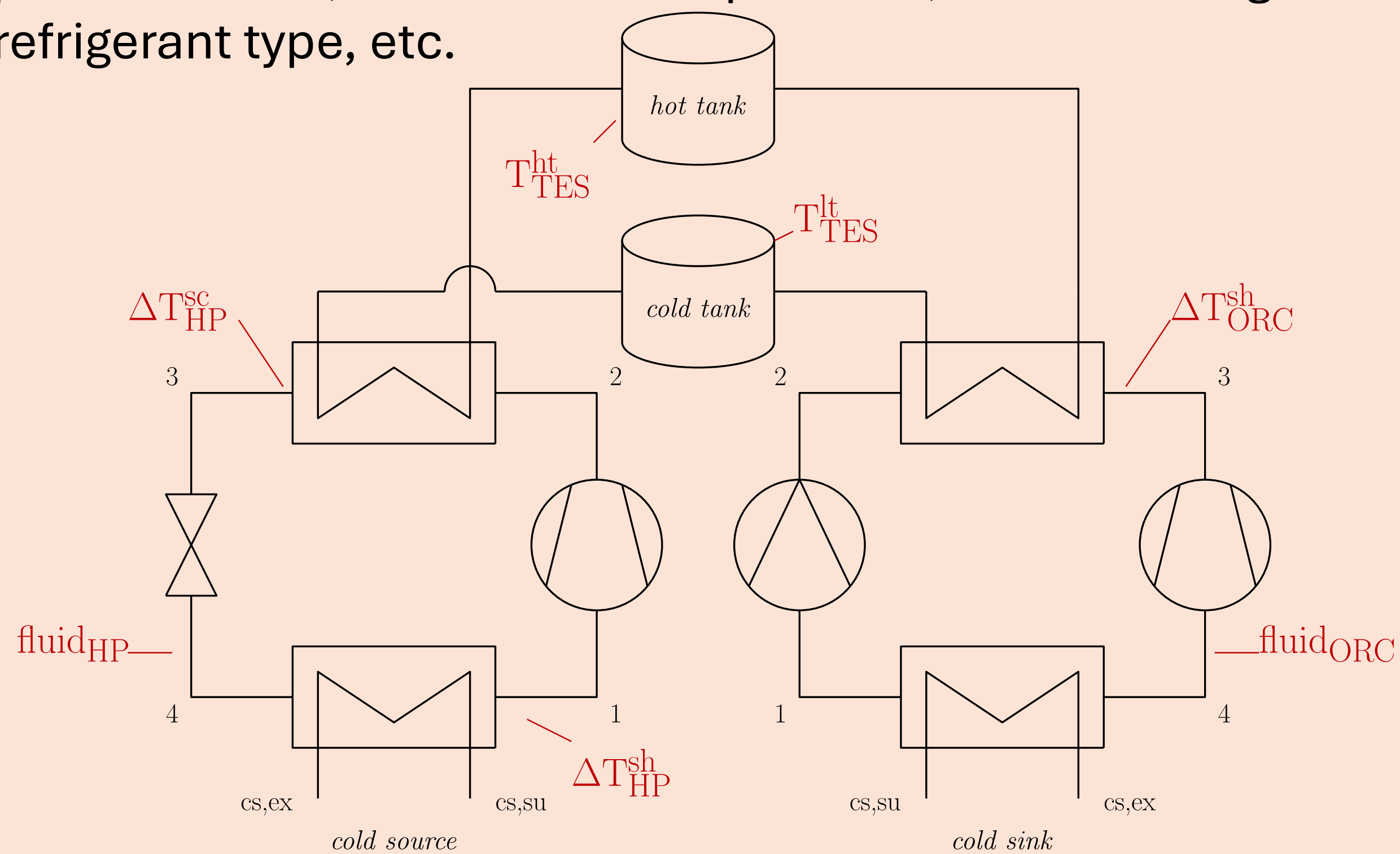
<sup>1</sup>UCLouvain and <sup>2</sup>ULiège (antoine.laterre@uclouvain.be)

## Objective

Conducting near-optimal analyses to generate multiple alternatives for the thermodynamic design of Carnot batteries, tailored to meet manufacturers technological preferences.

## The Optimum is Not Enough

- Different thermodynamic designs of Carnot batteries can achieve **similar performance** (efficiency  $\eta_{CB}^{elec}$ , density  $\rho_{CB}^{elec}$ ).
- Yet, they involve **technological trade-offs**, such as storage pressurisation, number of compressors, heat exchangers size, refrigerant type, etc.



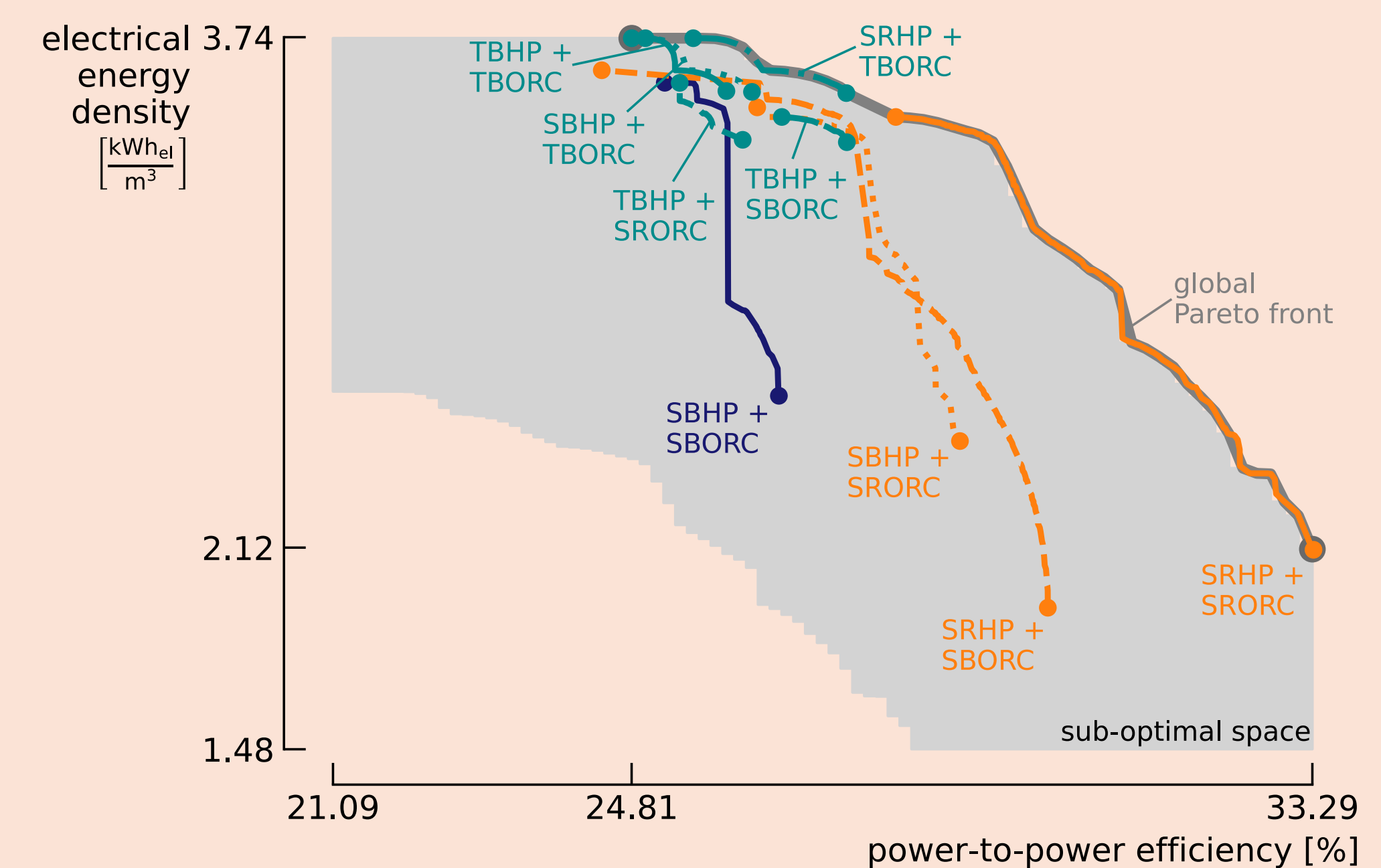
- These factors affect techno-economic outcomes and depend on **manufacturers strategic choices**, based on, e.g., supply chain, experience, service lifetime, maintenance needs, business model and risk tolerance.
- **Near-optimal exploration** can offer design alternatives to help manufacturers select the **best fit for their needs**.

## Identifying the Sub-Optimal Space

- Nine Carnot battery types are optimised with **NSGA-II** to **maximise  $\eta_{CB}^{elec}$  and  $\rho_{CB}^{elec}$** .

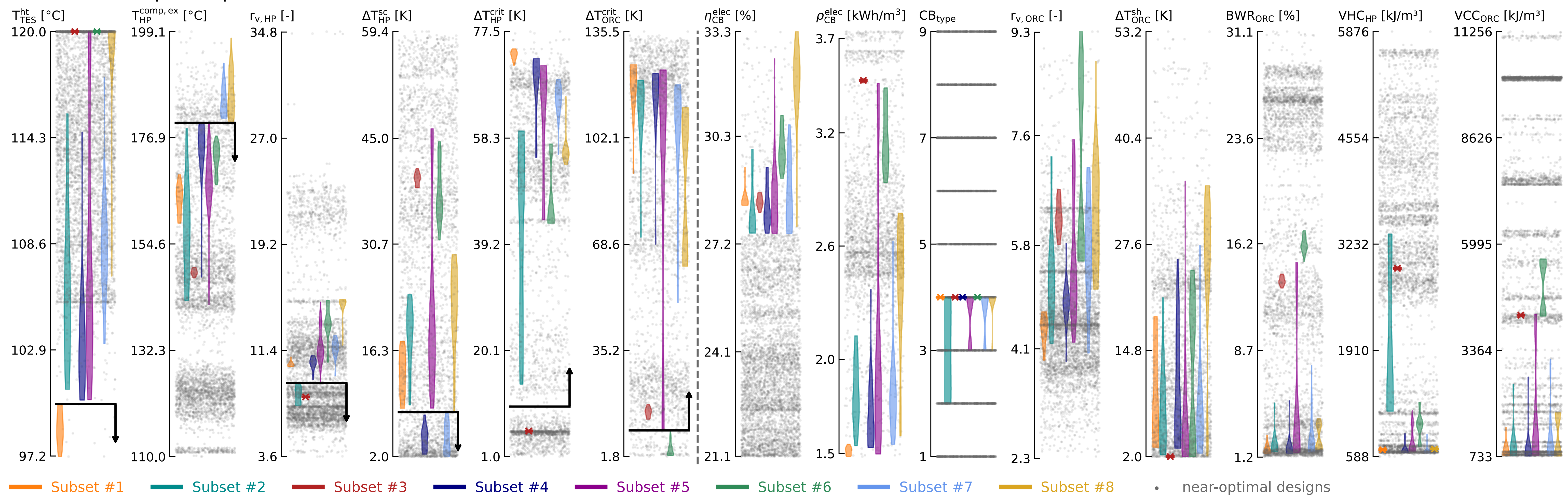
Organic Rankine Cycle	Heat Pump				
	Subcrit.	Subcritical		Transcritical	
		Basic	Recuperated	Basic	Basic
Recup.	#1: SBHP + SBORC	#3: SRHP + SBORC	#6: TBHP + SBORC		
Transcrit.	#2: SBHP + SRORC	#4: SRHP + SRORC	#8: TBHP + SRORC		
	Basic	#5: SBHP + TBORC	#7: SRHP + TBORC	#9: TBHP + TBORC	

- Resulting fronts are combined to create a **global Pareto front**.



- The **sub-optimal space** is then defined, allowing for near-optimal designs with maximum **sub-optimality coefficients of 15% for  $\eta_{CB}^{elec}$  and 30% for  $\rho_{CB}^{elec}$** .

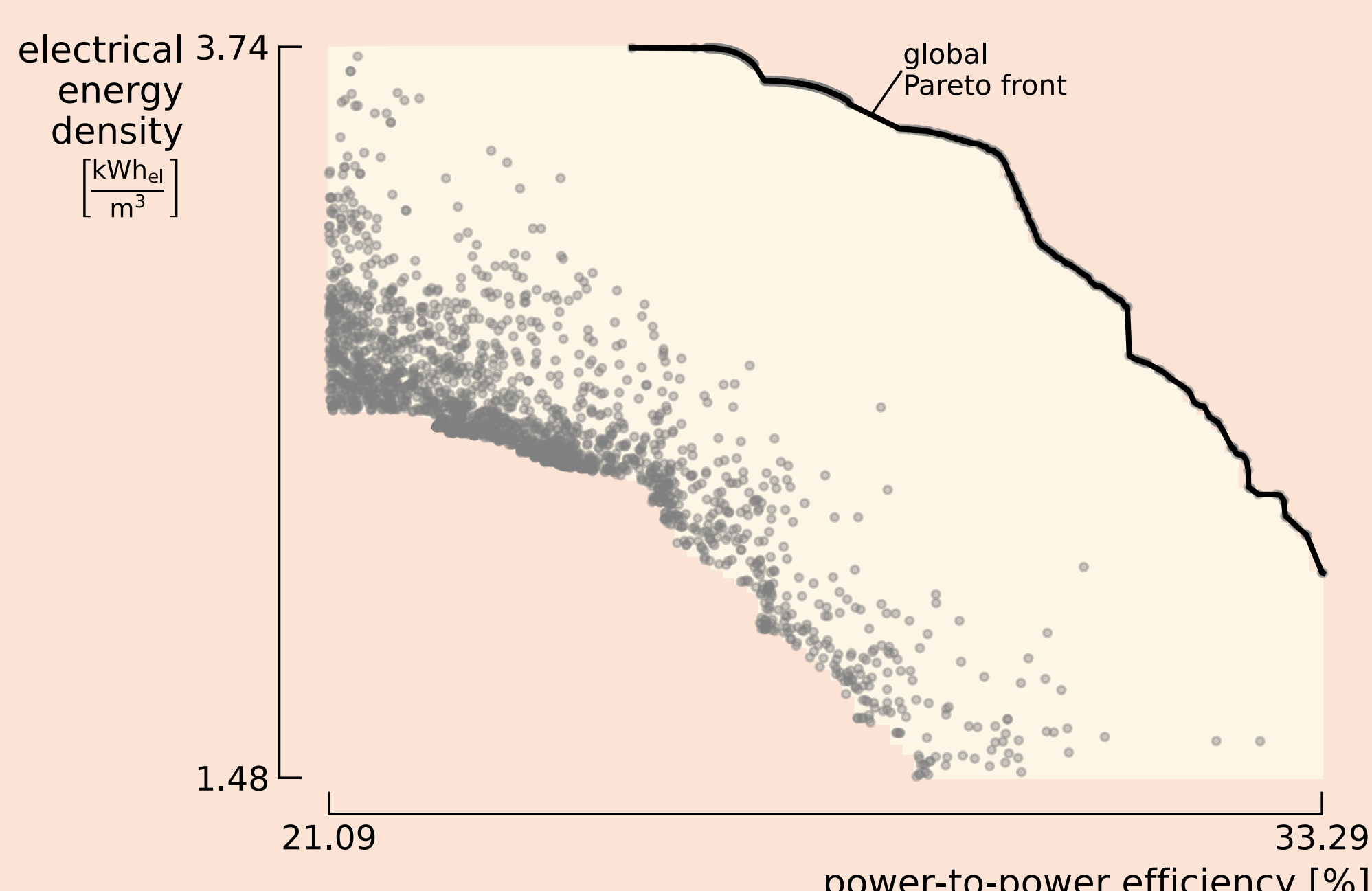
## KPIs across sub-optimal space



	$T_{TES}^{ht} [^{\circ}C] < 100$	$T_{HP}^{comp,ex} [^{\circ}C] < 180$	$r_{v,HP} [-] < 9$	$\Delta T_{HP}^{sc} [K] < 8$	$\Delta T_{HP}^{crit} [K] > 10$	$\Delta T_{ORC}^{crit} [K] > 10$
Subset #1	✓	✓	✗	✗	✓	✓
Subset #2	✗	✓	✓	✗	✓	✓
Subset #3	✗	✓	✓	✗	✗	✓
Subset #4	✗	✓	✗	✓	✓	✓
Subset #5	✗	✓	✗	✗	✓	✓
Subset #6	✗	✓	✗	✗	✓	✗
Subset #7	✗	✗	✗	✓	✓	✓
Subset #8	✗	✗	✗	✗	✓	✓

## Generating the Near-Optimal Designs

- The **near-optimal designs** are then generated for each type of Carnot battery, also using NSGA-II.
- These **maximise the Euclidean distance (i.e., the difference) from the nearest design** of the corresponding Pareto front.



## Choosing the Design that Suits Your Needs

- Manufacturers **select designs based on their own criteria**.
- In this case, designs are chosen with  $\eta_{CB}^{elec} > 27.5\%$  and meeting the following conditions:
  1. No pressurization required for storage  $T_{TES}^{ht} < 100^{\circ}C$  (cost reduction).
  2. Compressor discharge temperature  $T_{HP}^{comp,ex} < 180^{\circ}C$  (lubrication).
  3. Compression volume ratio  $r_{v,HP} < 9$  (limits machines in series).
  4. Sub-cooling in heat pump  $\Delta T_{HP}^{sc} < 8 K$  (charge and condenser design).
  5. Saturation temperatures far from critical point  $\Delta T_{HP,ORC}^{crit} > 10 K$  (avoids near-critical regimes).
- No design meets all criteria simultaneously: different **subsets are highlighted**, along with their **associated design choices** (the so called 'real choices') and **fixed requirements** (the so called 'must-haves').

## Conclusion

Method to generate diverse Carnot battery designs beyond the single thermodynamic optimum, allowing for the inclusion of other performance indicators based on manufacturers needs.

### Acknowledgements

The first author acknowledges the support of Fonds de la Recherche Scientifique - FNRS [40021673 FRIA-B2]. Computational resources have been provided by the Consortium des Équipements de Calcul Intensif (CÉCI), funded by the Fonds de la Recherche Scientifique de Belgique (F.R.S.-FNRS) under Grant No. 2.5020.11 and by the Walloon Region.