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Surface tension of nanoparticle dispersions unravelled by size-dependent non-occupied sites free energy versus adsorption kinetics

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The surface tension of dispersions presents many types of behaviours. Although some models, based on classical surface thermodynamics, allow partial interpretation, fundamental understanding is still lacking. This work develops a single analytical physics-based formulation experimentally validated for the surface tension of various pure nanoparticle dispersions, explaining the underlying mechanisms. Against common belief, surface tension increase of dispersions appears not to occur at low but rather at intermediate surface coverage, owed by the relatively large size of nanoparticles with respect to the fluid molecules. Surprisingly, the closed-form model shows that the main responsible mechanism for the various surface tension behaviours is not the surface chemical potential of adsorbed nanoparticles, but rather that of non-occupied sites, triggered and delicately controlled by the nanoparticles 'at a distance', introducing the concept of the 'non-occupancy' effect. The model finally invites reconsidering surface thermodynamics of dispersions and provides for criteria that allow in a succinct manner to quantitatively classify the various surface tension behaviours.

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INTRODUCTION

Fluid dynamics of complex fluids represent a field of study that concerns a series of energetic, medical and industrial engineering applications. Since these applications concern, in many cases, fluids wherein dispersions are used for material printing or separation processes at the surface level, it is important to control the behaviour of surface-related mechanisms¹. Stability requirements during the dispersion processing and the printing process depend on the physical properties, such as the viscosity, and its deposition quality depends on controlling the fluid dynamics of the deposited fluids and the underlying mechanisms^{2,3}. Moreover, the wettability is a relevant physical property for processes where droplet impingement, thin film flows, microfluidics, surface speciation and heat transfer are implied^{4,5}.

In order to focus on surface-related mechanisms of complex fluid dynamics, microgravity experiments are useful, cancelling thereby the interference of buoyancy. A sounding rocket experiment took place under the framework of the Advanced Research on Liquid Evaporation in Space (ARLES) experiment supported by the European Space Agency (ESA). ARLES was part of the payload in a SubOrbital Express rocket (MASER 14) and aims at studying the evaporation of pure and complex sessile droplets. It also serves as a preparation of an experiment to be performed in the near future at the European Drawer Rack 2 on board the International Space Station. The evaporation of the complex droplets resulted into pattern depositions of nanoparticles, interesting for future printing applications. These experiments allowed studying the depositions, but not how fluid dynamics, surface effects and particle–fluid interactions controlled those depositions. Another sounding rocket experiment is planned to be performed in the near future, where one of the focuses will be to monitor the fluid dynamics of the complex droplets. In order to prepare the flight scenario, a numerical model has been

developed. The condition expressing the tangential stress balance, including surface-tension-induced convection, i.e. Marangoni convection, at the interface is given by

$$-(\sigma_g \cdot \mathbf{n}) + (\sigma_l \cdot \mathbf{n}) + \gamma(\nabla \cdot \mathbf{n})_{\Sigma} \mathbf{n} - \gamma_T \nabla_{\Sigma} T - \gamma_{\varphi} \nabla_{\Sigma} \varphi = 0 \quad (1)$$

where σ_g and σ_l are the stress tensors at the interface on the gas and liquid sides, respectively, \mathbf{n} the normal vector on the interface, γ the surface tension, $(\nabla \cdot \mathbf{n})_{\Sigma}$ stands for the curvature of the interface, $\nabla_{\Sigma} = \nabla - \mathbf{nn} \cdot \nabla$ for the surface gradient, T and φ stand for the temperature and nanoparticle volume fraction at the interface, respectively, whereas γ_T defines the surface tension derivative with respect to the temperature and γ_{φ} the surface tension derivative with respect to the volume fraction. Generally, γ_T is readily available and reasonably approximated to be constant. However, the behaviour of γ_{φ} is not so clear. Since at microgravity, convection responsible for fluid patterns is of the surface-tension type, it is crucial to not only have a physics-based analytical expression for the surface tension of nanoparticle-laden fluids but also to understand the underlying mechanisms that govern the surface tension of such complex fluids.

It appears from several experimental studies that apparently contradictory tendencies of the surface tension as a function of nanoparticle content are observed: the surface tension is observed to increase, decrease or pass through a minimum as a function of the nanoparticle content in the dispersions^{6–15}. Even for the same nanoparticle, e.g. SiO₂, a constant and increasing trend is observed^{9,13}, while for Al₂O₃ both decreasing and increasing trends, in two separate cases, are observed⁷. Due to the diversity of nanodispersions, there is no universal relation yet that could comprehend and clarify quantitatively such observed trends. Fitted correlations or empiric relations may give good comparison to experimental values, but are specific to experiment conditions, do not explain physically why certain surface tension phenomena

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occur and lack often generality^{7,10}. One may find some explanations, but mostly based on a qualitative assessment of the Gibbs free energy or on mere intuition. Some works have explained surface tension behaviour by an energy variation upon nanoparticle transfer to the interface¹⁶, attractive van der Waals or attractive capillary forces^{6,17} or even by analogy with electrolyte solutions¹⁸. Interestingly, it is just the presence of nanoparticles at the surface that is given as reason for surface tension increase in ref. ¹¹, while the nanoparticle adsorption is suggested to cause a decrease in the surface tension elsewhere¹⁷. Others explain surface tension decrease by a high ionic strength of the base fluid countering the otherwise repulsive force between the nanoparticles and the liquid–gas interface¹⁸. This, however, does not explain the decrease of surface tension of nanoparticle-laden fluids with low ionic strength, such as nanoparticle dispersions in distilled water¹⁹ nor for surface tension minima. The initial decrease of the surface tension is suggested to be due to the large spacing between the nanoparticles, favouring electrostatic forces between the nanoparticles⁶ or to initial adsorption of nanoparticles at the liquid–gas interface¹⁷.

The apparently contradictory explanations for surface tension behaviour are often intuitively provided and many existing models, useful as they might be, only predict part of the tendencies, which is a consequence of universal underlying mechanisms still remaining unelucidated. This work develops an analytical model proposing a new insight in surface thermodynamics, surface energy and, more particularly, in the interaction between the dispersed phase and the liquid–gas interface. The model mainly aims at elucidating the underlying mechanisms of the surface tension of nanoparticle dispersions, both correctly predicting and explaining thereby the different experimentally observed tendencies. We start by formulating the framework within which the liquid–gas interface is defined. This will also allow introducing definitions of nanoparticle (excess) surface concentrations based on geometrical and size considerations. The nanoparticles are modelled as being incompressible, non-stretchable and the only material that can be adsorbed on the liquid–gas interface. Then, an analytical expression for the surface tension of nanoparticles will be calculated and compared to several experimental data of different nanoparticle dispersions. The model will be used to explain the different observed phenomena. Finally, it will be shown that two parameters can predict the type of surface tension behaviour for all the considered material systems.

METHODS

Representation of an interfacial layer on a dividing surface

The surface energy of a nanoparticle dispersion can commonly be described by Gibbs adsorption isotherm $dy = -\Gamma_p d\eta_p^\Sigma - \Gamma_f d\eta_f^\Sigma$, an exact differential. Here, η_p^Σ and η_f^Σ are the surface chemical potentials induced by nanoparticle and fluid surface coverage, respectively, whereas Γ_p and Γ_f stand, respectively, for the excess surface concentrations of the nanoparticles and the base fluid. Choosing the Gibbs dividing surface to be there where the excess surface concentration of the liquid equals zero, we set $\Gamma_f \equiv 0$. This leaves us with $dy = -\Gamma_p d\eta_p^\Sigma$. We will start discussing the excess surface concentration first. This inherently entails the definition of a framework that explains how to deal with the representation of a three-dimensional interfacial layer, whilst Gibbs adsorption isotherm imposes to work with a two-dimensional one, i.e. the Gibbs dividing surface. As excess surface concentrations of nanoparticles Γ_p are not widely documented, such a framework will allow us to propose analytical expressions for Γ_p . The excess surface concentration is composed out of a surface equivalent of the bulk concentration, discussed later, and an actual surface concentration. Let us

begin with the latter. The surface concentration of the nanoparticles Γ_p^Σ is defined by the surface coverage θ_p times the maximum surface concentration $\Gamma_{p,\max}^\Sigma$:

$$\Gamma_p^\Sigma = \theta_p \Gamma_{p,\max}^\Sigma \quad (2)$$

the surface coverage θ_p stems from principles concerning thermodynamic equilibrium and adsorption kinetics and it is more appropriate to discuss it later in a proper context. For now, we will focus on the framework of the dividing surface and how the surface concentration is represented within its context.

In Eq. (2), $\Gamma_{p,\max}^\Sigma$ is the maximum surface concentration of the nanoparticles, assumed to be determined by the principle of maximum stacking via a maximum coverage fraction f_∞ ^{20–22}. Other geometrical considerations of particle adsorption have been treated in refs. ^{21,22}, but we only need here their results for maximum coverage. In the presence of nanoparticles, the liquid–gas layer can be defined as the layer where the nanoparticles go gradually from a bulk concentration c_p to a purely surface concentration Γ_p^Σ . The surface concentration is then usually obtained by integrating the concentration profile over the thickness of that layer. It has therefore, generally, a thickness that is larger than the size of the nanoparticles, a thickness that is defined by the difference between the dividing surface and an imaginary parallel surface, beyond which the bulk concentration is attained. The degree of strength of the interaction energy between the fluid molecules and the nanoparticles in that layer will determine the amount of nanoparticles that are ‘trapped’, i.e. adsorbed, or allowed to disperse in the bulk. Each nanoparticle that adsorbs will push away fluid molecules. In analogy to the bulk, according to the lattice model, (where each lattice fits a liquid molecule), we can define that the surface area that is occupied by a fluid molecule harbours a possible adsorption site. As such, the adsorption sites are *geometrically* equivalent to the fluid molecules in the interfacial layer. In order to represent this framework in a manner that fits Gibbs’ isotherm, we have defined a dividing surface. Speaking of the maximum surface concentration, this also necessitates to project the real maximum concentration in the interfacial layer onto the dividing surface (that has zero thickness). This projection method is depicted in Fig. 1a, while Fig. 1b focusses on the projection of an adsorbing nanoparticle with the corresponding parameters that will be used in the model. Figure 1c shows the surface that is deemed to participate to the adsorption. In fact, upon adsorption, it can be imagined that not the whole surface of the nanoparticles participates in the process. It is quite difficult to assess the portion of surface that participates to this process and not much is known about this. In this work, we will heuristically assume that only half of a nanoparticle’s surface, i.e. the half that faces the dividing surface, participates in its adsorption. The reason for this will be discussed later. We will call this the participating surface. Later in ‘*Three counter-intuitive effects of K_p on surface tension*’, a verification will be discussed to show that such an assumption appears to be quite reasonable.

Let us, at maximum coverage, order the nanoparticles into several layers that are parallel to the dividing surface. As we are in maximum coverage, *each layer* contains the same amount of nanoparticles. Let us then project, *in each such layer*, the participating surface of the nanoparticles (as if a nanoparticle was a balloon that is cut in half, of which one half is spread over the surface) on the dividing surface (for the first layer at the dividing surface) and on subsequent imaginary layers parallel to the dividing surface. This gives in each layer the same maximum surface concentration per unit surface, so that considering only the layer adjacent to the dividing surface is sufficient to determine the maximum surface concentration *per unit surface*, as Fig. 1a shows.

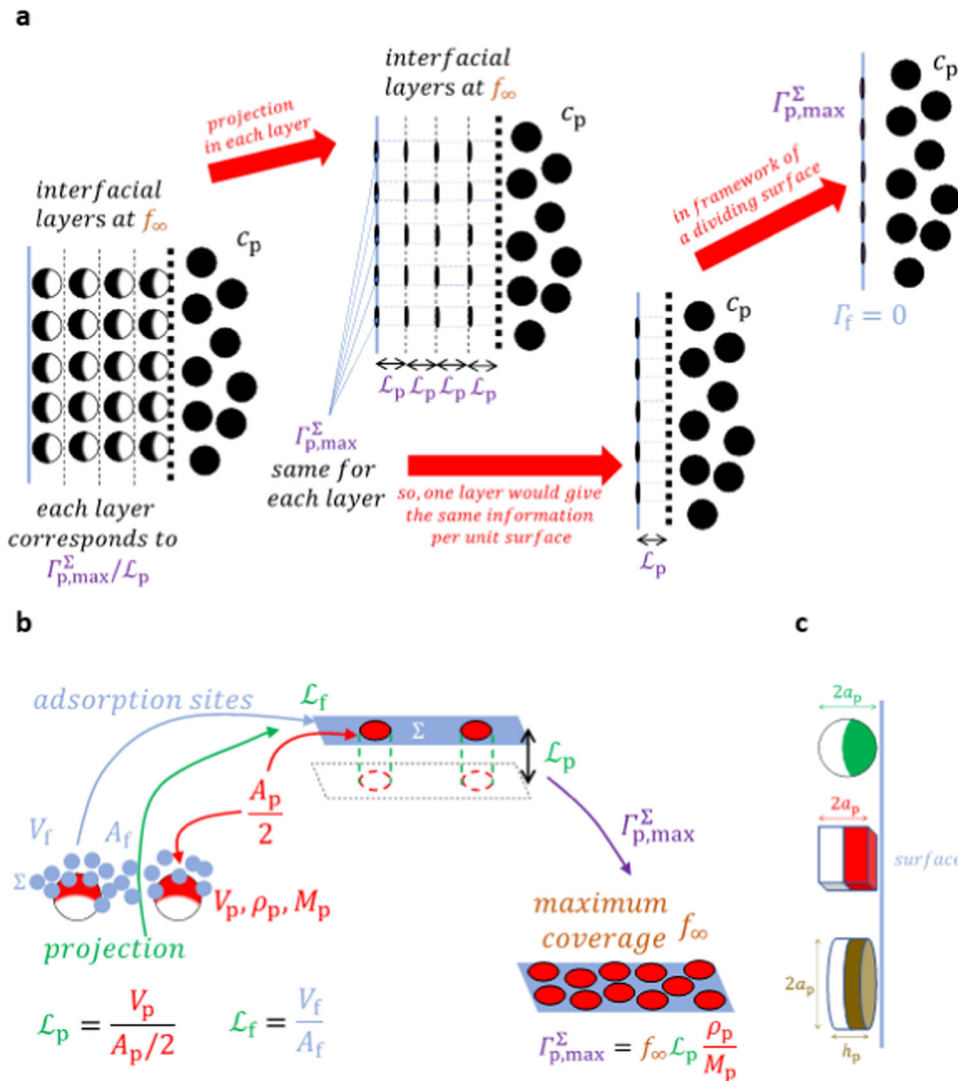


Fig. 1 The projection of nanoparticles on the dividing surface. **a** Principle of projecting nanoparticles on dividing surface at maximum coverage. Note that at a coverage below the maximum one, the principle is the same. **b** Projection of nanoparticles (with volume V_p and surface A_p) on a two-dimensional surface. The projected circles are oval because they are drawn in perspective, but they should be seen as circular for the spherical and disk nanoparticles, and as a square for the cubical nanoparticles. The fluid molecules (with volume V_f and surface A_f) at the surface Σ , on which a nanoparticle adsorbs, also participate to the adsorption and are illustrated as fluid molecules that become projected (on the dividing surface) as two-dimensional adsorption sites, depicted for simplicity as a flat plane Σ at exactly the dividing surface. **c** Illustration of the surfaces that come into play in the volume-to-surface ratio for the spherical, cubical and disk nanoparticles. The images are not in scale.

This will result in a molar concentration of nanoparticles per unit surface on the dividing surface that would be equivalent to the corresponding real molar concentration in a realistic adsorption layer, through scaling by a certain defined characteristic length, so-defined as \mathcal{L}_p . As Fig. 1b shows, the projected maximum surface concentration per unit surface times the characteristic length gives the same volume as that of the nanoparticle. It follows then that that characteristic length must be a volume-to-surface ratio.

We define this volume-to-surface ratio by the total volume divided by half of the total surface (the participating surface, as is shown in Fig. 1c). The fluid particles that surround this participating surface of a nanoparticle in a real interfacial layer are fully projected on the dividing surface as they represent geometrically the adsorption sites on that surface (see the schematic representation in Fig. 1b). The characteristic length of these fluid particles, or adsorption sites, is calculated by a standard volume-to-surface ratio.

The projected surfaces depend on the size of the nanoparticles and the fluid molecules (geometrically equivalent to that of the adsorption sites). This means that the difference in sizes between the nanoparticles and the adsorption sites can be expected to have a great impact on the adsorption process. Each adsorbed nanoparticle will induce a change in the possible entropic configurations of a great number of adsorption sites. As these sites are not occupied, yet have a large influence on the entropy, they are named as non-occupied sites, because their non-occupancy matters entropically. We can say that the total area of these non-occupied sites (denoted by subscript NO) per total surface area is given by

$$c_{NO} m_{NO}^\Sigma = c_f m_f^\Sigma - c_p m_p^\Sigma \tag{3}$$

where m_f^Σ and c_i are, respectively, the number of particles of a constituent per unit interface surface and the specific surface area per particle of that constituent, whilst the superscript Σ indicates that it concerns a surface property. The specific surface

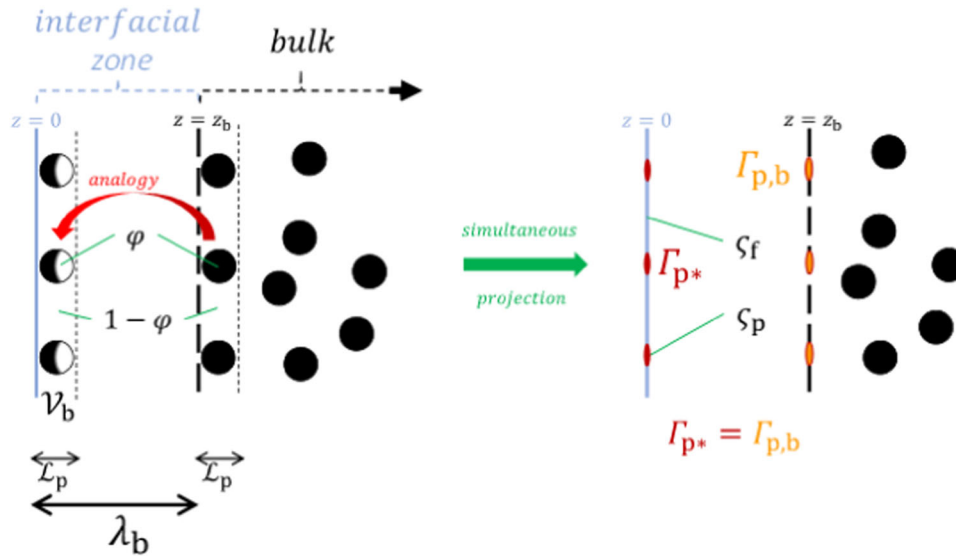


Fig. 2 Projection of bulk concentration. Analogy of an imaginary projection of the nanoparticles at an imaginary surface at $z = z_b$ with respect to the real projection on the dividing surface at $z = 0$. The two resulting molar concentrations per unit surface should be equal in the definition of the surface excess concentration.

area of a constituent is given by $\zeta_i \equiv \frac{M_i}{\rho_i \zeta_i N_A}$, with $i = NO, f, p$, standing for non-occupied sites, the fluid and nanoparticles, respectively. Equivalently, the specific surface area of a constituent may conveniently also be given per mole, i.e. $\zeta_i \equiv \frac{M_i}{\rho_i \zeta_i}$. In that case, m_i^ζ would simply be the number of mole of a constituent per unit surface via scaling by N_A and Eq. (3) remains valid. Expressions for the characteristic length \mathcal{L}_i will be developed later (with $\mathcal{L}_{NO} = \mathcal{L}_f$ as geometrically the adsorption sites are equivalent to the fluid molecules). It is important to notice here that ζ_i introduces a size effect, i.e. the number densities depend on the size of the nanoparticles and the surface fluid particles.

We have now defined the framework for calculating the surface concentrations and may proceed with proposing a formula that allows calculating these concentrations. The maximum surface concentration is given by the maximum number of nanoparticle moles, $\frac{m_{p,max}}{N_A}$, divided by a unit surface, i.e. $\Gamma_{p,max}^\Sigma = \frac{1}{N_A} \frac{m_{p,max}}{A_t}$, where A_t is a total (arbitrary portion of) unit surface. This can conveniently be rewritten as $\Gamma_{p,max}^\Sigma = \frac{V_p}{A_p/2} \frac{m_{p,max} A_p/2}{A_t} \frac{1}{N_A V_p}$, where A_p and V_p are the surface and volume per nanoparticle, respectively. It can be noted that $\frac{V_p}{A_p/2}$ is nothing else than two times the nanoparticle's volume to surface ratio, defined as \mathcal{L}_p (see Fig. 1). Moreover, $\frac{1}{N_A V_p}$ is the mole of nanoparticles per unit volume, also given by $\frac{\rho_p}{M_p}$, where ρ_p and M_p are the nanoparticle's density and molar mass, respectively. Also $\frac{m_{p,max} A_p/2}{A_t}$ is simply the maximum geometric coverage fraction f_∞ , being $f_\infty \approx 0.547$ for spherical non-overlapping hard particles on a two-dimensional surface^{21,22}. This value is obtained by considering random packing of spheres after their projection on the interface. It is therefore not the same as the random packing of circles as the latter would neglect the purpose of the projection method, where it is sought to obtain expressions on a 2D surface whilst preserving the information from realistic 3D interfaces as Fig. 1 shows. For cubic nanoparticles, it is reasonable to expect that the maximum coverage will be close to unity, to that we take $f_\infty \approx 1$ for cubic nanoparticles^{21,22}. For disk-like nanoparticles, of which the circular part faces the dividing surface, we take a maximum coverage that corresponds to maximum standard hexagonal stacking of circles on a surface, i.e. $f_\infty = \frac{\pi\sqrt{3}}{6} \approx 0.907$

for disk nanoparticles. This leads to

$$\Gamma_{p,max}^\Sigma = f_\infty \mathcal{L}_p \frac{\rho_p}{M_p} \quad (4)$$

It should be noted that when nanoparticles are coated or surface treated, the maximum coverage might be less due to possible repulsive forces or more if the nanoparticles have a soft compressible coating with interparticle attractive forces. Note that similar expressions have been proposed in refs. ^{20,23}. Nanoparticles may come in various shapes, the main ones being often of spherical, cubical or disk shape. We will, for the demonstration, limit ourselves to such undeformable shapes. The volume and participating surface, i.e. $(V_p, \frac{A_p}{2})$, as defined in Fig. 1c, would then be $(\frac{4\pi}{3} a_p^3, 2\pi a_p^2)$, $(8a_p^3, 12a_p^2)$ and $(\pi a_p^2 h_p, \pi a_p^2 + \pi a_p h_p)$ for a spherical, cubical and disk nanoparticle, respectively. The volume-to-surface ratio \mathcal{L}_p can then be calculated. For a spherical nanoparticle, $\mathcal{L}_p = \frac{2a_p}{3}$ (with radius a_p), for a square-like nanoparticle, $\mathcal{L}_p = \frac{2a_p}{3}$ (with $2a_p$ the side of the cube) and for a disk-like nanoparticle, $\mathcal{L}_p = \frac{a_p h_p}{a_p + h_p}$ (with radius a_p and thickness h_p). Note that it is not straightforward to define a molar mass of a nanoparticle, since it is not a molecule nor an atom. We will approximate the molar mass of a nanoparticle, in analogy with that of a polymer constituted by many monomers, as an ensemble of atoms or molecules chemically connected to one another. The molar mass of a nanoparticle equals then $M_p = M_{p'} f_p \frac{V_p}{V_{p'}}$, where f_p represents the maximum stacking factor of spheres in a three-dimensional setting, assumed here to be $f_p = \frac{\pi}{3\sqrt{2}}$ (that of an fcc or hcp structure), $M_{p'}$ the molar mass of one atom or molecule, V_p the volume of one nanoparticle and $V_{p'} = \frac{4\pi}{3} \rho_p^3$ the volume of one atom or molecule, assumed to be of spherical form, with ρ_p the radius of that atom or molecule $\rho_p = \sqrt[3]{\frac{M_{p'}}{\rho_p N_A \frac{4\pi}{3}}}$. The effective radius of a fluid molecule, assuming sphericity, can be calculated in the same manner as $\rho_f = \sqrt[3]{\frac{M_f}{\rho_f N_A \frac{4\pi}{3}}}$, where ρ_f and M_f are the fluid's density and molar mass, respectively. With $V_f = \frac{4\pi}{3} \rho_f^3$ and $A_f = 4\pi \rho_f^2$, the volume-to-surface ratio for a fluid particle is given by $\mathcal{L}_f = \frac{\rho_f}{3}$. With these definitions, the geometric definition of the

maximum surface concentration Γ_p^Σ can be calculated from material properties and size values.

The difference between the excess surface concentration Γ_p and the surface concentration Γ_p^Σ is usually defined as

$$\Gamma_p - \Gamma_p^\Sigma \equiv - \int_{z_0}^{z_b} c_p dz = -c_p \lambda_b \quad (5)$$

where c_p is the nanoparticle concentration in the bulk layer, and $\lambda_b = z_b - z_0$, with z_0 the position at which $\Gamma_f = 0$ and z_b at which we can consider conceptually to have a bulk concentration. In order to determine λ_b , let us make a preliminary remark. The maximum surface concentration has been obtained by projecting a layer of adsorbed nanoparticles on a two-dimensional surface at the dividing surface, which we defined as $\Gamma_f = 0$. When doing this, it has been explained that the characteristic length of nanoparticle projection equals \mathcal{L}_p . For consistency, we should do the same here. In the definition of the excess surface concentration, the term $(-\int_{z_0}^{z_b} c_p dz)$ denotes a deduction from the surface concentration of an imaginary extrapolation of the bulk concentration, integrated over the interfacial thickness λ_b . So, it should rather be seen as an imaginary surface-equivalent of the bulk concentration, $\Gamma_{p,b} \equiv \int_{z_0}^{z_b} c_p dz = c_p \lambda_b$, defined at an imaginary surface at $z = z_b$. This also means that it is analogous to the projection of the bulk nanoparticle concentration on the dividing surface, named here Γ_{p^*} , so that $\Gamma_{p^*} \equiv \Gamma_{p,b}$. It remains to find Γ_{p^*} . Imagine at the dividing surface $\Gamma_f = 0$ a slab \mathcal{V}_p of thickness \mathcal{L}_p , of which the contents are projected on that surface. If the projected nanoparticle surface concentration is given by Γ_{p^*} , then the corresponding nanoparticle concentration in \mathcal{V}_p would be $\frac{\Gamma_{p^*}}{\mathcal{L}_p}$ as defined by the projection procedure in Fig. 1. If the projected specific surface area per mole of nanoparticles is given by c_p , then the corresponding volume per mole of nanoparticles in \mathcal{V}_p would be $c_p \mathcal{L}_p$. The same could be done for the fluid particles, so that the volume fraction φ in that slab would be described by $\frac{\varphi}{1-\varphi} = \frac{c_p \Gamma_{p^*}}{c_f \Gamma_{f^*}}$. Within the slab \mathcal{V}_p , the projected surface concentration for the fluid particles Γ_{f^*} would simply be equal to the bulk concentration c_f times the thickness of \mathcal{V}_p , i.e. $\Gamma_{f^*} = c_f \mathcal{L}_p$. We then have $\Gamma_{p^*} = c_f \mathcal{L}_p \frac{\varphi}{1-\varphi}$. Note that $c_f = (1-\varphi) \frac{\rho_f}{M_f}$. Filling in the definitions of c_p and c_f leads to $\Gamma_{p^*} = \frac{\rho_f}{M_f} \mathcal{L}_p \frac{M_f}{\rho_f \mathcal{L}_f} \left(\frac{M_p}{\rho_p \mathcal{L}_p} \right)^{-1} \varphi = \frac{\rho_p}{M_p} \frac{\mathcal{L}_p^2}{\mathcal{L}_f} \varphi$. Figure 2 illustrates the analogy that we have discussed here.

As $c_p = \varphi \frac{\rho_p}{M_p}$, it follows that $\lambda_b = \frac{\mathcal{L}_p^2}{\mathcal{L}_f}$. Filling this in (5) gives, with Eq. (2), for the excess surface concentration

$$\Gamma_p \equiv \theta_p \Gamma_{p,\max}^\Sigma - \varphi \Gamma_b^\Sigma = (\theta_p K_\Sigma - \varphi) \Gamma_b^\Sigma \quad (6)$$

with

$$\Gamma_b^\Sigma = \frac{c_p}{\varphi} \lambda_b = \frac{\rho_p}{M_p} \frac{\mathcal{L}_p^2}{\mathcal{L}_f} \quad (7)$$

$$K_\Sigma = \frac{\Gamma_{p,\max}^\Sigma}{\Gamma_b^\Sigma} \quad (8)$$

where $\Gamma_{p,\max}^\Sigma$ is given by Eq. (4) and $\varphi \Gamma_b^\Sigma$ is the surface equivalent of the bulk concentration and K_Σ a constant that measures the potential of the nanoparticles to rather adsorb at the interface than stay dispersed in the bulk. As will be seen later, K_Σ is a function of nanoparticle size, maximum packing and fluid molecule size. The surface coverage θ_p in Eq. (6) will be treated in the context of surface kinetics, but we will first deduce the surface chemical potentials and surface adsorption.

Surface chemical potential

If we have m_i^Σ number densities of adsorption sites, containing m_{NO}^Σ number densities of non-occupied sites and m_p^Σ number

densities of adsorbed nanoparticles, the total number of microstates would equal $W = \frac{(m_{NO}^\Sigma + m_p^\Sigma)!}{m_p^\Sigma! m_{NO}^\Sigma!}$. Boltzmann's equation of

entropy would give $S_d = k_B \ln(W) = k_B \ln \left(\frac{(m_{NO}^\Sigma + m_p^\Sigma)!}{m_p^\Sigma! m_{NO}^\Sigma!} \right)$. For a pure fluid, only one undistinguishable combination exists, i.e. $S_f = k_B \ln(1) = 0$. The corresponding surface fraction is given by

$y_p = \frac{m_p^\Sigma}{m_{NO}^\Sigma + m_p^\Sigma}$. The surface coverage is defined to be equal to the surface fraction, $\theta_i \equiv y_i$, so that $\theta_p + \theta_{NO} = 1$. Defining the configurational entropy of dispersing, due to nanoparticle coverage and non-occupied sites, as $\Delta s_d = S_d N_A - S_f N_A$, and using Stirling's approximation for the logarithm of factorials, gives

$$\Delta s_d^\Sigma = -k_B N_A (\theta_p \ln(\theta_p) + \theta_{NO} \ln(\theta_{NO})) \quad (9)$$

where k_B and N_A are, respectively, Boltzmann's constant and Avogadro's number. In dilute conditions, the enthalpy of dispersing can be neglected. It should be noted that this enthalpy results from heat liberated or absorbed due to new interactions that stem from the mixing process, while it is not the same as the enthalpy of adsorption, which plays a role in the equilibrium adsorption constant. In such conditions, we deal with an ideal dispersion, being consistent with the Langmuir's adsorption isotherm, of which a detailed deduction is presented in the next section. The Gibbs surface free energy of dispersing is then given by $\Delta g_d^\Sigma = -T \Delta s_d^\Sigma$ resulting into

$$\Delta g_d^\Sigma = k_B T N_A (\theta_p \ln(\theta_p) + \theta_{NO} \ln(\theta_{NO})) \quad (10)$$

We define $\omega_p \equiv \frac{c_p}{c_{NO}}$ and $\omega_f \equiv \frac{c_f}{c_{NO}}$. The chemical potentials of a component i are defined by

$$\eta_i^\Sigma = N_A \frac{\partial}{\partial m_i^\Sigma} \left(\frac{m_{NO}^\Sigma + m_p^\Sigma}{N_A} \Delta g_d^\Sigma \right)_{T,p,m_{ij}^\Sigma} \quad (11)$$

with $i = p, f$ and $j = p, f$. The number ω_p can also be understood as the number of adsorption sites per nanoparticle. We then use the aforementioned definition $\theta_i = \frac{m_i^\Sigma}{m_{NO}^\Sigma + m_p^\Sigma}$, fill this in in Eq. (10), apply Eq. (11) and rewrite the result back in terms of θ_i . This finally gives $\eta_f^\Sigma = k_B T N_A \omega_f \ln(1 - \theta_p)$ and

$$\eta_p^\Sigma = k_B T N_A (\ln(\theta_p) - \omega_p \ln(1 - \theta_p)) \quad (12)$$

where $\omega_p \equiv \frac{c_p}{c_{NO}} \equiv \frac{c_p}{c_f}$ (as $\omega_f \equiv \frac{c_f}{c_{NO}}$ and $\omega_f \equiv 1$ because the adsorption sites are within the present framework geometrically equivalent to the projected liquid molecules, see Fig. 1b and corresponding discussion) is given by

$$\omega_p = \frac{M_p \rho_f \mathcal{L}_f}{\rho_p M_f \mathcal{L}_p} \quad (13)$$

Surface adsorption isotherm

Equilibrium of the adsorption process is described by a net zero change of the total Gibbs free energy of the system: $d\Delta G_a = d\Delta G_{ad}^\Sigma + d\Delta G_{ad}^b + d\Delta G_d^\Sigma + d\Delta G_d^b \equiv 0$, where the subscripts 'ad' and 'd' denote the adsorption (due to translational or confinement effects, or effects related to particle surface energies, dipole-dipole and coulomb interactions²⁴, for instance) and the dispersion (mixing) free energies, respectively, and 'Σ' and 'b' the surface and bulk phases, respectively. We focus first on the dispersing. We can then define $\Delta G_d^\Sigma = A \frac{m_{NO}^\Sigma + m_p^\Sigma}{N_A} \Delta g_d^\Sigma$ and $\Delta G_d^b = V \frac{m_1^b + m_p^b}{N_A} \Delta g_d^b$, where m_1^b and m_p^b are the number of bulk fluid particles and nanoparticles per unit volume of the dispersion, whereas A and V are an arbitrary unit surface and volume, respectively. Note here that $\frac{m_{NO}^\Sigma + m_p^\Sigma}{N_A}$ has unit moles per unit surface

and $\frac{m_p^b + m_p^s}{N_A}$ unit moles per unit volume. Note also that we can define a mole fraction of nanoparticles in the bulk as $x_p = \frac{m_p^b}{m_p^b + m_p^s}$. Neglecting the enthalpy of dispersing as mentioned before, an addition of nanoparticles to the surface would result into a change $d\Delta G_d^\Sigma(m_p^\Sigma, m_f^\Sigma)$, which can mathematically be written as $d\Delta G_d^\Sigma = N_A \frac{\partial}{\partial m_p^\Sigma} \left(A \frac{m_{No}^\Sigma + m_p^\Sigma}{N_A} \Delta g_d^\Sigma \right)_{T,p,m_f^\Sigma} dm_p^\Sigma + N_A \frac{\partial}{\partial m_f^\Sigma} \left(A \frac{m_{No}^\Sigma + m_p^\Sigma}{N_A} \Delta g_d^\Sigma \right)_{T,p,m_p^\Sigma} dm_f^\Sigma = A \left(\eta_p^\Sigma dm_p^\Sigma + \eta_f^\Sigma dm_f^\Sigma \right)$. From (3) and the total number density, it can be derived that $dm_f^\Sigma = (\omega_p - 1) dm_p^\Sigma$. With the definitions for η_p^Σ and η_f^Σ (see Eq. (12) and text above), this leads with $\omega_f = 1$ to $d\Delta G_d^\Sigma = k_B T N_A \ln \left(\frac{\theta_p}{1 - \theta_p} \right) A dm_p^\Sigma$. An equivalent procedure can be performed for the bulk phase leading, under the approximation of diluted dispersion, to the relation $d\Delta G_d^b = k_B T N_A \ln(x_p) V dm_p^b$. Mass conservation stipulates that the net mass change is zero, i.e. $A dm_p^\Sigma + V dm_p^b = 0$. This leads to $d\Delta G_d^\Sigma + d\Delta G_d^b = k_B T N_A \left(\ln \left(\frac{\theta_p}{1 - \theta_p} \right) - \ln(x_p) \right) A dm_p^\Sigma$.

A change in the nanoparticles number in both phases upon adsorption also induces a change in the free energy of the adsorption, which can be symbolically (as an already existing thermodynamic relation for the free energy of adsorption will be used, there is no need to enter into details as we did for the free energy of dispersion earlier) written as $d\Delta G_{ad}^\Sigma(A m_p^\Sigma) + d\Delta G_{ad}^b(V m_p^b) = \Delta g_{ad}^\Sigma A dm_p^\Sigma + \Delta g_{ad}^b V dm_p^b$. We can use the mass conservation principle $A dm_p^\Sigma + V dm_p^b = 0$ and write $d\Delta G_{ad}^\Sigma + d\Delta G_{ad}^b = (\Delta g_{ad}^\Sigma - \Delta g_{ad}^b) A dm_p^\Sigma \equiv \Delta g_{ad} A dm_p^\Sigma$, where Δg_{ad} stands for the net difference of the free energy of adsorption per mole of adsorbed nanoparticles. At equilibrium, Δg_{ad} is related to the thermodynamic equilibrium constant K_e via Van't Hoff's equation for adsorption $\Delta g_{ad} = -RT \ln(K_e)$ with K_e the thermodynamic equilibrium constant of adsorption. The total Gibbs free energy of the system $d\Delta G_a$ becomes finally $d\Delta G_a = k_B T N_A \left(\ln \left(\frac{\theta_p}{1 - \theta_p} \right) - \ln(x_p) \right) A dm_p^\Sigma - RT \ln(K_e) A dm_p^\Sigma \equiv 0$ at equilibrium.

This leads finally to $-\ln K_e + \ln \left(\frac{\theta_p}{1 - \theta_p} \right) - \ln(x_p) = 0$, which is known as an adsorption isotherm for ideal dispersions or solutions. The equilibrium constant K_e is for ideal cases related to the dimensional Langmuir equilibrium constant K_p^d , which can be traditionally described by the equilibrium adsorption reaction: $c_p + [*] \rightleftharpoons [P - *]$, where c_p is the nanoparticle molar bulk concentration, $[*]$ the surface molar concentration of empty adsorption sites and $[P - *]$ the surface molar concentration of adsorbed nanoparticles, respectively. If we define $\Gamma_{p,max}^\Sigma$ as the maximum surface concentration, we can write $[*] + [P - *] = \Gamma_{p,max}^\Sigma$, which is equivalent to defining the surface coverage as $\theta_p = \frac{[P - *]}{\Gamma_{p,max}^\Sigma}$ and therefore $\frac{[*]}{\Gamma_{p,max}^\Sigma} \equiv 1 - \theta_p$. Note that later, we will use the notation $\Gamma_{p,max}^\Sigma$ for $[P - *]$. Thermodynamically, $K_p^d = \frac{[P - *]}{c_p [*]} = \frac{\theta_p}{c_p (1 - \theta_p)}$. As c_p has unity moles per unit volume, K_p^d has unity volume per mole. Furthermore, as K_e is dimensionless, this means that we can define $K_e = c_t K_p^d$, where c_t must have unity moles per volume. Similar discussions on the various definitions of K_e and K_p^d have been performed in the literature, indicating that K_e in Van't Hoff's equation is dimensionless and that K_p^d in the Langmuir's adsorption equation has a dimension depending on the concentrations, confirming this analysis^{25,26}. We can also deduce (in dilute systems, $c_f \approx c_t$, with c_f and c_t the molar concentrations of the base fluid and the bulk phase, respectively) that c_t can be represented by the molar concentration of the bulk phase^{25,26}. Filling this in the adsorption isotherm gives finally

$-\ln(c_t K_p^d) + \ln \left(\frac{\theta_p}{1 - \theta_p} \right) - \ln(x_p) = 0$, which (keeping in mind that $x_p c_t = c_p$) simplifies to $\frac{\theta_p}{1 - \theta_p} = K_p^d c_p$, which is the well-known Langmuir's adsorption isotherm, subject to further discussion in the next section. This can be rearranged into

$$\theta_p = \frac{K_p^d c_p}{1 + K_p^d c_p} \quad (14)$$

The equilibrium adsorption constant K_e could be calculated thermodynamically via Van't Hoff's relation. However, experimental values for the molar adsorption enthalpies and entropies are not readily available for the studied nanoparticle dispersions and especially not for various concentrations. Other expressions and methods make use of more available surface energies and surface tensions. However, even if one may perform such measurements, such a procedure would not allow an analytical physics-based analysis of the behaviour of the surface tension and would not offer the understanding of the underlying mechanisms for the various surface tension behaviours. Therefore, it would not align with the purposes of this work. In order to obtain theoretical parameters, independent of the experimental surface tension data, experimental regression procedures or any fitting methods, one of the often-used ways is to use a kinetic model. Adsorption and desorption are often described kinetically. Material properties for kinetic models are readily available for solid-liquid interfaces and the methods are widely used and understood. As less data are available for liquid-fluid interfaces, it is the question whether similar kinetic models would be applicable. One can argue that the adsorption of surface-charged nanoparticles (an important method to obtain stable dispersions) on liquid-fluid interfaces (often charged with the same sign) can be approximated by adsorption on solid-liquid interfaces. Although subject to more investigation, it has already been applied successfully for liquid-fluid interfaces²⁴. This motivates that within such a reasonable assumption the equilibrium adsorption constant for the nanoparticle dispersions can be obtained without fitting. The interpretation of underlying mechanisms would benefit from such a physics-based approach.

Surface kinetics

It remains to find the equilibrium adsorption constant K_p^d or for later convenience, a dimensionless version K_p thereof. 'Surface adsorption isotherm' presented the thermodynamic theory behind the Langmuir adsorption isotherm. It was mentioned that unavailable experimental data for the nanoparticle dispersions studied here and the aim to provide for a physics-based model encourage the use of another way. Commonly, the equilibrium adsorption constant is determined kinetically, where material properties necessary for the model are readily available. The kinetic model is based on an equilibrium between standard adsorption and desorption kinetics and is treated in details in the literature²⁷⁻³⁰. We mention the main points here. Note that desorption becomes relevant when the energy of particle trapping is of the order of the thermal energy. Adsorption (with standard rate k_a) depends on the bulk concentration c_p and the available adsorption sites $(1 - \theta_p)$. Desorption (with standard rate k_d) depends on the adsorbed nanoparticles θ_p per specific surface area of adsorbed nanoparticles c_p . This writes as

$$j_a = k_a c_p (1 - \theta_p) \quad (15)$$

$$j_d = k_d \theta_p \frac{1}{c_p} \quad (16)$$

From kinetic considerations, it can be stated that nanoparticle accumulation, through a flux balance equation, at the interface is given by $\frac{1}{c_p} \frac{\partial \theta_p}{\partial t} = j_a - j_d$, where we remind that here c_p is the

specific surface area per mole of nanoparticles. At quasi-stationarity, i.e. $\frac{\partial \theta_p}{\partial t} = 0$, we have from Eqs. (15) and (16) that

$$\theta_p = \frac{k_a c_p}{k_d \frac{1}{c_p} + k_a c_p} = \frac{\frac{k_a}{k_d} c_p c_p}{1 + \frac{k_a}{k_d} c_p c_p} \quad (17)$$

Comparison with (14) learns that $K_p^d = \frac{k_a}{k_d} c_p$. As the molar concentration can also be expressed into the volume fraction φ by $c_p \equiv \frac{\rho_p}{M_p} \varphi$, we can rewrite (17) as

$$\theta_p = \frac{\frac{k_a}{k_d} \frac{\rho_p}{M_p} c_p \varphi}{1 + \frac{k_a}{k_d} \frac{\rho_p}{M_p} c_p \varphi} \quad (18)$$

This allows defining a dimensionless Langmuir's equilibrium constant $K_p \equiv \frac{k_a}{k_d} \frac{\rho_p}{M_p} c_p = \frac{k_a}{k_d} \frac{1}{L_p}$, and relating the surface coverage with the bulk volume fraction as

$$\theta_p = \frac{K_p \varphi}{1 + K_p \varphi} \quad (19)$$

If we assume that particle transport occurs under a quasi-linear and stationary diffusional regime (this is a valid approximation because of the very small relaxation time), it has been shown that general analytical solutions for the adsorption and desorption constants can be obtained^{27–30}, i.e. $\frac{k_a}{k_d} = \delta_m \sqrt{\frac{\pi k_B T}{|\Phi_m|}} e^{-\frac{\Phi_m}{k_B T}}$, which finally leads to

$$K_p \equiv \frac{\delta_m}{L_p} \sqrt{\frac{\pi k_B T}{|\Phi_m|}} e^{-\frac{\Phi_m}{k_B T}} \quad (20)$$

where Φ_m is the total potential energy, Φ_v at a distance $z = \delta_m$, i.e. $\Phi_m = \Phi_{t|z=\delta_m}$. The total potential energy stands here for the potential energy between a particle and the liquid-air interface, being composed of many mechanisms. The DLVO theory mentions that the most important interactions are the electrostatic ($\Phi_{p-\Sigma}^{EDL}$) and van der Waals ($\Phi_{p-\Sigma}^{vdW}$) interaction energies^{24,31–33}. Image charge effects in the form of a repulsive particle-image ($\Phi_{p-p'}^{EDL}$) potential energy are esteemed to be of importance, the reason being that in cases of particles being oppositely charged to the interface, repulsion was still observed^{24,34}. Non-DLVO interaction energies ($\Phi_{p-\Sigma}^{Hy}$), suggested to be of the Lewis acid-base type, also appear to be of great importance, such as hydrophilic repulsive interactions and hydrophobic attraction energies^{35–38}. The electrostatic double layer interaction potential between a nanoparticle and a flat fluid-air interface is given by³²

$$\Phi_{p-\Sigma}^{EDL} = 64\pi\epsilon_r\epsilon_0 \left(\frac{k_B T}{e_e}\right)^2 \text{Tanh}\left(\frac{\zeta_p e_e}{4k_B T}\right) \text{Tanh}\left(\frac{\zeta_\Sigma e_e}{4k_B T}\right) \left(a_p \left(e^{-\frac{z}{\lambda_D}} + e^{-\frac{z+2a_p}{\lambda_D}}\right) + \lambda_D \left(-e^{-\frac{z}{\lambda_D}} + e^{-\frac{z+2a_p}{\lambda_D}}\right)\right) \quad (21)$$

where ϵ_r , ϵ_0 , e_e , ζ_p , ζ_Σ , and λ_D , are, respectively, the relative permittivity, the absolute permittivity, the elementary charge, the zeta potential of the nanoparticles, the zeta potential of the liquid-air interface and Debye length. Debye's length is given by $\lambda_D = \sqrt{\frac{\epsilon_r \epsilon_0 k_B T}{2N_A e_e^2 I}}$, where I stands for the ionic strength of the base fluid. The potential energy between a particle, p , and its image, p' , in the phase at the other side of the fluid-air interface is given by refs. 24,34

$$\Phi_{p-p'}^{EDL} = 32\pi\epsilon_r\epsilon_0 \left(\frac{k_B T}{e_e}\right)^2 \text{Tanh}\left(\frac{\zeta_p e_e}{4k_B T}\right) \text{Tanh}\left(\frac{\zeta_{p'} e_e}{4k_B T}\right) a_p e^{-2\frac{z}{\lambda_D}} \quad (22)$$

where $\zeta_{p'}$ stands for the zeta potential of the image particle, given by $\zeta_{p'} = \frac{2k_B T}{e_e} \text{ArcSinh}\left(\frac{\epsilon_r - \epsilon_r'}{\epsilon_r + \epsilon_r'} \text{Sinh}\left(\frac{\zeta_p e_e}{2k_B T}\right)\right)$ ³³. Here, ϵ_r' is the relative

permittivity of the phase at the opposite side of the interface opposed to the relative permittivity of the phase where the nanoparticles are dispersed, ϵ_r . The van der Waals potential energy between the nanoparticle and the interface is given by

$$\Phi_{p-\Sigma}^{vdW} = -\frac{A_{p-\Sigma}}{6} \left(\frac{a_p}{z} + \frac{a_p}{z+2a_p} + \ln\left(\frac{z}{z+2a_p}\right)\right) \quad (23)$$

where $A_{p-\Sigma}$ is the non-retarded Hamaker constant for the particle-interface interaction, where the particle (p) interaction with air (a) through the base fluid (f) is assessed. This constant is derived by the theory of London-dispersion forces and is often approximated by the combining relation $A_{p-\Sigma} = A_{pfa} = (\sqrt{A_{pp}} - \sqrt{A_{ff}})(\sqrt{A_{aa}} - \sqrt{A_{ff}})$ ^{39,40}. Non-DLVO interaction energies may be considered as one potential energy, being either repulsive or attractive depending on the solid-water contact angle³⁶. In another work, a Hydra parameter, depending on the hydrophobicity of the surface, was introduced in one expression, being either negative or positive, defining, respectively, a hydrophilic repulsive or hydrophobic attractive potential energy. The Hydra potential energy is given by refs. 36,37,41,42

$$\Phi_{p-\Sigma}^{Hy} = -2\pi a_p \lambda_0 \gamma_0 (1 - \text{Cos}(\vartheta)) e^{-\frac{z_0 - z}{\lambda_0}} \quad (24)$$

where λ_0 is a decay length, ϑ the radial liquid-solid static contact angle and z_0 a constant of the value of 0.16 nm^{41,42}. The total potential energy is given by $\Phi_t = \Phi_{p-\Sigma}^{EDL} + \Phi_{p-p'}^{EDL} + \Phi_{p-\Sigma}^{vdW} + \Phi_{p-\Sigma}^{Hy}$.

Material properties

Table 1 shows the material properties of the used nanodispersions at ambient temperature. Effect of temperature on solid properties is neglected. For the base fluids, only the densities are adapted for temperatures different than ambient. Since these values are well

Table 1. Material properties and physical constants.

Component ^a	Density [$kg\ m^{-3}$]	Molar mass [$kg\ mol^{-1}$]
Al ₂ O ₃	3950	0.102
Al	2700	0.027
B	2370	0.011
MgO	3580	0.040
SiO ₂	2650	0.060
Ag	10490	0.108
Laponite	2530	2.287
ZnO	5610	0.0814
Dodecanethiol-ligated Au ^b	4720	0.198
Water (W)	997	0.018
n-decane (D)	730	0.142
Ethanol	789	0.046
Ethylene glycol (EG)	1110	0.062
Tri-ethylene glycol (TEG)	1120	0.150
n-dodecane (DD)	750	0.170
n-hexadecane (HD)	773	0.226

^aFirst nine rows concern the nanoparticle densities ρ_p and molar masses M_p . The tenth to sixteenth-row concern the base fluid densities ρ_f and molar masses M_f .

^bVolume-averaged and mole-averaged values are given for the density and molecular weight, respectively, based on the dimensions of the core gold nanoparticle and the dodecanethiol ligand shell. Note that the molar mass M_p' given here is the one of an atom or molecule. To obtain the molar mass of a nanoparticle, one must make the conversion $M_p = M_p' f_p \frac{V_p}{V_p'} = \frac{4\pi r_p^3}{9\sqrt{2}} a_p^3 \rho_p N_A$. The values of the used physical constants are $N_A = 6.02 * 10^{23}$ [mol⁻¹], $R_g = 8.3145$ [J mol⁻¹ K⁻¹], $\epsilon_0 = 8.854 * 10^{-12}$ [C V⁻¹ m⁻¹], $e_e = 1.602 * 10^{-19}$ [C] and $k_B = 1.38 * 10^{-23}$ [J K⁻¹].

Table 2. Data needed for calculation of equilibrium constant K_p .

NP-L	A_{pp} [10^{-20} J]	A_{ff} [10^{-20} J]	ϵ_r [–]	ϑ [°]	λ_0 [nm]	$-\zeta_p$ [mV]	T [K]	$2a_p$ [nm]	Ref.
Al ₂ O ₃ -W	15 ^a	3.7 ^b	80 ^c	35 ^d	0.72	64	300	50 ^w	6
Al ₂ O ₃ -D	15 ^a	5.45 ^b	2 ^e	26 ^f	1.16	55	300	50 ^w	6
Al-D	15 ^g	5.45 ^b	2 ^e	33 ^h	0.87	57	300	18	6
B-D	6.23 ⁱ	5.45 ^b	2 ^e	33 ^h	0.35	55	300	46 ^x	6
Al ₂ O ₃ -E	15 ^a	4.2 ^b	25.3 ⁱ	23 ^j	1.83	38	300	50 ^w	6
Al-E	15 ^g	4.2 ^b	25.3 ⁱ	36 ^k	0.98	61	300	18	6
B-E	6.23 ^l	4.2 ^b	25.3 ⁱ	36 ^k	0.71	63	300	46 ^x	6
Al ₂ O ₃ -TEG	15 ^a	5.8 ^b	23.3 ^m	30 ⁿ	0.8	59	298	20	10
MgO-TEG	12.1 ^o	5.8 ^b	23.3 ^m	30 ⁿ	0.67	46	298	20	10
SiO ₂ -W	6.5 ^a	3.7 ^b	80 ^c	20.7 ^p	0.8	50	298	30	9
Ag-W	50 ^g	3.7 ^b	80 ^c	40 ^q	0.78	45	298	100	9
Lap-W	1.06 ^r	3.7 ^b	80 ^c	24 ^s	0.57	49	300	25 (1.5) ^y	19
ZnO-EG	9.2 ^a	5.6 ^b	40 ^t	36.4 ^u	0.57	60	300	67	11
(dl)Au-D	28 ^v	5.45 ^b	2 ^e	30.5 ^v	1.95	30	303	5 (1.7) ^z	38,47
(dl)Au-DD	28 ^v	5.8 ^b	2 ^e	33 ^v	1.71	35	303	5 (1.7) ^z	38,47
(dl)Au-HD	28 ^v	5.2 ^b	2 ^e	36 ^v	1.5	70	303	5 (1.7) ^z	38,47
Al ₂ O ₃ -Ws	15 ^a	3.7 ^b	80 ^c	35 ^d	0.72	75	300	40	48

The base fluids W, D, DD, HD E, TEG, and EG stand for water, n-decane, n-dodecane, n-hexadecane, ethanol, tri-ethylene glycol, and ethylene glycol, respectively. Ws stands for fully stabilised water dispersion⁴⁸. The temperatures for which the experimental data are obtained from the literature are indicated in the table. If in the literature it is mentioned that the experimental data are obtained at ambient temperature, the value of 300 K is used.

^aref. 52.

^bref. 53, the value of TEG is approximated as that of di-ethylene glycol.

^cref. 54.

^dref. 55.

^eref. 56, same value assumed for n-dodecane and n-hexadecane.

^fref. 57.

^gref. 58.

^href. 59, the value of B is approximated as that of Al.

ⁱref. 60.

^jrefs. 60–63, interpolative estimation.

^kref. 64, the value of B is approximated as that of Al.

^lref. 65.

^mref. 66.

ⁿref. 67, assumed from values of EG on mixed ceramic substrates.

^oref. 68.

^pref. 69.

^qrefs. 70,71, averaged value.

^rref. 72.

^srefs. 73,74, averaged values.

^trefs. 75,76, averaged values.

^uref. 77, approximated.

^vref. 38.

^wTEM images in ref. 6 show agglomeration so that the size of the nanoparticles is ~2 times that of the initial one (25 nm).

^xSEM images in ref. 6 show cubic-like particles with an averaged size of 80 nm so that, taking this size between opposite corners of a cube, one cube side would be $80/\sqrt{3} \approx 46$ nm.

^yThe value between the brackets is the thickness of the nanodisks.

^zThe core diameter of Au is 5 nm and the ligand shell thickness is 1.7 nm with an overall reported diameter of $2a_p = 8.4$ nm^{38,47}. The B nanoparticles were approximated as cubic particles, evidenced from SEM images in ref. 6 and the Laponite nanoparticles are nanodisks of a flat (the thickness is much smaller than the radius) cylindrical shape¹⁹, while the rest are spherical nanoparticles^{6,7,9–11,38,47,48}.

tabulated, not more attention is given. Some data are reported in the literature as a function of the mass fraction. If ξ is the nanoparticle mass fraction, ρ_p the nanoparticle density and ρ_f the fluid density, then the nanoparticle volume fraction φ can be calculated as $\varphi = \frac{\xi}{\rho_p} \left(\frac{\xi}{\rho_p} + \frac{1-\xi}{\rho_f} \right)^{-1}$. Table 1 also shows general physical constants used in the model.

Equations (20)–(24) allow calculating the equilibrium constant K_p . Several data are needed for this calculation. These data are collected from the literature and tabulated in Table 2. A summary of the variables and their meaning is given in Table 3.

It should be noted that it is difficult to obtain precise values for the parameters ϑ , δ_m , ζ_{int} , l , λ_0 , and ζ_p , which need some discussion. Reasonable values can be obtained from experimental data for ϑ , δ_m , ζ_{int} , l . The minimum thickness between the nanoparticle and the interface at adsorption, δ_m , is often assumed to be of the order of $\delta_m = 0.5$ nm^{27,43}. For the interface zeta potential, ζ_{int} , the approximated mean value of $\zeta_{int} = -40$ mV is taken for water^{44,45}. For ethanol, tri-ethylene glycol, ethylene glycol and glycerol the same value is assumed, while n-decane, n-dodecane and n-hexadecane are considered to be an oily liquid as hexane and a value of $\zeta_{int} = -10$ mV is taken⁴⁴. The ionic

Table 3. Variables used in the model and their meaning.

Symbol	Description	Unit
a_p	Nanoparticle radius	[m]
$A_{p-\Sigma}$	Non-retarded Hamaker constant	[J]
c_p	Bulk concentration	[mol m ⁻³]
D_p	Ratio excess surface to surface-equivalent of bulk concentrations	[–]
e_e	Elementary charge	[C]
f_∞	Maximum geometric coverage fraction	[–]
h_p	Disk nanoparticle thickness	[m]
\mathcal{H}_{NO}	Non-occupancy effect	[J m ⁻²]
I	Ionic strength	[mol m ⁻³]
k_a	Adsorption rate	[m s ⁻¹]
k_B	Boltzmann constant	[J K ⁻¹]
k_d	Desorption rate	[s ⁻¹]
K_p	Equilibrium adsorption constant	[–]
K_Σ	Ratio surface to bulk preference	[–]
ℓ_f	Equivalent size of fluid molecule	[m]
ℓ_p	Equivalent size of nanoparticle	[m]
\mathcal{L}_f	Characteristic length of fluid molecule	[m]
\mathcal{L}_p	Characteristic length of nanoparticle	[m]
m_f^Σ	Number of fluid molecules per unit surface	[particles m ⁻²]
m_{NO}^Σ	Number of non-occupied sites per unit surface	[particles m ⁻²]
m_p^Σ	Number of nanoparticles per unit surface	[particles m ⁻²]
M_f	Molar mass fluid molecule	[kg mol ⁻¹]
M_p	Molar mass nanoparticle molecule unit	[kg mol ⁻¹]
$M_{p'}$	Molar mass nanoparticle	[kg mol ⁻¹]
n	Normal vector	[–]
N_A	Avogadro's number	[particles mol ⁻¹]
R_g	Universal gas constant	[J mol ⁻¹ K ⁻¹]
T	Temperature	[K]
Greek symbol		
γ	Surface tension	[N m ⁻¹]
γ_f	Surface tension of fluid	[N m ⁻¹]
γ_T	Temperature derivative of the surface tension	[N m ⁻¹ K ⁻¹]
γ_φ	Volume-fraction derivative of the surface tension	[N m ⁻¹]
Γ_f	Excess surface concentration of fluid	[mol m ⁻²]
Γ_p	Excess surface concentration of nanoparticles	[mol m ⁻²]
Γ_p^Σ	Surface concentration of nanoparticles	[mol m ⁻²]
Γ_b^Σ	Surface-equivalent of bulk concentration	[mol m ⁻²]
$\Gamma_{p,max}^\Sigma$	Maximum surface concentration	[mol m ⁻²]
δ_m	First minimum of potential well	[m]
ϵ_0	Absolute electric permittivity	[CV ⁻¹ m ⁻¹]
ϵ_r	Relative electric permittivity	[–]
ζ_{int}	Zeta-potential interface	[V]
ζ_p	Zeta-potential nanoparticles	[V]
η_f^Σ	Surface chemical potential fluid	[J mol ⁻¹]
η_p^Σ	Surface chemical potential nanoparticles	[J mol ⁻¹]
θ_{NO}	Non-occupied site coverage	[–]
θ_p	Nanoparticle coverage	[–]
ϑ	Contact angle	[°]
λ_0	Decay length in hydra potential	[m]

Table 3 continued

Symbol	Description	Unit
λ_D	Debye's length	[m]
ρ_f	Density of fluid	[kg m ⁻³]
ρ_p	Density of nanoparticles	[kg m ⁻³]
σ_g	Stress tensor gas-side of interface	[N m ⁻²]
σ_l	Stress tensor liquid-side of interface	[N m ⁻²]
ζ_f	Specific surface area of fluid molecule	[m ² per particle]
ζ_{NO}	Specific surface area of non-occupied site	[m ² per particle]
ζ_p	Specific surface area of nanoparticle	[m ² per particle]
φ	Volume fraction	[–]
Φ_m	Total potential energy at first minimum	[J]
$\Phi_{p-p'}^{EDL}$	Repulsive particle-image potential energy	[J]
$\Phi_{p-\Sigma}^{EDL}$	Electrostatic particle-interface potential energy	[J]
$\Phi_{p-\Sigma}^{Hy}$	Hydra potential energy	[J]
$\Phi_{p-\Sigma}^{vdW}$	Van der Waals potential energy	[J]
Φ_t	Total potential energy	[J]
ω_p	Number of adsorption sites for one nanoparticle	[–]
Subscript		
p	Nanoparticle	
NO	Non-occupied site	
f	Fluid	

strength of a fluid is somewhat an unknown. However, works have indicated that for deionized water, typical ionic strength values are measured of the order of $I = 1 \text{ mol/m}^3$ ⁴⁶. This value is assumed for all the fluids used. The values for λ_0 and ζ_p depend strongly on the experimental conditions and only ranges can be indicated. Decay lengths, λ_0 , of values up to 2.2 nm are reported for several systems^{20,37,41}. The zeta-potentials ζ_p of nanodispersions were typically found to be approximately between -75 and -25 mV ^{20,34,43}. Educated guesses, not affecting the analysis in this work, for these two parameters within these indicated ranges are implemented in Table 4 for the calculation of the equilibrium constant. The obtained equilibrium constants for the nanoparticle dispersions are shown later in Table 5.

Reporting summary

Further information on research design is available in the Nature Research Reporting Summary linked to this article.

RESULTS AND DISCUSSION

Comparison of model with experimental data

Gibbs adsorption isotherm $d\gamma = -\Gamma_p d\eta_p^\Sigma$ can now be integrated. We use Eq. (6) for Γ_p (with (19) for θ_p) and Eq. (12) for η_p^Σ . The surface tension of nanoparticle dispersions is finally given by

$$\gamma = \gamma_f + R_g T \Gamma_b^\Sigma \left(\frac{\omega_p + \omega_p K_p (\varphi + K_\Sigma) - K_p K_\Sigma \varphi - \omega_p + \omega_p K_p K_\Sigma - 1}{1 + K_p \varphi} \ln(1 + K_p \varphi) \right) \quad (25)$$

where γ_f is the surface tension of the base fluid, R_g the universal gas constant, T the temperature, K_Σ given by (8), K_p given by (20), ω_p given by (13) and φ the nanoparticle volume fraction. The equilibrium constant is a kinetic parameter obtained by models from the literature, summarised in 'Surface kinetics'. The other parameters are developed in this work using geometric principles and characteristic length scales, which would, for clarity, benefit from a summary in Table 4.

Table 4. Definitions, necessary for the calculation of the surface tension.

Symbol	Definition ^{a,b}			
\mathcal{L}_p	$\frac{2a_p}{3}$	$\frac{2a_p}{3}$	$\frac{a_p h_p}{a_p + h_p}$	—
f_∞	0.547	1	0.907	—
\mathcal{L}_f	—	—	—	$\frac{\ell_f}{3}$
M_p	$\frac{4\pi^2}{9\sqrt{2}} a_p^3 \rho_p N_A$			
$\Gamma_{p,\max}^\Sigma$	$f_\infty \mathcal{L}_p \frac{\rho_p}{M_p}$			
Γ_b^Σ	$\frac{\rho_p}{M_p} \frac{\mathcal{L}_p^2}{\mathcal{L}_f}$			
ω_p	$\frac{M_p \rho_f \mathcal{L}_f}{\rho_p M_f \mathcal{L}_p}$			
K_Σ	$\frac{\Gamma_{p,\max}^\Sigma}{\Gamma_b^\Sigma}$			
K_p	$\frac{\delta_m}{\mathcal{L}_p} \sqrt{\frac{\pi k_B T}{ \Phi_m }} e^{-\frac{\Phi_m}{k_B T}}$			

^aFor the first two rows, the first column stands for spherical nanoparticles, the second column for cubical nanoparticles and the third column for disk-like nanoparticles, while for the third row only the fourth column is used, standing for the fluid molecules.

^bFor the fourth to ninth rows, the definitions are general for all nanoparticle shapes and fluid molecules. The symbol a_p stands either for the radius of a spherical nanoparticle, half of the side of a cubical nanoparticle or the radius of a disk nanoparticle, the latter of which has thickness h_p . Further, ℓ_f is the equivalent radius of a sphere corresponding to the volume of a fluid molecule, while ρ_p , ρ_f , M_p , and M_f stand for the nanoparticle and fluid densities and the nanoparticle and fluid molar masses, respectively. It is worthy to note that it is not necessary to know the molar mass and density of the nanoparticles to calculate the definitions in this Table and that it is mainly a question of size. Nevertheless, the values of ρ_p and M_p (from which M_p is obtained) are still given in Table 1 should one need to know the values of $\Gamma_{p,\max}^\Sigma$ and Γ_b^Σ in terms of unit mass per unit surface. The values of f_∞ have been adapted for the (dl)Au nanoparticles due to the presence of ligands at the gold surface inducing possible repulsion or blocking mechanisms. In ref. ⁴⁷, it has been established that the (dl)Au nanoparticles occupy 0.2, 0.34, and 0.72 of the theoretical maximum coverage when dispersed in D, DD, and HD, respectively. Therefore, for the (dl)Au-D, (dl)Au-DD and (dl)Au-HD systems, f_∞ has been multiplied by 0.2, 0.34, and 0.72, respectively. It is recalled that δ_m and Φ_m represent the primary minimum of the total potential energy and Φ_m its value, whereas k_B and T are Boltzmann's constant and the temperature.

Table 5 shows the nanoparticle dispersions that we consider in this work. For completeness, the calculated numerical parameters that are necessary for determining the surface tension as a function of the volume fraction, i.e. γ_f , K_Σ , ω_p and Γ_b^Σ , are given in Table 5 for these nanoparticle dispersions.

Different kinds of behaviours for the surface tension of nanoparticle dispersions are represented by several experimental case studies, representing different materials (for both the nanoparticles and liquids) with different sizes^{6,9–11,19,38,47,48}. The surface tension is calculated from Eq. (25) for these nanoparticle dispersions and compared to the experimental data in Fig. 3a–f. The experimental data in Fig. 3 show different types of behaviours and the present model has an overall good agreement with those data. This motivates to use the model to explain these observations.

Non-occupancy contribution

We can divide the surface chemical potential, $\eta_p^\Sigma \equiv \eta_p + \eta_{NO}$, in a part that stands for the contribution by non-occupied sites $\eta_{NO} \equiv -\omega_p R_g T \ln(1 - \theta_p)$ and a part that represents the contribution of the adsorbed nanoparticles $\eta_p \equiv R_g T \ln(\theta_p)$. We can also split the surface tension change into two parts as

$\gamma - \gamma_f = \Delta\gamma_p + \Delta\gamma_{NO}$, where

$$\Delta\gamma_p = - \int_0^\varphi \Gamma_p \frac{\partial \eta_p}{\partial \varphi} d\varphi = \int_0^\varphi \left(-\Gamma_b^\Sigma \frac{\partial \eta_p}{\partial \varphi} \right) \left(\frac{\Gamma_p}{\Gamma_b^\Sigma} \right) d\varphi \quad (26)$$

$$\Delta\gamma_{NO} = - \int_0^\varphi \Gamma_p \frac{\partial \eta_{NO}}{\partial \varphi} d\varphi = \int_0^\varphi \left(-\Gamma_b^\Sigma \frac{\partial \eta_{NO}}{\partial \varphi} \right) \left(\frac{\Gamma_p}{\Gamma_b^\Sigma} \right) d\varphi \quad (27)$$

Equations (26) and (27) show the multiplication of two terms in the integral. The term $(-\Gamma_b^\Sigma \frac{\partial \eta_{NO}}{\partial \varphi})$ in Eq. (27) stands physically for the change in the surface chemical potential of non-occupied adsorption sites *per unit surface* upon a change in the nanoparticle bulk concentration. It is worthy to note that this emphasises the influence that non-adsorbed bulk nanoparticles have on the surface chemical potential of non-occupied sites, called here the *non-occupancy effect*. For later use, we assign for this term the following symbol

$$\mathcal{H}_{NO} = -\Gamma_b^\Sigma \frac{\partial \eta_{NO}}{\partial \varphi} \quad (28)$$

A larger *absolute* value of \mathcal{H}_{NO} means a greater non-occupancy effect, i.e. one bulk nanoparticle will have more impact on the surface energy (and thus the surface chemical potential) of the non-occupied sites. Note that an equivalent analysis can be made for the adsorbed nanoparticles contribution (see Eq. (26)) through the term $(-\Gamma_b^\Sigma \frac{\partial \eta_p}{\partial \varphi}) = \mathcal{H}_p$, called the *occupancy effect*. The term $(\frac{\Gamma_p}{\Gamma_b^\Sigma})$ stands for the excess surface concentration normalised by the surface-equivalent of the bulk concentration. We will assign the following symbol to it

$$\mathcal{D}_p = \frac{\Gamma_p}{\Gamma_b^\Sigma} \quad (29)$$

A positive value of \mathcal{D}_p means a high degree of adsorption of nanoparticles (decreasing the surface energy), while a negative value indicates a preference of nanoparticles to remain dispersed in the bulk. In summary, the sign of \mathcal{D}_p indicates whether the surface tension will increase or decrease and the value of \mathcal{H}_{NO} with what amplitude. As both depend on φ , it is easy to understand that the magnitude and variation of the surface tension might be different as a function of φ , generating the different observed trends. More interestingly, Table 5 shows that the several nanoparticle dispersions considered here have quite different values for the nanoparticle equilibrium adsorption constant K_p . This implies that this property plays an important role in determining the behaviour of the surface tension. Note that the parameters \mathcal{D}_p and \mathcal{H}_{NO} also depend on the surface coverage θ_p , which is linked to φ through K_p . This encourages to consider φ and the property K_p as suitable parameters for the present analysis.

We should define a certain reference system that represents a nanoparticle dispersion of which we can change freely the parameters φ and K_p and monitor their influence on the behaviour of \mathcal{H}_{NO} and \mathcal{D}_p and therefore on that of the surface tension. To perform numeric demonstrations, allowing the quantification of our analysis, we may choose data from any dispersion. Only because the B-D system is an example of an interesting decrease-increase behaviour, its data are used for the present demonstration. As the discussion should be followed in a general sense, and we only use the physical properties of this dispersion but changing freely K_p , it is appropriate to name it differently: the reference system R1.

Figure 4a shows the surface tension of the R1 system as a function of φ for various imposed K_p values and two different nanoparticle sizes.

Note that for small K_p values, the surface tension remains significantly constant. As this is counter intuitive (usually non-adsorption should lead to an increase in the surface tension

Table 5. Calculated parameters used in Eq. (25) for the nanoparticle dispersions.

NP-L	γ_f [mN m ⁻¹]	K_Σ [10 ⁻³]	K_p [10 ²]	ω_p [10 ³]	Γ_b^Σ [nmol m ⁻²]	T [K]
Al ₂ O ₃ -W	72.3	2.11	0.0562	6.23	148	300
Al ₂ O ₃ -D	23.8	4.66	11.5	1.28	67.1	300
Al-D	23.8	12.9	3.19	0.165	186	300
B-D	23.8	9.22	4.16	2.08	38.0	300
Al ₂ O ₃ -E	22.4	3.12	0.294	2.85	100	300
Al-E	22.4	8.66	0.103	0.369	279	300
B-E	22.4	6.17	0.0988	4.65	56.8	300
Al ₂ O ₃ -TEG	44.45	10.3	10.3	0.262	190	298
MgO-TEG	44.25	10.3	4.34	0.262	190	298
SiO ₂ -W	72.5	3.51	O (0)	2.24	247	298
Ag-W	68.0	1.05	0.209	24.9	74.1	298
Lap-W	73.6	43.5	193	0.872	85.1	300
ZnO-EG	47.3	2.29	0.0964	5.27	75.9	300
(dl)Au-D	22.96	27.7	8726	0.036	399	303
(dl)Au-DD	24.75	29.2	8.55 * 10 ⁴	0.033	380	303
(dl)Au-HD	26.96	31.8	2.23*10 ⁶	0.027	349	303
Al ₂ O ₃ -Ws	72.3	2.64	O (0)	3.99	185	300

The symbols W, Ws, D, DD, HD, E, TEG, EG and G stand for the base fluids water, extra stabilised dispersion, n-decane, n-dodecane, n-hexadecane, ethanol, triethylene glycol, ethylene glycol, and glycerol, respectively. Lap stands for laponite and (dl)Au for dodecanethiol-ligated gold. Note that K_p values that are orders of magnitude smaller than unity have been considered here as being virtually zero, $O(0)$, i.e. negligibly small.

as this entails that $\Gamma_p < 0$), special attention will be given to the small K_p -case later. Figure 4a shows that, as K_p increases, $\gamma(\varphi)$, for a given φ , first increases and then starts to decrease for small φ , followed by an overall decrease in the depicted φ -range. This first increase is also counter intuitive (usually more adsorption should lead to a decrease of the surface tension), a second point given special attention later. As K_p continues to increase, even a minimum in $\gamma(\varphi)$ as a function of φ is observed, a third point discussed later as well. For even higher K_p , the surface tension shows a decreasing trend, which is what one would expect. Figure 4a also shows that a smaller nanoparticle size tends to favour a decrease in the surface tension. The latter effect can be understood by noticing that smaller nanoparticles will increase, for the same φ , the number of nanoparticles and therefore also the number of adsorbed nanoparticles, which leads eventually (for sufficiently small nanoparticles) to a decrease in the surface tension.

Let us, before entering into such an analysis, first determine what contribution to the surface tension is more important, $\Delta\gamma_p$ or $\Delta\gamma_{NO}$. Figure 4b shows, through $\Delta\gamma_i$ ($i = p, NO$) scaled by $R_g T$, that the contribution of the non-occupied sites ($i = NO$, the solid lines) is the main one, especially at larger K_p -values. The main reason for this is size-related. The nanoparticles are much larger than the fluid molecules, which constitute the adsorption sites. This means that the number of fluid molecules involved in the adsorption of a nanoparticle is quite large, expressed in large ω_p -values, i.e. $\omega_p \gg 1$, as Table 5 shows. So, it is now evident that the non-occupied site contribution of the surface chemical potential will be a key part in the following discussions.

Three counter-intuitive effects of K_p on surface tension

Figure 4c shows $\Delta\gamma_{NO}$ and Γ_p for two volume fractions for the R1 system as a function of K_p . To facilitate the discussion three markers have been introduced for $\Delta\gamma_{NO}$: one corresponding to the K_p from Table 5 for the B-D system ($\equiv K_{p^*}$), a smaller $\frac{K_{p^*}}{1000}$ one and a larger $100K_{p^*}$ one. Figure 4d represents $\Delta\gamma_{NO}$ and Γ_p for two volume fractions as a function of K_p for a so-called R2 system, where we use the data from the Ag-W system, merely to illustrate

that K_p has the same type of effect on the surface tension for whatever nanoparticle dispersion's physical properties. Figure 4e shows \mathcal{H}_{NO} , \mathcal{D}_p and $\mathcal{D}_p \mathcal{H}_{NO}$ (combined contribution of the latter two) versus φ for three K_p values for the R1 system.

For small K_p ($= \frac{K_{p^*}}{1000}$), Fig. 4e shows that \mathcal{D}_p is significantly negative over the whole volume fraction range. Figure 4e shows that at small K_p there is a negligible contribution of the absolute value (being, by the way, always negative) of \mathcal{H}_{NO} (dotted blue line), it is significantly constant over the φ range. Although \mathcal{D}_p is clearly negative (dotted red line in Fig. 4e), which stands for a negative surface excess concentration and would conventionally imply an increase in the surface tension, the resulting surface tension remains significantly constant as shown by Fig. 4a (straight solid lines). To understand why this is, we take the limit of Eq. (25) for $K_p \rightarrow 0$, which gives

$$\gamma_{K_p \rightarrow 0} = \lim_{K_p \rightarrow 0} \gamma = \gamma_f + R_g T \Gamma_b^\Sigma \varphi \quad (30)$$

Filling in Eq. (30) the data for the R1 system reveals that $\gamma_{K_p \rightarrow 0} - \gamma_f = O(10^{-5} - 10^{-4})\varphi$. This explains the seemingly (in reality, very weakly increasing) constant value of the surface tension. The reason behind the seemingly constant value of the surface tension at $K_p \rightarrow 0$ lies in the value of Γ_b^Σ . From Table 4 one may easily deduce that $\Gamma_b^\Sigma \propto \frac{1}{a_p a_f}$. Nanoparticles have generally a larger size than fluid molecules and apparently large enough for Γ_b^Σ to be sufficiently small and hence a seemingly constant behaviour of the surface tension can be predicted. *This explains the first counter-intuitive observation.*

At $K_p = K_{p^*}$, Fig. 4e shows that for a small range of φ we have $\mathcal{D}_p > 0$ (equivalent to $\Gamma_p > 0$, let us recall), while $|\mathcal{H}_{NO}|$ becomes bigger than for the previous case (see solid line in Fig. 4e as opposed to the dotted line). As $\mathcal{H}_{NO} < 0$ (always), this leads to $\mathcal{D}_p \mathcal{H}_{NO} < 0$ (solid line in Fig. 4f). As we increase φ , Fig. 4e shows that \mathcal{D}_p changes sign, i.e. $\mathcal{D}_p < 0$, with $|\mathcal{H}_{NO}|$ still being significantly larger than zero, resulting into $\mathcal{D}_p \mathcal{H}_{NO} > 0$. As the surface tension depends on the integration of $\mathcal{D}_p \mathcal{H}_{NO}$ from 0 to φ , the surface tension will decrease as long as $\mathcal{D}_p \mathcal{H}_{NO} < 0$ and increases as long

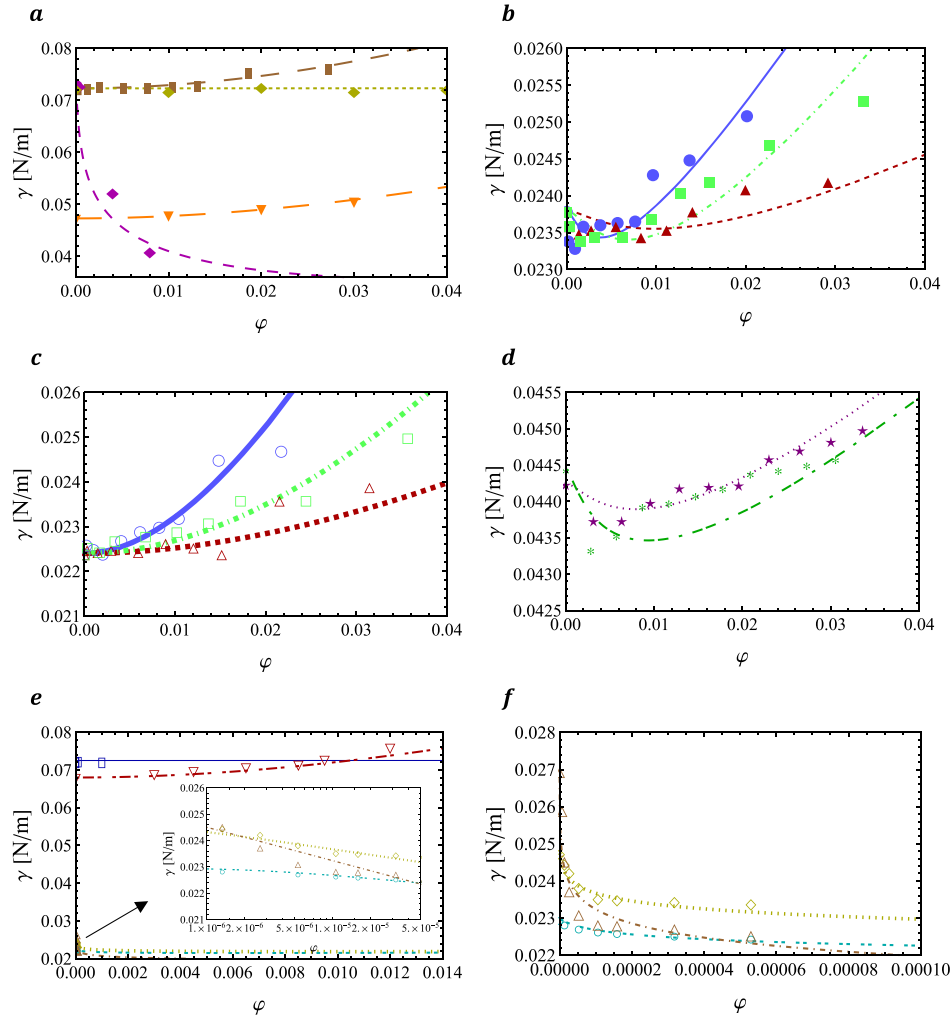


Fig. 3 Modelled surface tension as a function of the volume fraction of nanoparticle dispersions, compared to experimental data^{6,9–11,19,38,47,48}. **a** Al₂O₃-W (—, ■), Al₂O₃-Ws (·····, ◆), Laponite-W (—, ◆) and ZnO-EG (—, ▼), **b** Al₂O₃-D (—, ●), Al-D (—, ▲) and B-D (—, ■), **c** Al₂O₃-E (—, ○), Al-E (—, ▲) and B-E (—, ■), **d** Al₂O₃-TEG (—, *) and MgO-TEG (·····, ★), **e** SiO₂-W (—, □), Ag-W (—, ▼), (dl)Au-D (—, ○), (dl)Au-DD (·····, ◆) and (dl)Au-HD (—, ▲), the inset being a zoom of the (dl)Au-D system concentrating at the region of smaller ϕ -values, **f** a magnification of the systems (dl)Au-D (—, ○), (dl)Au-DD (·····, ◆) and (dl)Au-HD (—, ▲). The studied systems are indicated in the form “nanoparticle-fluid”. The model values are indicated by lines, while the experimental data are given by markers in the form (line,marker).

as $\mathcal{D}_p \mathcal{H}_{NO} > 0$, passing thus through a minimum. This analysis implies that the sign of the integrated surface of $\mathcal{D}_p \mathcal{H}_{NO}$ as a function of ϕ will determine the existence and positioning of a surface tension minimum. It is then logical to elaborate further on the dependence of \mathcal{H}_{NO} and \mathcal{D}_p on ϕ . From Eqs. (6) and (19), we have that

$$\mathcal{D}_p = \frac{K_p \phi}{1 + K_p \phi} K_\Sigma - \phi \quad (31)$$

and from Eqs. (19) and (28) that

$$\mathcal{H}_{NO} \propto -\Gamma_b^\Sigma \frac{K_p \omega_p}{1 + K_p \phi} \quad (32)$$

The analysis of Eqs. (31) and (32) needs some mathematical considerations. From Eq. (31), we can easily deduce that $\mathcal{D}_p = 0$

when $\phi = \frac{K_p K_\Sigma - 1}{K_p}$ or $\phi = 0$, but the latter is a trivial solution not considered further. The sign of \mathcal{D}_p depends on the values of K_p and K_Σ . With respect to this, two cases can be considered: $K_p \leq \frac{1}{K_\Sigma}$ and $K_p > \frac{1}{K_\Sigma}$. These cases will depend on the parameter K_Σ . From Table 4, we can deduce that $K_\Sigma \propto f_\infty \frac{\ell_f}{a_p}$. The values of parameter f_∞ (see Table 4) are constant for a certain shape and K_Σ will depend on the ratio $\frac{\ell_f}{a_p}$ much more than on f_∞ . Therefore, for the discussion of Eq. (31) we will only take into consideration $K_\Sigma \propto \frac{\ell_f}{a_p}$

We treat the case $K_p \leq \frac{1}{K_\Sigma}$. When $K_p \leq \frac{1}{K_\Sigma}$, we have $\frac{K_p K_\Sigma - 1}{K_p} \leq 0$ and it can be verified that this means that for all $\phi > 0$ we have $\mathcal{D}_p < 0$. As \mathcal{H}_{NO} is always negative, the result is a strictly increasing surface tension. Depending on the amplitude of $|\mathcal{H}_{NO}|$, this increase will be significantly measurable or not. Focussing mainly on the value of K_p (the value of which may vary orders of magnitude more than

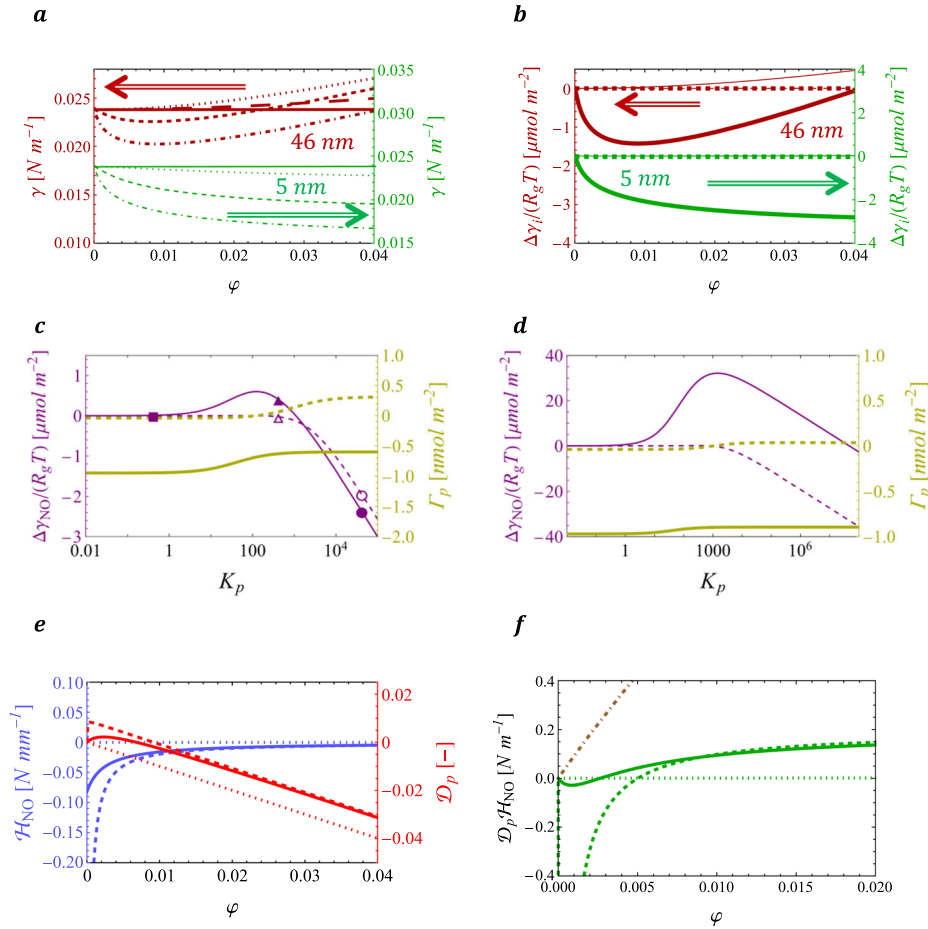


Fig. 4 Analysis of surface tension behaviour. **a** γ of the R1 system vs ϕ for theoretically imposed K_p values (— = ~ 0 , — — = 10, = 10^2 , - - - = 10^3 , - · · = 5×10^3 for $2a_p = 46$ and 5 nm. **b** $\frac{\Delta\gamma_i}{R_g T}$ with $i = p, \text{NO}$ vs ϕ of the R1 system, where thin and thick lines stand for $K_p = 10$ and 5×10^3 , respectively, and dashed and solid lines stand for $i = p$ and $i = \text{NO}$, respectively, for $2a_p = 46$ and 5 nm. Note that all the dashed lines are significantly horizontal. **c** $\frac{\Delta\gamma_{\text{NO}}}{R_g T}$ of the R1 system vs K_p for $\phi = 0.001$ (dashed line) and $\phi = 0.025$ (solid line) and $2a_p = 46$ with three specific values of K_p based on the value from Table 5 ($K_{p^*} = 416$): $\frac{K_{p^*}}{1000}$ (□ for $\phi = 0.001$ and ■ for $\phi = 0.025$), K_{p^*} (▲ for $\phi = 0.001$ and ▲ for $\phi = 0.025$) and $100K_{p^*}$ (○ for $\phi = 0.001$ and ● for $\phi = 0.025$). On the second axis, Γ_p of the reference system vs K_p for $\phi = 0.001$ (dashed line) and $\phi = 0.025$ (solid line) and $2a_p = 46$, **d** $\frac{\Delta\gamma_{\text{NO}}}{R_g T}$ of the R2 system vs K_p for $\phi = 0.001$ (dashed line) and $\phi = 0.025$ (solid line) and $2a_p = 100$. On the second axis, Γ_p of the R2 system vs K_p for $\phi = 0.001$ (dashed line) and $\phi = 0.025$ (solid line) and $2a_p = 100$, **e** \mathcal{H}_{NO} vs ϕ , and \mathcal{D}_p vs ϕ , for three specific values of K_p : $\frac{K_{p^*}}{1000}$ (dotted line), K_{p^*} (solid line) and $100K_{p^*}$ (dashed line) for the R1 system, **f** $\mathcal{D}_p \mathcal{H}_{\text{NO}}$ vs ϕ for three specific values of K_p : $\frac{K_{p^*}}{1000}$ (dotted line), K_{p^*} (solid line) and $100K_{p^*}$ (dashed line) for the reference system and $\mathcal{D}_p \mathcal{H}_{\text{NO}}$ for $K_p = K_{p^*}$ (dot-dashed line) for the Ag-W system.

ω_p and Γ_b^Σ , see Table 5), two cases are thus possible: vanishing K_p values ($K_p \rightarrow 0$) and non-vanishing K_p values ($O(0) \ll K_p \leq \frac{1}{K_\Sigma}$, where $O(0)$ stands for a value that is so low that considering it zero would reflect a measured reality).

o $K_p \rightarrow 0$

Equation (32) shows that for small K_p (e.g. $K_p \rightarrow 0$), we have $|\mathcal{H}_{\text{NO}}| \rightarrow 0$, so that the surface tension increase is not noticeable. This has been discussed previously around Eq. (30) for small K_p values and a real example for this is the SiO₂-W system (see Fig. 3e Table 5 where indeed $K_p \ll \frac{1}{K_\Sigma}$).

o $O(0) \ll K_p \leq \frac{1}{K_\Sigma}$

When K_p is significantly non-zero but not too large, i.e. $O(0) \ll K_p \leq \frac{1}{K_\Sigma}$ (defined as the lower-intermediary region), so that it can

be verified that $|\mathcal{H}_{\text{NO}}|$ has a significant value, the increase of the surface tension will be measurable. A real example for this is the Ag-W system, where Table 5 shows that $K_p \gg O(0)$ and $K_p < \frac{1}{K_\Sigma}$. Moreover, Fig. 4f illustrates this as well by a continuously increasing $\mathcal{D}_p \mathcal{H}_{\text{NO}}$ (brown dot-dashed line). Departing from a fully desorbed case ($K_p \rightarrow 0$), we can say that upon enhancement ($K_p \gg O(0)$) of the surface adsorption kinetics (up to the limit $K_p \leq \frac{1}{K_\Sigma}$), the surface tension behaviour becomes a strictly increasing one due to the combination of $\mathcal{D}_p < 0$ and a significant value of $|\mathcal{H}_{\text{NO}}|$. So, initially, a higher adsorption appears not to lead to a lower but rather to a higher surface tension. As $\frac{1}{K_\Sigma} \propto \frac{a_p}{\ell_f}$, nanoparticles (having much higher size than the fluid molecules) allow for a much larger limit for K_p for which \mathcal{D}_p remains negative. So, within this limit, upon increasing K_p , the strength of the non-occupancy effect $|\mathcal{H}_{\text{NO}}|$ becomes significant, whilst the excess surface concentration remains $\mathcal{D}_p < 0$, resulting into a surface

tension increase and not decrease. This explains the second counter-intuitive observation.

We treat the case $K_p > \frac{1}{K_\Sigma}$. When $K_p > \frac{1}{K_\Sigma}$, we have a particular situation where $\mathcal{D}_p > 0$ (and therefore a decreasing surface tension) for $0 < \varphi < \frac{K_p K_\Sigma - 1}{K_p}$ and $\mathcal{D}_p < 0$ (increasing surface tension) for $\varphi > \frac{K_p K_\Sigma - 1}{K_p}$, where we limit φ to a certain maximum value φ_{\max} , considered reasonable for typical nanoparticle dispersions (as discussed later). It can be verified that the surface tension is strictly decreasing if $\frac{K_p K_\Sigma - 1}{K_p} \geq 1$, which means for $K_\Sigma \geq 1 + \frac{1}{K_p}$. This gives two regions, the one given by the latter condition and $K_\Sigma < 1 + \frac{1}{K_p}$.

$$\circ K_\Sigma < 1 + \frac{1}{K_p}$$

The values given in Table 5 show that for nanoparticle dispersions typically $K_\Sigma \ll 1$. This means that $K_p \gg 1$. The smaller $\frac{K_p K_\Sigma - 1}{K_p}$ (due to larger nanoparticles as $K_\Sigma \propto \frac{\ell_i}{a_p}$ or due to lower K_p) is, the closer the value of φ for which \mathcal{D}_p changes sign will be to zero. As a consequence, this fits within the typical operating φ -ranges ($\varphi < \varphi_{\max}$), resulting into an observable minimum for the surface tension. This is the case for e.g. the B-D, Al-D, Al₂O₃-D systems (see Fig. 3b and Table 5 for the values). As, however, $\frac{K_p K_\Sigma - 1}{K_p}$ becomes somewhat larger (smaller nanoparticles or higher K_p) the φ for which \mathcal{D}_p changes sign will increase and may fall out of the aforementioned typical operating φ -ranges ($\varphi > \varphi_{\max}$). This results into a minimum that is no longer observed (mathematically still present, but experimentally not observed within typical φ -ranges) and the surface tension is *virtually* decreasing. This can also be numerically verified in Table 5 and visually in Fig. 3a for e.g. the Lap-W system. For systems with even higher K_p , Eq. (32) shows that $|\mathcal{H}_{\text{NO}}|$ as well as the negative part of $\mathcal{D}_p \mathcal{H}_{\text{NO}}$ become more important, confirmed by the $100K_p$ case for the R1 system in Fig. 4(e) and (f) (dashed lines). The (dl)Au dispersions (see again Table 5 and also Fig. 3(e) and (f)) illustrate this situation by presenting surface tensions that decrease quickly for very low volume fractions. In summary, this means that an observable surface tension minimum is the result of a delicate balance between a sufficiently large, but not too small, nanoparticle (through $K_\Sigma \propto \frac{\ell_i}{a_p}$) and a sufficient amount of adsorption (through $K_p > \frac{1}{K_\Sigma}$). This effect is therefore not an external one but stems from the same parameters that cause strictly increasing or decreasing behaviours, merely because the conditions are right. This explains the third counter-intuitive observation.

$$\circ K_\Sigma \geq 1 + \frac{1}{K_p}$$

Mathematically speaking, a strict decrease (over the whole range $0 < \varphi < 1$) in the surface tension would occur if, next to $K_p > \frac{1}{K_\Sigma}$, we have $K_\Sigma \geq 1 + \frac{1}{K_p}$. We have mentioned earlier that typically $K_p \gg 1$. This means that, as approximation, we are practically dealing here with the condition $K_\Sigma \geq 1$, which entails that $a_p \leq O(\ell_i)$. This would besides possibly quantum dots or surfactants, be rather untypical for nanoparticle dispersions. Therefore, this case can be disregarded as well for nanoparticle dispersions in general.

Trends and comments







In fine, it seems that the right combination between adsorption strength (K_p) and nanoparticle size (a_p of which the main effect is represented by the parameter K_Σ) is responsible for the different behaviours. Table 6 shows a summary of the different surface tension behaviours as a function of the parameters K_p and K_Σ , in the form of the product $K_p K_\Sigma$.

Table 6 shows that as one goes from left to right, the value of $K_p K_\Sigma$ increases by several orders of magnitude. This is by either increasing K_p , K_Σ or both. Table 5 shows that K_Σ for all the nanoparticle dispersions is of the order of 10^{-2} – 10^{-3} . This means that when $K_p K_\Sigma$ increases several orders of magnitude, this is mainly due to K_p . Nevertheless, for quantitative assessments, it is more convenient to mention $K_p K_\Sigma$.

In order to put the results in perspective, some additional comments are in place here. In the case $K_p > \frac{1}{K_\Sigma}$ and $K_\Sigma < 1 + \frac{1}{K_p}$, we have made a distinction for the surface tension behaviour between three ranges of orders of magnitude for $K_p K_\Sigma$. *Mathematically*, these three cases represent all a minimum in the surface tension somewhere in the range $0 < \varphi < 1$. The reason for making the three distinctions is on a conceptual level, involving measured data and a defined framework. As Fig. 3 shows, most of nanoparticle dispersions that are used for engineering purposes (one might also think of medical ones as well, for that matter) present *operating conditions* that involve φ values that are often limited by a value φ_{\max} that is of the order of $\varphi_{\max} \approx O(10^{-2})$ or slightly higher, but still $\varphi_{\max} < O(10^{-1})$. In Table 6, φ_{\max} is schematically indicated for the case $K_p > \frac{1}{K_\Sigma}$ and $K_\Sigma < 1 + \frac{1}{K_p}$ by blue vertical dotted lines, set to a same hypothetical value for the three images in question. It shows that as $K_p K_\Sigma$ increases the minimum of the surface tension becomes less pronounced and shifts towards higher φ values (not on scale), falling out of the range limited by φ_{\max} . At φ values beyond φ_{\max} it is the question whether we can still speak of dispersions and we then might have to deal with another type of “fluid” with additional phenomena at the surface. When working with nanoparticle dispersions, we have limited the analysis within the range $0 < \varphi < \varphi_{\max}$ (named the “operating range”). As such, depending on the value of $K_p K_\Sigma$, the mathematical minimum of the surface tension may well be out of that range and therefore not observed nor experimentally measured. Then, it is justified to indicate conditions (that is, within the range $0 < \varphi < \varphi_{\max}$), where we can observe a minimum in the surface tension (for $K_p K_\Sigma \approx O(10^0 - 10^1)$) and where we observe a virtual decrease. Even for the virtual decrease of the surface tension, we have made a distinction between a “soft” decrease ($K_p K_\Sigma \approx O(10^2 - 10^3)$) and a “steep” decrease ($K_p K_\Sigma \approx O(10^4 - 10^6)$), the upper limit 10^6 being indicative with respect to the observed experiments, but may conceptually be even higher). The soft decrease is defined as the surface tension having a steady decrease over the whole operating range, such as the Lap-W case. The steep decrease is characterised by a strong decrease of the surface tension for $\varphi \ll O(\varphi_{\max})$ with a seemingly constant value afterwards, such as the dl(Au) dispersions.

For the parameter K_Σ , we have mentioned that for nanoparticles we have $K_\Sigma \propto \frac{\ell_i}{a_p}$, not considering f_∞ in the discussions. There are, however, cases where this parameter may play a role. When strong repulsive forces are present or when the nanoparticle surfaces (because of their nature or their functionalization) are such that we cannot consider them as hard spheres, the maximum coverage may, respectively, decrease or increase, whereas the shape may also be altered by the stretching or compressing of the adsorbed nanoparticles. In such cases, additional considerations should be made in order to include these forces between nanoparticles⁴⁹. One may say that these forces will be effective there where the nanoparticles are present at the interface, so that the surface tension of particle-laden interfaces is argued to be an effective magnitude⁴⁹. In some cases, the nanoparticles are grafted with polymers, which may cause additional effects on the surface tension due to the dangling chains of the polymers⁵⁰. When ions are present (one may think of electrolytes or charged organic molecules) strong coulomb interactions may also influence the maximum coverage.

Table 6. Surface tension behaviours as function of K_p (adsorption) and K_Σ (size).

	$K_p \leq \frac{1}{K_\Sigma}$		$K_p > \frac{1}{K_\Sigma}$				
$\{K_p, K_\Sigma\}$	$K_p \rightarrow 0$	$O(0) \ll K_p \leq \frac{1}{K_\Sigma}$	$K_\Sigma < 1 + \frac{1}{K_p}$		$K_\Sigma \geq 1 + \frac{1}{K_p}$		
$\gamma(\varphi)$							Irrelevant for nanoparticle dispersions: untypical a_p
$O(K_p K_\Sigma)$	$O(0)$	$10^{-2} - 10^{-1}$	$10^0 - 10^1$	$10^2 - 10^3$	$10^4 - 10^6$		

The effect of the nanoparticle size has been mainly expressed through the parameter K_Σ . It should be recalled that the nanoparticle size also figures in the parameter ω_p . The parameter ω_p (standing for the number of adsorption sites) can also quantitatively interfere with the magnitude of the surface tension change through its linear relation with the non-occupancy effect Eq. (32). Moreover, the parameter ω_p , when much larger than unity, is responsible for the non-occupancy effect to outnumber the occupancy effect through the surface chemical potential (see Eq. (12)). Should it be around unity, the free energy contribution of the adsorbed nanoparticles would also be important for the chemical potential and our discussion would be different. Nevertheless, once it is established that for nanoparticles generally $\omega_p \gg 1$, and that the variation of K_p is, as mentioned earlier, of far more importance for the non-occupancy effect, the variation of the parameter ω_p is not given more attention in our analysis.

The size of the nanoparticles also matters from another point of view. The projection method necessitates that the radius of curvature (reciprocal of the curvature) should be much larger than the nanoparticle radius. In other words, the interface should be “flat” with respect to the size of the nanoparticles. If the pressure difference over the interface is negligible, Young’s equation (where the pressure difference is related to the surface tension and the interface curvature) predicts that such an assumption would be realistic.

In ‘Representation of an interfacial layer on a dividing surface’, we mentioned that we used half the surface to calculate the volume-to-surface ratio. A heuristic reason was employed for this, assuming that only half the surface facing the dividing surface would matter in the adsorption process for particles that are much larger than the fluid molecules that constitute the adsorption sites. As a verification, we performed surface tension calculations using cases with a fourth, a sixth and the whole particle’s surface to calculate the volume-to-surface ratio. It appeared that the heuristic choice we have made for the calculation of the volume-to-surface ratio, i.e. using half the nanoparticle’s surface, was the most appropriate one with respect to the experimental data. It would be interesting to investigate the degree of this participating surface experimentally. However, for this work, the heuristic choice we have made appeared to be sufficient.

It should be noted that the way K_p has been calculated assumes that it is enough to take into account the wettability of the nanoparticles in the potential energy. The DLVO theory is known to be used for adsorption on solid-liquid interfaces. In refs.^{24,51} as well as in the present work, it is assumed that the DLVO theory, albeit extended, is applicable for liquid-fluid interfaces as well. Although already used by others^{24,51}, such a kinetic model should

be studied in more details. In addition, it would be encouraged to provide benchmark studies with experimental data on the adsorption coefficients of various nanoparticle adsorption on liquid–air (fluid) interfaces.

Finally, the present model considers the adsorption of nanoparticles alone in order to focus on this phenomenon. It would be interesting to generalise or adapt Eq. (3) for the inclusion of the adsorption of molecular species, which could generalise the model for the application of studying the surface tension of solutions containing surfactants or other (in)organic molecules. Should multiple adsorption occur, the thermodynamic model presented in this work lends itself to be extended starting, most importantly, from an adaptation of Eq. (3).

Mapping of the surface tension behaviour

The previous analysis has shown a general dependence of the surface tension behaviour on $K_p K_\Sigma$, where K_Σ and K_p stand for the effect of nanoparticle size and adsorption strength, respectively. In order to quantify this dependence and map these behaviours, we choose four representative systems, having, respectively, seemingly constant, strictly increasing, minimum containing and virtually decreasing behaviours for the surface tension. Figure 5a shows the values of \mathcal{D}_p , $|\mathcal{H}_{NO}|$ and $\mathcal{D}_p \mathcal{H}_{NO}$ for these four nanoparticle dispersions, at two volume fractions, that have distinct behaviours with low to high $K_p K_\Sigma$ in the following order: $\text{SiO}_2\text{-W} < \text{Al}_2\text{O}_3\text{-W} < \text{B-D} < \text{Lap-W}$. Figure 5a shows that, although $\text{SiO}_2\text{-W}$ and $\text{Al}_2\text{O}_3\text{-W}$ have comparable negative \mathcal{D}_p values, $\mathcal{D}_p \mathcal{H}_{NO}$ is only significant for $\text{Al}_2\text{O}_3\text{-W}$ due to a much higher $|\mathcal{H}_{NO}|$, confirming the analysis in the previous section, which means a non-measurable increasing surface tension for $\text{SiO}_2\text{-W}$ and a measurable one for $\text{Al}_2\text{O}_3\text{-W}$. As $K_p K_\Sigma$ increases, i.e. for B-D, we can see a positive \mathcal{D}_p for $\varphi = 0.005$ and a negative one for $\varphi = 0.01$. As the value $|\mathcal{H}_{NO}|$ is significant enough, this results into a visibly negative $\mathcal{D}_p \mathcal{H}_{NO}$ for $\varphi = 0.005$ and a positive one for $\varphi = 0.01$, meaning first a decrease and then an increase in the surface tension. For even larger $K_p K_\Sigma$, i.e. for Lap-W, we can see a positive \mathcal{D}_p for both φ 's. With a large $|\mathcal{H}_{NO}|$, $\mathcal{D}_p \mathcal{H}_{NO}$ is considerably negative for both φ 's, corresponding to a virtually decreasing surface tension behaviour that was observed for Lap-W.

In the present study, we aimed at proposing a framework, model and explanation dealing with the different behaviours of the surface tension of nanoparticle dispersions. We have seen that the adsorption strength ($K_p K_\Sigma$) and the nanoparticle size (through K_Σ) collaborate or compete in determining these different tendencies. It is then interesting to map the surface tension behaviours of all the nanoparticle dispersions that were presented in Fig. 3 as a function of K_p and K_Σ . Such a mapping is presented in Fig. 5b and gives the opportunity to tailor nanoparticle

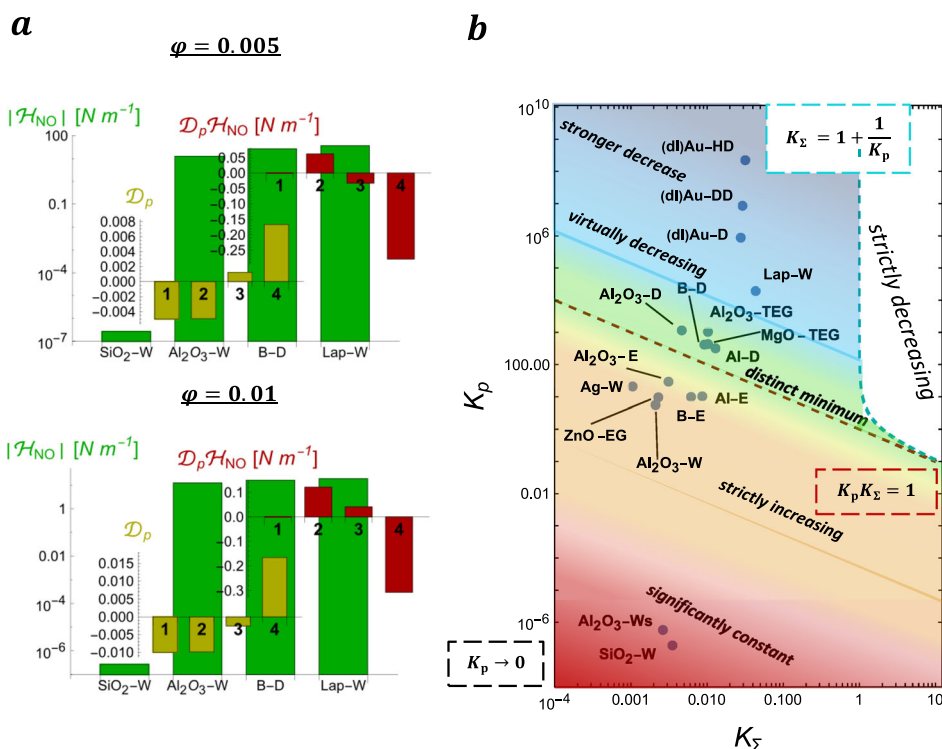


Fig. 5 Mapping of surface tension behaviour. **a** Competition of key parameters $|\mathcal{H}_{\text{NO}}|$, \mathcal{D}_p and $\mathcal{D}_p \mathcal{H}_{\text{NO}}$ for the nanoparticle dispersions SiO₂-W (1), Al₂O₃-W (2), B-D (3) and Lap-W (4) for two volume fractions: $\varphi = 0.005$, $\varphi = 0.01$. Note that for a better visualisation both the values of \mathcal{D}_p and $\mathcal{D}_p \mathcal{H}_{\text{NO}}$ for only the Lap-W system have been divided by 5 and 2 for the cases $\varphi = 0.005$, $\varphi = 0.01$, respectively. **b** All the considered nanoparticle dispersion systems are resumed in a $K_p - K_\Sigma$ map, representing five observed γ -vs- φ behaviours: “significantly constant” where the change (proven to be mathematically an increase) in γ is not observable (less than 1%) on the 1 mN/m range, “strictly increasing” where $\partial_\varphi \gamma > 0$ over any φ -range, “distinct minimum” where a clear minimum is visible at operating φ ranges and “stronger decrease” where $\partial_\varphi \gamma$ decreases distinctly steeper than the previous case. It is to be reminded that the latter three cases are distinguished within the φ -range under which typical nanoparticle dispersions are used. Moreover, the latter two cases are conceptually the same but are distinguished for application or engineering purposes: much higher adsorption kinetics and/or smaller nanoparticles induce (although theoretically having the same tendency) for the observer a decrease that is much steeper and occurs at much lower nanoparticle concentrations, which justifies to make a distinction between them. The colours indicate qualitatively the transition from one region to another, whereas the model gives two mathematical limits: the limit $K_p K_\Sigma = 1$ (red dashed line) designates formally the crossover from $\partial_\varphi \gamma|_{\varphi \rightarrow 0} > 0$ to $\partial_\varphi \gamma|_{\varphi \rightarrow 0} < 0$, while the limit $K_\Sigma = 1 + \frac{1}{K_p}$ (blue dashed line) stands for the crossover from $\partial_\varphi \gamma|_{\varphi \rightarrow 0} < 0$ to $\partial_\varphi \gamma|_{\varphi \rightarrow 0} < 0$. Interestingly, **b** shows that the dispersions seem to correspond to sets of simultaneously increasing K_p and K_Σ , indicated by the left-to-right diagonally up-going set of points. This confirms the link between $K_p K_\Sigma$ and the behaviour of the surface tension.

dispersions, e.g. through size (affecting K_Σ) and surface properties (affecting K_p , since the surface of the nanoparticles have a direct influence on their adsorption strengths), for the envisioned effect of the surface tension.

DATA AVAILABILITY

The data in this study are available upon reasonable request.

CODE AVAILABILITY

The commercial software Mathematica has been used to analyse the results.

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AUTHOR CONTRIBUTIONS

H.M. developed the model, performed the calculations and comparison with experimental data, analysed the results, wrote and approved the manuscript.

COMPETING INTERESTS

The author declares no competing interests.

ADDITIONAL INFORMATION

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