

VANE-PROBE INTERACTIONS IN TRANSONIC FLOWS

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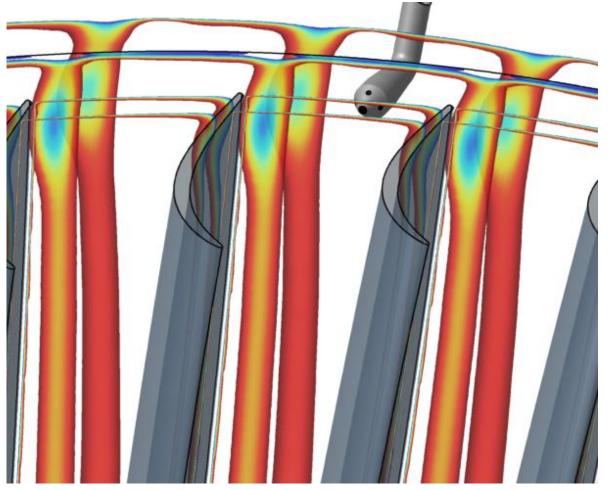
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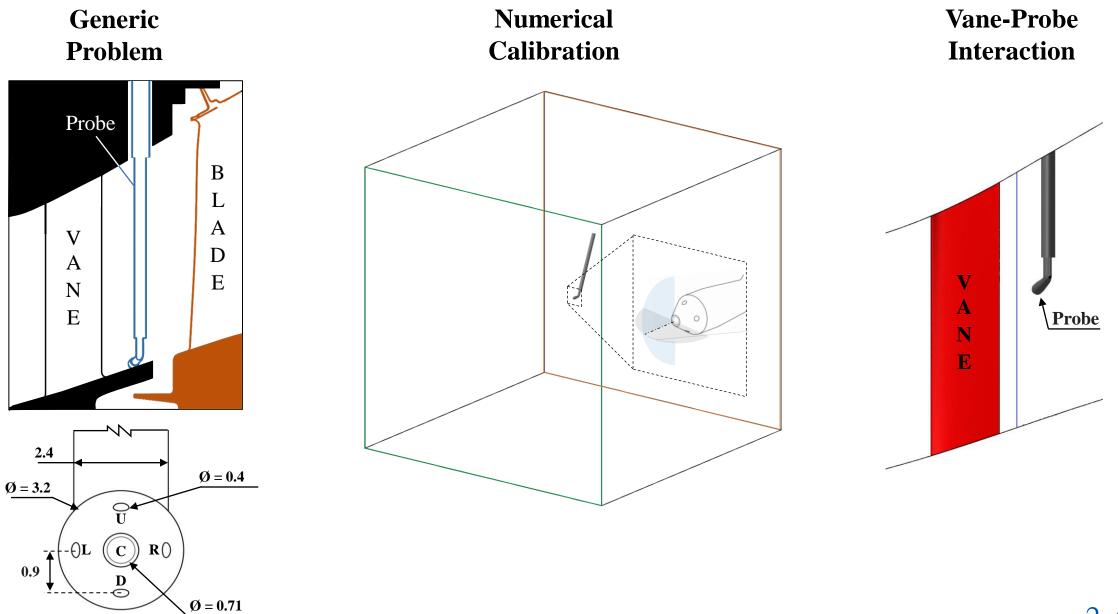
Motivation



□ Higher intrusiveness at transonic Mach numbers

- Probe measurements error due to velocity gradients
- Objective: interaction between vane and probe at transonic Mach numbers posing the attention on the effect on the measured quantities

Methodology



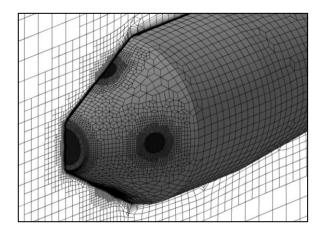
Numerical Calibration

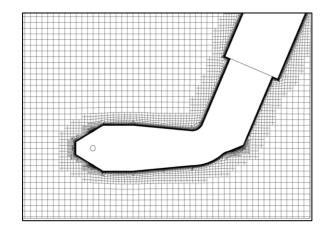
Numerical setup

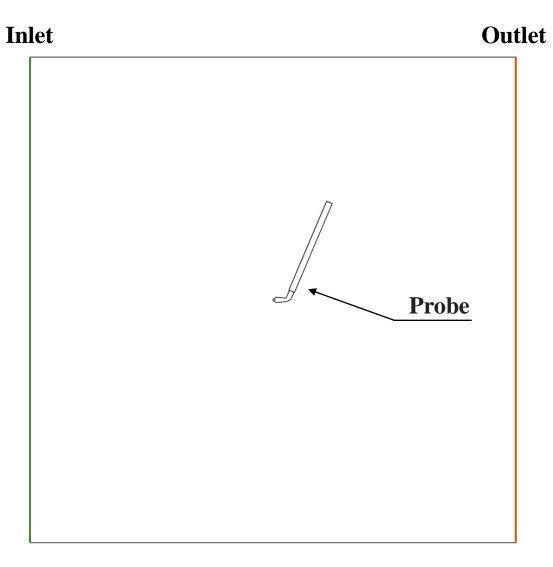
□ Top, bottom and side surfaces set as periodic

 \Box Unstructured mesh size is ~3M cells (y+ < 1)

RANS on Numeca FineOpen 8.2







Numerical Calibration

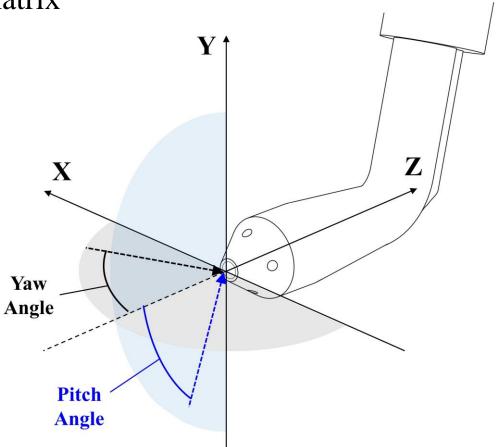
□ Inlet flow angle varied to match the calibration matrix

□ Fixed inlet total pressure

• Outlet static pressure to adjust the Mach

	Min	Max	Step
Pitch angles	-15°	15°	5°
Yaw angles	0°	15°	5°
Mach numbers	0.55 - 0.70 - 0.8 - 0.9 - 0.95		

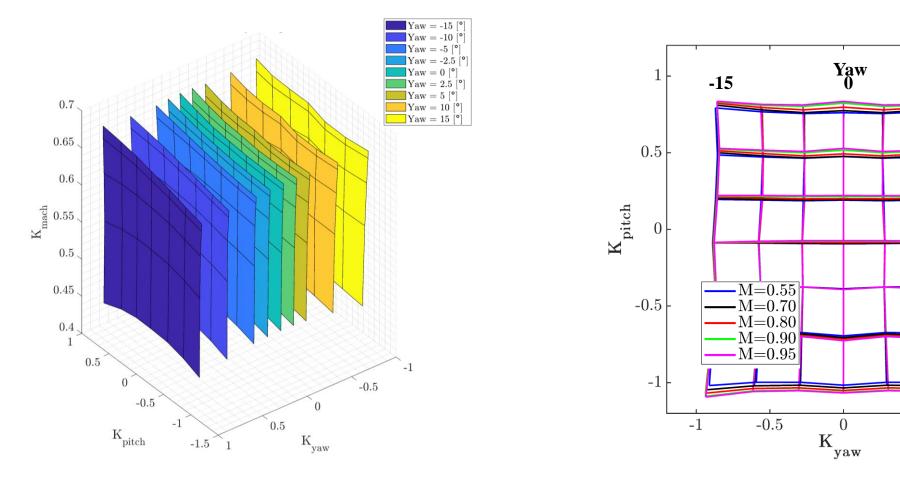
140 calibration points



Numerical Calibration

Calibration Results

 \Box Calibration coefficients (K_{yaw} , K_{pitch} , K_{Mach} and K_{tot}) used to build calibration maps



15 -15

> 0 Pitch

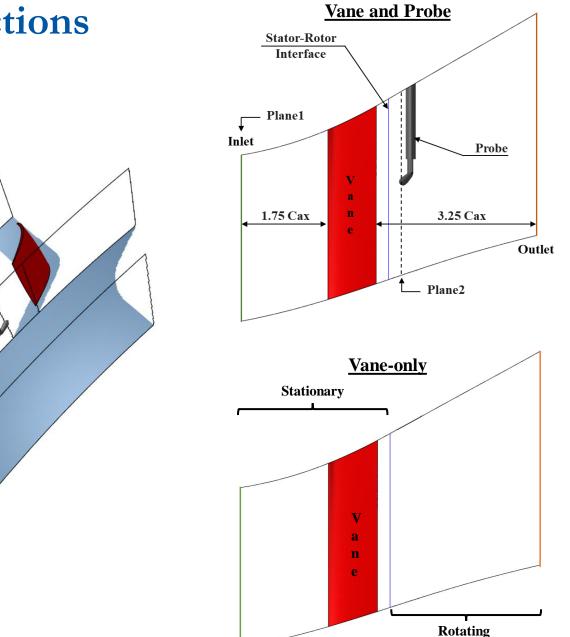
> > 15

1

0.5

Numerical Setup

- □ Two numerical setups
 - □ Vane and probe
 - □ Vane-only
- □ Rotating probe domain
- $\Box \quad \text{Stator-to-Rotor Periodicity} = 8:1$
- □ Probe traverse at 14 spanwise locations



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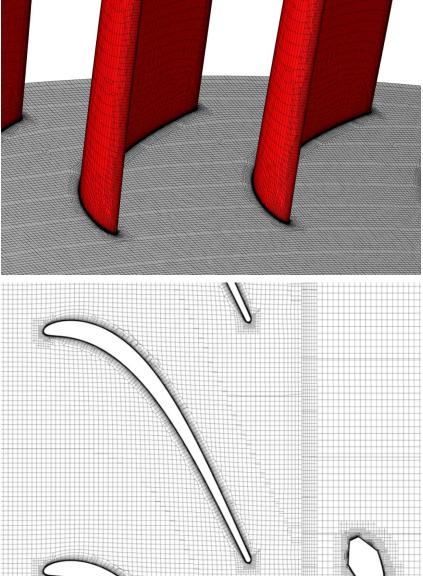
Mesh and operating conditions

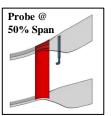
 \Box Unstructured mesh size is ~11M cells (y+ < 1)

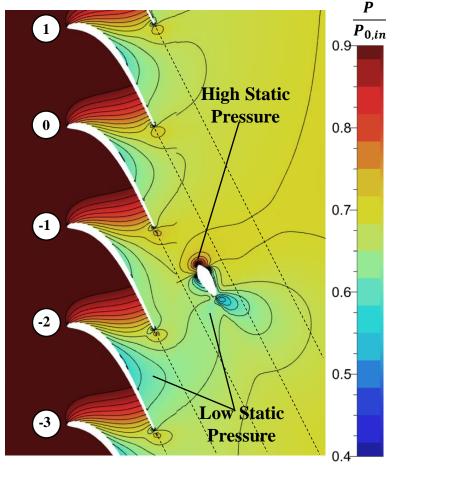
□ NLH on Numeca FineOpen 8.2

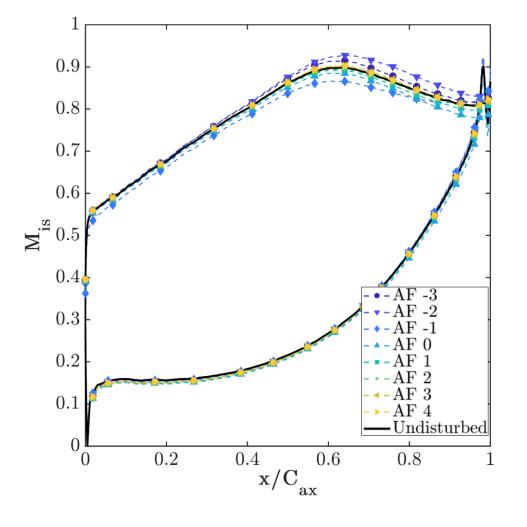
5 Harmonics

Parameter	Value
Reynolds number (vane outlet and C_{ax}), Re	~1.7 x 10 ⁵
Vane exit Mach number, <i>M</i>	0.8



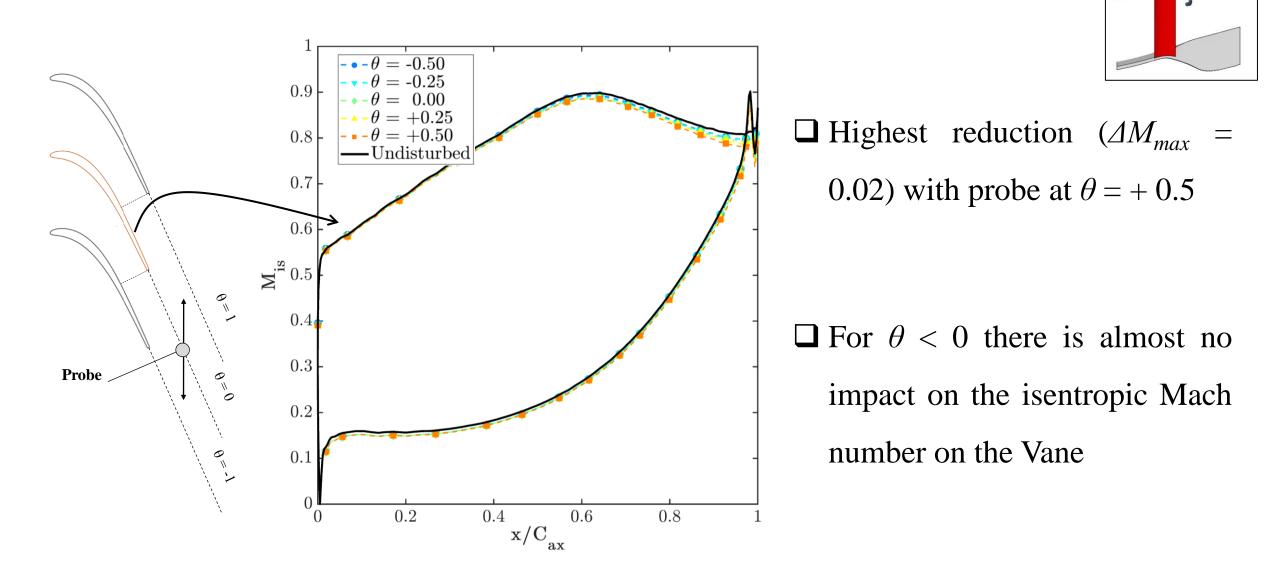






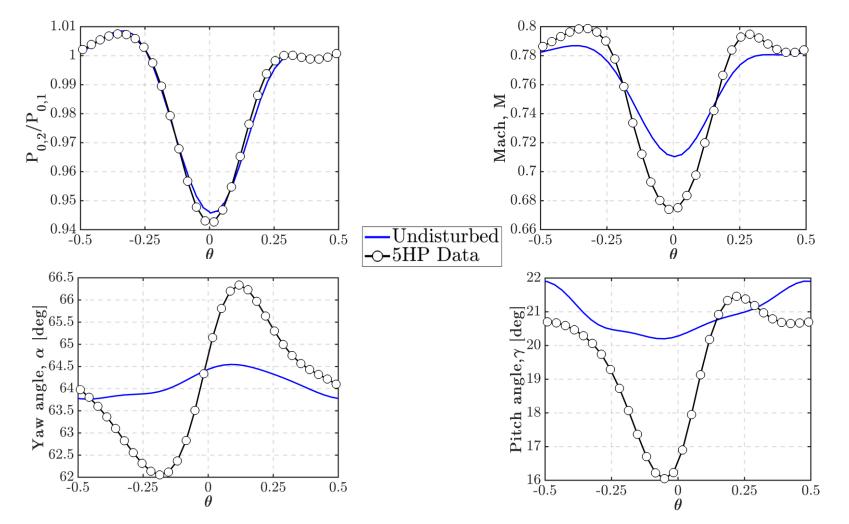
Effect on the flow-field – Probe at mid-passage

- □ High static pressure increase the pressure at exit of nozzle (Vanes -1 to 1)
- □ Low static pressure interacts with Vane -2 and -3 promoting expansion through the nozzle

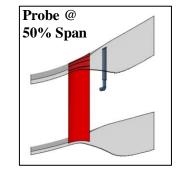


Probe @ 50% Span

Probe traverses at midspan



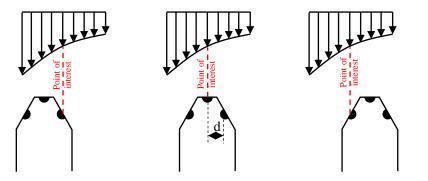
Noticeable short-fallings of the probe on the measured quantities except for the Total pressure measurements



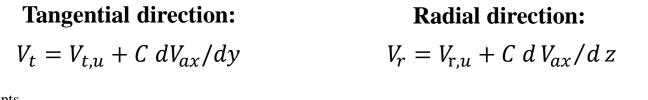
Correction procedure

Two step correction (Ligrani et al.)

1. Compensate the spatial displacement between side holes and central hole

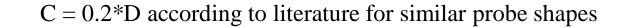


2. Compensate for transversal velocity rising when blunt bodies are immersed in shear flows:





 $V_{t,u} V_{r,u}$ = uncorrected velocity components $V_t V_r$ = corrected velocity components V_{ax} = axial velocity components



Ligrani, P. M., Baun, L. R., & Singer, B. A. (1989). Spatial resolution and downwash velocity corrections for multiple-hole pressure probes in complex flows. Experiments in Fluids, 7(6), 424-426 Chernoray, V., & Hjärne, J. (2008, January). Improving the accuracy of multihole probe measurements in velocity gradients. In Turbo Expo: Power for Land, Sea, and Air (Vol. 43123, pp. 125-134). 1 / 21

Correction procedure

□ Introduced a wake at the inlet of the domain

 \Box Inlet angle = 0 deg.

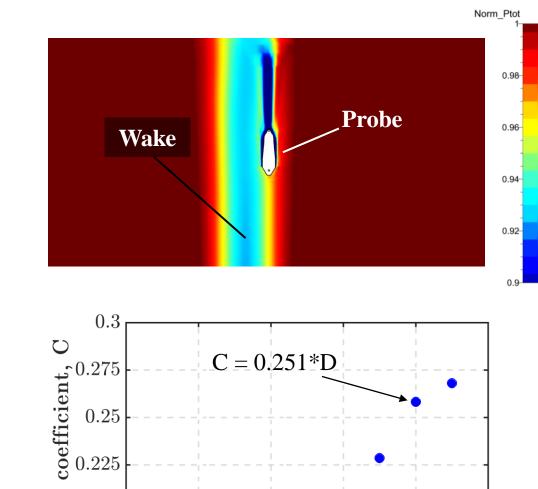
Tests:

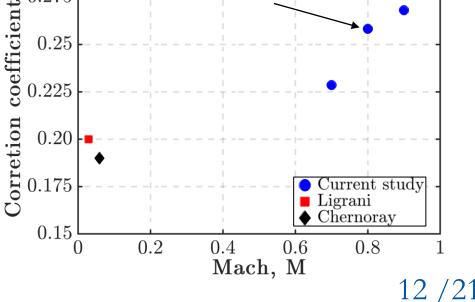
□ M=0.7 □ M=0.8 (nominal Mach) □ M=0.9

Pressure taps spatial displacement correction

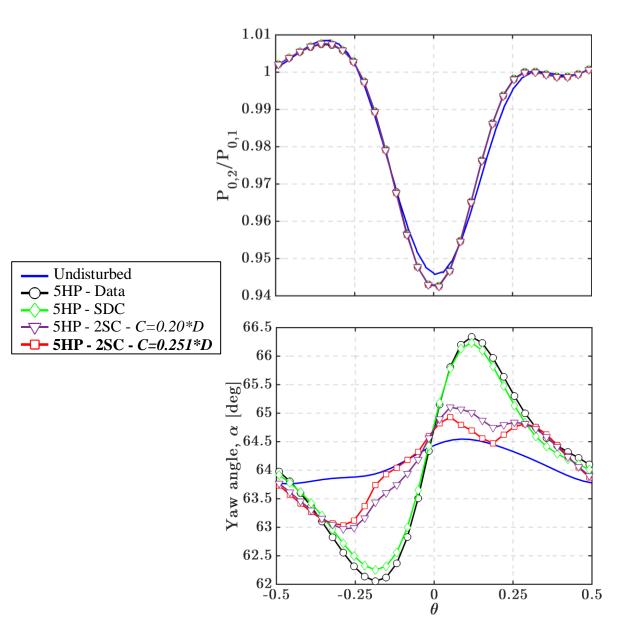
Definition of the correction coefficient

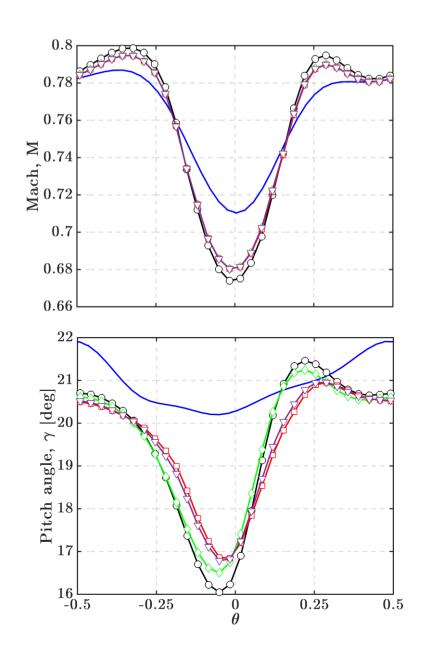
$$C = \frac{-V_{tu}}{\frac{dVax}{dy}D}$$

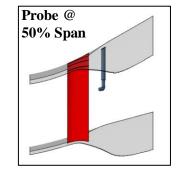




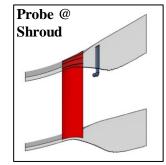
Probe traverses at midspan

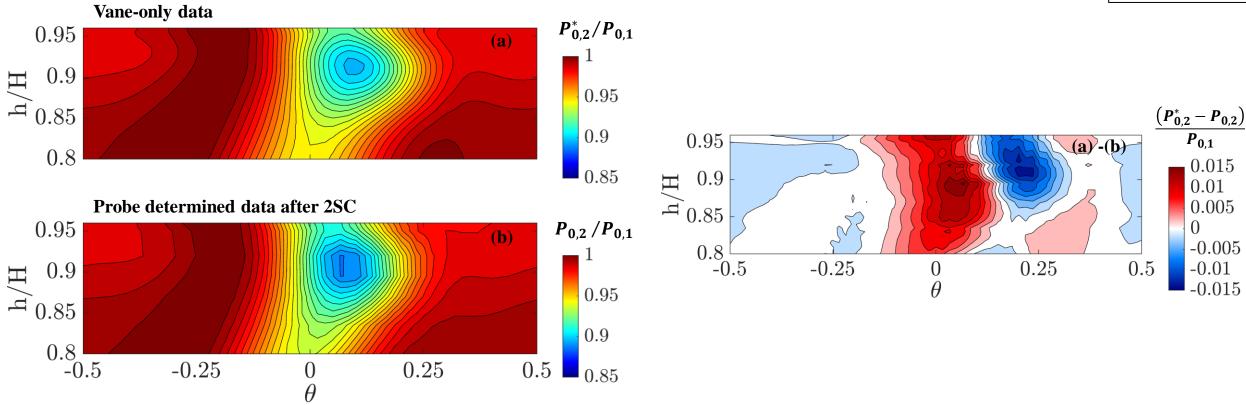




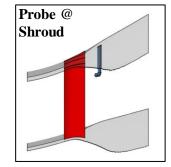


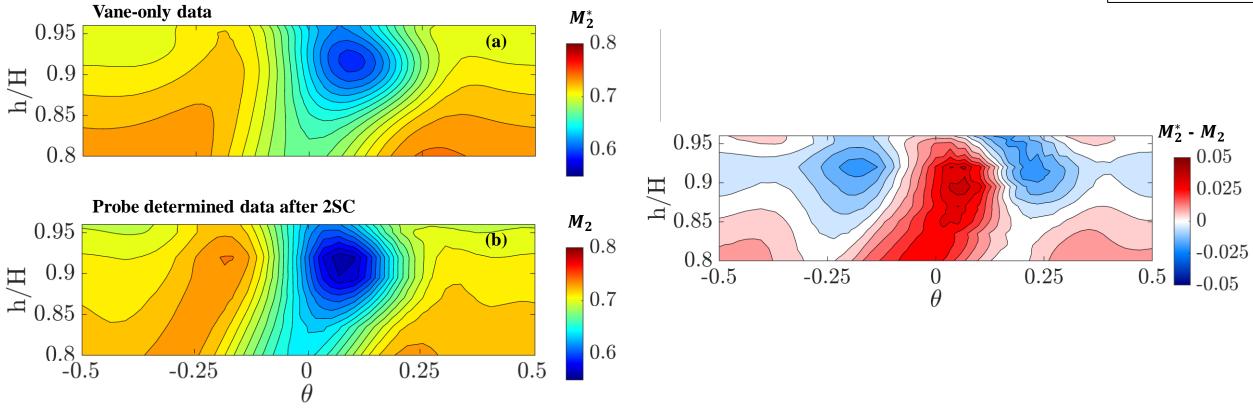
Probe traverses at shroud



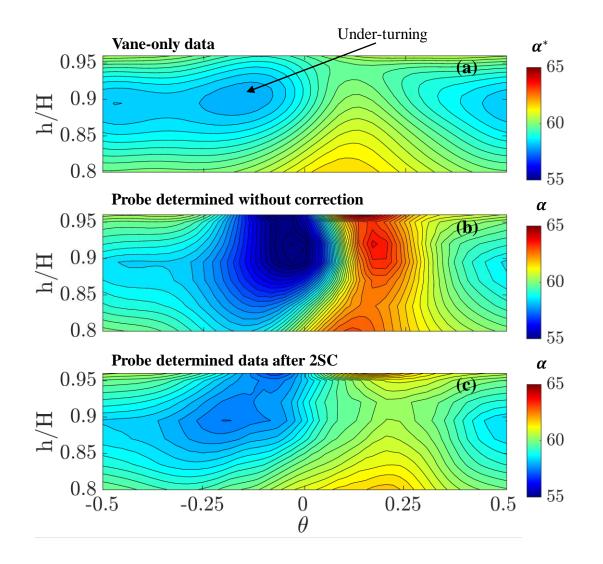


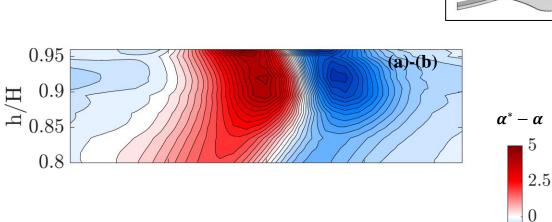
Probe traverses at shroud

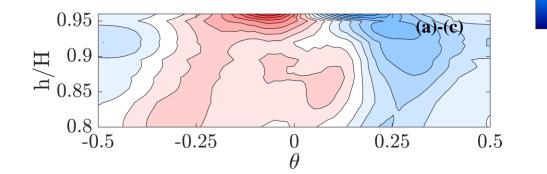


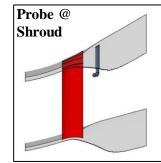


Probe traverses at shroud





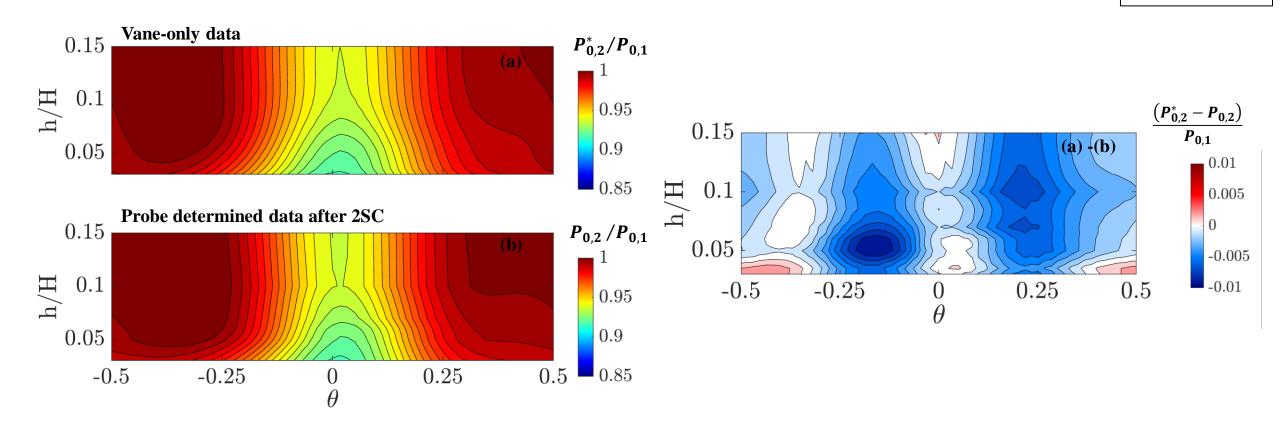




-2.5

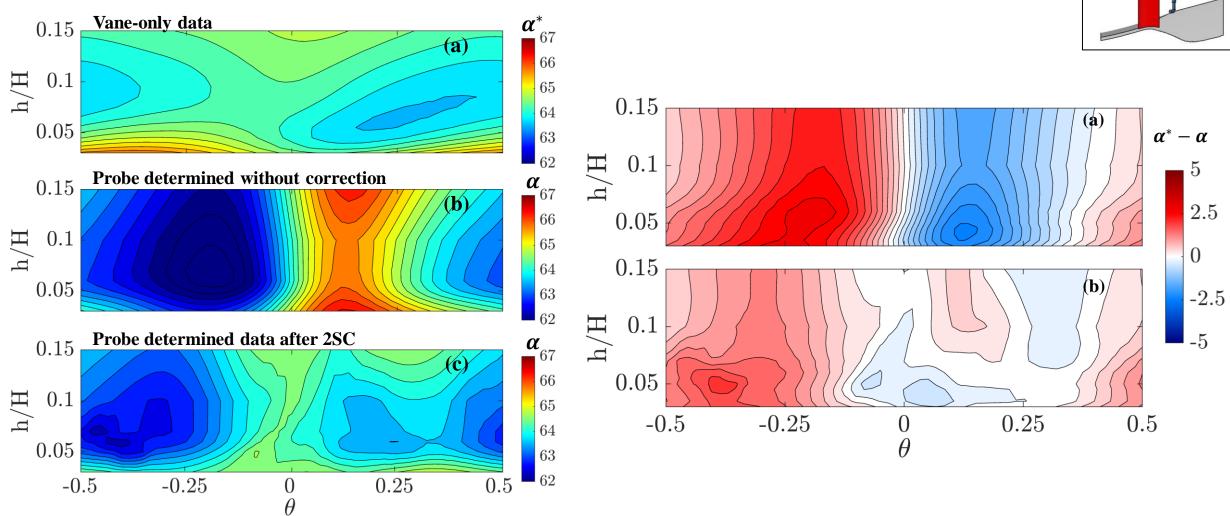
-5

Probe traverses at hub



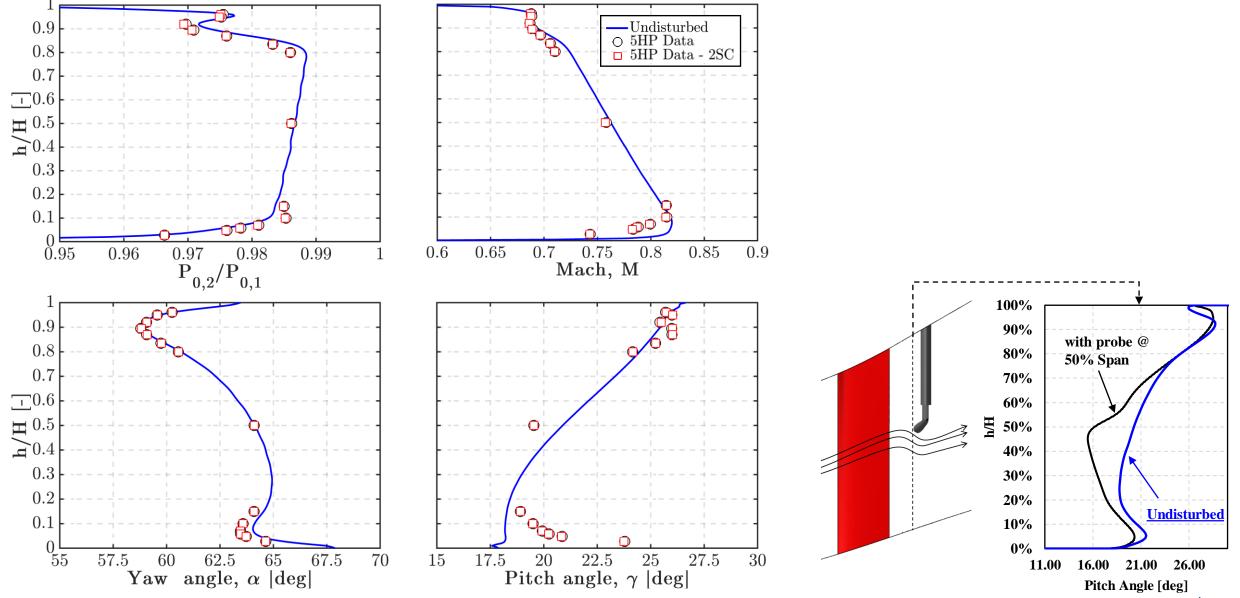
Probe @ Hub

Probe traverses at hub



Probe @ Hub

Pitch-wise averaged quantities



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Conclusions

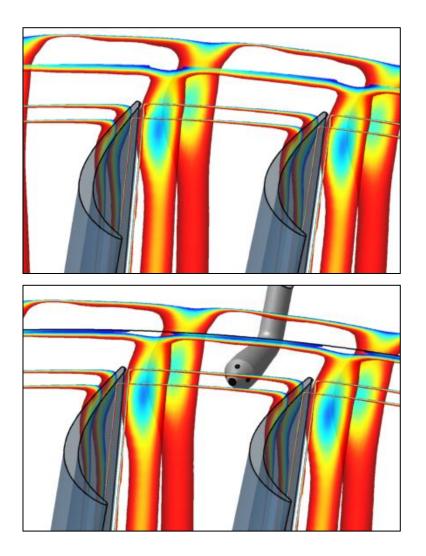
Mutual impact between test article and probe:

- The impact of the probe is confined between Vane 3 and +2
 Measurement error are higher than variation of Mis on the vane due to blockage of the probe
- 2. A new correction coefficient was computed for transonic Mach numbers
 □ Correction coefficient found in literature does not lose validity at high subsonic regimes
- 3. The correction does not affect the pitch-wise averaged quantities.

Use the two-step corrections to reduce the measurement error on the flow angles.

□ Miniaturize the probe to be less susceptible to velocity gradients!

Thanks for your attention!



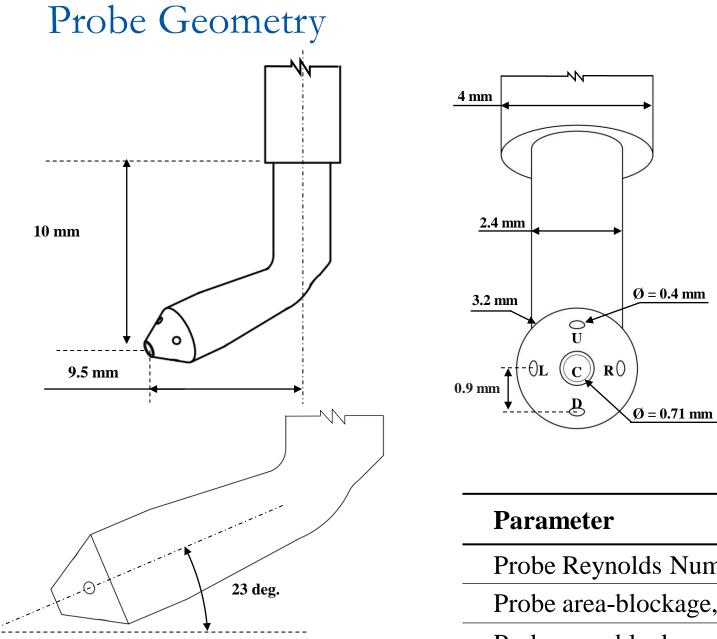
Acknowledgements:

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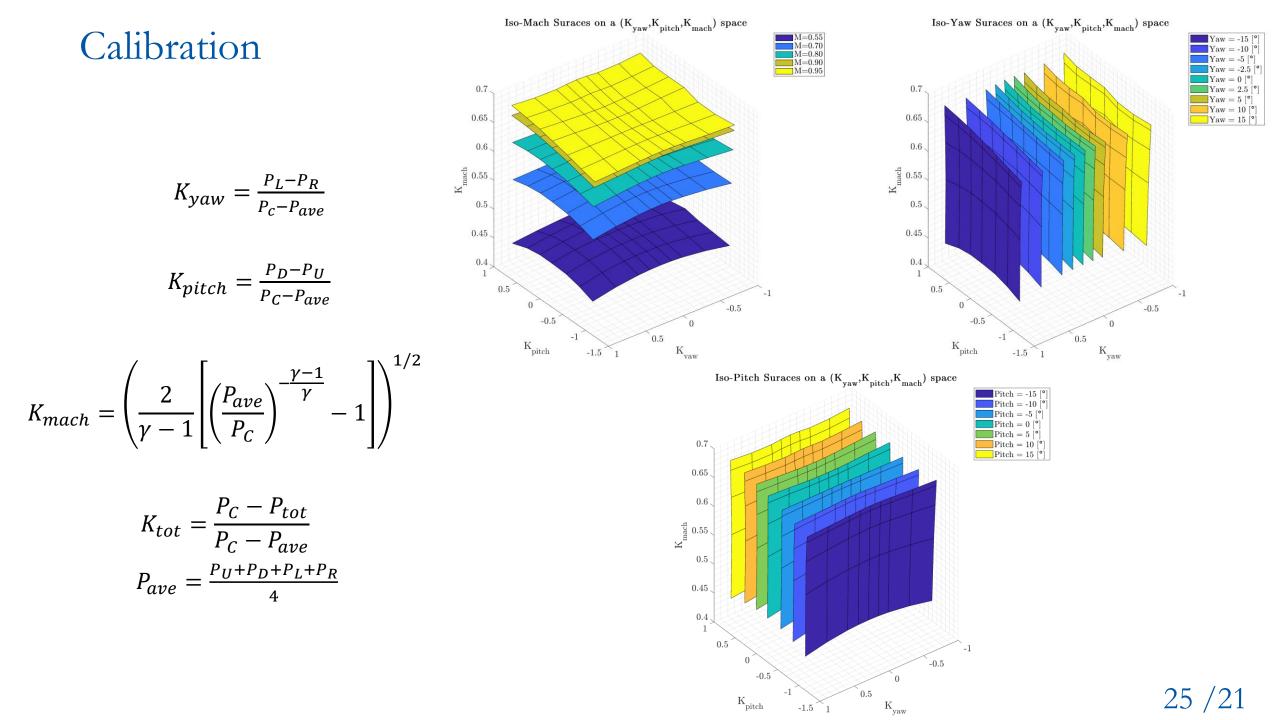
The authors also acknowledge SAFRAN Aircraft Engines for the collaboration.



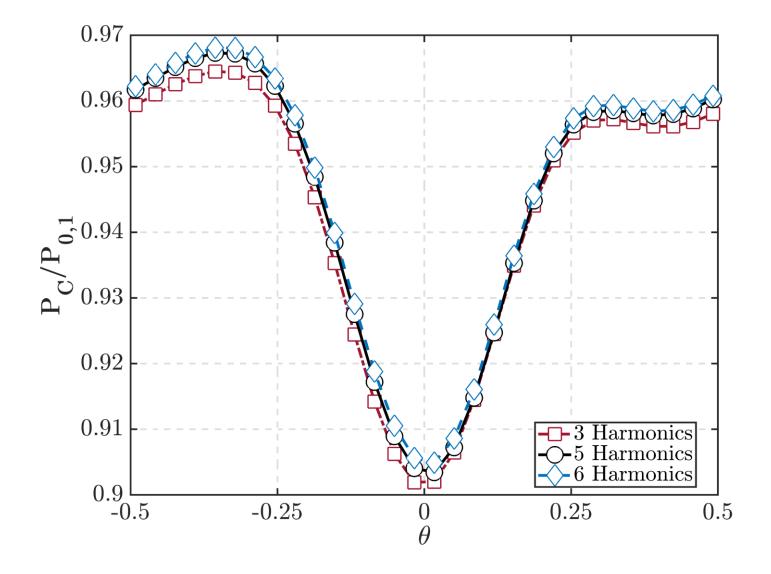
Backup Slides



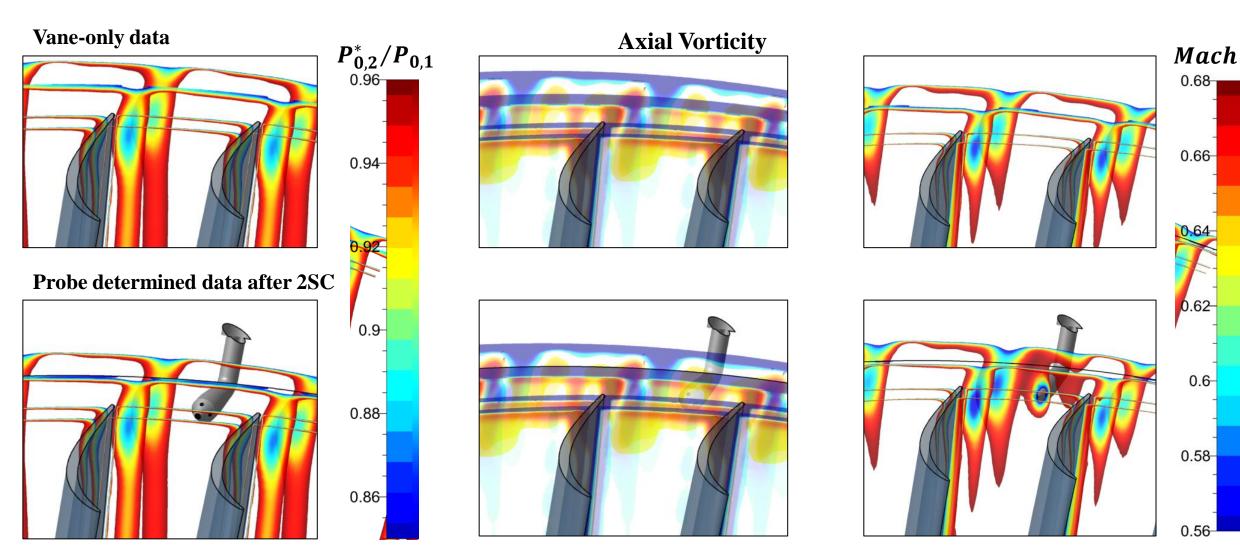
Parameter	Value
Probe Reynolds Number, Re (-)	~2.7 x 10 ⁴
Probe area-blockage, A_P/A_{pass} (-)	8.4%
Probe area-blockage, A_P/A_{dom} (-)	1.04%

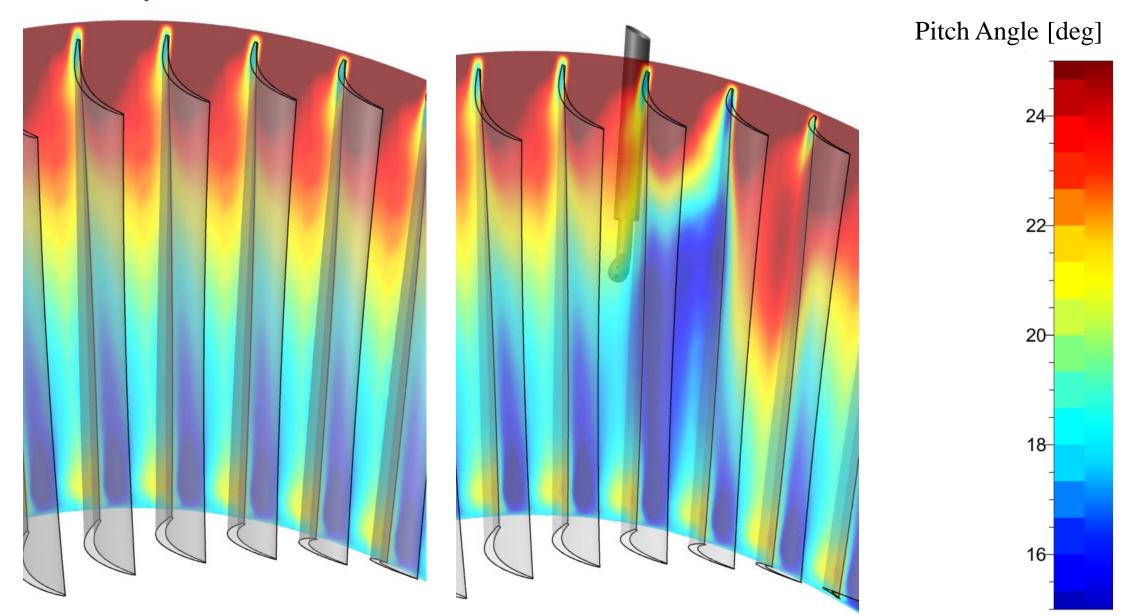


Number of Harmonics

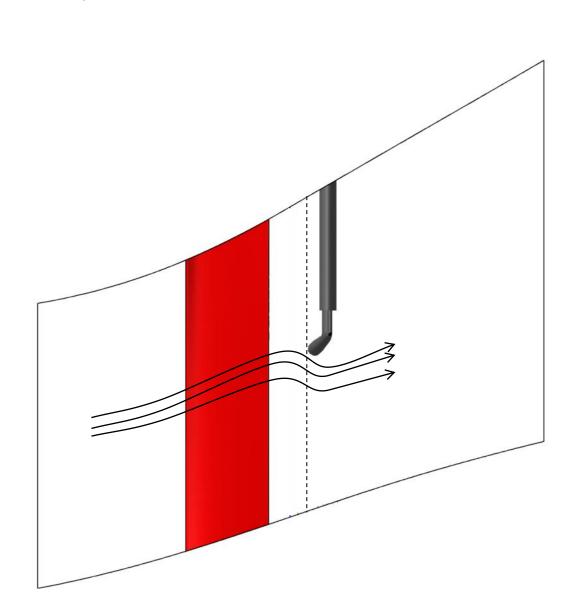


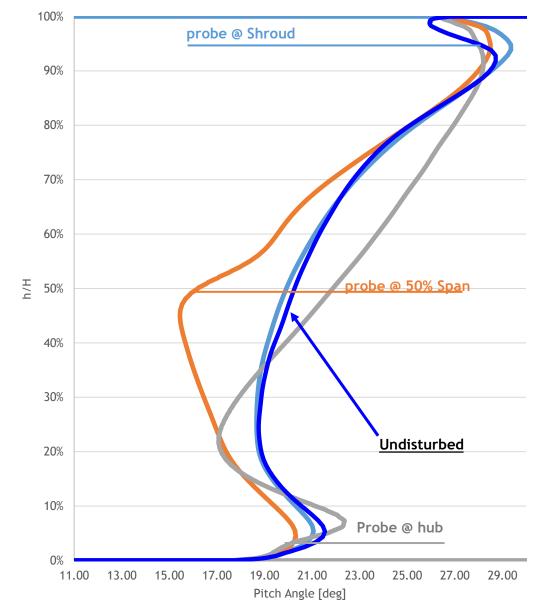
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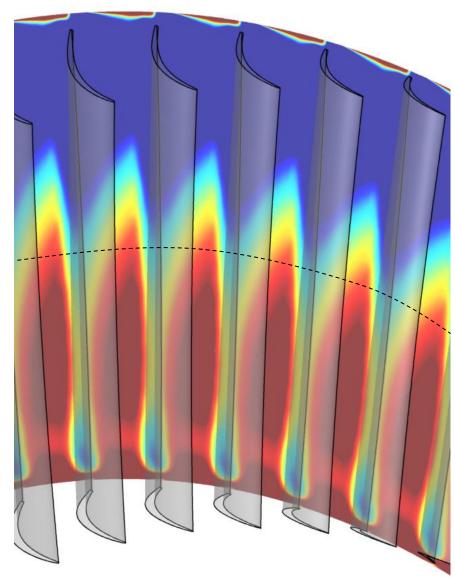
Pitch Angles upstream of the probe

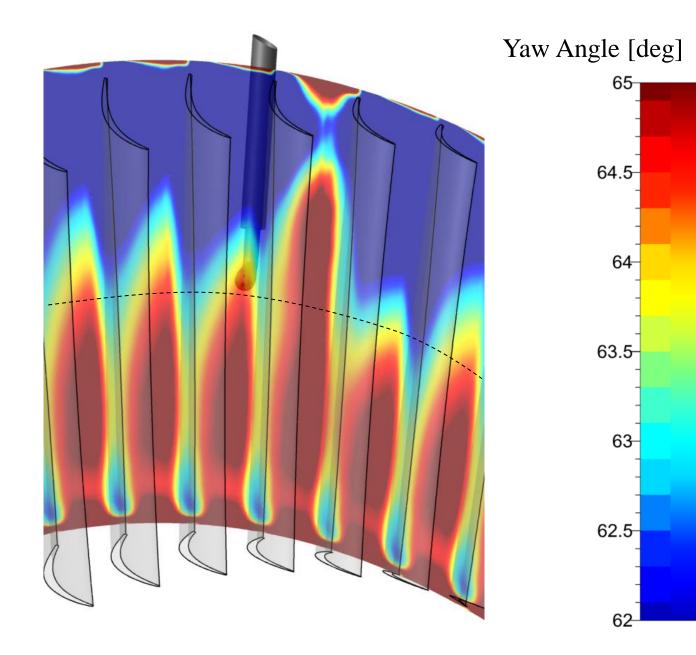




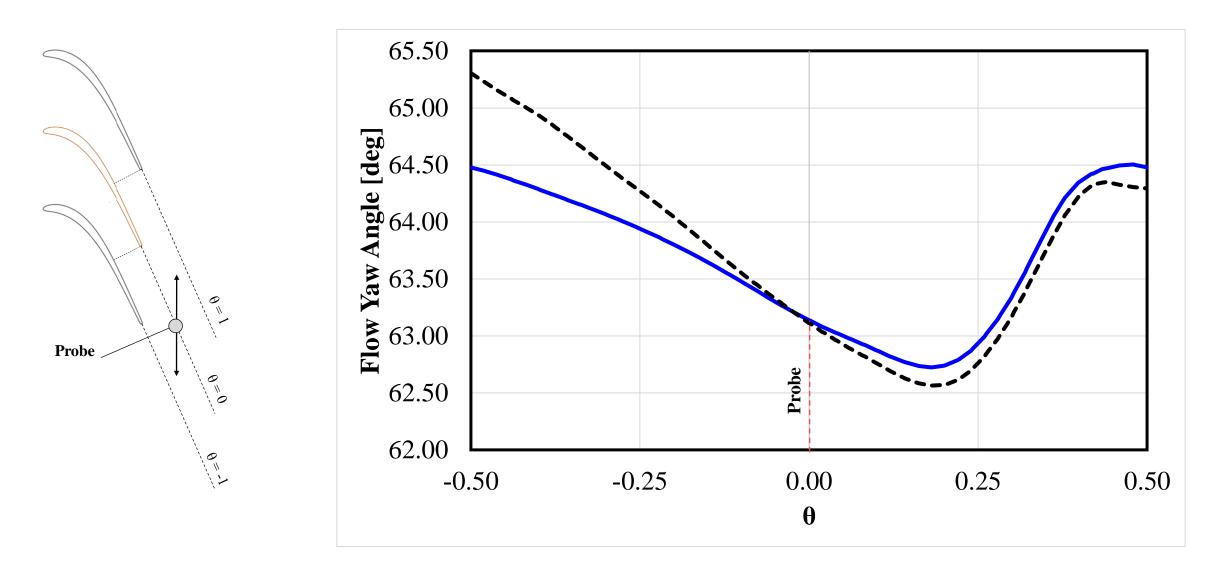
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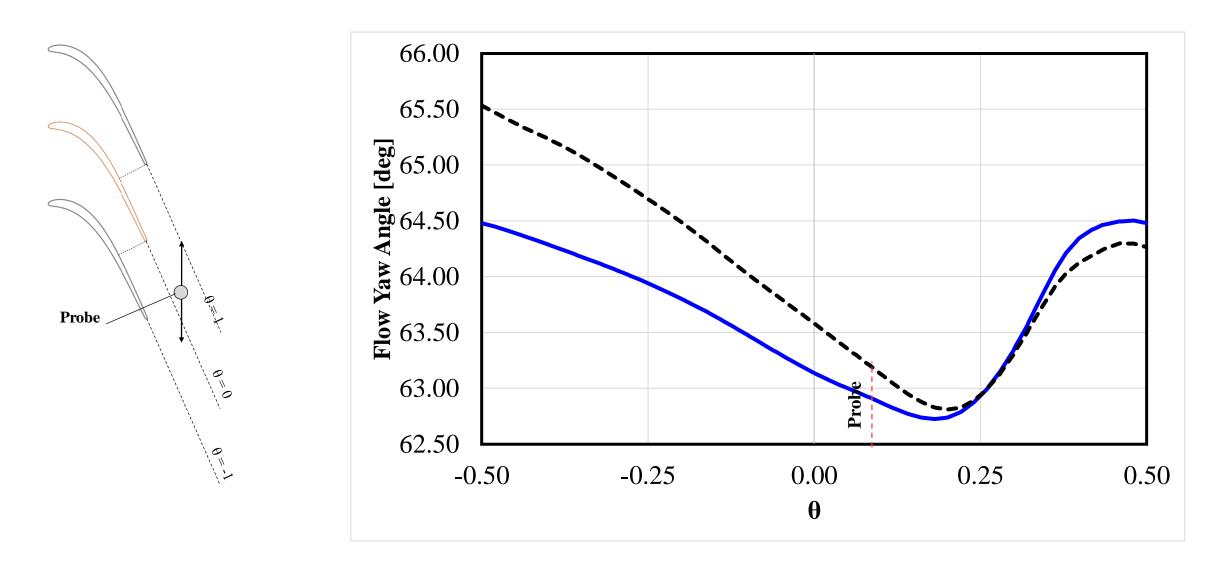


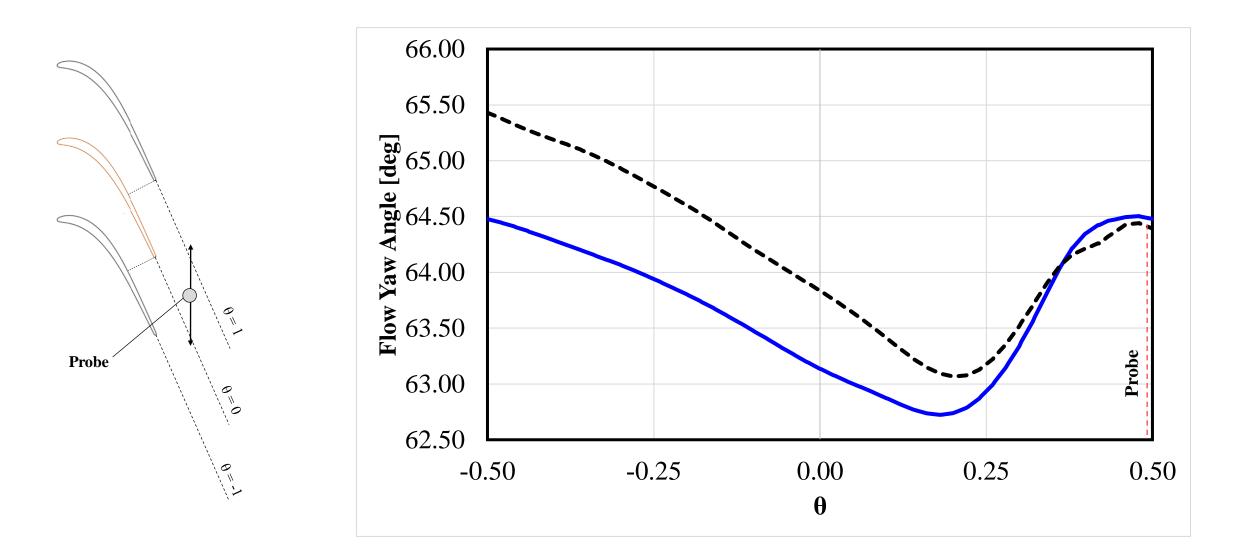


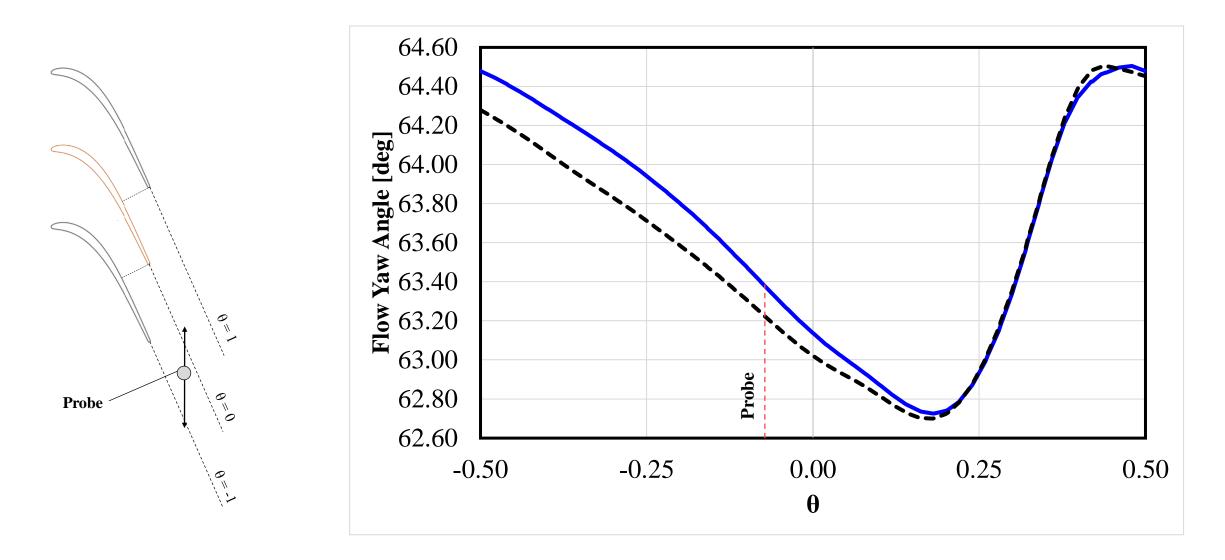


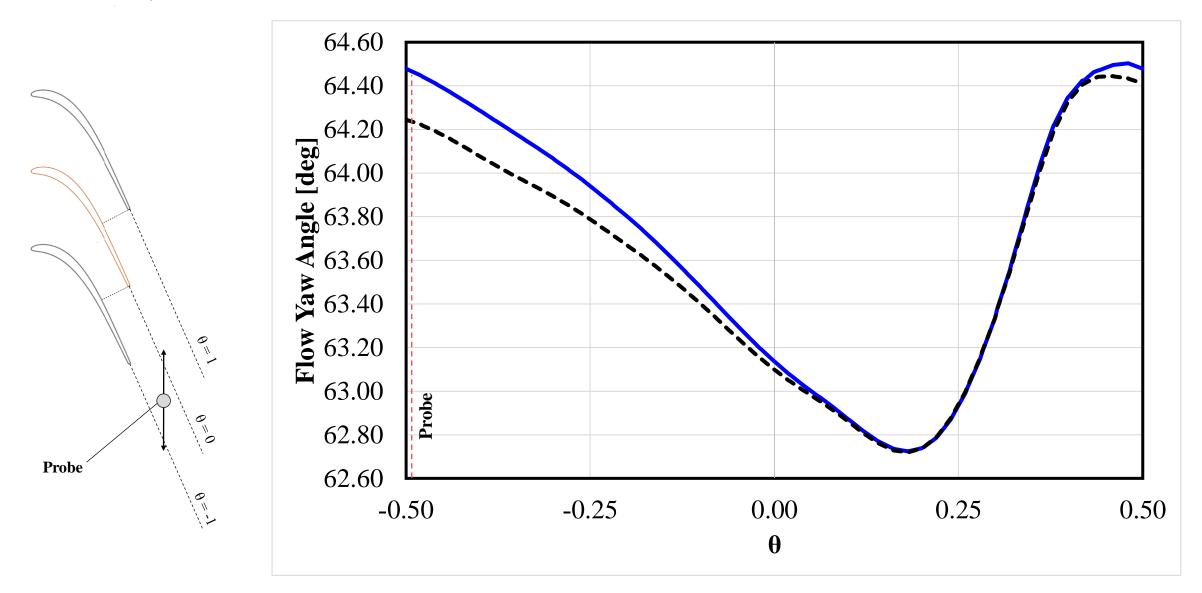
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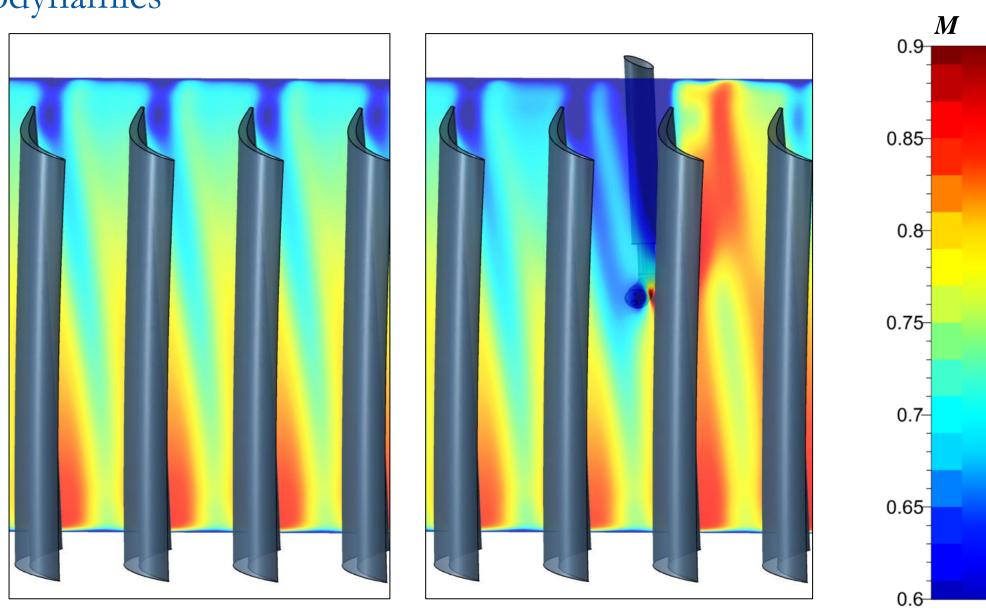


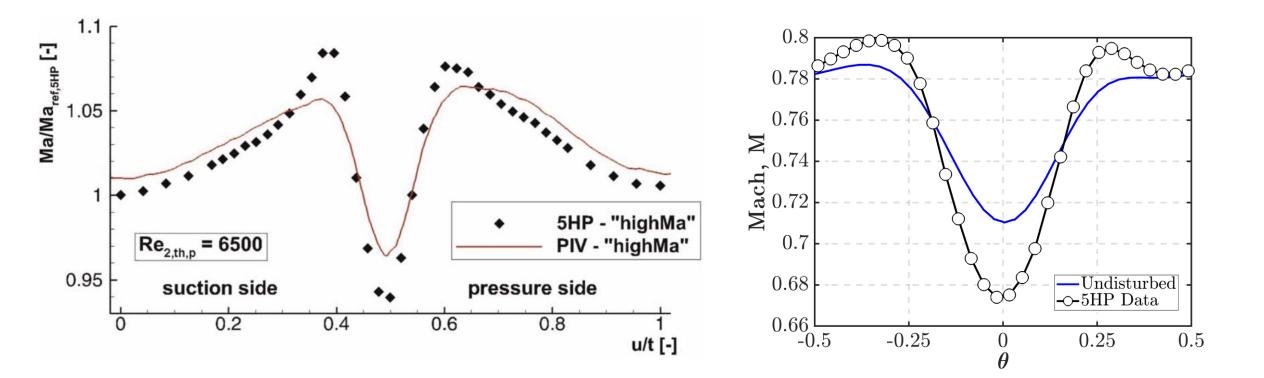


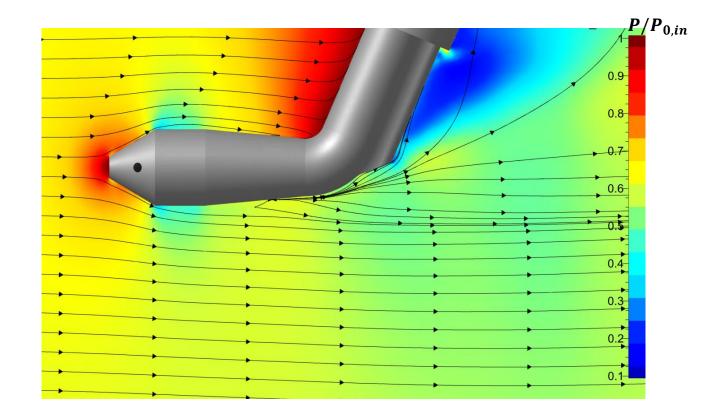












Probe-determined data: Errors

	Validation Case #1	Validation Case #2	Validation Case #3
Inlet Yaw Angle [deg]	12.5	0	15
Inlet Pitch Angle [deg]	0	12.5	-15
Mach Number	0.9	0.9	0.915

