

Bayesian Inference of Visco-Elastic Visco-Plastic Material Model Parameters for SLS-printed polyamide lattices

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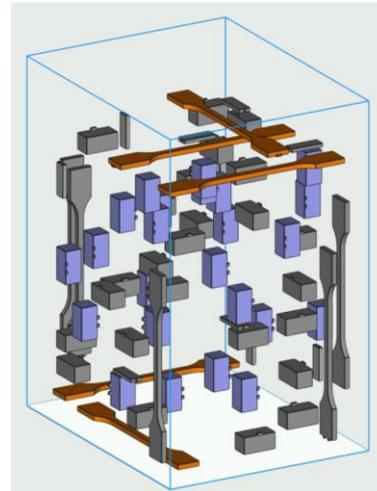
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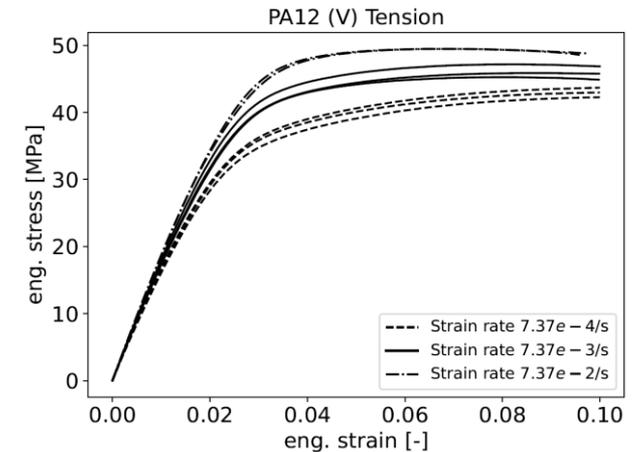
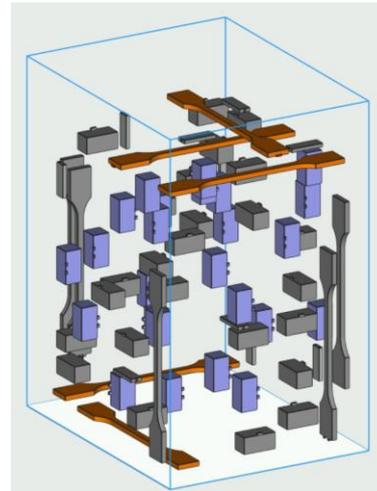
- Selective Laser Sintering (SLS) Polyamide 12 (PA12)

- SLS-printed polyamide lattices
- Material constitutive for numerical modelling of structure
- Bulk sample preparation

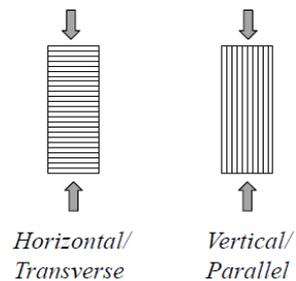


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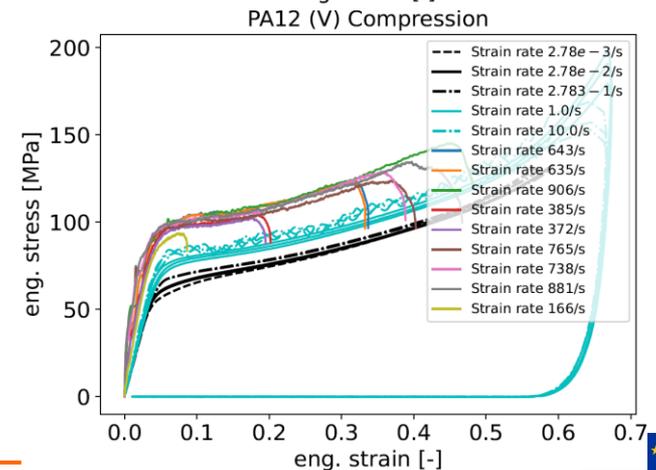
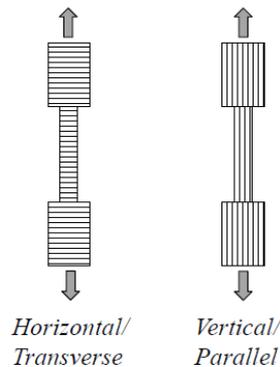
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- Material constitutive for numerical modelling of structure
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Compression test specimens



Tensile test specimens



- Model: Hyperelastic visco-elastic-visco-plastic material model

- Strain measure:

- $\mathbf{F} = \mathbf{F}^{\text{ve}} \cdot \mathbf{F}^{\text{vp}}$, $\mathbf{C}^{\text{ve}} = \mathbf{F}^{\text{veT}} \cdot \mathbf{F}^{\text{ve}}$, $\mathbf{E}^{\text{ve}} = \frac{1}{2} \ln(\mathbf{C}^{\text{ve}})$

- $\mathbf{L}^{\text{vp}} = \dot{\mathbf{F}}^{\text{vp}} \cdot \mathbf{F}^{\text{vp}-1}$, $\mathbf{D}^{\text{vp}} = \mathbf{L}^{\text{vp}}$

- Visco-elastic part

$$\left\{ \begin{array}{l} \boldsymbol{\tau}^{\text{dev}} = \int_{-\infty}^t G(t-s) \frac{d}{ds} \text{dev}(\mathbf{E}^{\text{ve}}(s)) ds \\ p = \frac{1}{3} \boldsymbol{\tau}^{\text{tr}} = \int_{-\infty}^t K(t-s) \frac{d}{ds} \text{tr}(\mathbf{E}^{\text{ve}}(s)) ds \end{array} \right.$$



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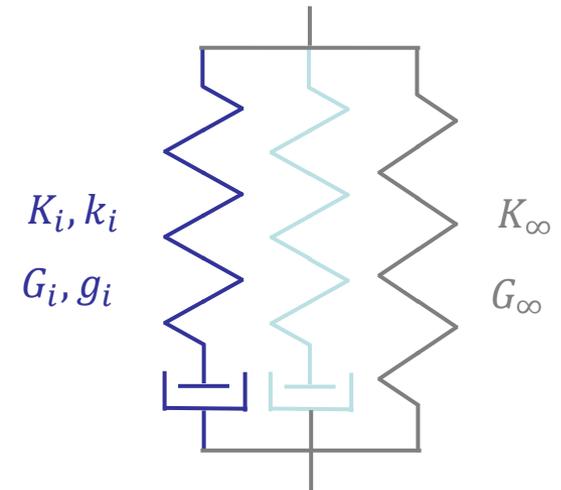
- Maxwell model

- $G(t) = G_{\infty} + \sum_{i=1}^N G_i \exp(-\frac{t}{g_i})$

- $K(t) = K_{\infty} + \sum_{i=1}^N K_i \exp(-\frac{t}{k_i})$

- Parameters:

$$K_{\infty}, G_{\infty}, G_i, g_i, K_i, k_i, \quad i = 1, \dots, N$$



- Model: Hyperelastic visco-elastic-visco-plastic material model

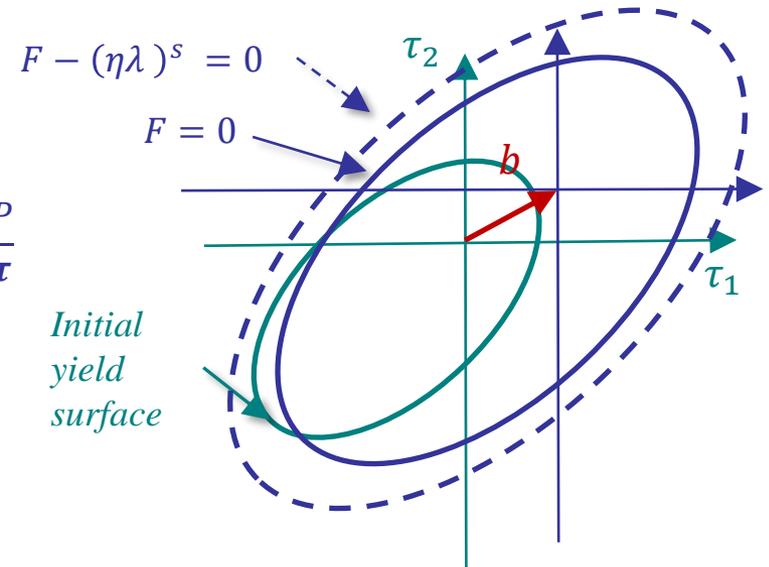
- Visco-plastic part

- back-stress

$$\boldsymbol{\varphi} = \boldsymbol{\tau} - \boldsymbol{b}$$

- Perzina plastic flow rule

$$\mathbf{D}^{\text{vp}} = \dot{\mathbf{F}}^{\text{vp}} \cdot \mathbf{F}^{\text{vp}-1} = \frac{1}{\eta} \langle F \rangle^{\frac{1}{s}} \frac{\partial P}{\partial \boldsymbol{\tau}} = \lambda \frac{\partial P}{\partial \boldsymbol{\tau}}$$



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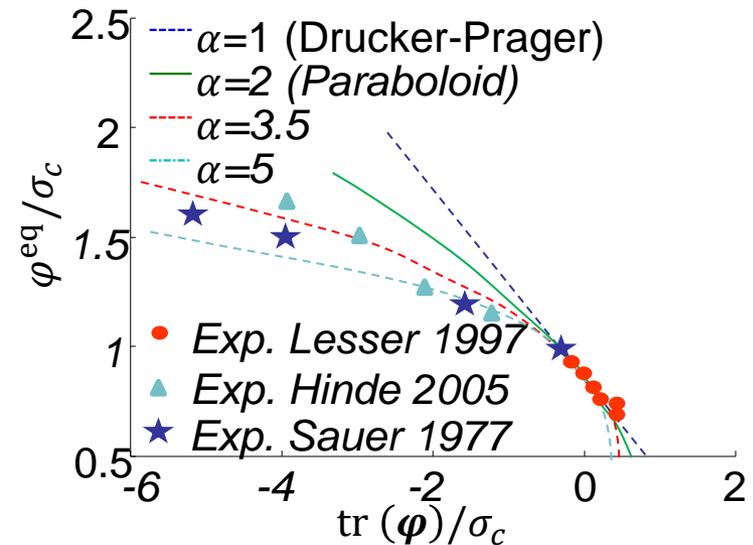
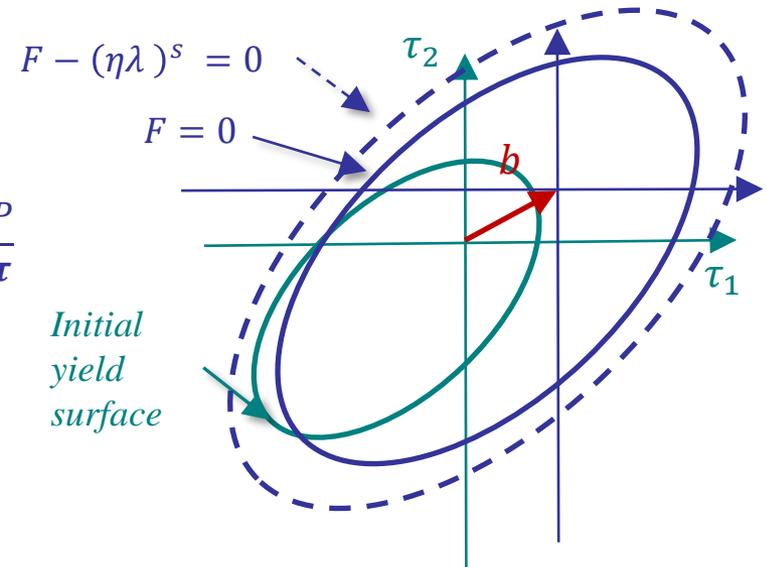
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- Yield surface, flow potential

$$\left\{ \begin{array}{l} F = \left(\frac{\varphi^{\text{eq}}}{Y_c} \right)^\alpha - \frac{m^\alpha - 1}{m + 1} \frac{\text{tr} \boldsymbol{\varphi}}{Y_c} - \frac{m^\alpha + m}{m + 1} \\ m = \frac{\sigma_t}{\sigma_c} \\ P = (\varphi^{\text{eq}})^2 + \beta \left(\frac{\text{tr} \boldsymbol{\varphi}}{3} \right)^2 \end{array} \right.$$

- Equivalent plastic strain rate:

$$\left\{ \begin{array}{l} \dot{\gamma} = \frac{\sqrt{\mathbf{D}^{\text{vp}} : \mathbf{D}^{\text{vp}}}}{\sqrt{\mathbf{1} + 2\nu_p^2}} \\ \nu_p = \frac{9 - 2\beta}{18 + 2\beta} \end{array} \right.$$

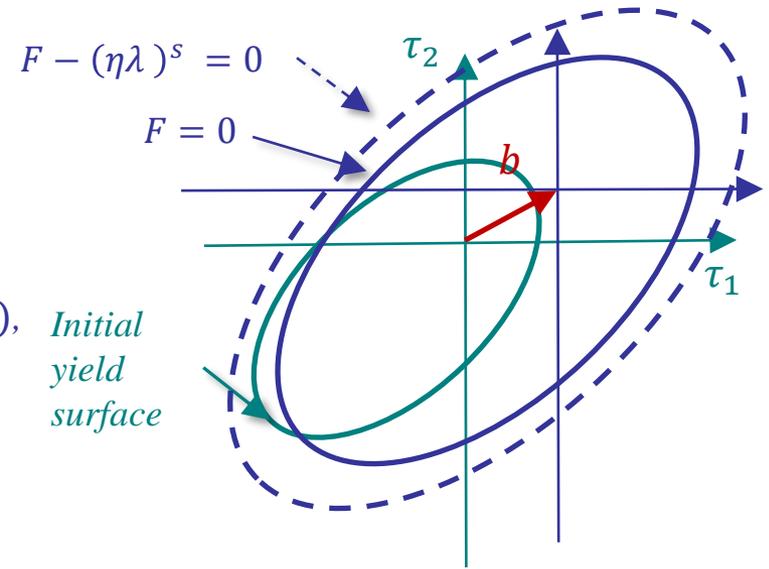


- Model: Hyperelastic visco-elastic-visco-plastic material model

- Visco-plastic part

- Hardening

$$\left\{ \begin{array}{l} \dot{\gamma}_c = H_c(\gamma) \dot{\gamma} \text{ with } H_c(\gamma) = c_0 + h_c H_c^1 \exp(-h_c \gamma), \\ \dot{\gamma}_t = H_t(\gamma) \dot{\gamma} \text{ with } H_t(\gamma) = t_0 + h_t H_t^1 \exp(-h_t \gamma), \\ \dot{\mathbf{b}} = \frac{H_b(\gamma)}{\sqrt{1+2\nu_p^2}} \mathbf{D}^{vp} \text{ with } H_b(\gamma) = b_0 + h_b H_b^0 \exp(-h_b \gamma), \end{array} \right.$$



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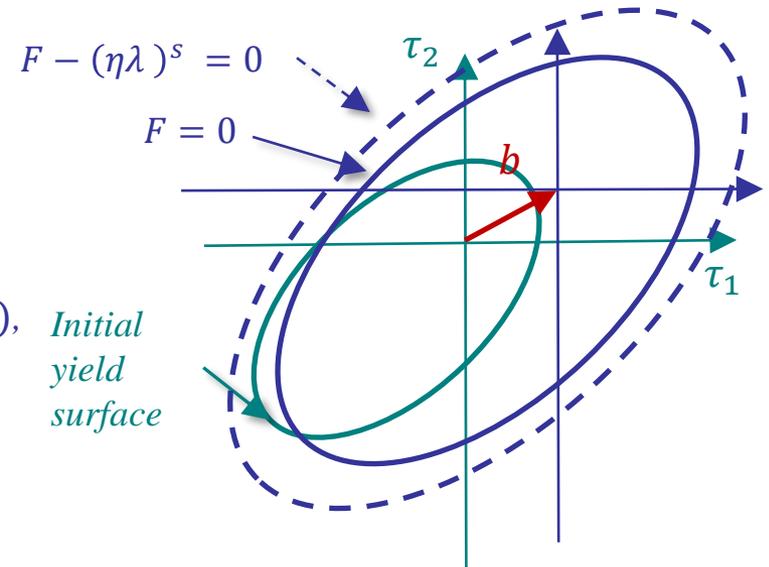
$$\left\{ \begin{array}{l} \dot{Y}_c = H_c(\gamma) \dot{\gamma} \text{ with } H_c(\gamma) = c_0 + h_c H_c^0 \exp(-h_c \gamma), \\ \dot{Y}_t = H_t(\gamma) \dot{\gamma} \text{ with } H_t(\gamma) = t_0 + h_t H_t^0 \exp(-h_t \gamma), \\ \dot{\mathbf{b}} = \frac{H_b(\gamma)}{\sqrt{1+2v_p^2}} \mathbf{D}^{vp} \text{ with } H_b(\gamma) = b_0 + h_b H_b^0 \exp(-h_b \gamma), \end{array} \right.$$

- Parameters: ~~(back stress)~~

- $\sigma_{c0}, c_0, h_c, H_c^0$

- σ_{t0} or m_0, t_0, h_t, H_t^0

- η, s, α, β



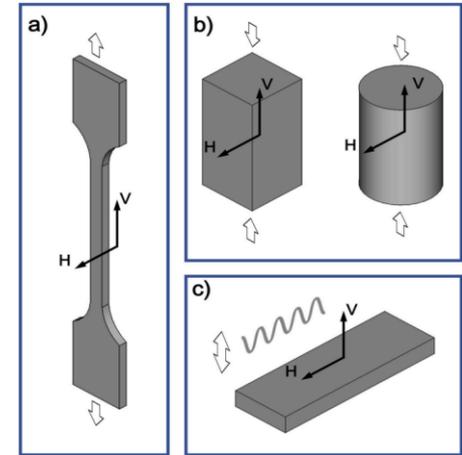
$$\left\{ \begin{array}{l} F = \left(\frac{\varphi^{eq}}{Y_c} \right)^\alpha - \frac{m^\alpha - 1}{m + 1} \frac{\text{tr} \varphi}{Y_c} - \frac{m^\alpha + m}{m + 1} \\ m = \frac{\sigma_t}{\sigma_c} \\ v_p = \frac{9 - 2\beta}{18 + 2\beta} \end{array} \right.$$



- **VE-Identification (PA12-V):**

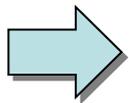
- Since, Poisson's ratio, ν , of polymer material is also a function of time
- We consider

$$\left\{ \begin{array}{l} G(t) = G_{\infty} + \sum_{i=1}^N G_i \exp\left(-\frac{t}{g_i}\right) \\ K(t) = K_{\infty} + \sum_{i=1}^N K_i \exp\left(-\frac{t}{k_i}\right) \\ G_{\infty} = \frac{E_{\infty}}{2(1 + \nu_{\infty})} \quad K_{\infty} = \frac{E_{\infty}}{3(1 - 2\nu_{\infty})} \end{array} \right.$$



- The testing strain rates vary from $10^{-4}/s$ to $10^3/s$, and the relaxation test lasts 1800 s
- In the relaxation test, no obvious stress decrease has been seen after 1000 s

$N = 8$ branches are considered



to have the characteristic relaxation times of $\propto 10^{-5}$, $\propto 10^{-4}$, $\propto 10^{-3}$, $\propto 10^{-2}$, $\propto 10^{-1}$, $\propto 10^0$, $\propto 10^1$ and $\propto 10^2$ s.



- Bayesian-Identification (PA12-V):

- Viscoelastic parameters ϑ^{ve} :

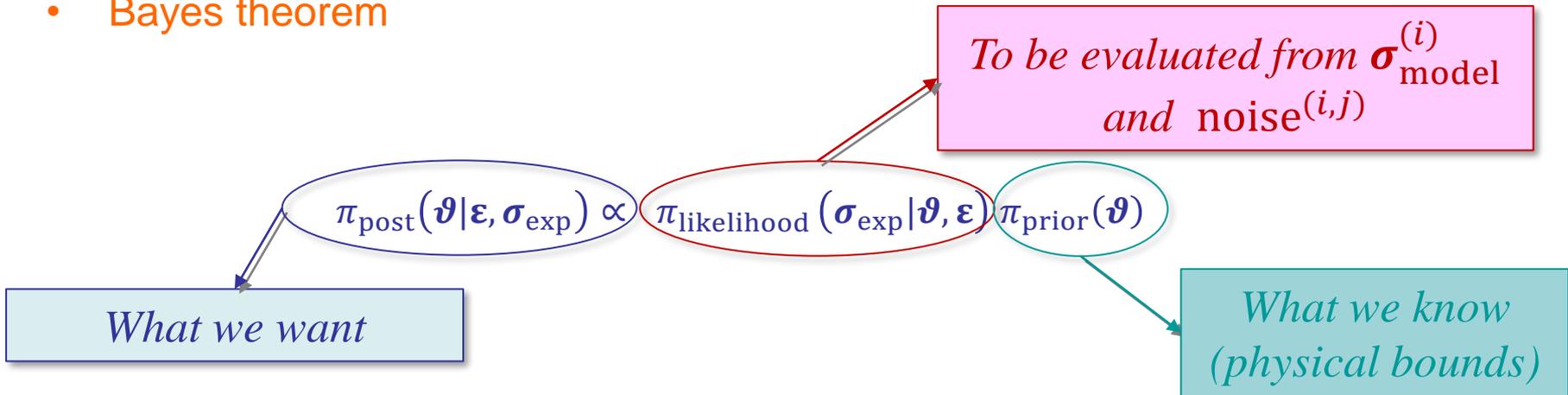
$$E_{\infty}, \nu_{\infty}, G_i, K_i, g_1, k_1,$$

$$g_i = \frac{g_1}{10^{i-1}}, k_i = \frac{k_1}{10^{i-1}} \text{ with } i = 1, \dots, 8$$

- Viscoplastic parameters ϑ^{vp} :

$$\eta, s, \alpha, \beta, \sigma_c^0, c_0, H_c^0, h_c, m^0, t_0, H_t^0, h_t$$

- Bayes theorem



- Bayesian-Identification (PA12-V):

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- Bayes theorem

$$\pi_{\text{post}}(\vartheta_1, \vartheta_2 | \beta_1, \beta_2) \propto \pi_{\text{likelihood}}(\beta_1, \beta_2 | \vartheta_1, \vartheta_2) \pi_{\text{prior}}(\vartheta_1, \vartheta_2)$$

$$\beta_1, \beta_2 \quad \text{independent observations} \quad \propto \pi_{\text{likelihood}}(\beta_2 | \vartheta_1, \vartheta_2) \pi_{\text{likelihood}}(\beta_1 | \vartheta_1, \vartheta_2) \pi_{\text{prior}}(\vartheta_1, \vartheta_2)$$

$$\vartheta_1, \vartheta_2 \quad \text{independent prior distribution} \quad \propto \pi_{\text{likelihood}}(\beta_2 | \vartheta_1, \vartheta_2) \pi_{\text{prior}}(\vartheta_2) \pi_{\text{likelihood}}(\beta_1 | \vartheta_1, \vartheta_2) \pi_{\text{prior}}(\vartheta_1)$$



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- Viscoelastic parameters ϑ^{ve} :

$$E_{\infty}, \nu_{\infty}, G_i, K_i, g_1, k_1,$$

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- Viscoplastic parameters ϑ^{vp} :

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independent observations

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independent prior distribution

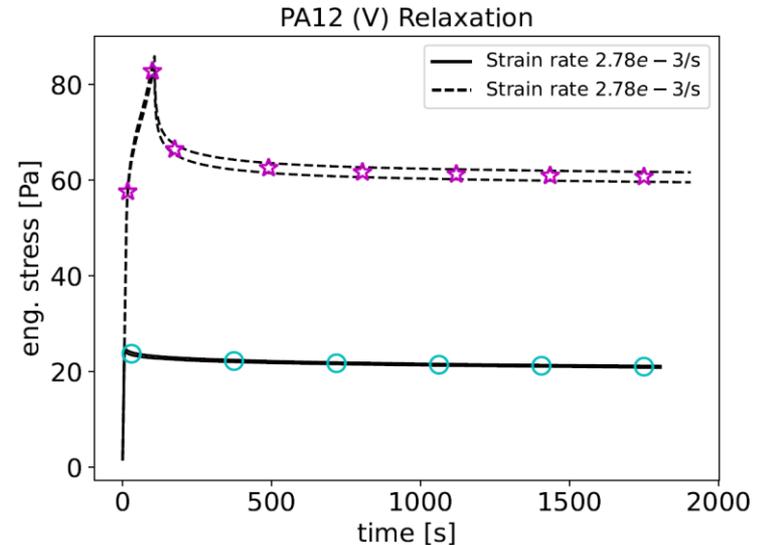
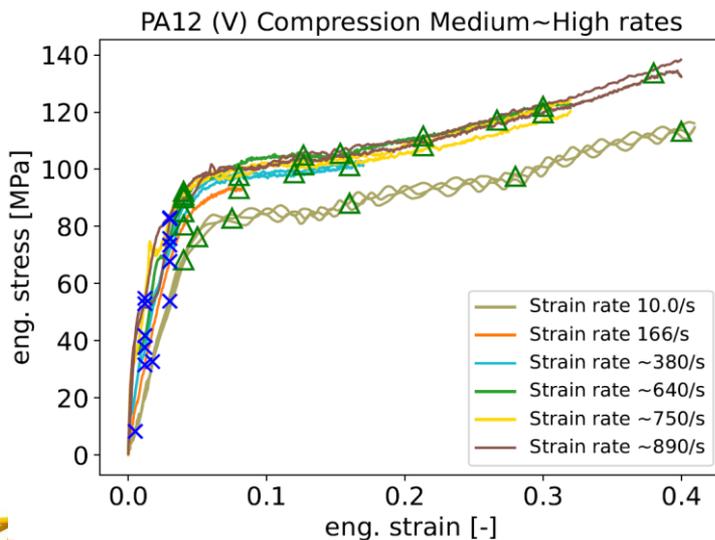
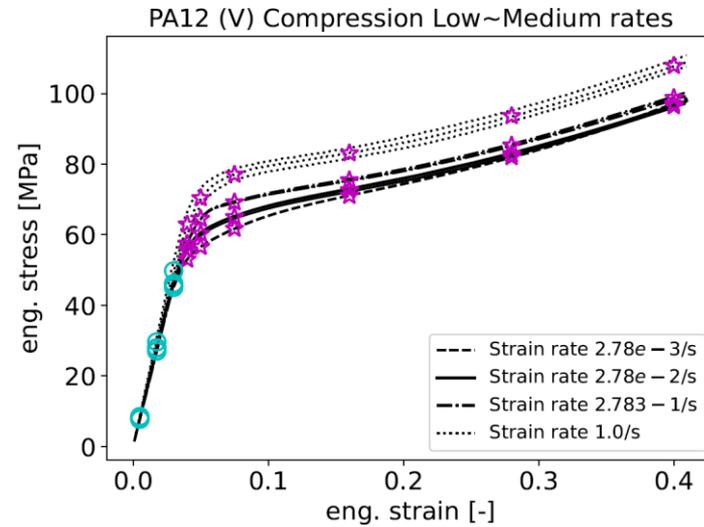
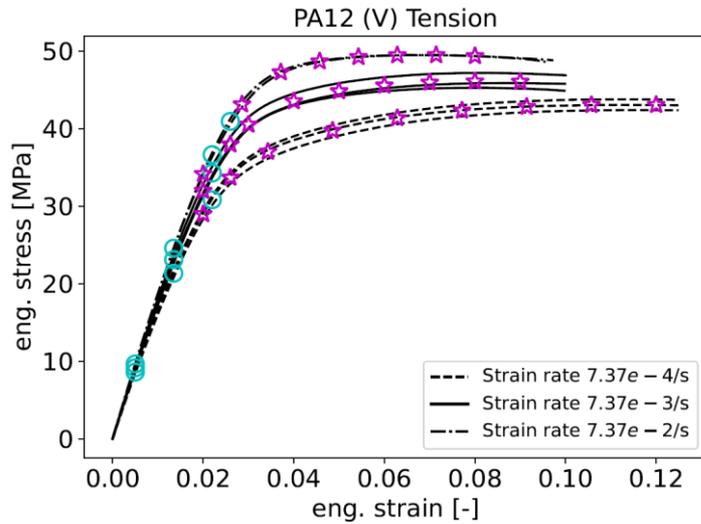
$$\beta_1, \vartheta_2 \propto \pi_{\text{likelihood}}(\beta_2 | \vartheta_1, \vartheta_2) \pi_{\text{prior}}(\vartheta_2) \pi_{\text{likelihood}}(\beta_1 | \vartheta_1) \pi_{\text{prior}}(\vartheta_1)$$

independent distribution

$$\pi_{\text{post}}(\vartheta_1 | \beta_1) \propto$$



- Observations $\beta = (\epsilon, \sigma_{\text{exp}})$



- Bayesian inference in sequence

- $\beta = [\beta^{ve}, \beta^{vp}]$, $\beta^{ve} = [\beta_1^{ve}, \beta_2^{ve}]$, $\beta^{vp} = [\beta_1^{vp}, \beta_2^{vp}]$
- Observations $\beta_1^{ve}, \beta_2^{ve}, \beta_1^{vp}, \beta_2^{vp}$ are used in sequence

Viscoelastic parameters ϑ^{ve}		
BI step	I	II
observation	β_1^{ve} , cyan circle	β_2^{ve} , blue "x"
likelihood	$\pi(\beta_1^{ve} \vartheta^{ve})$	$\pi(\beta_2^{ve} \vartheta^{ve})$
prior	$\pi_{\text{prior}}(\vartheta^{ve})$	$\pi_{\text{post}}(\vartheta^{ve} \beta_1^{ve})$
posterior	$\pi_{\text{post}}(\vartheta^{ve} \beta_1^{ve})$	$\pi_{\text{post}}(\vartheta^{ve} \beta^{ve})$
Viscoplastic parameters ϑ^{vp}		
BI step	III	IV
observation	β_1^{vp} , magenta star	β_2^{vp} , green triangles
likelihood	$\pi(\beta_1^{vp} \vartheta^{ve}, \vartheta^{vp})$	$\pi(\beta_2^{vp} \vartheta^{ve}, \vartheta^{vp})$
prior	$\pi_{\text{prior}}(\vartheta^{vp}) \pi_{\text{post}}(\vartheta^{ve} \beta^{ve})$	$\pi_{\text{post}}(\vartheta^{ve}, \vartheta^{vp} \beta^{ve}, \beta_1^{vp})$
posterior	$\pi_{\text{post}}(\vartheta^{ve}, \vartheta^{vp} \beta^{ve}, \beta_1^{vp})$	$\pi_{\text{post}}(\vartheta^{ve}, \vartheta^{vp} \beta^{ve}, \beta^{vp})$



- Bayesian inference

- The maximum a posteriori (MAP) estimate of viscoelastic material parameters

ϑ^{ve}	E_∞ [MPa]	ν_∞ [-]	g_1 [s]	k_1 [s]
Value	1366.7	0.278	7.36	9.12

G_i	G_1	G_2	G_3	G_4	G_5	G_6	G_7	G_8
[MPa]	0.33	27.23	18.55	1.62	21.66	9.91	1722.24	6.13

K_i	K_1	K_2	K_3	K_4	K_5	K_6	K_7	K_8
[MPa]	28281.49	0.30	747.17	467.82	0.51	7874.44	39.13	2422.40

- The maximum a posteriori (MAP) estimate of viscoelastic material parameters

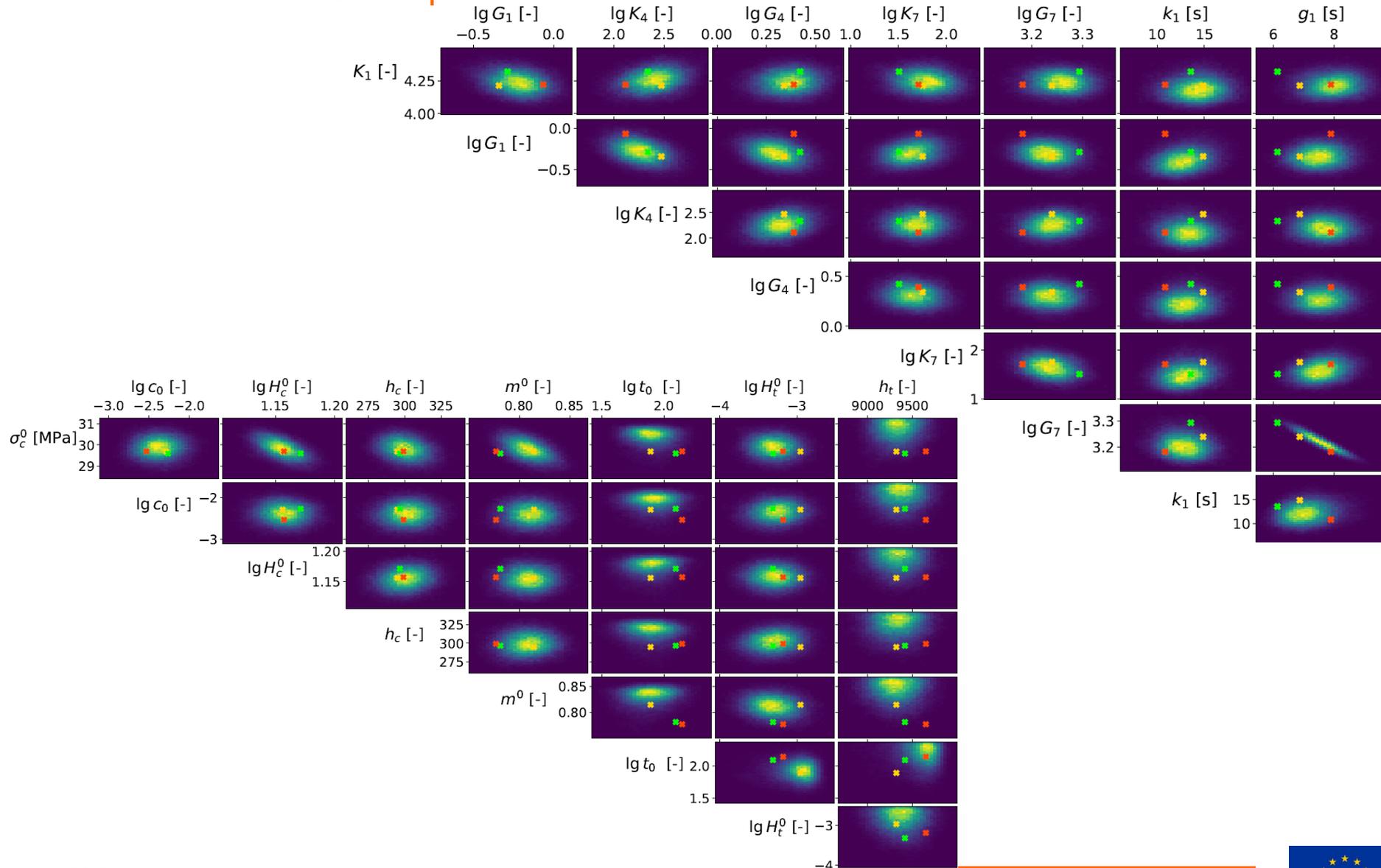
ϑ^{vp}	η [MPa·s]	s [-]	α [-]	β [-]
Value	1.33×10^5	0.18	3.63	0.18

ϑ^{vp}	σ_c^0 [MPa]	c_0 [MPa]	H_c^0 [MPa]	h_c [-]
Value	30.04	7.85×10^{-3}	14.41	296.38

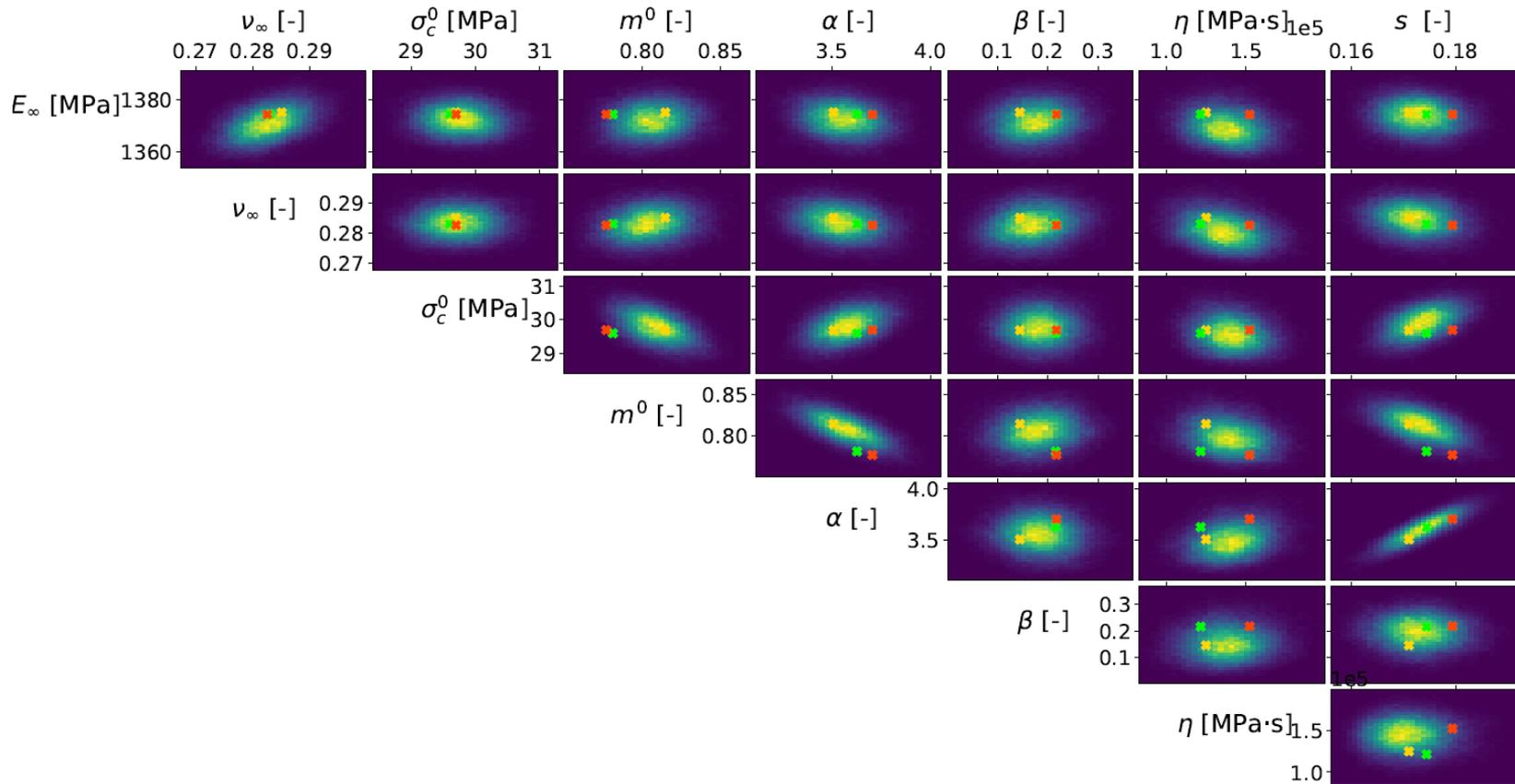
ϑ^{vp}	m^0 [-]	t_0 [MPa]	H_t^0 [MPa]	h_t [-]
Value	0.80	146.34	5.24×10^5	9955.79



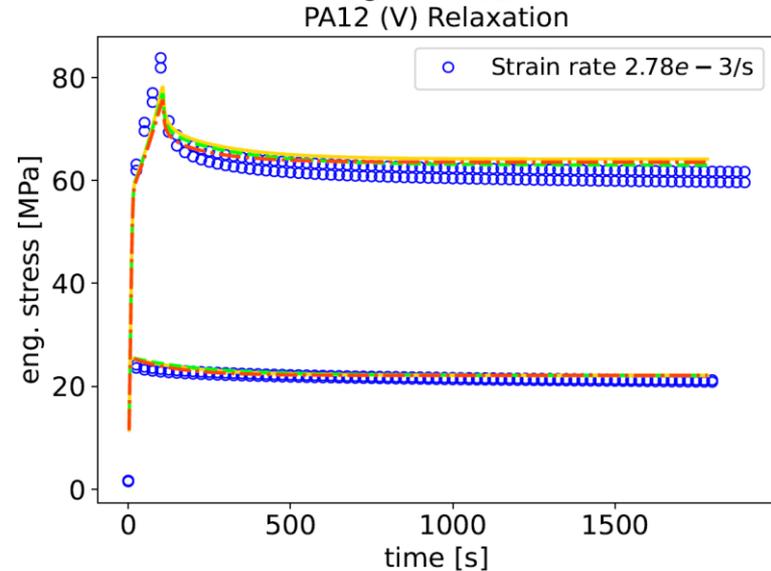
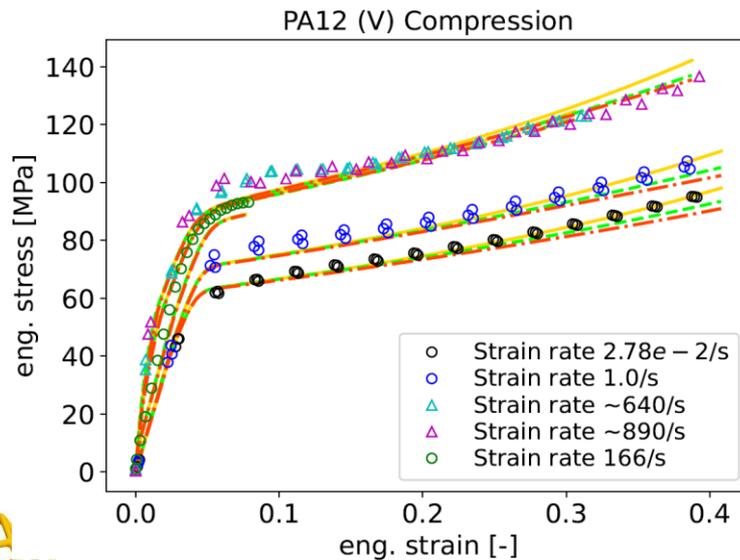
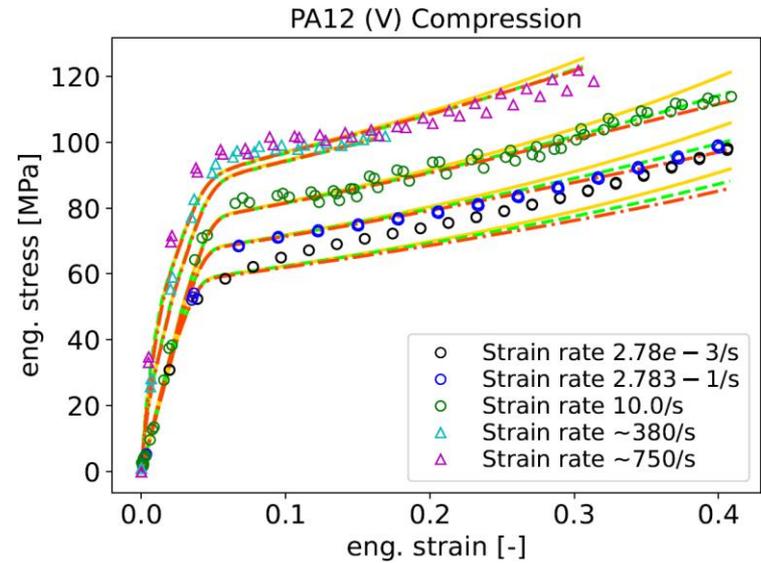
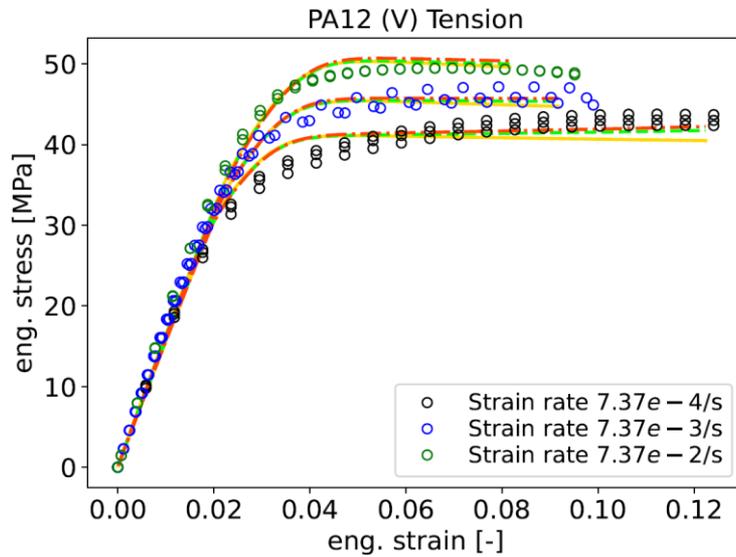
- Run a Markov Chain process



- Run a Markov Chain process

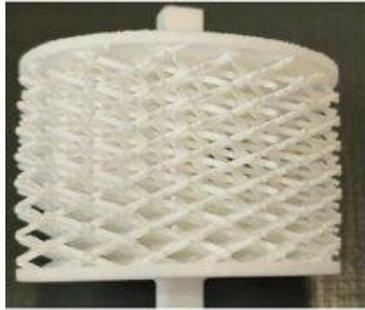


- Numerical modelling

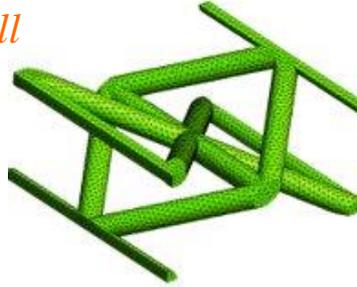


- Preliminary work: simulate a complex structure
 - Validate the infer parameters

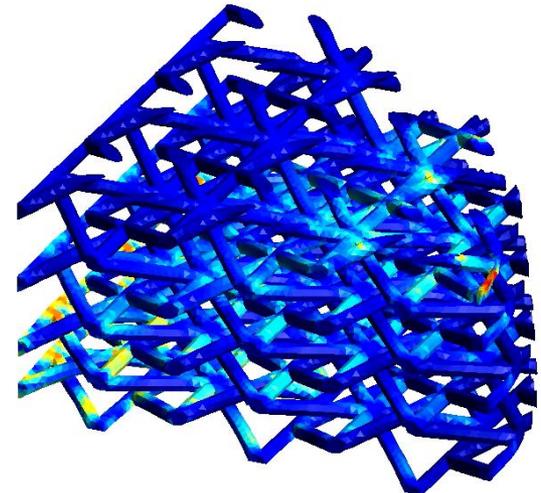
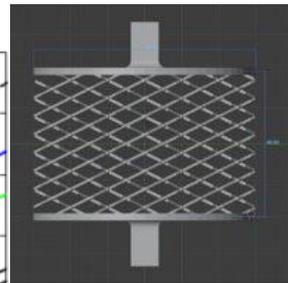
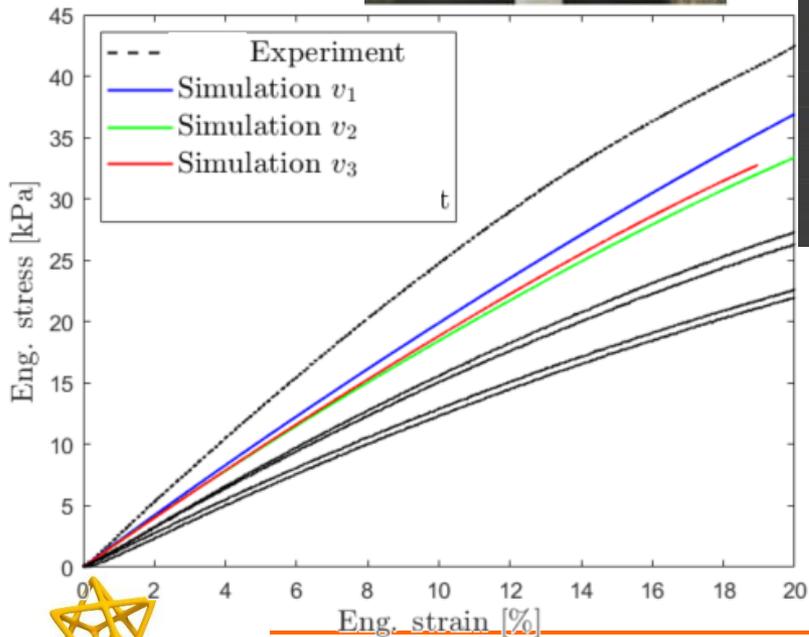
*Experimental test
JKU*



*Underlying USF
cell*



Numerical simulation



References

- More on
 - www.moammm.eu
 - High-Dimensional Parameter Identification with Bayesian Inference for Finite-Strain Visco-Elastic-Visco-Plastic Modeling of Selective Laser Sintering (Sls) Polyamide 12 (Pa12) and Neural Net-Work (Nnw)-Based Material Parameter Generator, <http://dx.doi.org/10.2139/ssrn.4457392>
 - Data on <https://dx.doi.org/10.5281/zenodo.7998798>

