

Numerical and Experimental Study of Chloride Ion Transport in Recycled Aggregates Concrete

NoMaD 2022

Arthur FANARA – 16 November 2022

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University of Liège, ArGEnCo Department, UEE Research Unit

Background

Environmental Concerns

- Concrete: 1 billion tons/year in EU *[Eurostat, 2014]*

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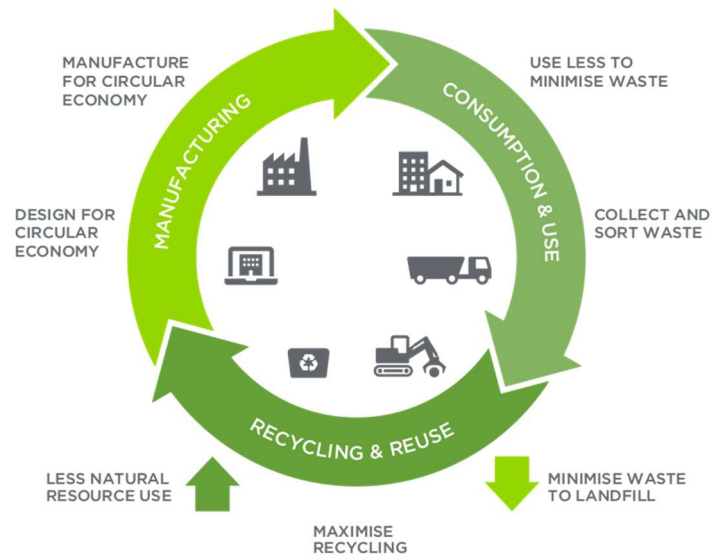
→ **Recycled Concrete Aggregates (RCA)** = NA + Residual mortar

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[<https://www.futurerecycling.com.au/sustainability/circular-economy/>,2020]

Background

Chlorides Attacks

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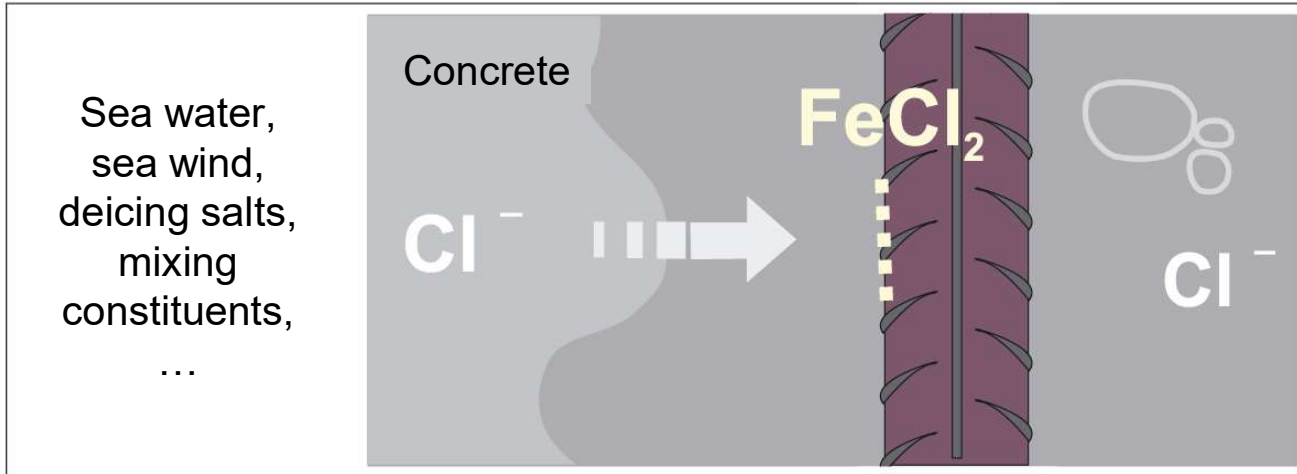
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[Ployaert, 2008]



Background

Chlorides Attacks

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Wallonie

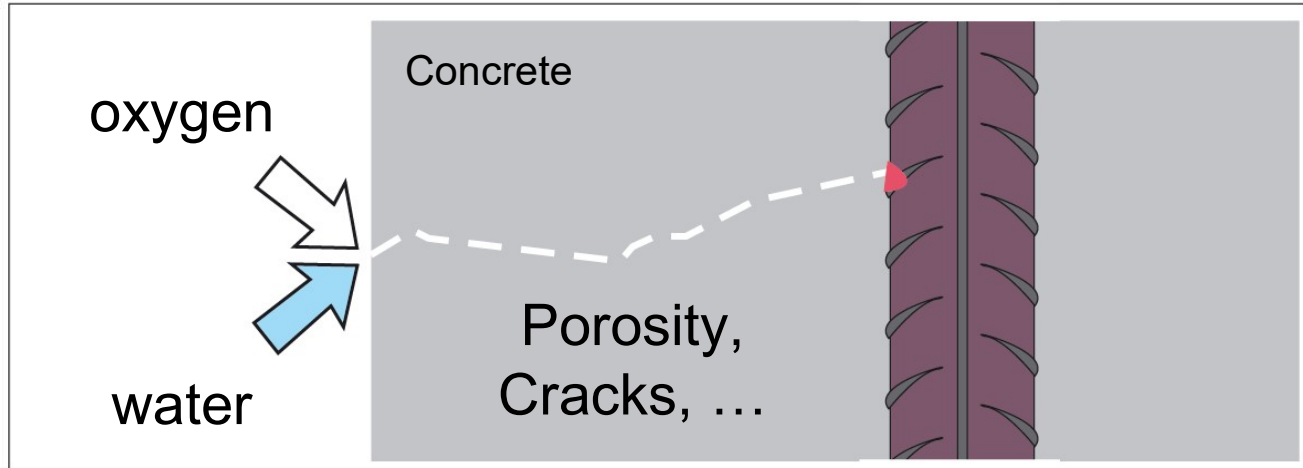
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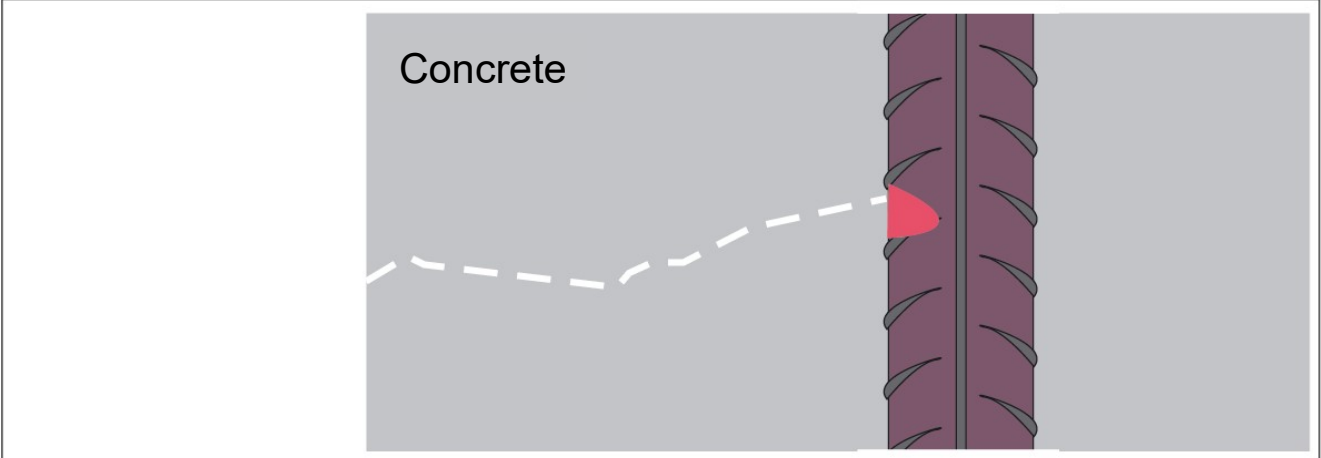
[Ployaert, 2008]



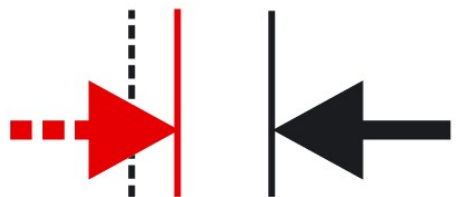
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Corrosion by
"pitting"



Background

Chlorides Attacks

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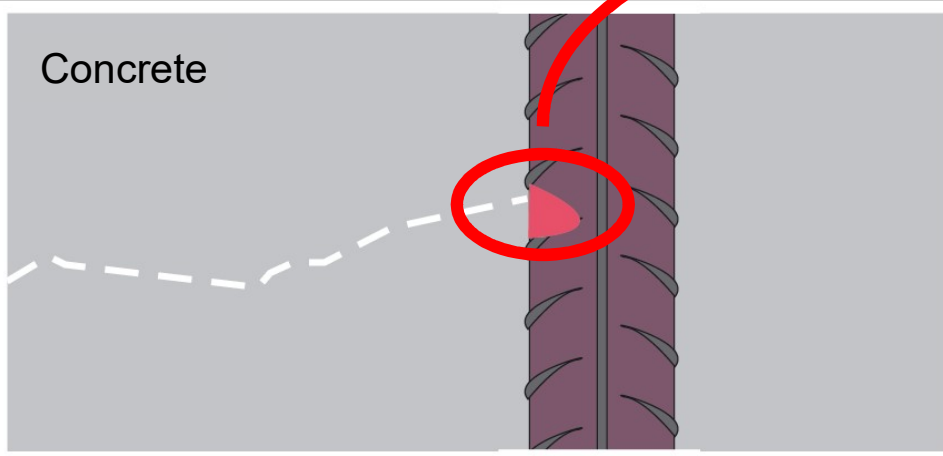
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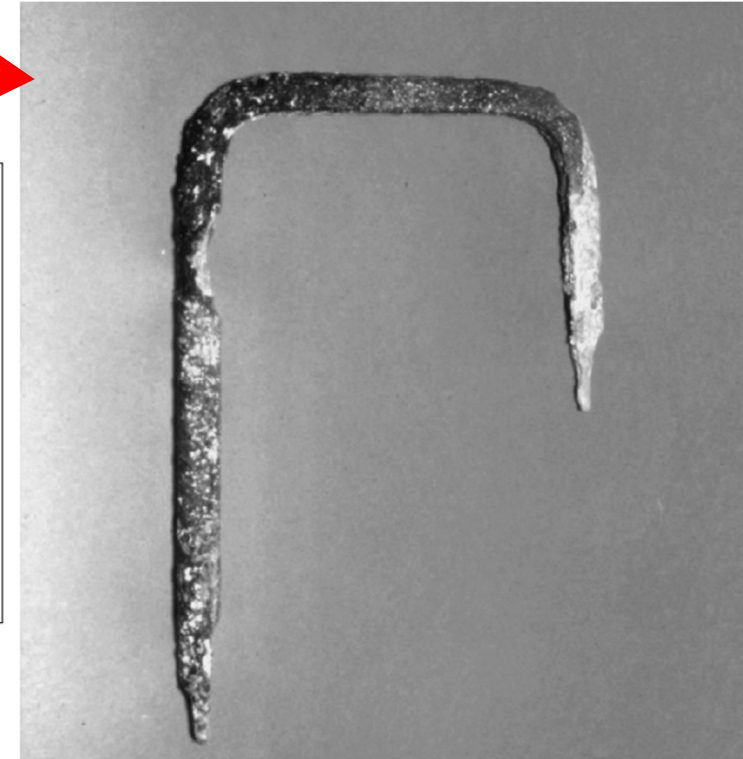
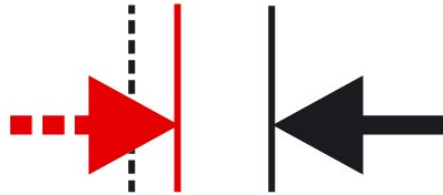


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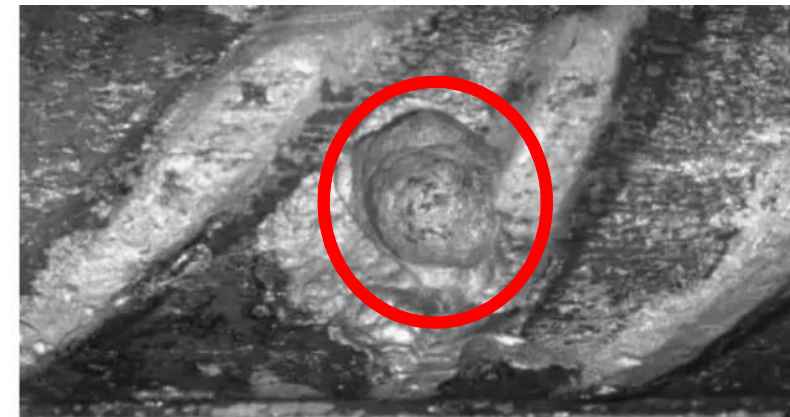
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[Raupach & Büttner, 2014]



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Background

Influence of RCA

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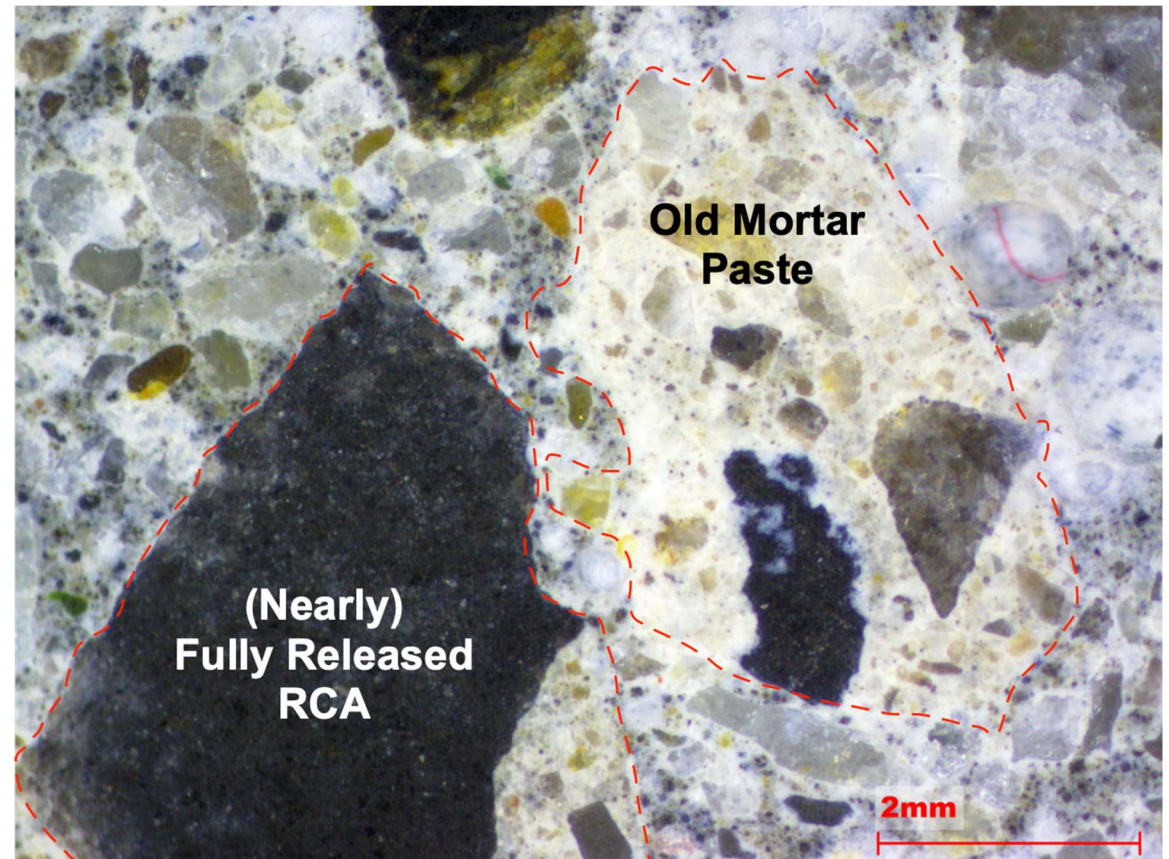
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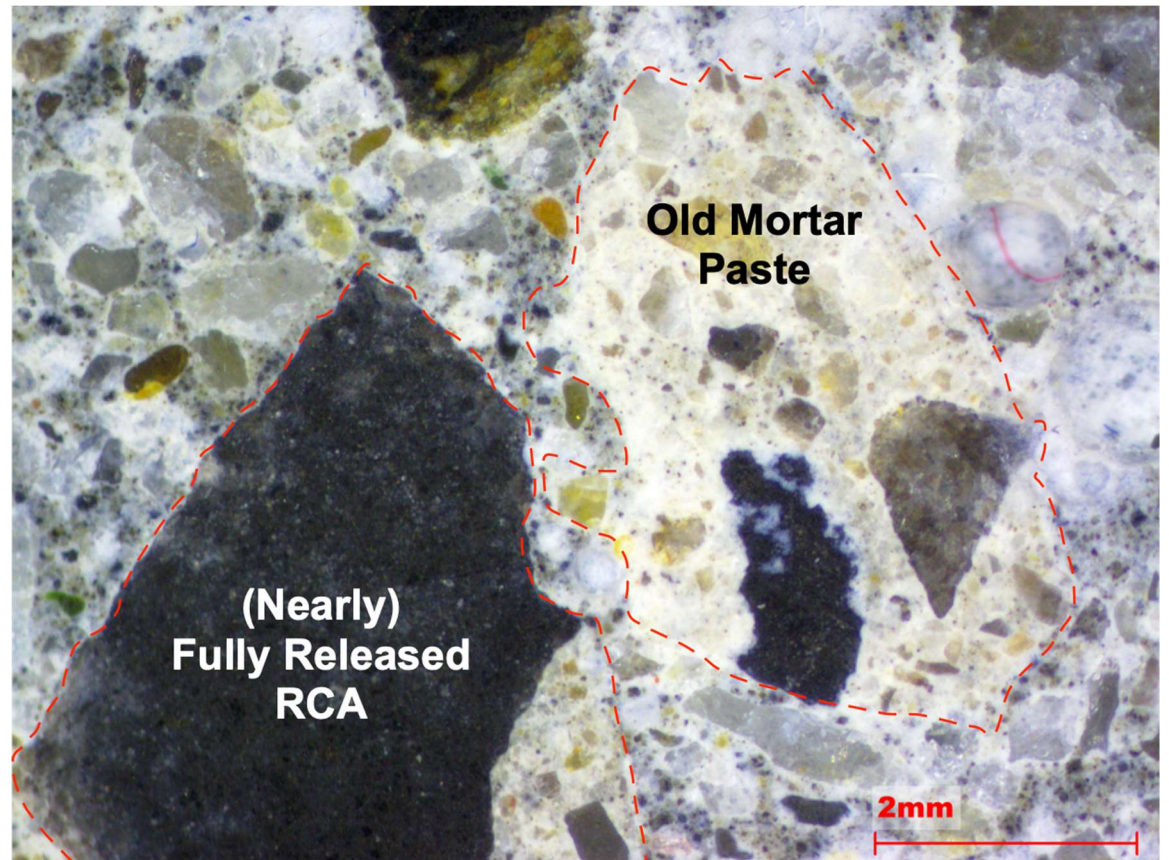


[Fanara, 2020]

Background

Influence of RCA

- RCA: increased porosity and water absorption

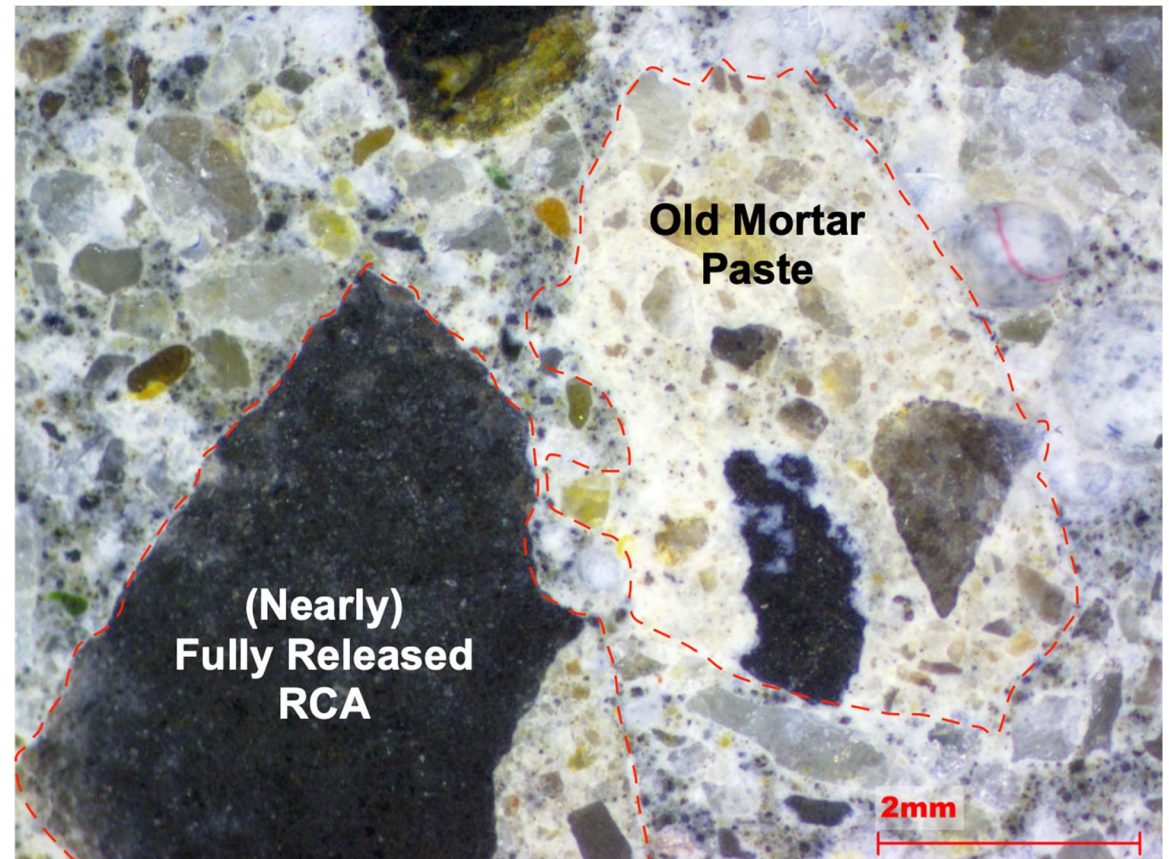


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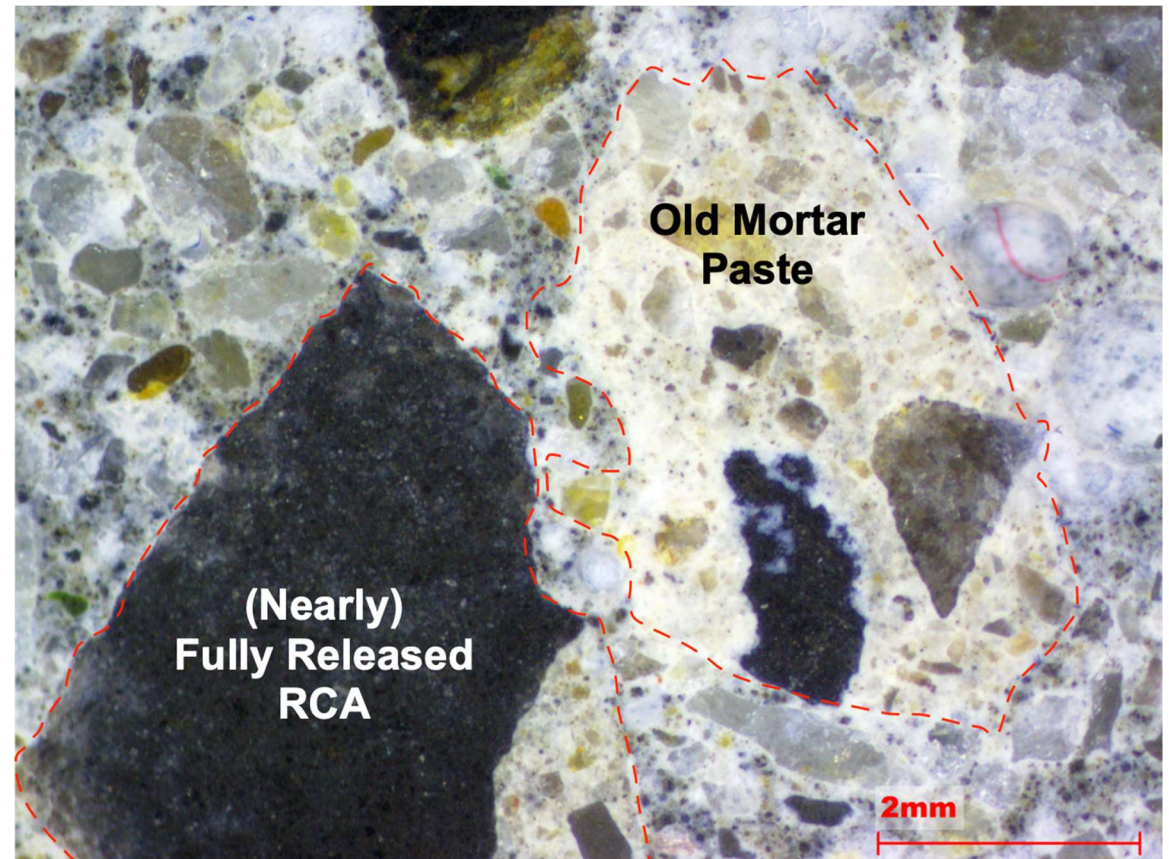


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- The chloride corrosion rate is maximum at around 85% RH

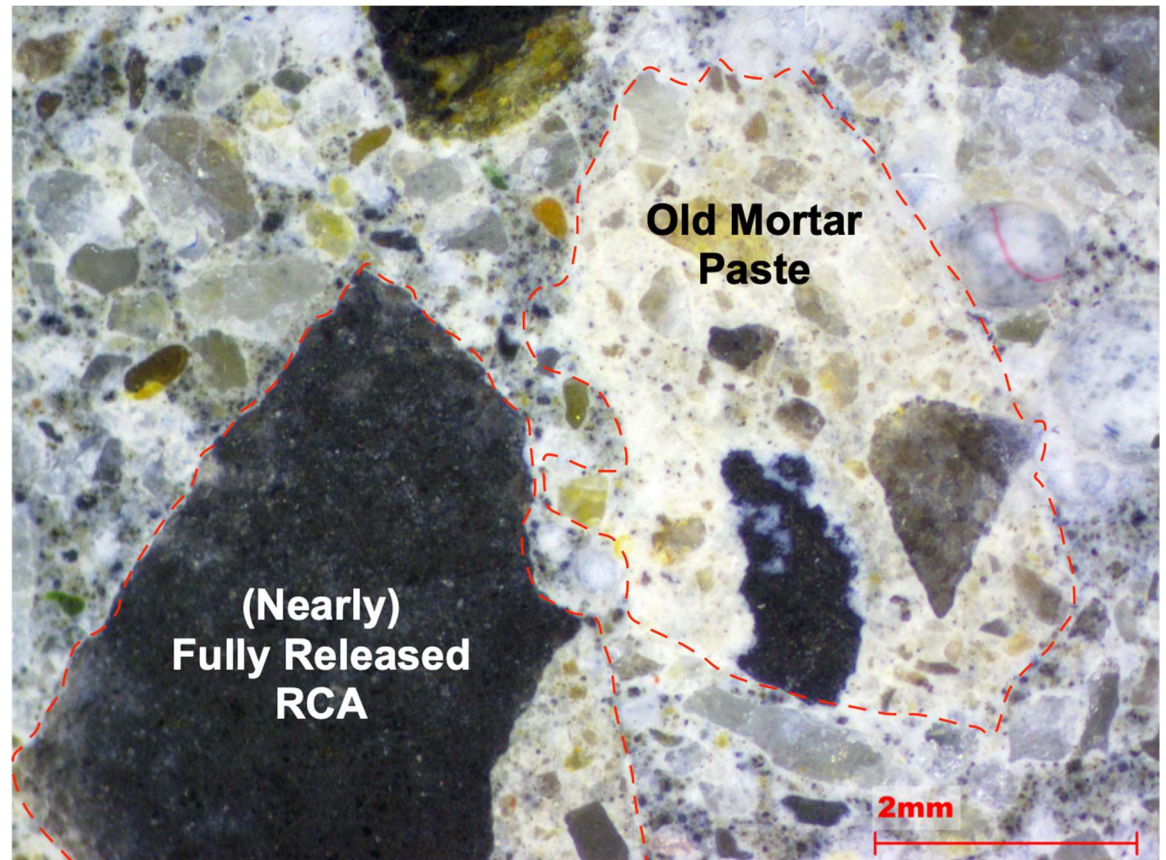


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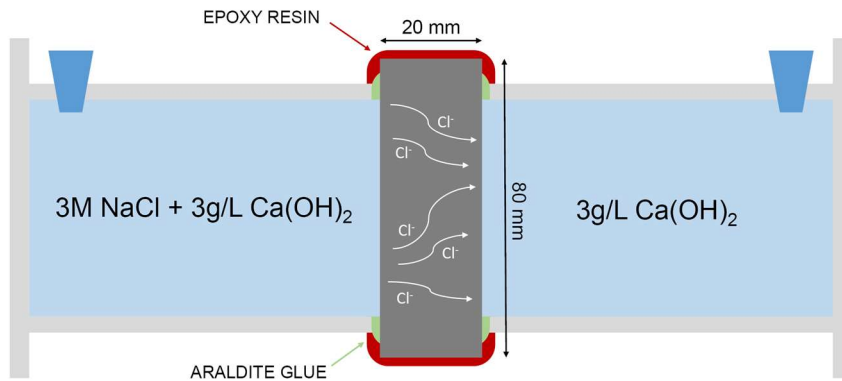
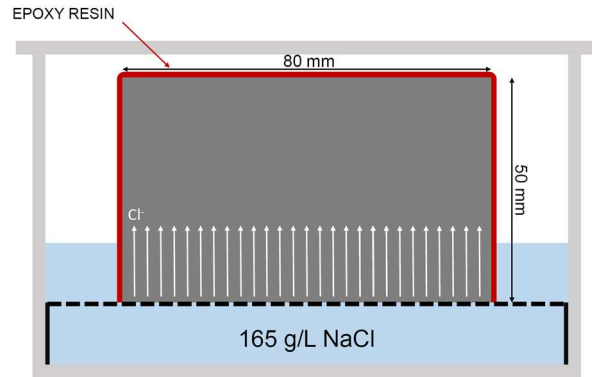


[Fanara, 2020]

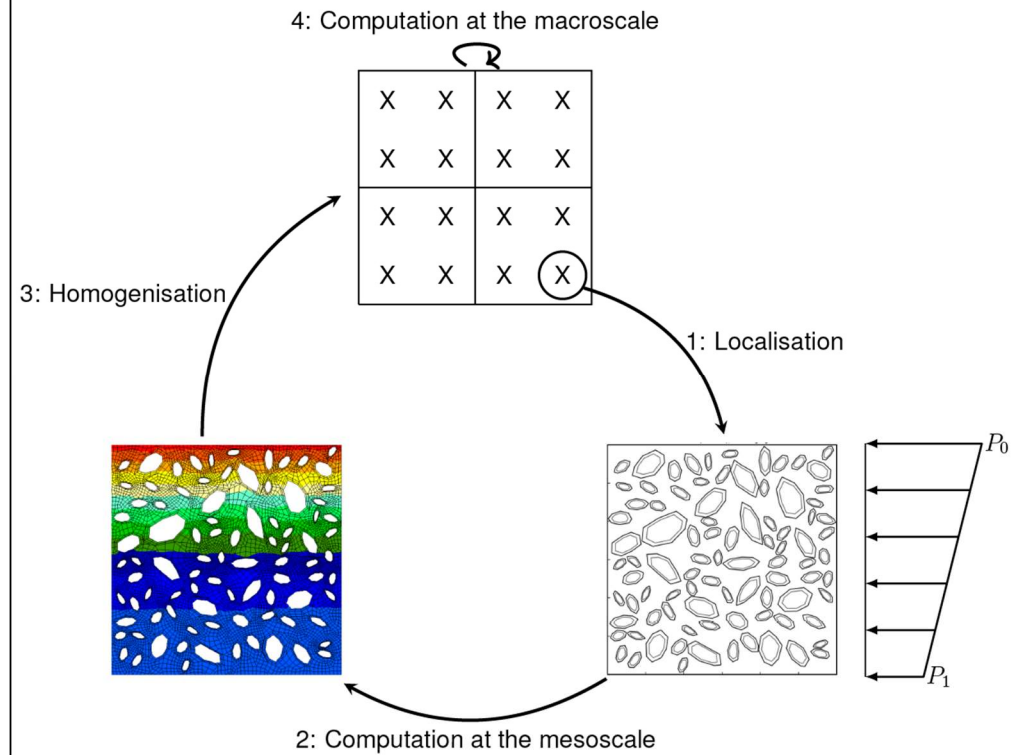
→ Influence of RCA on chloride attacks ?

Goals of this study

Experimental



Numerical



1. Introduction

2. Materials

3. Experimental Plan

4. Experimental Results

5. Numerical Validation with Experimental Results

6. Conclusion

Materials

- 3 main materials:

Materials

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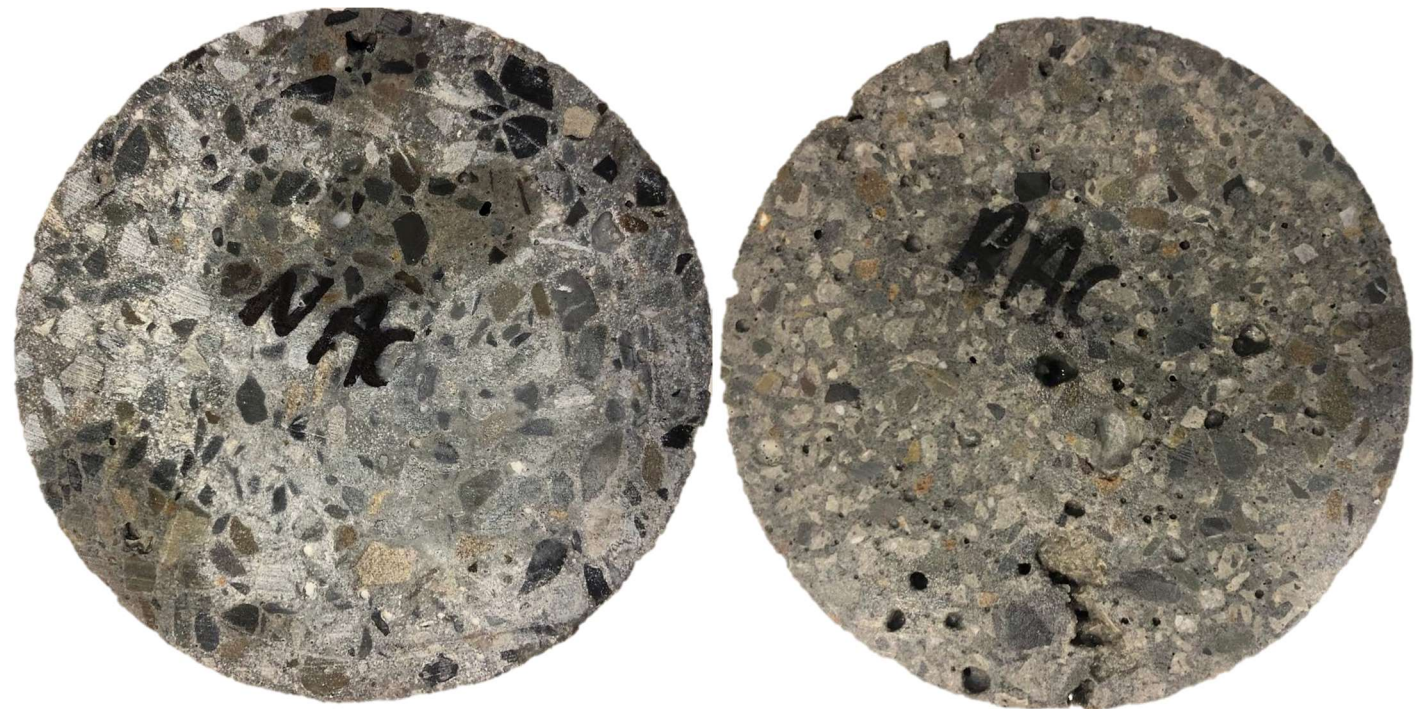
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- 3 main materials:
 - **NAC**: concrete with 2/7 limestone aggregates



Materials

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 - **NAC**: concrete with 2/7 limestone aggregates
 - **RAC**: concrete with 2/7 RCA (constant volume fraction and reconstructed PSD)



Materials

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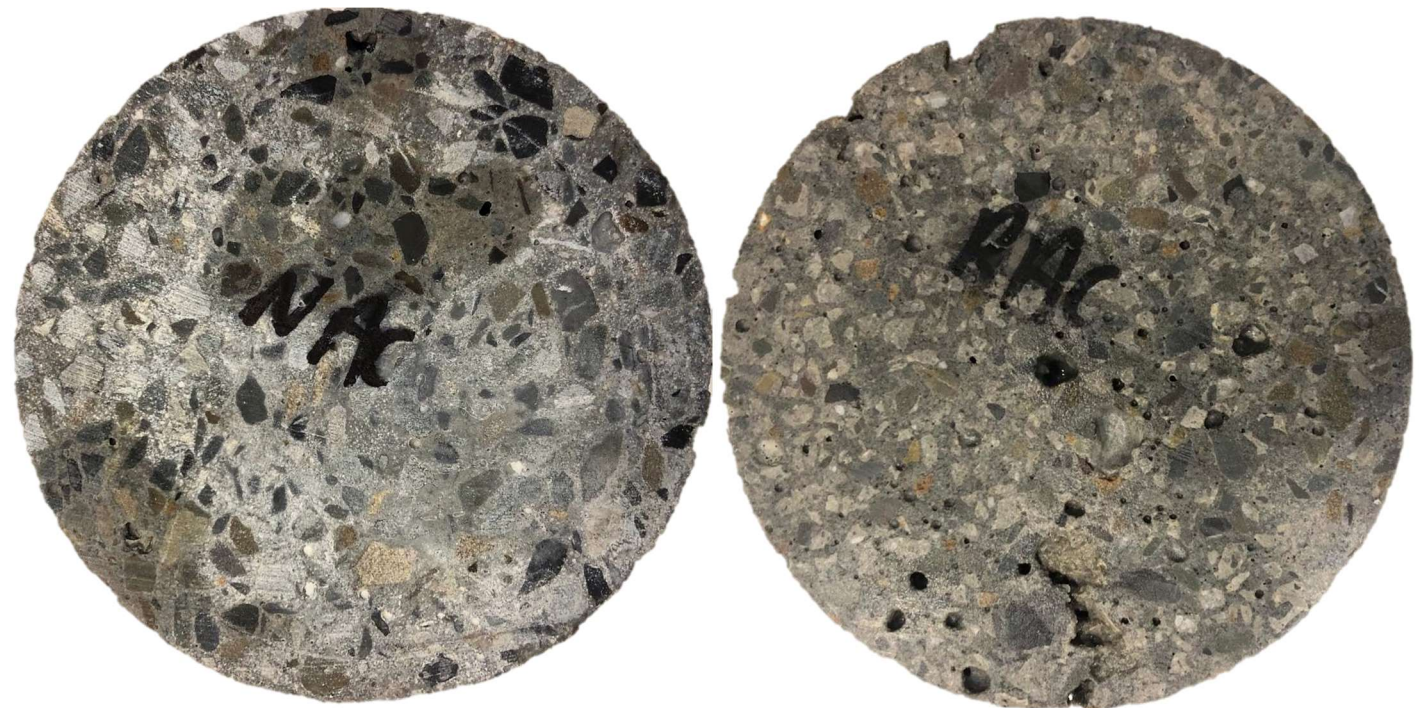
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 - **E-M**: equivalent mortar with 0/2 Rhine sand



Materials

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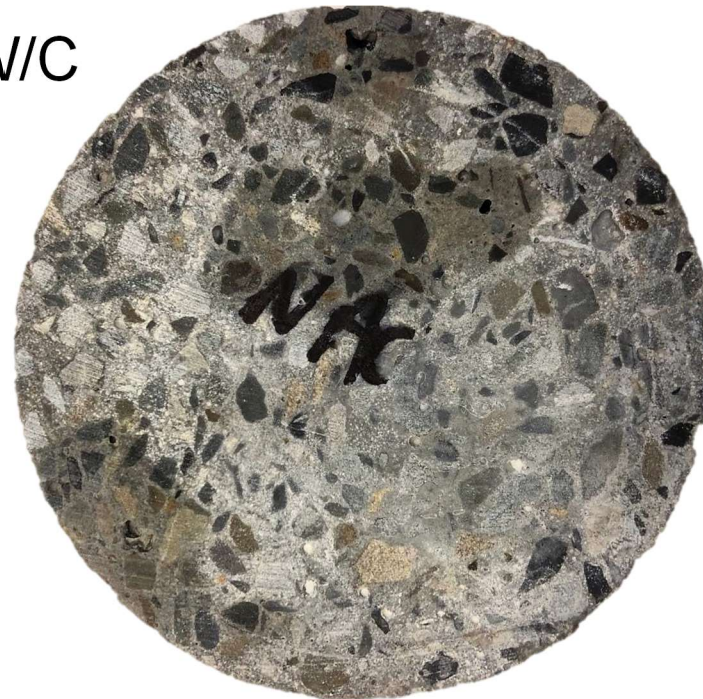
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Experimental Plan

Water transfer properties

- Water Absorption by Immersion (NBN B 15-215:2018 and NBN EN 772-4)
 - Dry and humid densities, water absorption and water accessible porosity



Experimental Plan

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 - Intrinsic permeability of the porous media



Experimental Plan

Water transfer properties

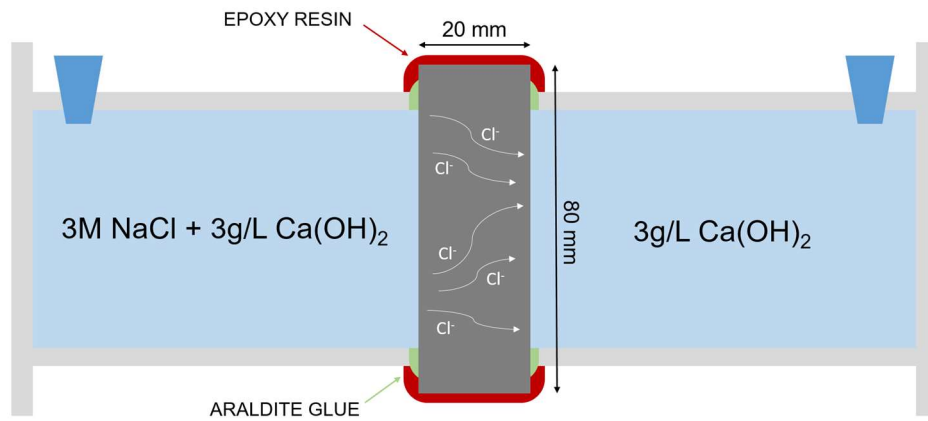
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- Static sorption and desorption
 - Water Retention Curves



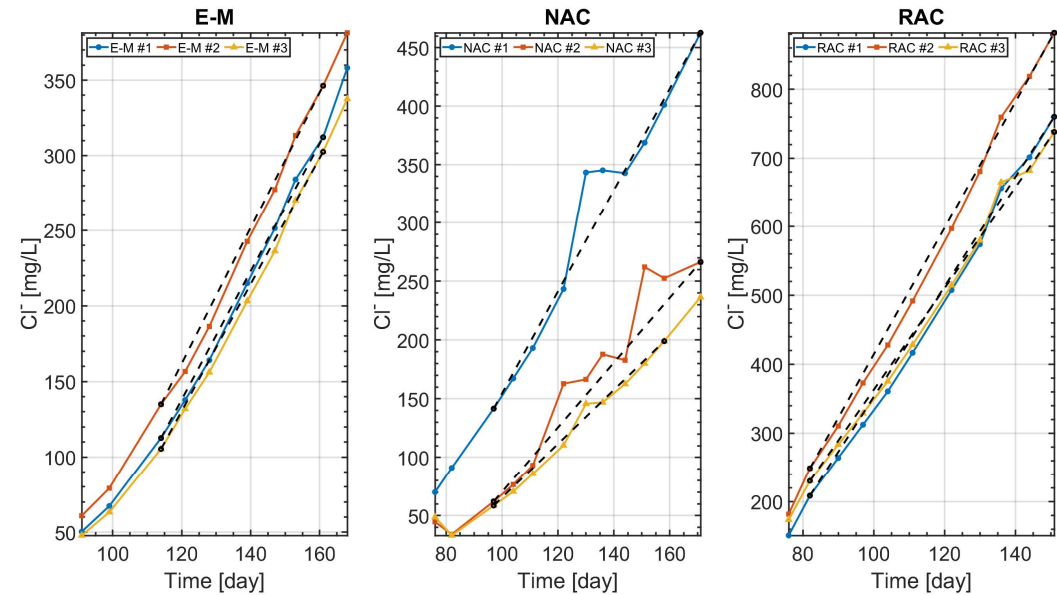
Experimental Plan

Chloride ions transfer properties

- Chloride Diffusion under steady-state



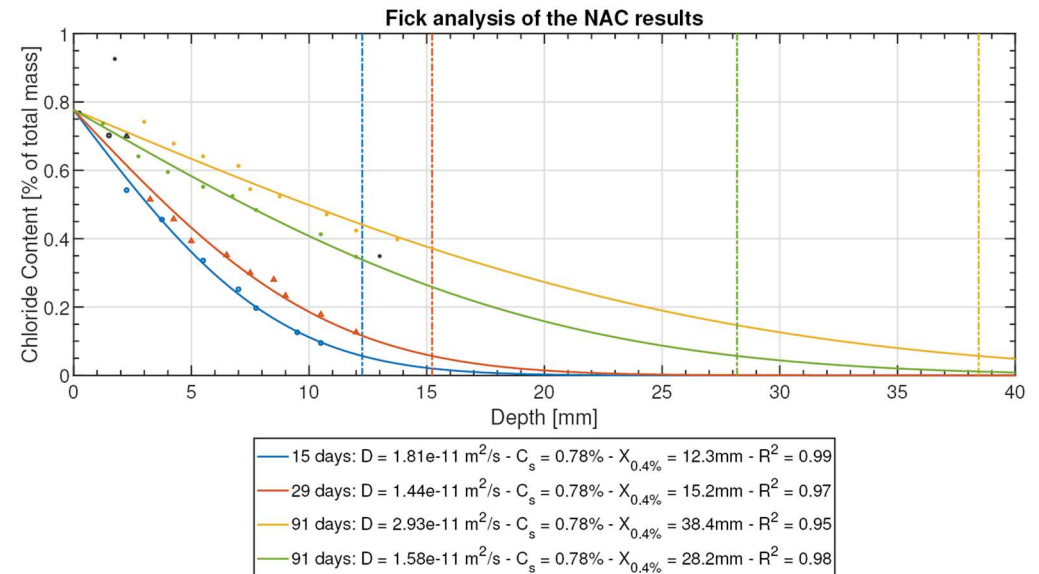
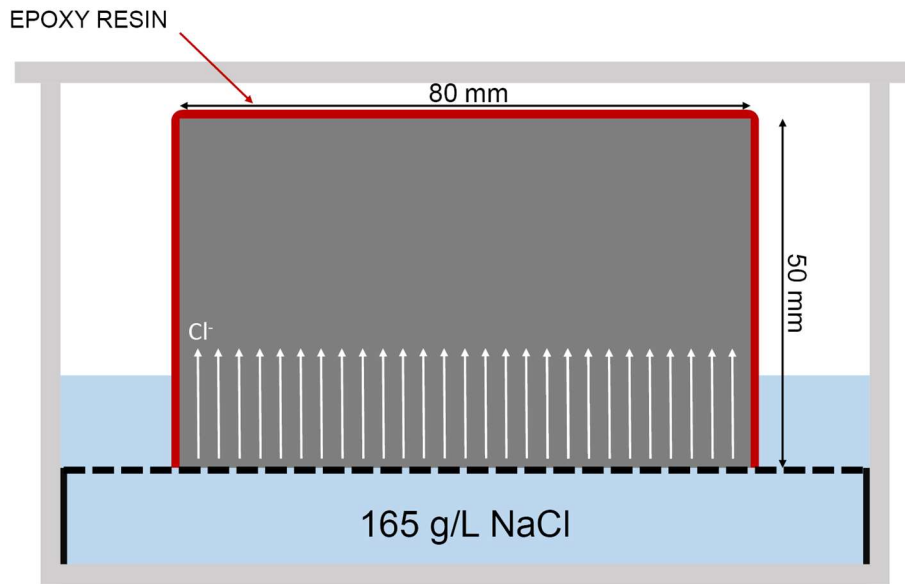
Chloride Diffusion Experiment in Steady State



Experimental Plan

Chloride ions transfer properties

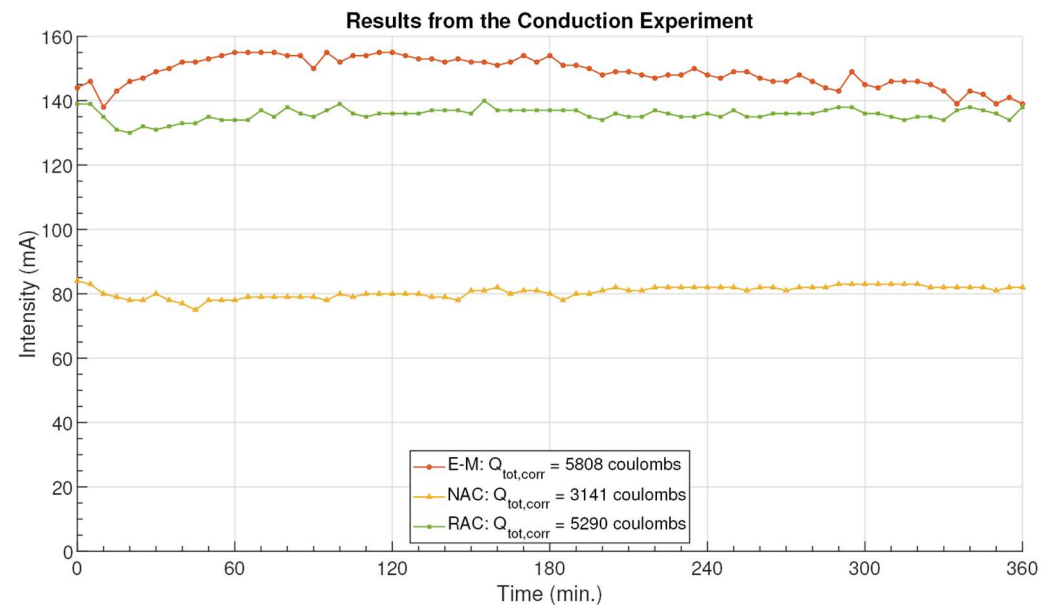
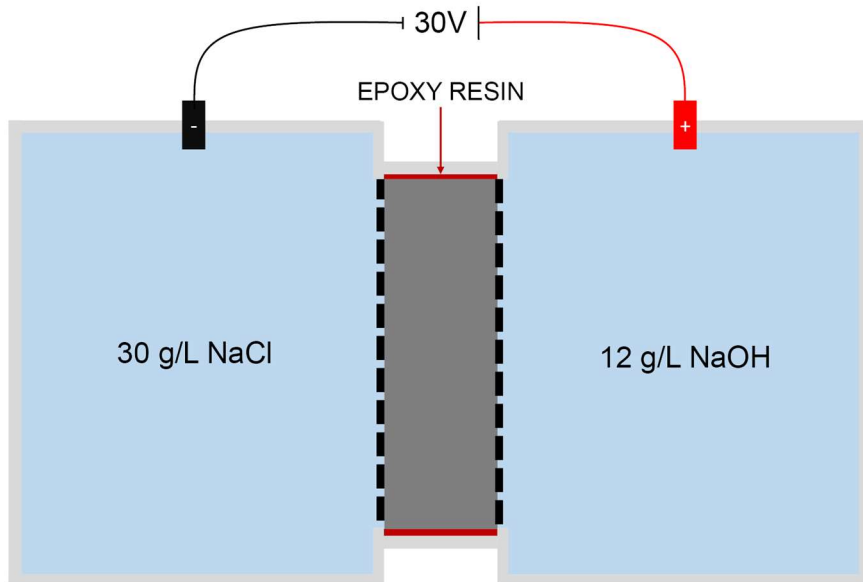
- Chloride Diffusion under steady-state
- **Chloride Diffusion under unsteady-state**



Experimental Plan

Chloride ions transfer properties

- Chloride Diffusion under steady-state
- Chloride Diffusion under unsteady-state
- **Conduction**



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Experimental Results

Water transfer properties

- $n, WA: E-M (22.83\%V, 11.27\%M) > RAC (20.5\%V, 9.95\%M) > NAC (14.16\%V, 6.26\%M)$
 - The porosity is induced by the mortar matrix (aggregates and sand rather not porous)

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- WRC: RAC \approx E-M > NAC
 - The RAC has a greater exchange rate of moisture with its environment than the NAC.

Experimental Results

Chloride ions transfer properties

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- Diffusion under steady-state:
 - RAC ($15.4E-13 \text{ m}^2/\text{s}$) > E-M ($8.17E-13 \text{ m}^2/\text{s}$) > NAC ($5.99E-13 \text{ m}^2/\text{s}$)

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 - E-M (1.45%) > RAC (1.27%) > NAC (0.78%) of surface concentration

Experimental Results

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- Conduction: E-M (5808 Coulombs) > RAC (5290 Coulombs) > NAC (3141 Coulombs)



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Multiscale modelling

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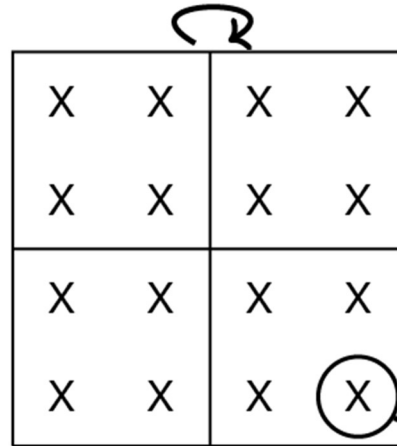
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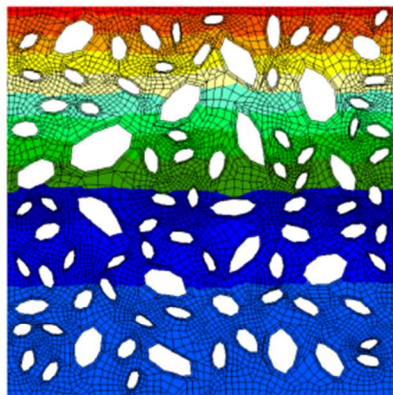


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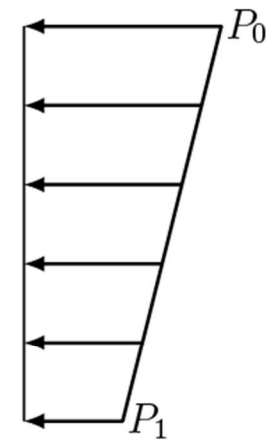
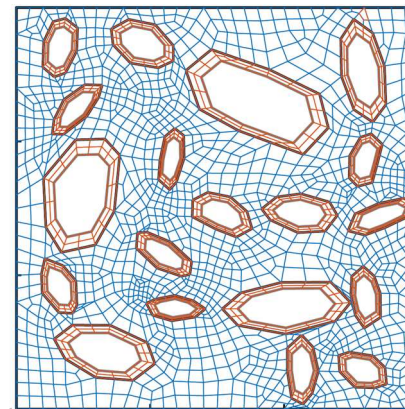
4: Computation at the macroscale



3: Homogenisation



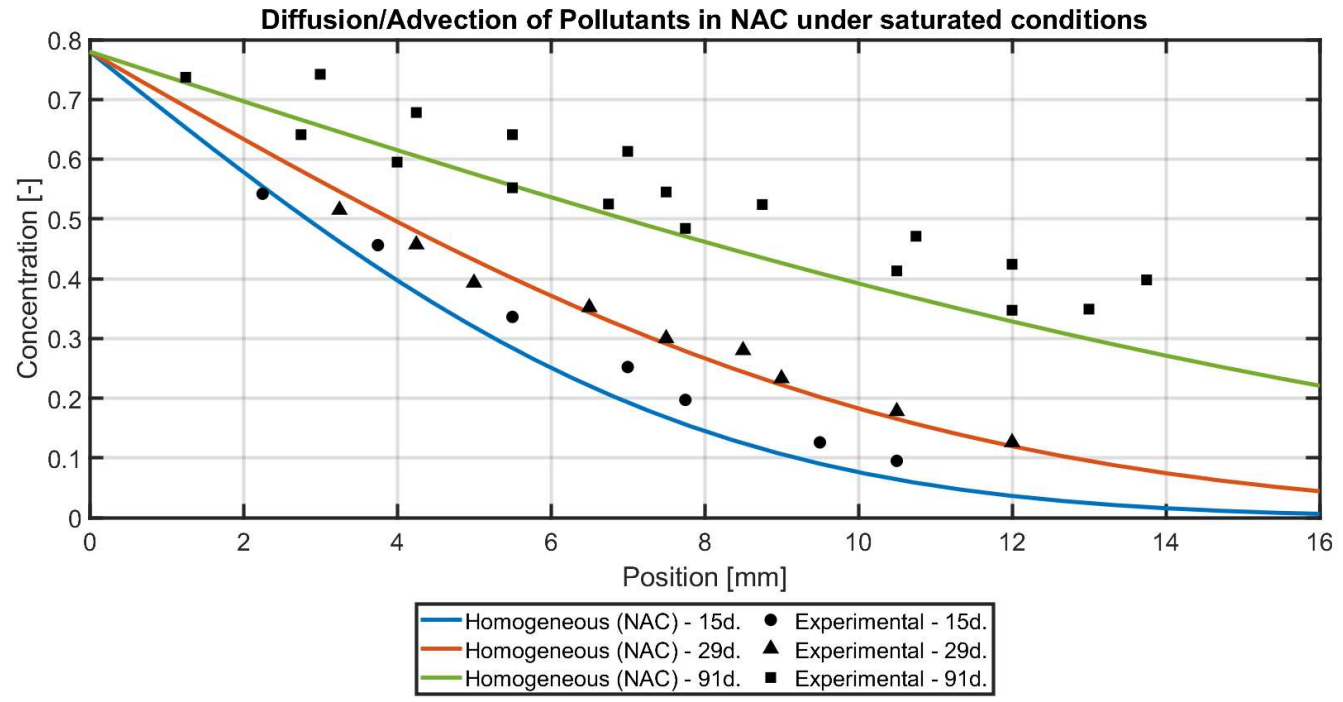
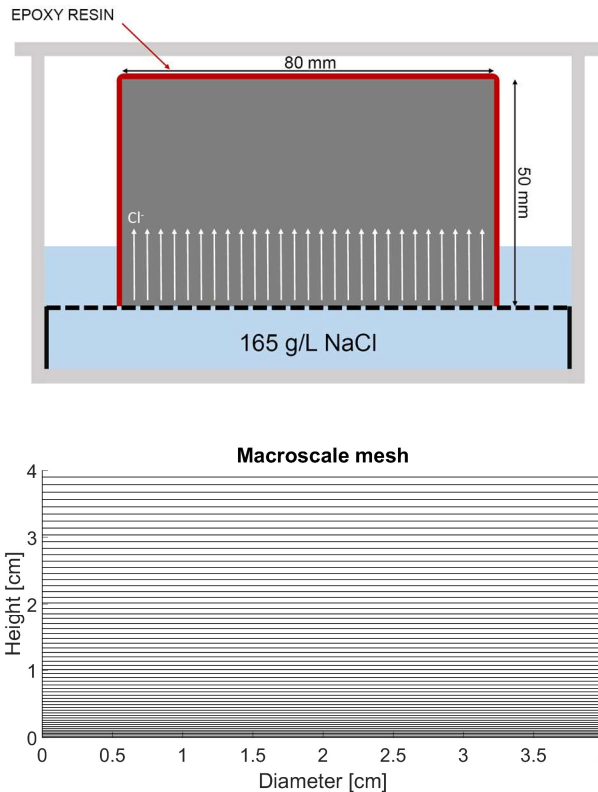
1: Localisation



2: Computation at the microscale*,
under permanent flow hypothesis

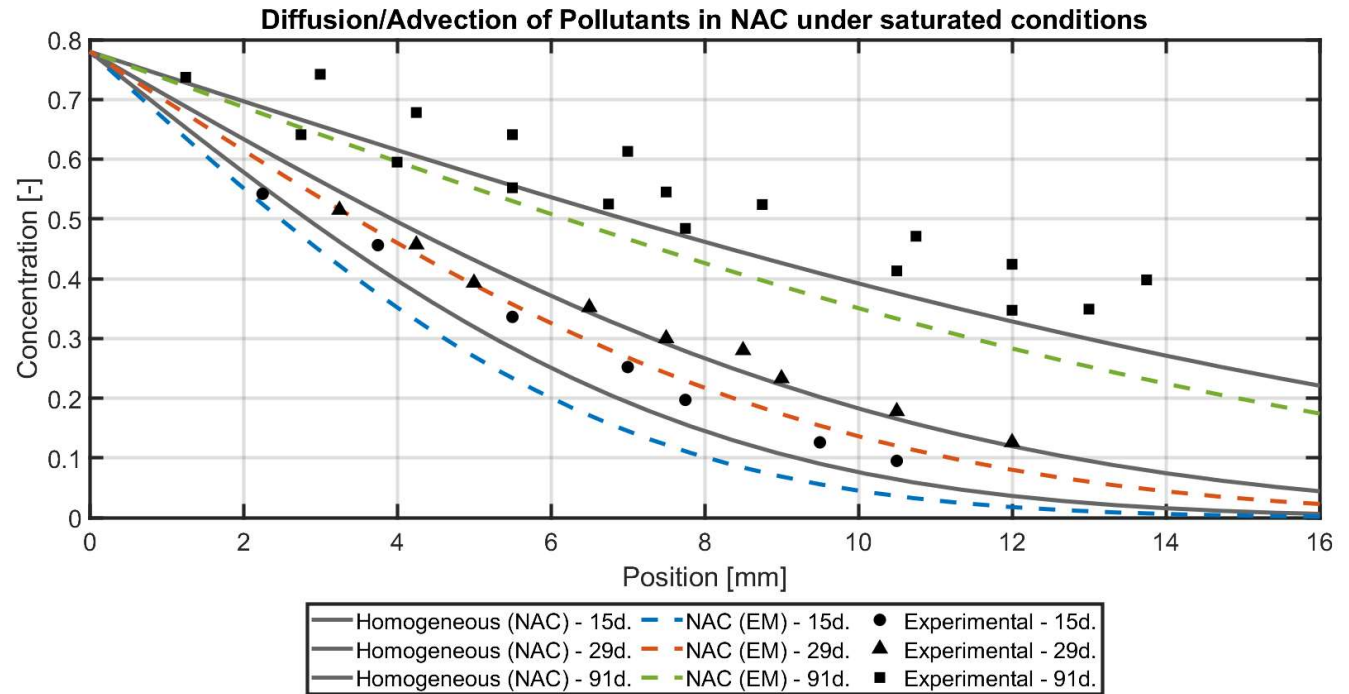
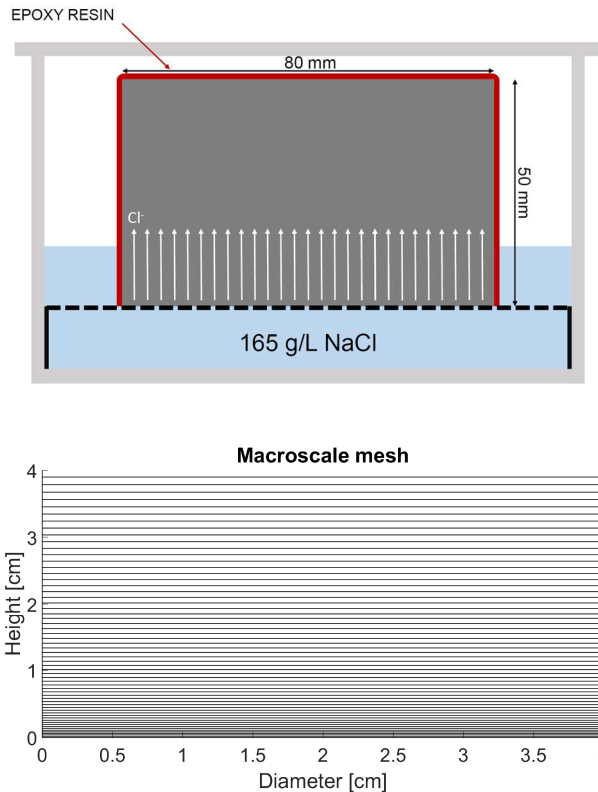
*Our microscale
is in the order of
the centimetre

Experimental modelling - NAC



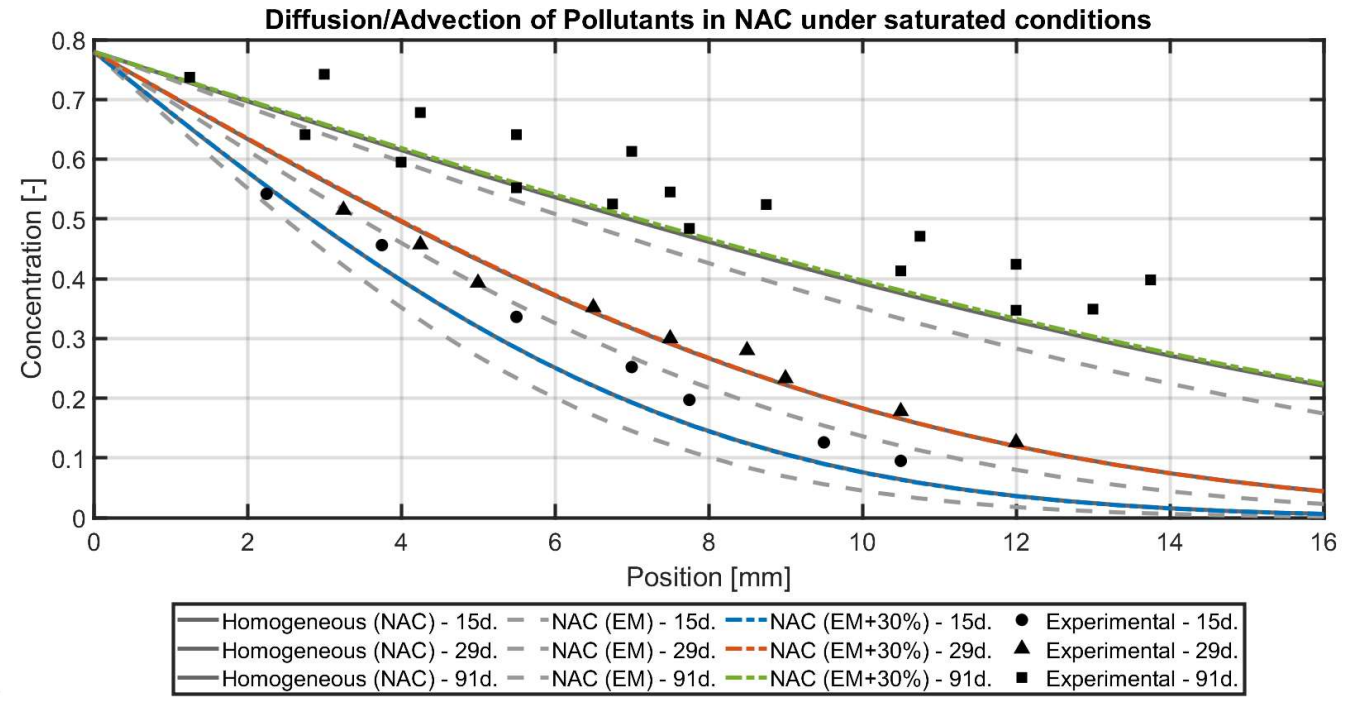
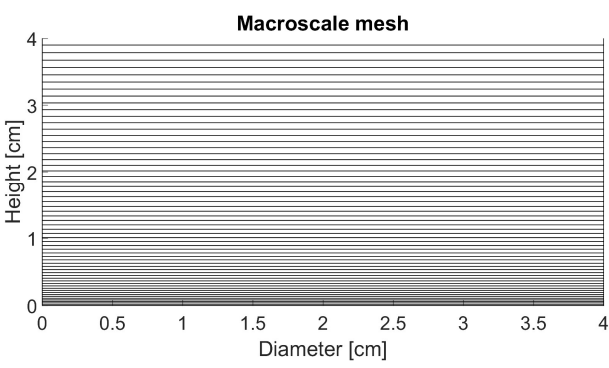
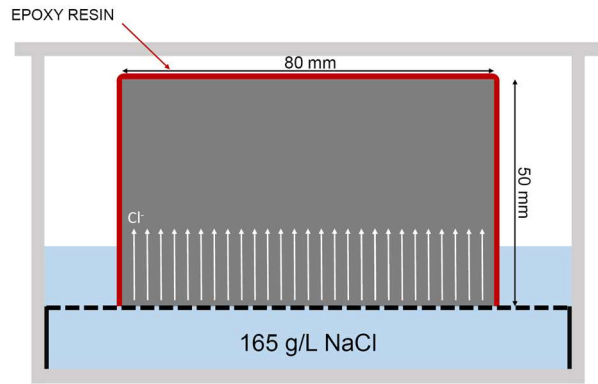
- For NAC microstructure with EM+30% Diffusion Coefficient, the numerical results are close enough to the experimental (and analytical) analysis. Other studies have found an increase of up to 40% of the diffusion in 3D compared to 2D [Nilenius, 2014]

Experimental modelling - NAC



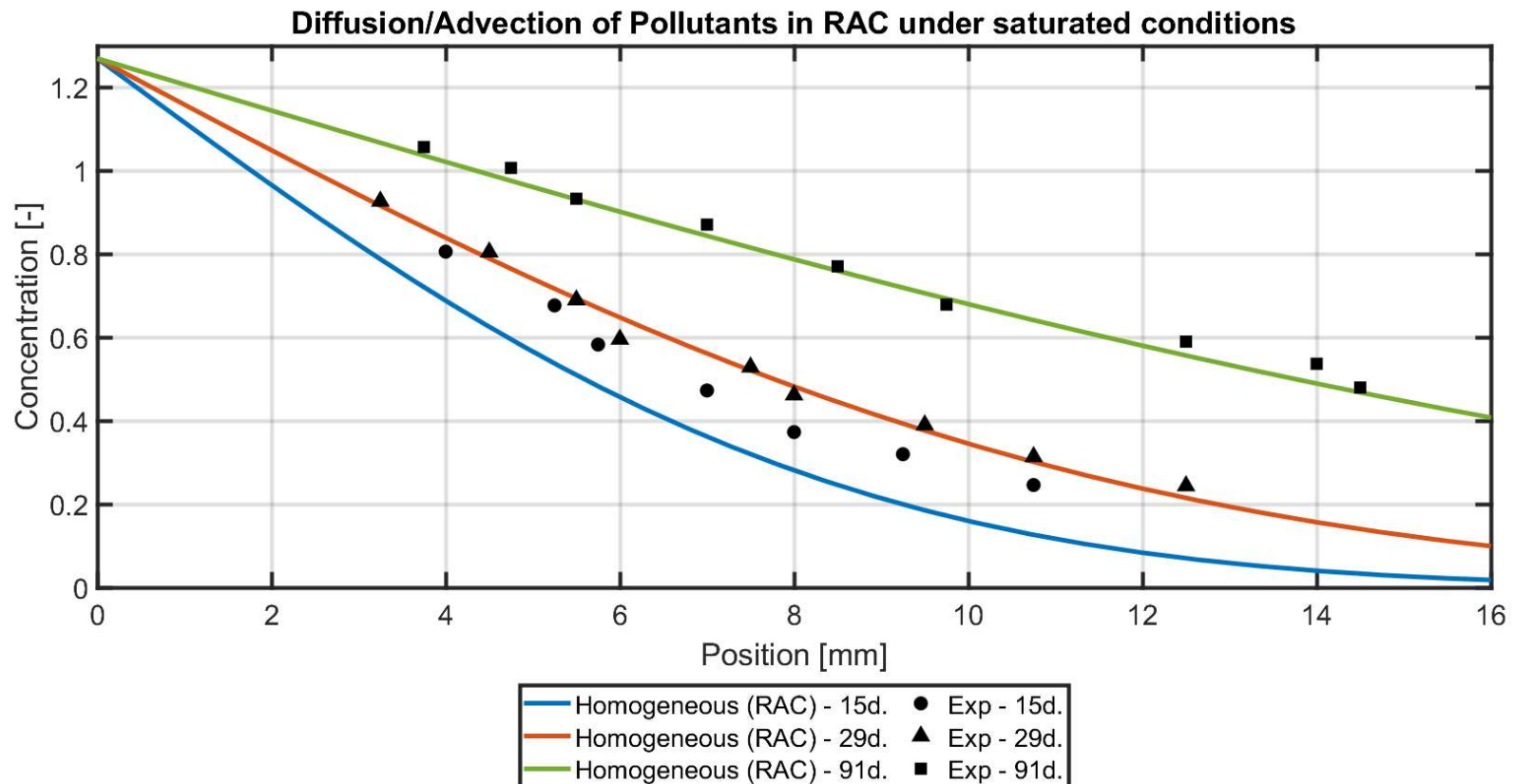
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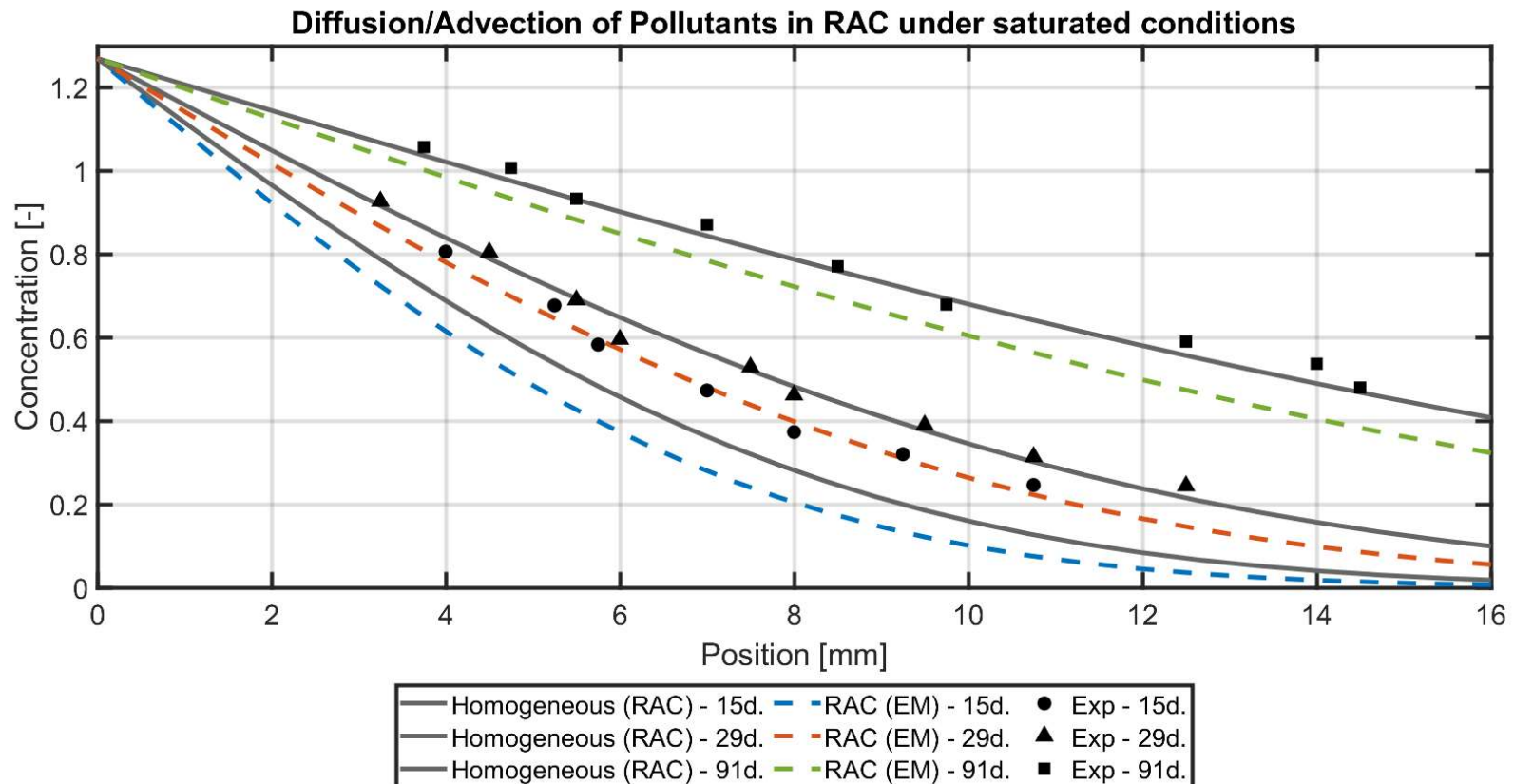
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Experimental modelling - RAC



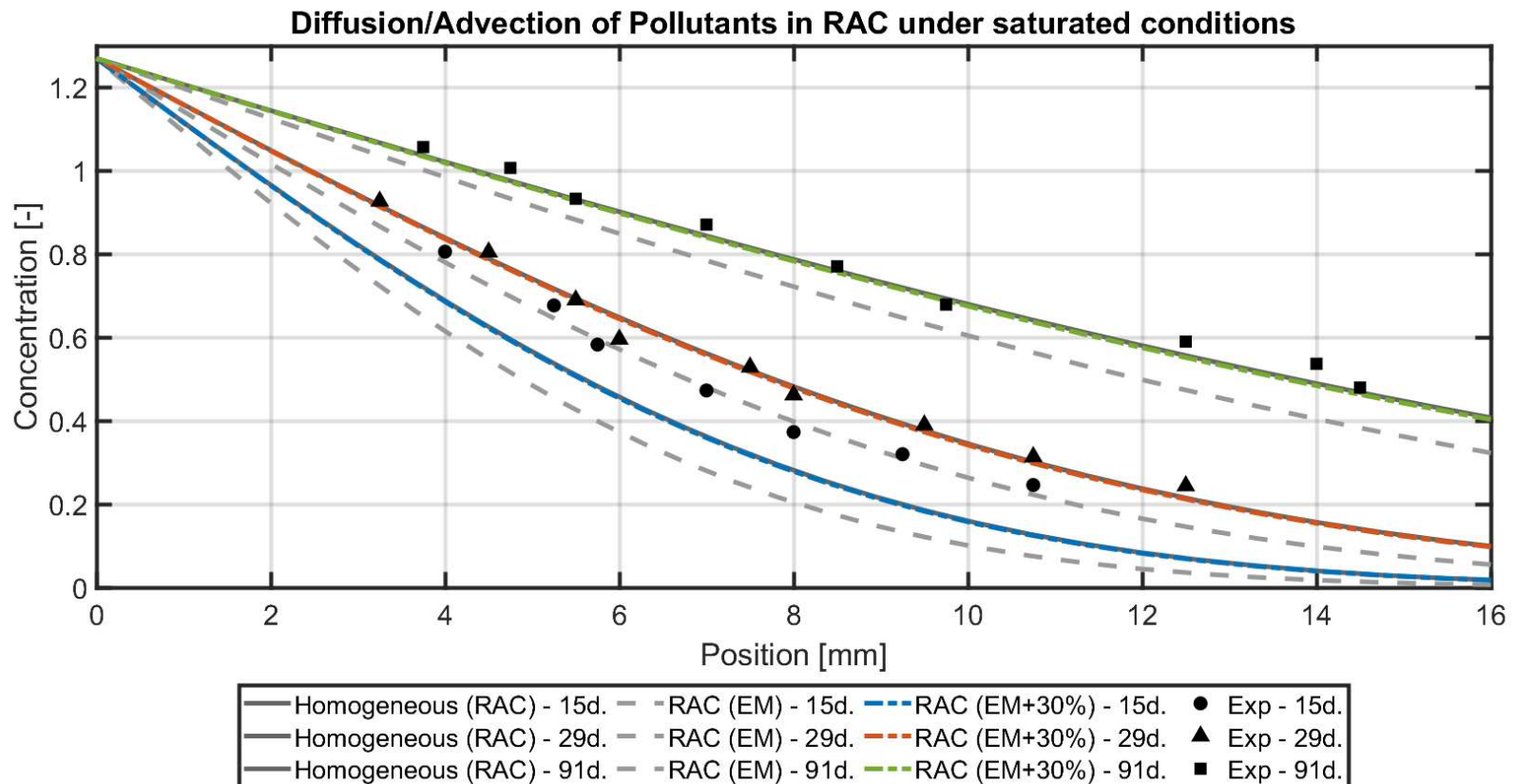
- For RAC microstructure with EM+30% Diffusion Coefficient, the numerical results are close enough to the experimental (and analytical) analysis.

Experimental modelling - RAC



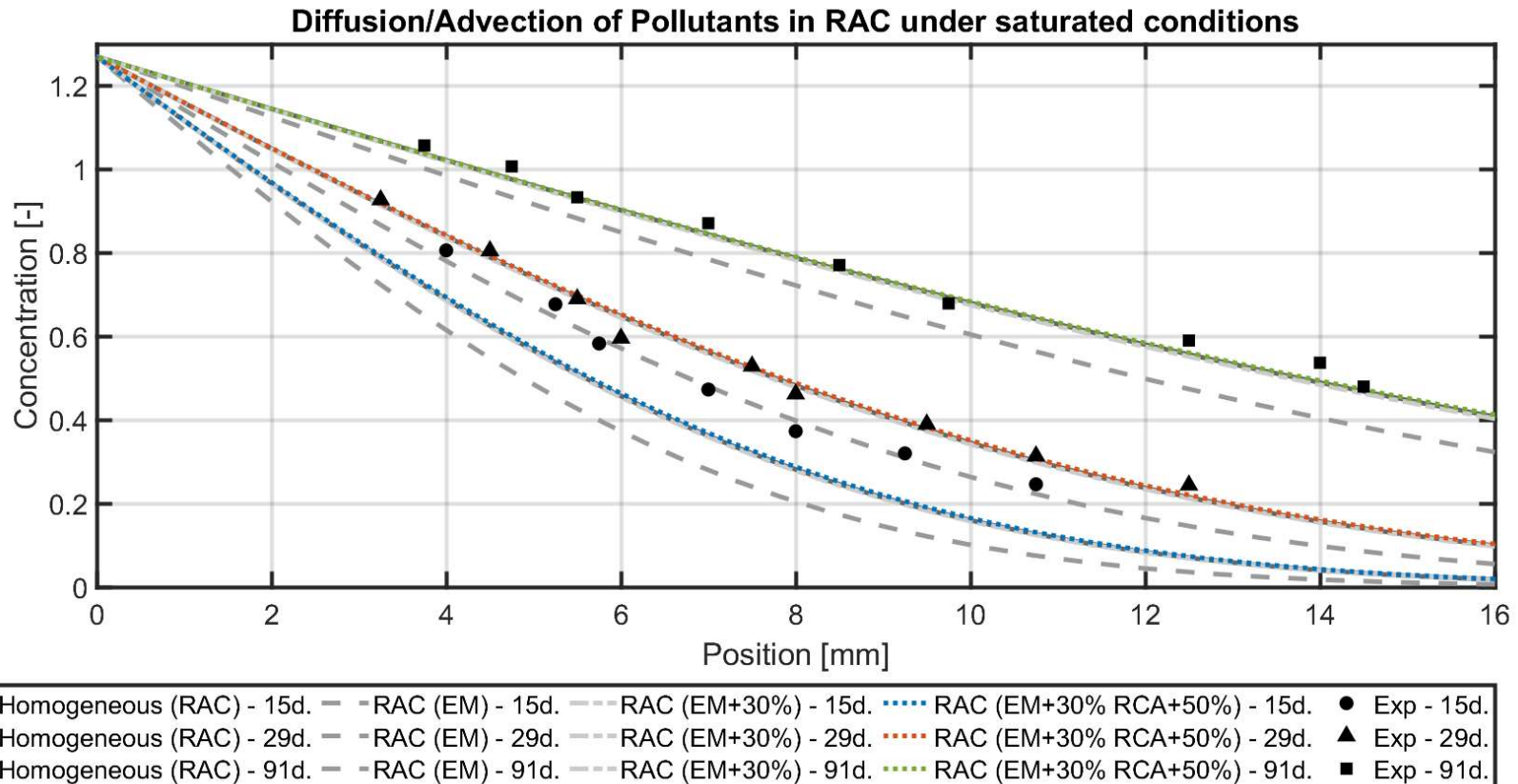
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Experimental modelling - RAC



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Thank you for your attention.

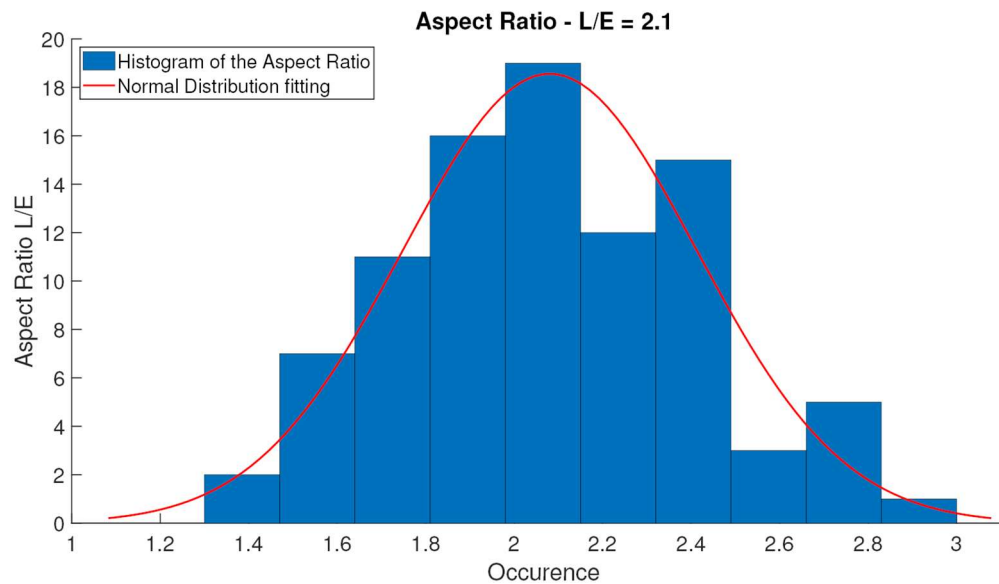
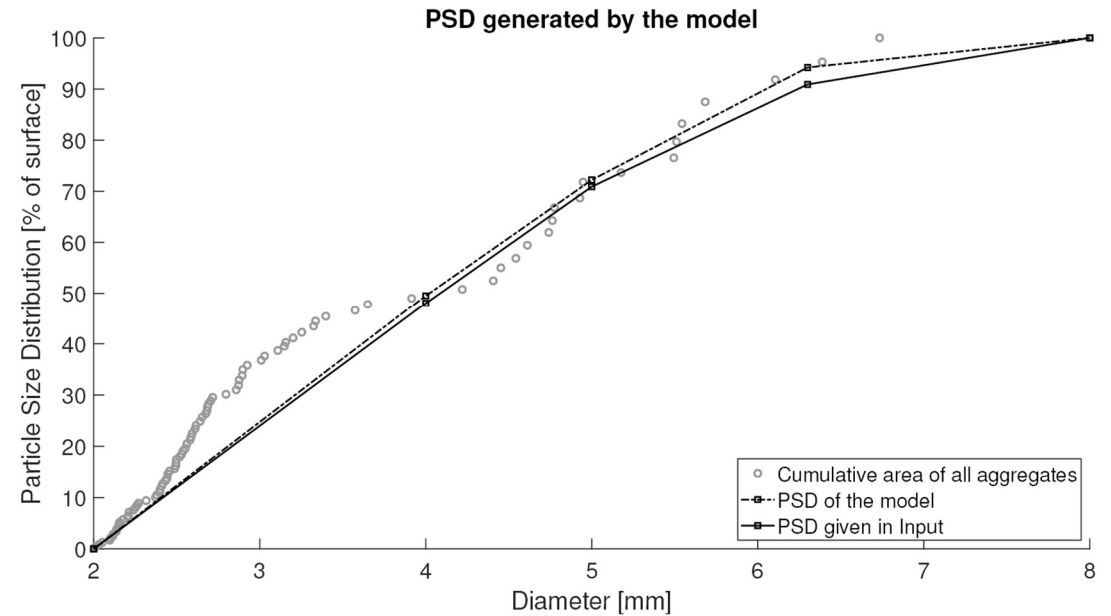
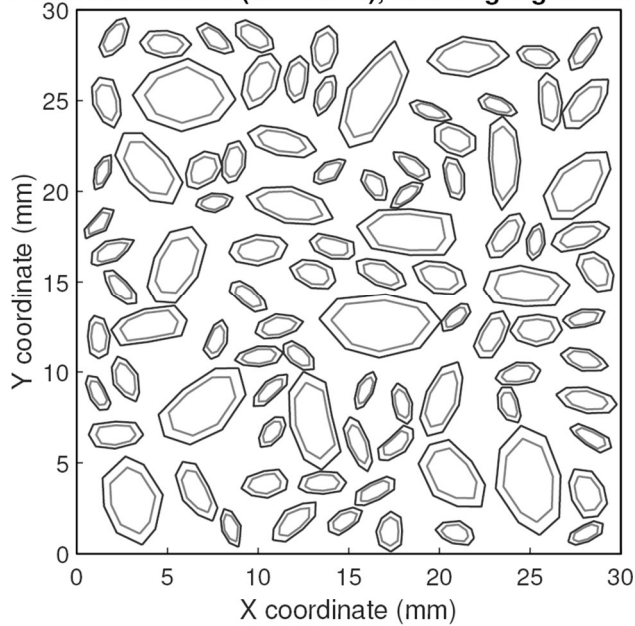
This work is co-funded by the FNRS and the Wallonia Regional Government in the framework of a FRIA grant.

RVE: parameters/results

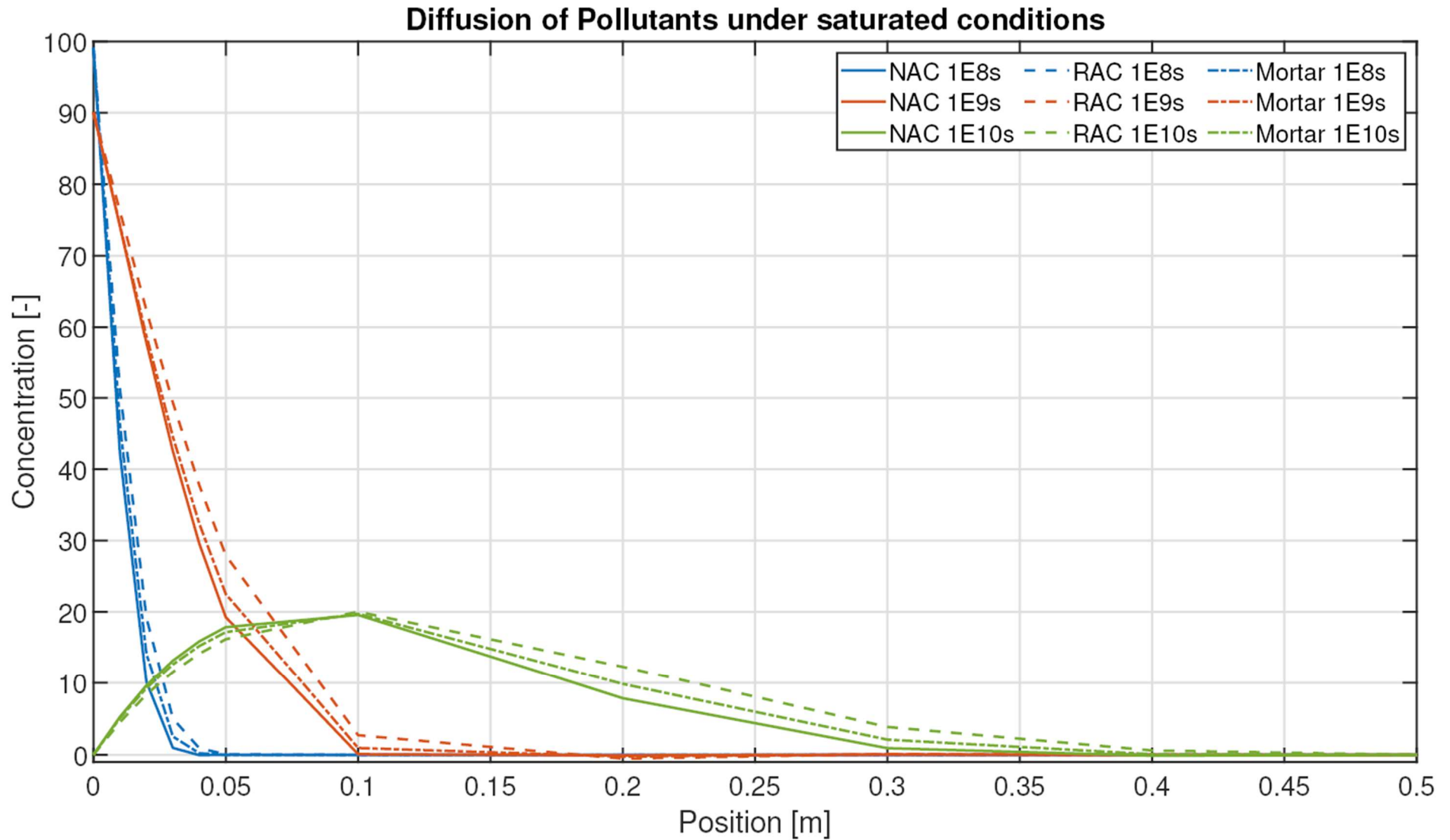
- PSD: 2-4mm 48%, 4-5mm 22.9%, 5-6.3mm 20%, 6.3-8mm 9.1%
- SF: 41% Volume/Surface for both NAC and RAC (mix hypothesis)
- AR: between 1.5 and 2.5
- % Adherent mortar in RCA (+-5%) : 50% for 2-4mm, 45% for 4-5mm, 40% for 5-6.3mm, 35% for 6.3-8mm
[de Juan & Gutiérrez, 2009][Akbarnezhad et al., 2013][Florea & Brouwers, 2013].

RVE: parameters/results

RVE - 60.7% of mortar (vs. 58.9%), 18% of gangue and L/E = 2.1



RVE: RCA influence



- Equal properties, except for RCA: 5x more diffusive

Analytical Validation

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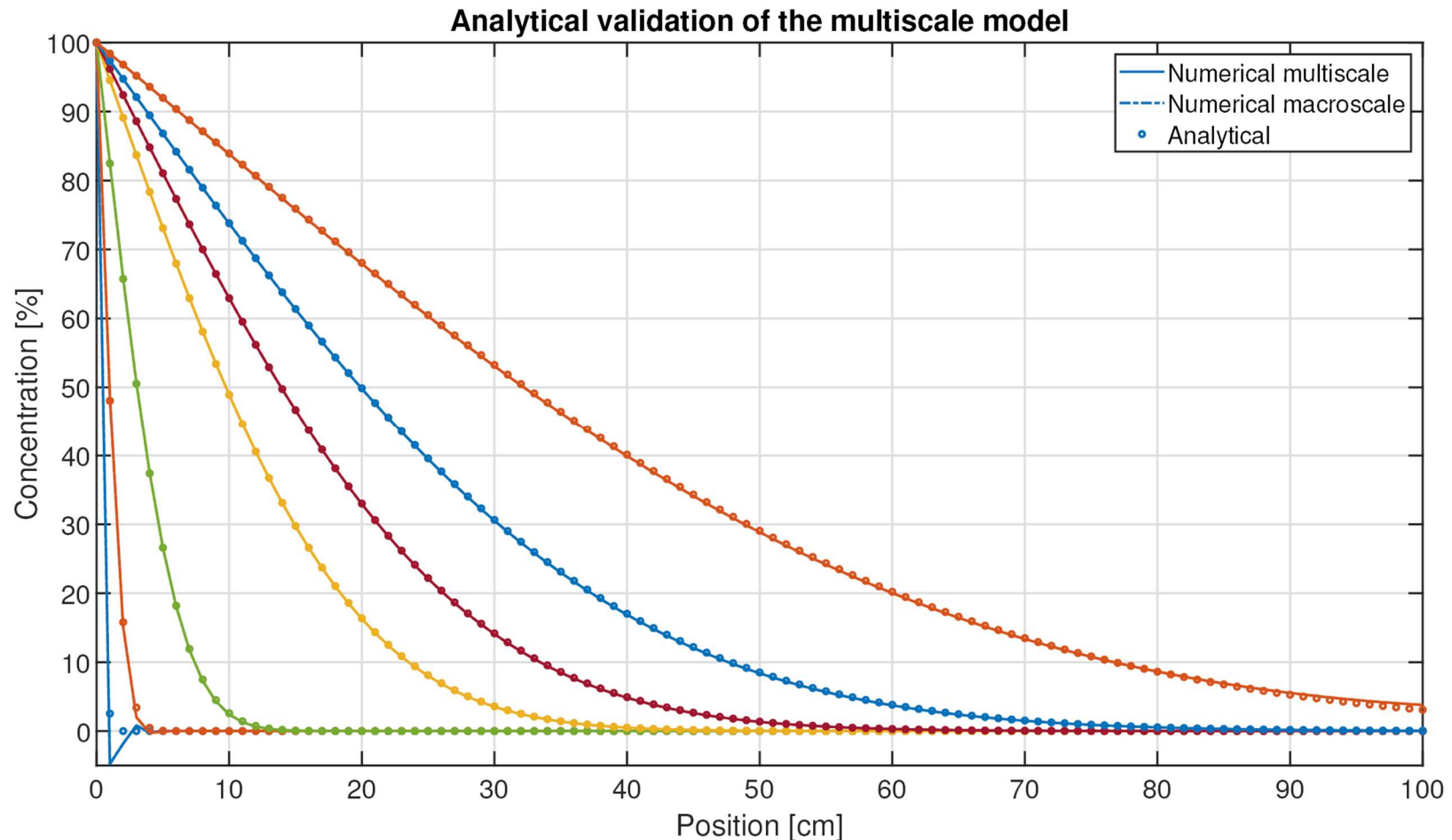
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Analytical solution for a 1D semi-infinite medium [Biver, 1993]:

$$C(x, t) = \frac{C_0}{2} \exp\left(\frac{ux}{2D}\right) \left[\exp\left(-x\frac{u}{2D}\right) \operatorname{erfc}\left(\frac{x}{2\sqrt{Dt}} - \sqrt{\frac{u^2t}{4D}}\right) + \exp\left(x\frac{u}{2D}\right) \operatorname{erfc}\left(\frac{x}{2\sqrt{Dt}} + \sqrt{\frac{u^2t}{4D}}\right) \right] \quad (1)$$

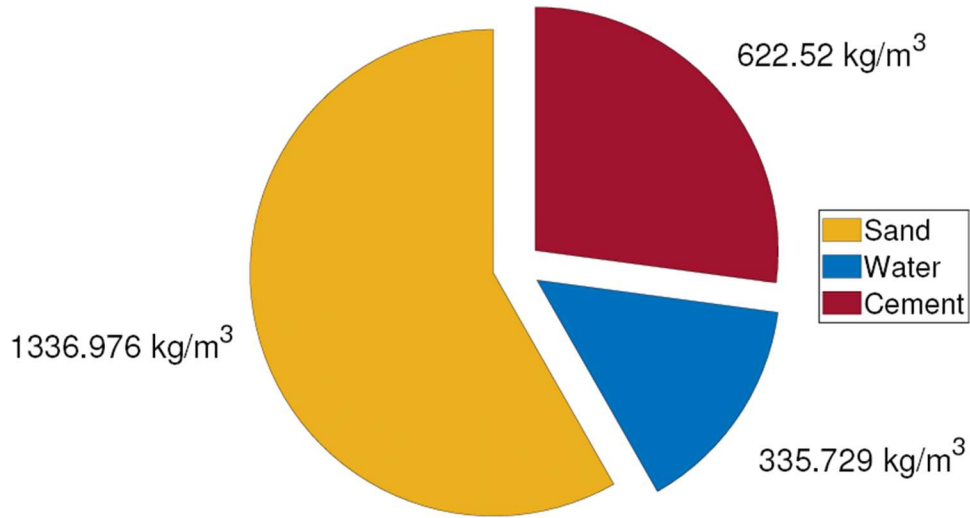


Case	C_0 [mg/ml]	D [cm^2/s]	u [cm/s]
$u \neq 0$	100	1E-8	4E-11

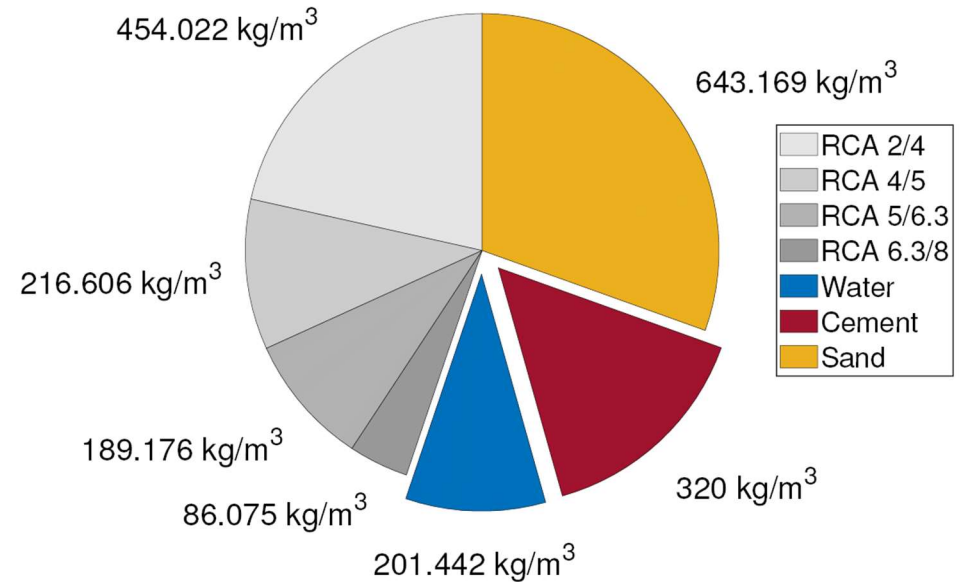
$$u = \frac{k_{int}}{\mu_w} \frac{\partial P_w}{\partial x} = \frac{10^{-19}}{10^{-3}} \frac{105325 - 101325}{1} = 4 * 10^{-11} \text{ cm/s} \quad (4)$$

Experimental compositions

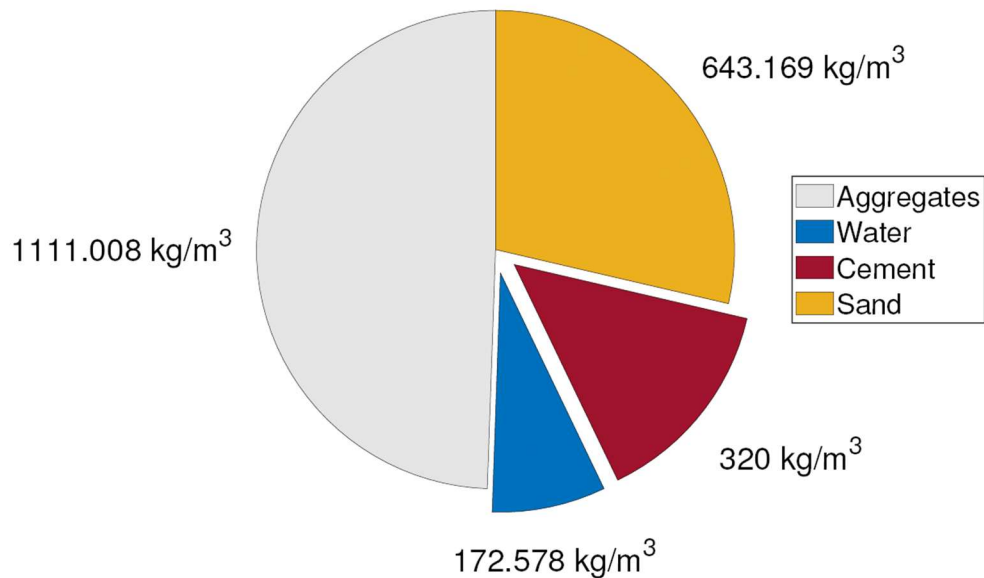
Composition of the E-M (W/C = 0.54)



Composition of the RAC (W/C = 0.63)

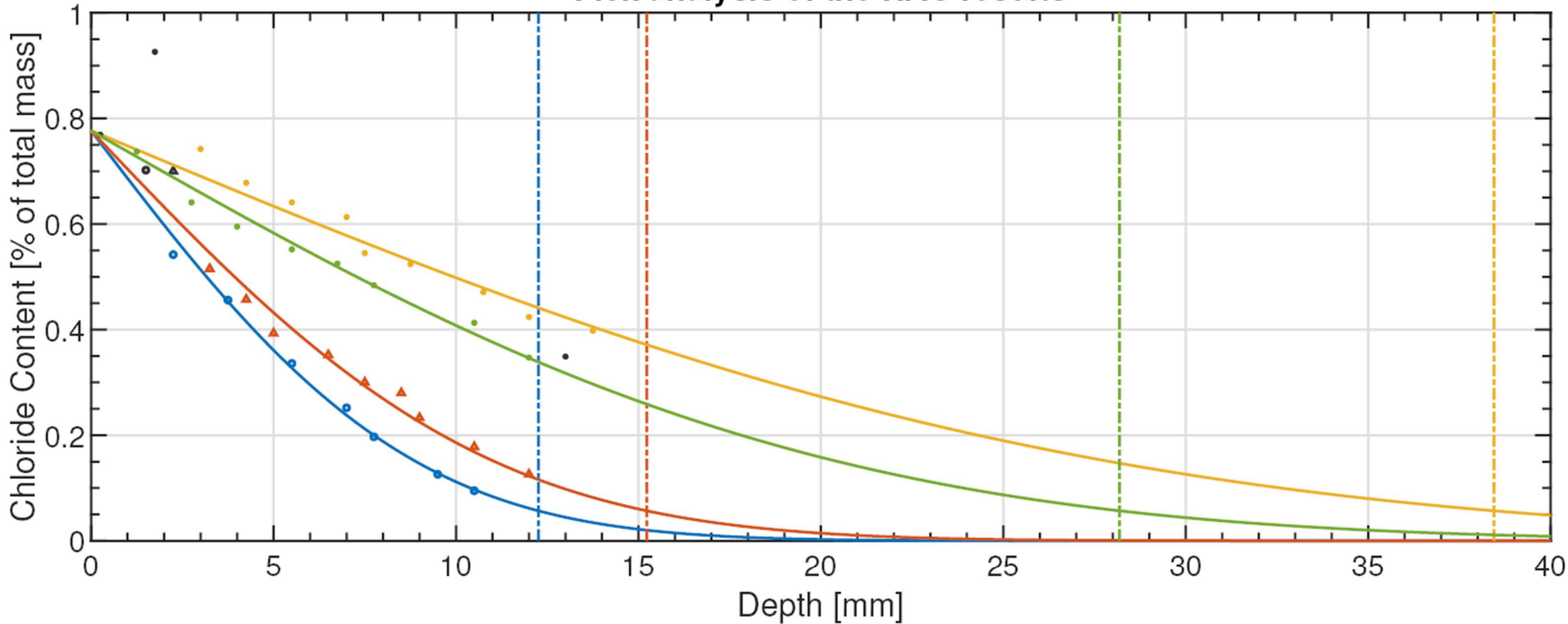


Composition of the NAC (W/C = 0.54)



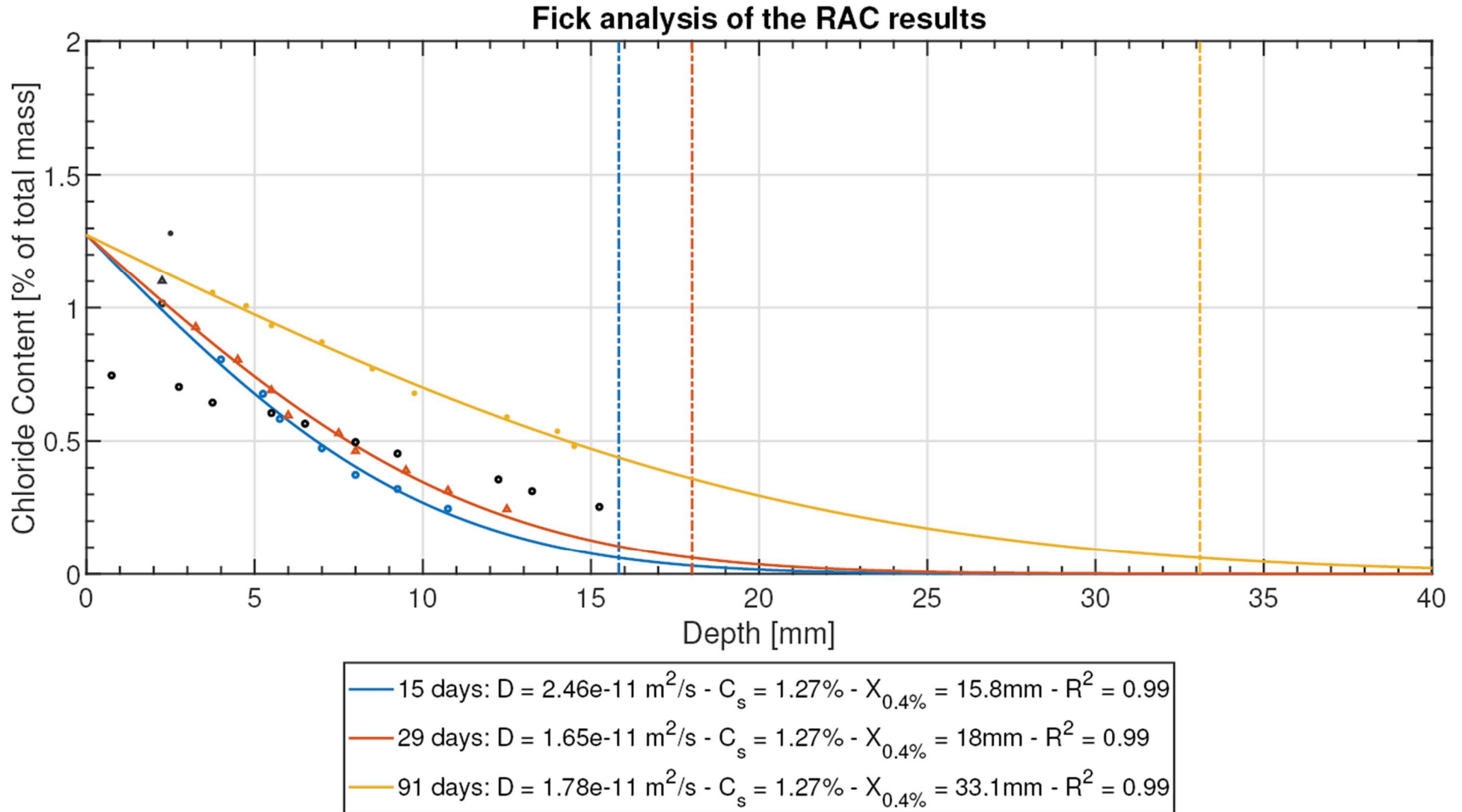
Experimental results

Fick analysis of the NAC results



— 15 days: $D = 1.81 \times 10^{-11} \text{ m}^2/\text{s}$ - $C_s = 0.78\%$ - $X_{0.4\%} = 12.3\text{mm}$ - $R^2 = 0.99$
— 29 days: $D = 1.44 \times 10^{-11} \text{ m}^2/\text{s}$ - $C_s = 0.78\%$ - $X_{0.4\%} = 15.2\text{mm}$ - $R^2 = 0.97$
— 91 days: $D = 2.93 \times 10^{-11} \text{ m}^2/\text{s}$ - $C_s = 0.78\%$ - $X_{0.4\%} = 38.4\text{mm}$ - $R^2 = 0.95$
— 91 days: $D = 1.58 \times 10^{-11} \text{ m}^2/\text{s}$ - $C_s = 0.78\%$ - $X_{0.4\%} = 28.2\text{mm}$ - $R^2 = 0.98$

Experimental results

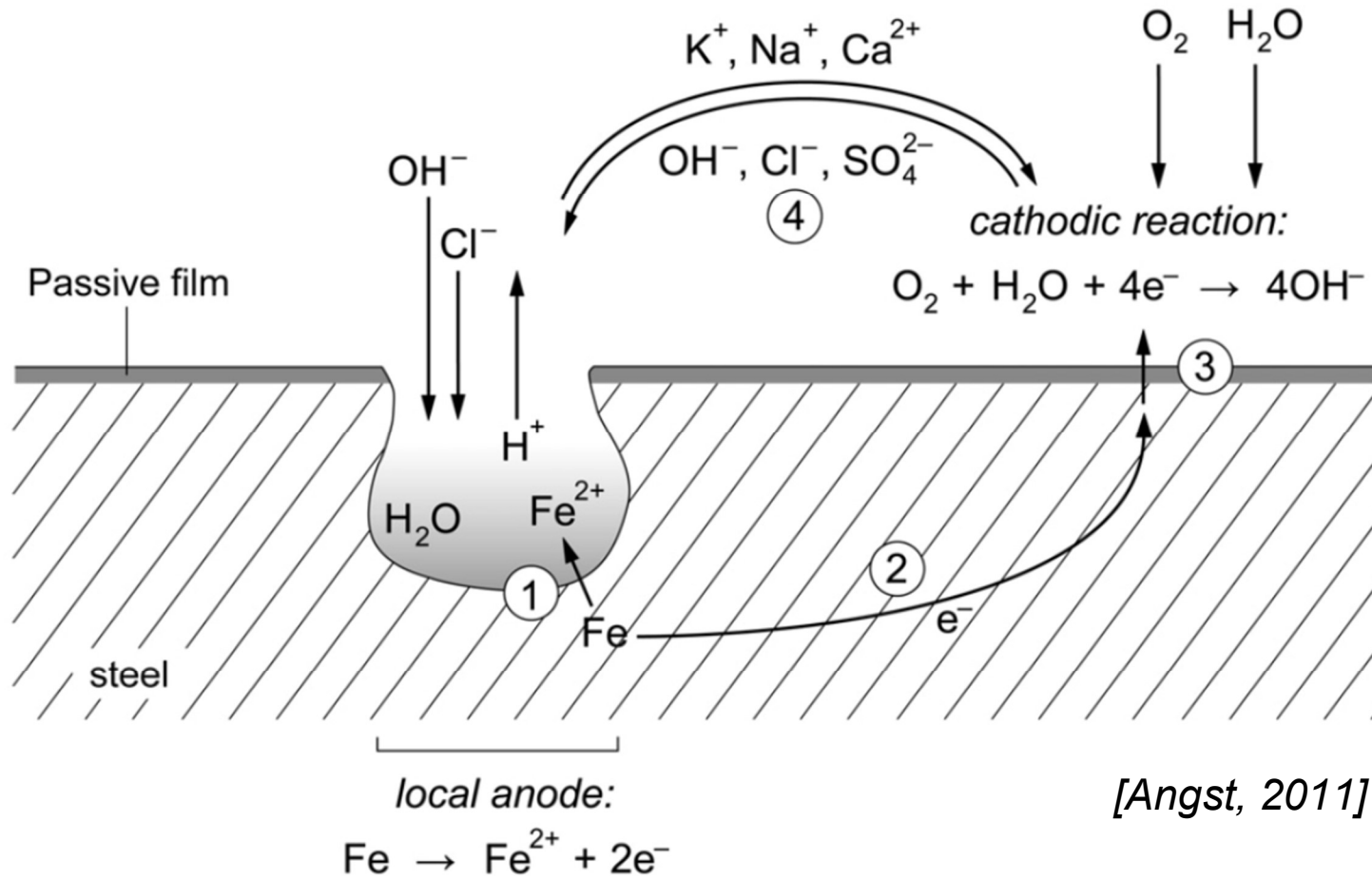


Corrosion process

Avec le soutien de la

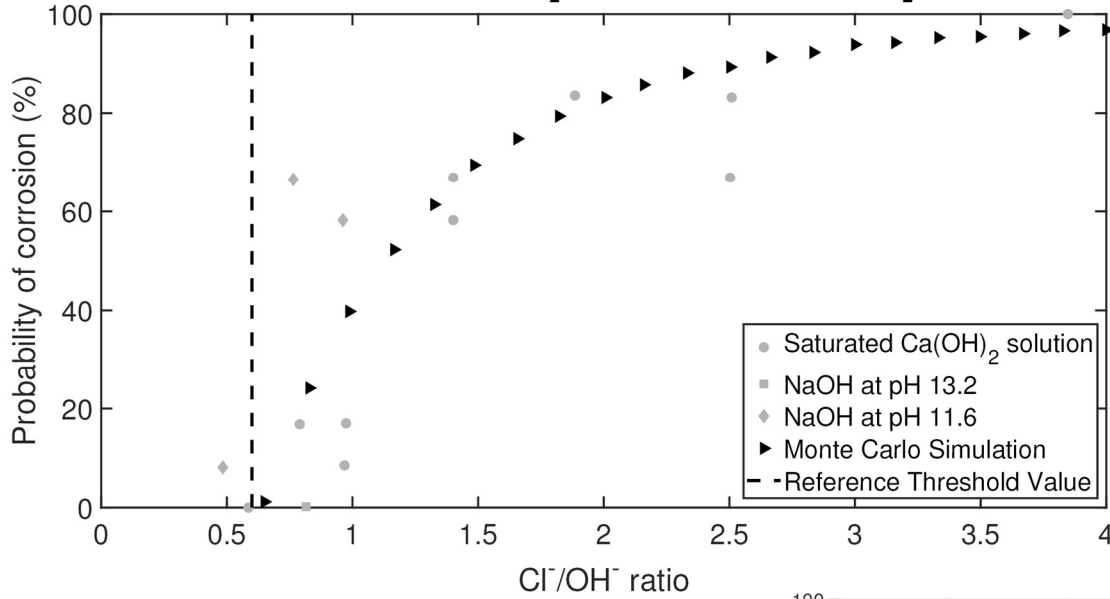


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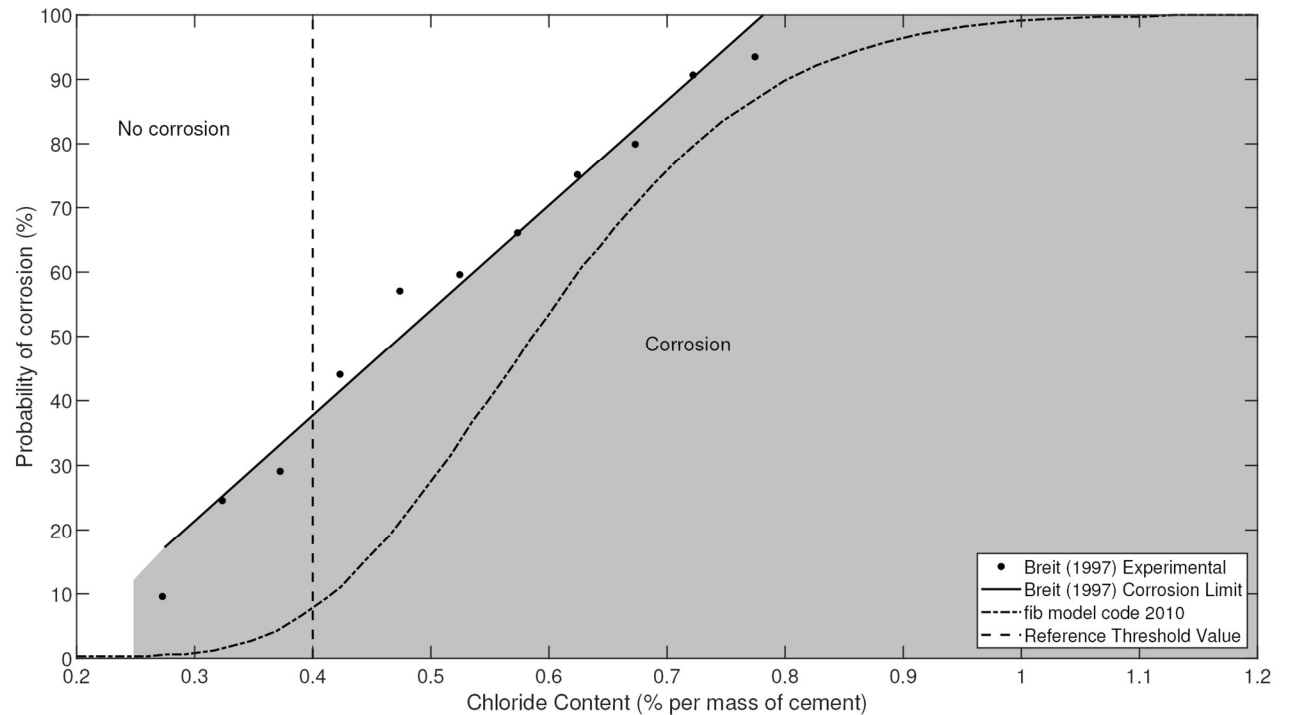


Chloride threshold

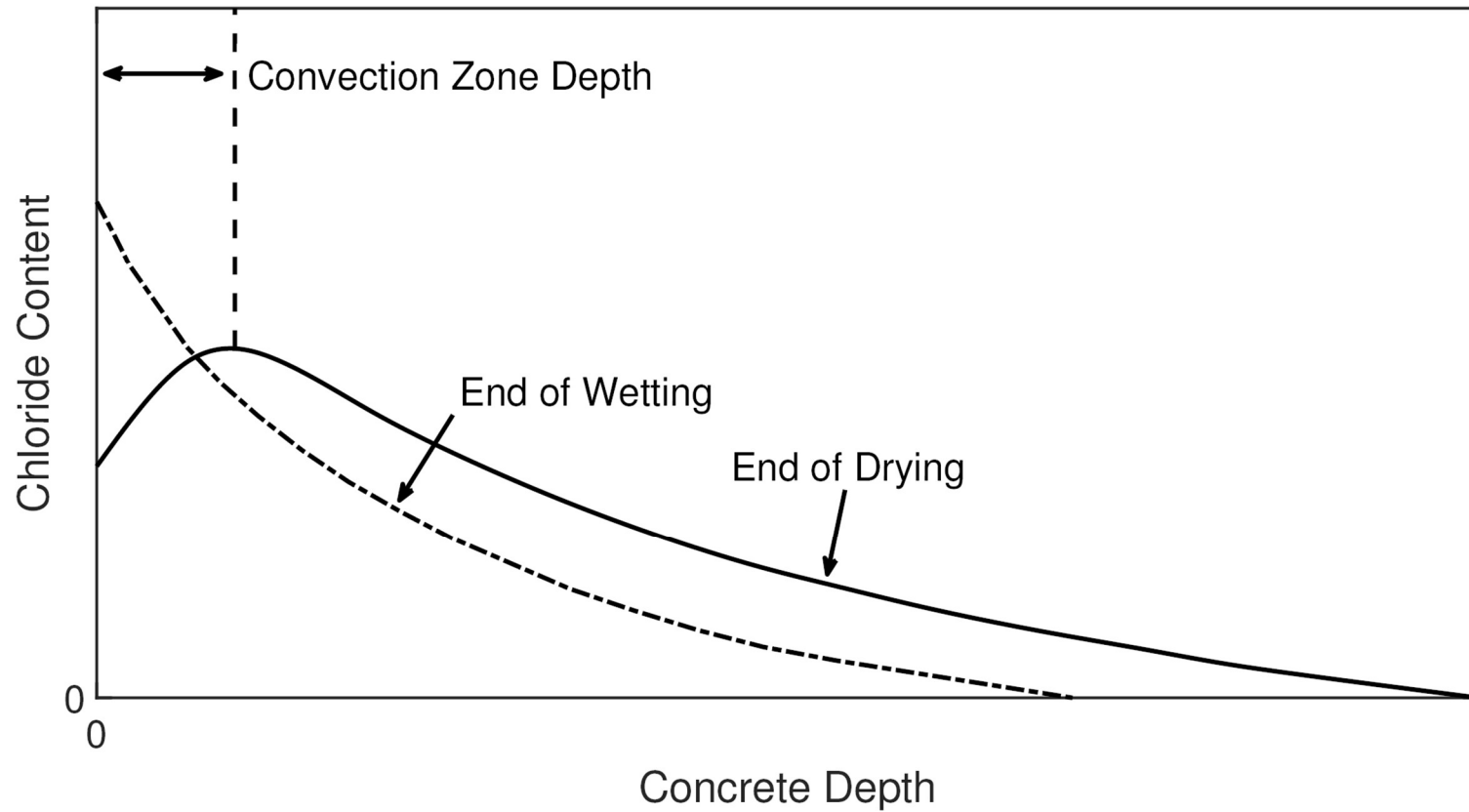
[Broomfield, 2007]



[Raupach & Büttner, 2014]



Influence of convection



Bibliography

- Eurostat. (2014). Archive: Cement and concrete production statistics - NACE Rev. 1.1. https://ec.europa.eu/eurostat/statistics-explained/index.php/Archive:Cement_and_concrete_production_statistics_-_NACE_Rev._1.1
- Commission, E. (2019). Construction and Demolition Waste (CDW). https://ec.europa.eu/environment/waste/construction_demolition.htm
- Ployaert, C. (2008). La corrosion des armatures des bétons armés et précontraints [Bulletin - Technologie]. FEBELCEM.
- Raupach, M., & Büttner, T. (2014). Concrete Repair to EN 1504: Diagnosis, Design, Principles and Practice. CRC Press, Taylor and Francis Group.
- Biver, P. (1993). Phenomenal and Numerical study on the propagation of miscible pollutants in a medium with multiple porosity. University of Liège.
- Nilenius, F. (2014). Moisture and Chloride Transport in Concrete - Mesoscale Modelling and Computational Homogenization. Chalmers University of Technology.
- Geuzaine, C., & Remacle, J.-F. (2009). Gmsh: a three-dimensional finite element mesh generator with built-in pre- and post-processing facilities. International Journal for Numerical Methods in Engineering, 79(11), 1309–1331.
- de Juan, M. S., & Gutiérrez, P. A. (2009). Study on the influence of attached mortar content on the properties of recycled concrete aggregate. Construction and Building Materials, 23, 872–877.
- Akbarnezhad, A., Ong, K. C. G., Tam, C. T., & Zhang, M. H. (2013). Effects of the Parent Concrete Properties and Crushing Procedure on the Properties of Coarse Recycled Concrete Aggregates. Journal of Materials in Civil Engineering, 25(12), 1795–1802.
- Florea, M. V. A., & Brouwers, H. J. H. (2013). Properties of various size fractions of crushed concrete related to process conditions and re-use. Cement and Concrete Research, 52, 11–21.
- Angst, U. (2011). Chloride induced reinforcement corrosion in concrete. Norwegian University of Science and Technology (NTNU).
- Broomfield, J. P. (2007). Corrosion of Steel in Concrete: Understanding, investigation and repair. (2 ed.). Taylor and Francis.