

Interaction-based material networks for efficiently estimating the homogenized behavior of microstructured materials

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Computational & Multiscale Mechanics of Materials

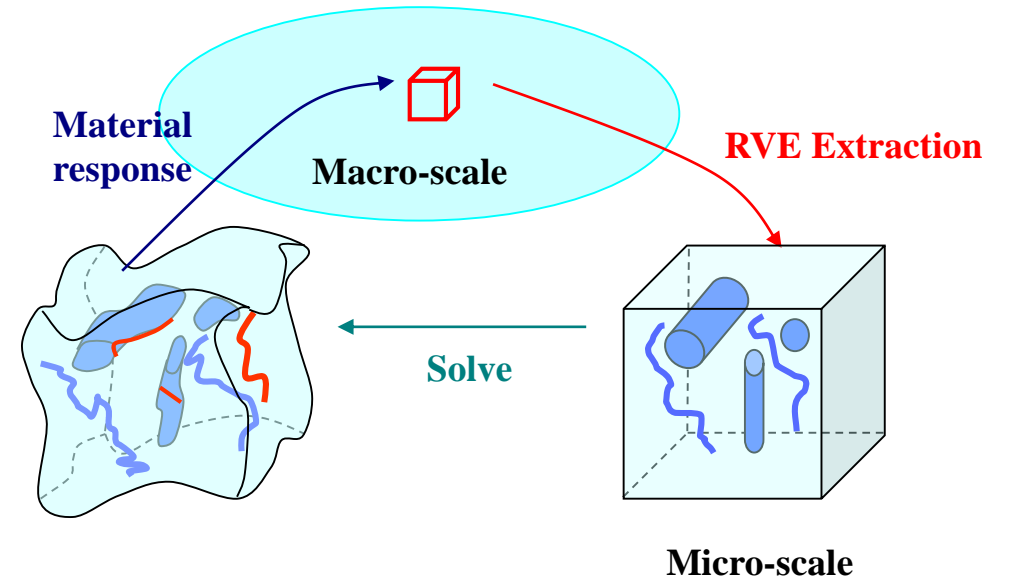
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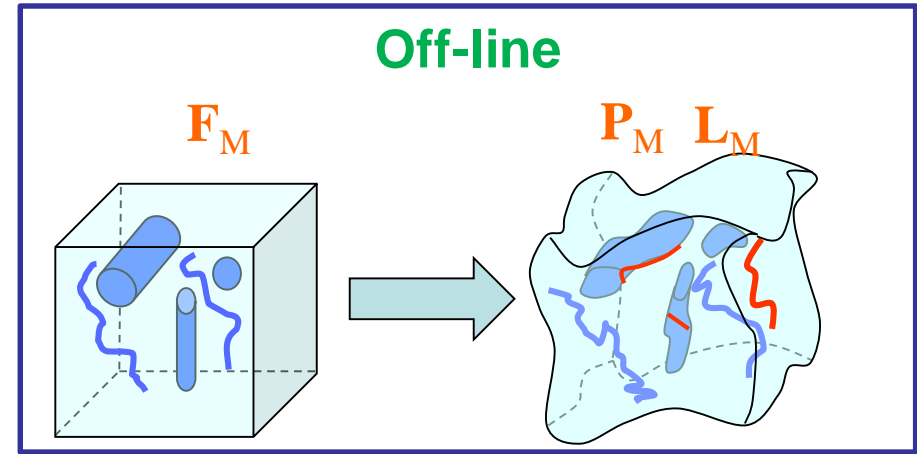
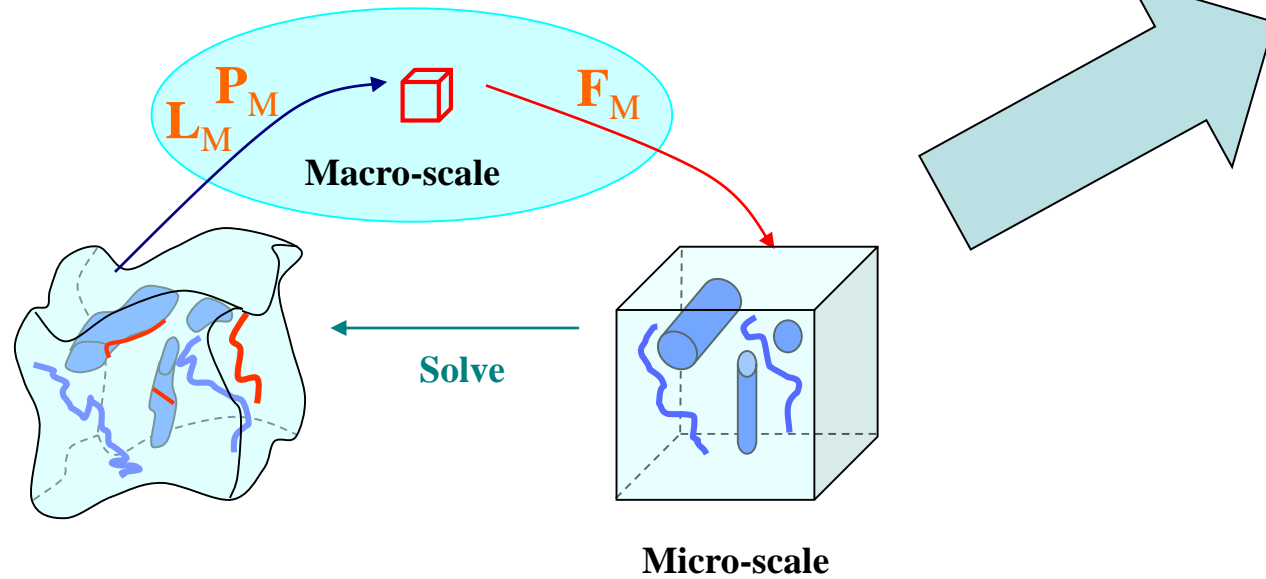
- **Computational homogenization (FE²)**
 - Microstructured materials
 - Two problems are solved concurrently
 - Macro-scale: seen as a continuum
 - Micro-scale: Representative Volume Element (**RVE**)
 - cell, grains, inclusions...
- **Advantage**
 - Account for directly micro-structural parameters (microstructure, constitutive behavior) with high accuracy.
- **Drawback**
 - Computational time & memory:
 - Iterations at macro-scale BVP
 - Sub-iterations at meso-scale BVPs
- **Solution**
 - Surrogate model of the microscopic BVP



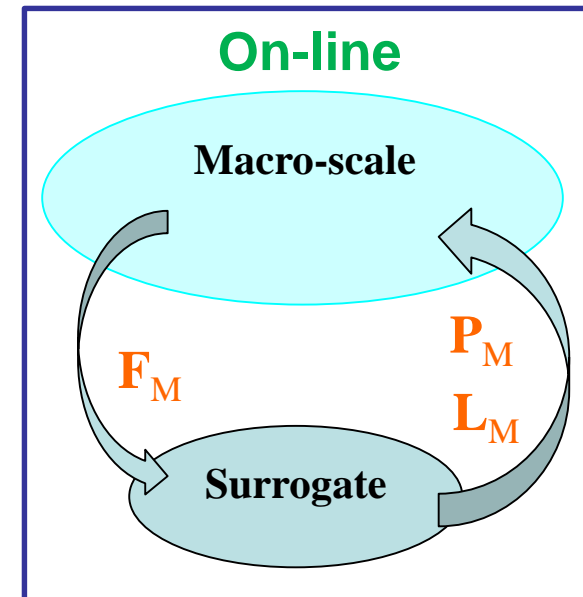
- Surrogate model of the microscopic BVP

- Define a surrogate model
- Off-line:
 - Construct off-line data-base (using RVE simulations)
 - Train surrogate model
- On-line:
 - Use the trained surrogate model during analyses

Interaction-based material network

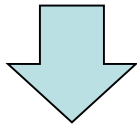
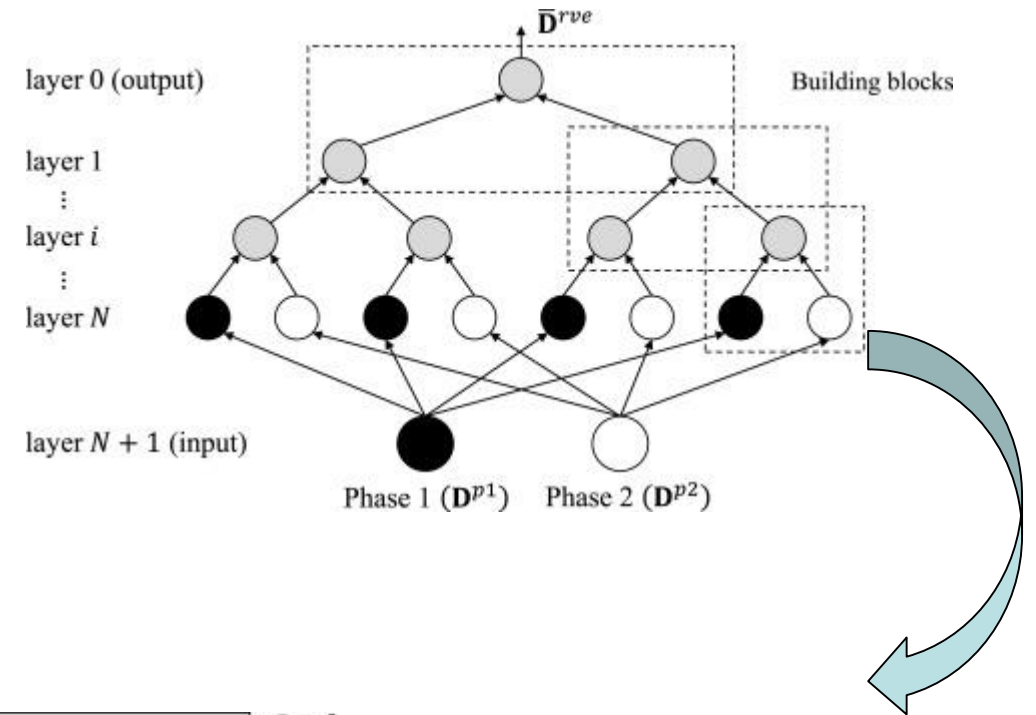


Trained

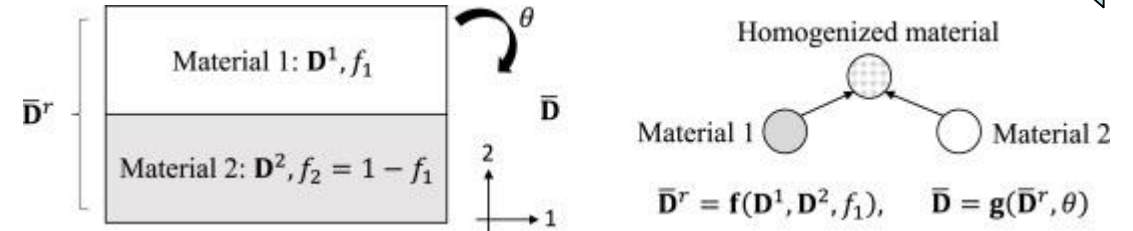
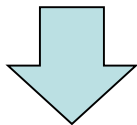


Deep material network

- **Deep material networks (DMN)**
 - Proposed by Liu et al. (2019)
 - Hierarchical laminate building blocks
 - Applicable for different kind of microstructures
 - Multiphase composites, polycrystalline materials, etc.
- **Limitations**
 - The solution is not provided under a closed form
 - The original DMN is still limited for porous microstructures



Revisit the DMN with interactions

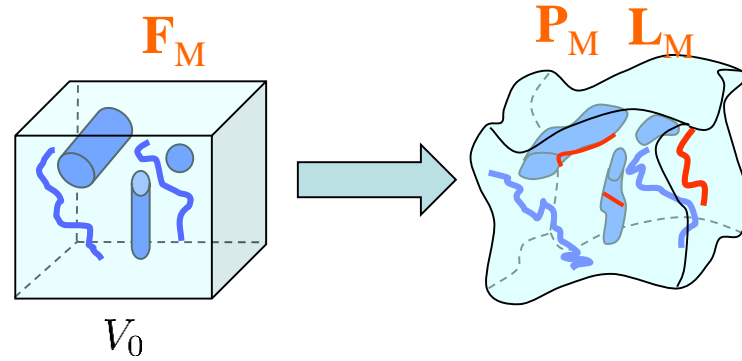


Interaction-based material network:

- A network of **interaction mechanisms**
- General framework for (porous) microstructured materials

Liu, Z., Wu, C.T. and Koishi, M., 2019. *Computer Methods in Applied Mechanics and Engineering*, 345, pp.1138-1168.

• **FE² full-field model**



Averaging strain

$$\mathbf{F}_M = \frac{1}{V_0} \int_{V_0} \mathbf{F} dV$$

Averaging stress

$$\mathbf{P}_M = \frac{1}{V_0} \int_{V_0} \mathbf{P} dV$$

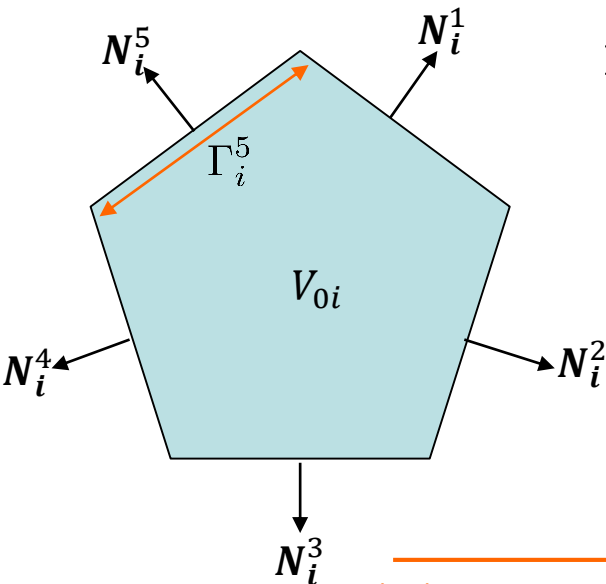
Hill-Mandel condition

$$\mathbf{P}_M : \delta \mathbf{F}_M = \frac{1}{V_0} \int_{V_0} \mathbf{P} : \delta \mathbf{F} dV$$

• **Virtual polyhedral decomposition** $V_0 = \cup_i V_{0i}$

- Weights $W_i = \frac{V_{0i}}{V_0}$ with $i = 0, \dots, N-1$
- Each polyhedral sub-volume V_{0i}

$$\mathbf{P}_i = \frac{1}{V_{0i}} \int_{V_{0i}} \mathbf{P} dV$$



$$\mathbf{F}_i = \frac{1}{V_{0i}} \int_{V_{0i}} \mathbf{F} dV = \mathbf{F}_M + \frac{1}{V_{0i}} \int_{\partial V_{0i}} \mathbf{w} \otimes \mathbf{N} dA$$

$$\mathbf{F}_i = \mathbf{F}_M + \sum_k \frac{\Gamma_i^k}{V_{0i}} \bar{\mathbf{w}}_i^k \otimes \mathbf{N}_i^k$$

$\mathbf{w} = \mathbf{x} - \mathbf{F}_M \cdot \mathbf{X}$: fluctuation field

$\bar{\mathbf{w}}_j^k$: average fluctuation on Γ_j^k

Averaging strain

$$\mathbf{F}_M = \sum_{i=0}^{N-1} W_i \mathbf{F}_i$$

Averaging stress

$$\mathbf{P}_M = \sum_{i=0}^{N-1} W_i \mathbf{P}_i$$

Hill-Mandel condition

$$\mathbf{P}_M : \delta \mathbf{F}_M = \sum_{i=0}^{N-1} W_i \mathbf{P}_i : \delta \mathbf{F}_i$$

- Virtual polyhedral connectivity

- Each polyhedral sub-volume: $\mathbf{F}_i = \mathbf{F}_M + \sum_k \frac{\Gamma_i^k}{V_{0i}} \bar{\mathbf{w}}_i^k \otimes \mathbf{N}_i^k$
- Define M interaction mechanisms: $[(\mathbf{a}_j, \mathbf{G}_j)]$ for $j = 0, \dots, M - 1$

$$\mathbf{F}_i = \mathbf{F}_M + \sum_j \alpha_{ij} \mathbf{a}_j \otimes \mathbf{G}_j$$

→ *Contribution of node i in mechanism j*
 → *Direction of mechanism j*
→ *Degrees of freedom of mechanism j definition the strain fluctuation*

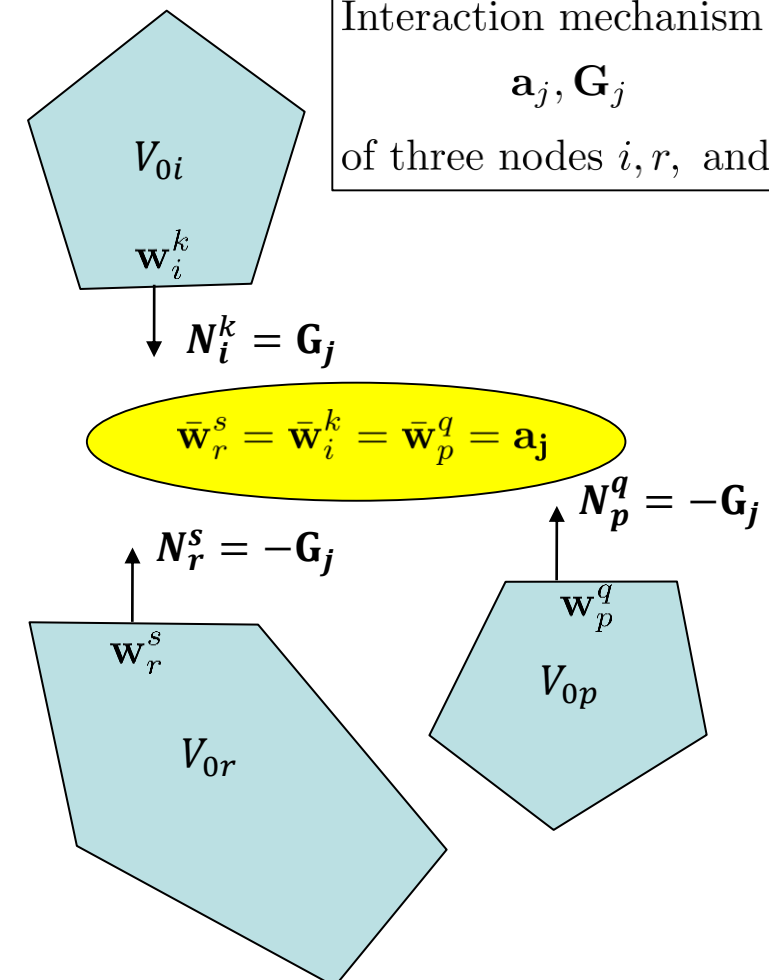
- Constraints from strain averaging

$$\mathbf{F}_M = \sum_{i=0}^{N-1} W_i \mathbf{F}_i \quad \forall [(\mathbf{a}_j, \mathbf{G}_j)] \text{ for } j = 0, \dots, M - 1 \quad \Rightarrow \quad \sum_{i=0}^{N-1} W_i \alpha_{ij} = 0 \quad \forall j = 0, \dots, M - 1$$

- Weak form from Hill-Mandel

$$\mathbf{P}_M : \delta \mathbf{F}_M = \sum_{i=0}^{N-1} W_i \mathbf{P}_i : \delta \mathbf{F}_i \quad \Rightarrow \quad \sum_{j=0}^{M-1} \left[\left(\sum_{i=0}^{N-1} W_i \mathbf{P}_i \alpha_{ij} \right) \cdot \mathbf{G}_j \right] \cdot \delta \mathbf{a}_j = 0$$

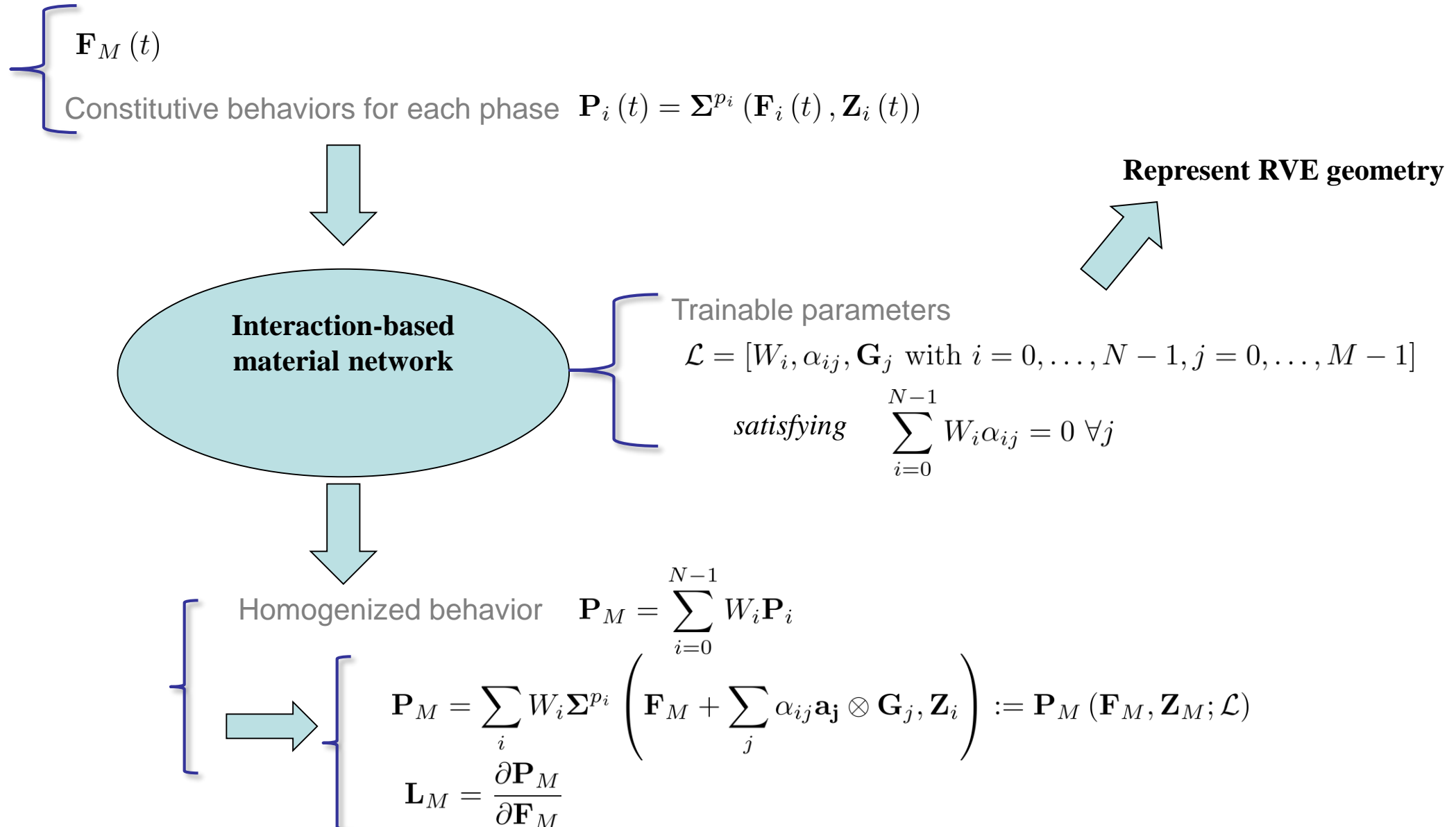
Interaction mechanism j:
 $\mathbf{a}_j, \mathbf{G}_j$
 of three nodes $i, r,$ and p




Nguyen & Noels 2022, CMAME

$W_i, \alpha_{ij}, \mathbf{G}_j$ with $i = 0, \dots, N - 1, j = 0, \dots, M - 1$ are known (by training) equations to find $[\mathbf{a}_j \text{ for } j = 0, \dots, M - 1]$

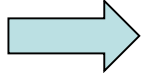
Interaction-based material network - summary



- **Linear elastic training**

- The tangent at zero strain is considered: $\mathbf{L}_M = \frac{\partial \mathbf{P}_M}{\partial \mathbf{F}_M}$ at $\mathbf{F}_M = \mathbf{I}$
- At zero strain, the elastic homogenized tensor predicted by the material can be expressed as a function of the elastic tangent tensors of P underlying phases $\mathbf{L}_0, \dots, \mathbf{L}_{P-1}$ and fitting parameters \mathcal{L}
 $\mathbf{L}_M = \mathbf{L}_M(\mathbf{L}_0, \dots, \mathbf{L}_{P-1}, \mathcal{L})$
- Offline data provided by elastic simulations
 - RVE & microscopic boundary condition
 - Inputs: $\mathbf{L}_0^k, \dots, \mathbf{L}_{P-1}^k$ with $k = 0, \dots, N_s - 1$ which can be artificially randomly generated
 - Outputs: \mathbf{L}_M^k with $k = 0, \dots, N_s - 1$ computed by computational micromechanics
- A loss function is defined to characterize the accuracy of the prediction of the material network.
- Gradient-descent optimizer to minimize this loss function

- **Nonlinear training**

- Consider history dependent  $\mathbf{P}_M(t) = \mathbf{P}_M(\mathbf{F}_M(\tau))$ for $\tau \in [0, t]; \mathcal{L}$
- Offline data provide by paths
 - RVE & microscopic boundary condition
 - Inputs: strain paths $[\mathbf{F}_M(t)]_k$ with $k = 0, \dots, N_s - 1$ which can be artificially randomly generated
 - Output: stress paths $[\mathbf{P}_M(t)]_k$ with $k = 0, \dots, N_s - 1$ is computed by computational micromechanics
- A loss function is defined to characterize the accuracy of the prediction of the material network.
- Gradient-descent optimizer to minimize this loss function

Interaction-based material network

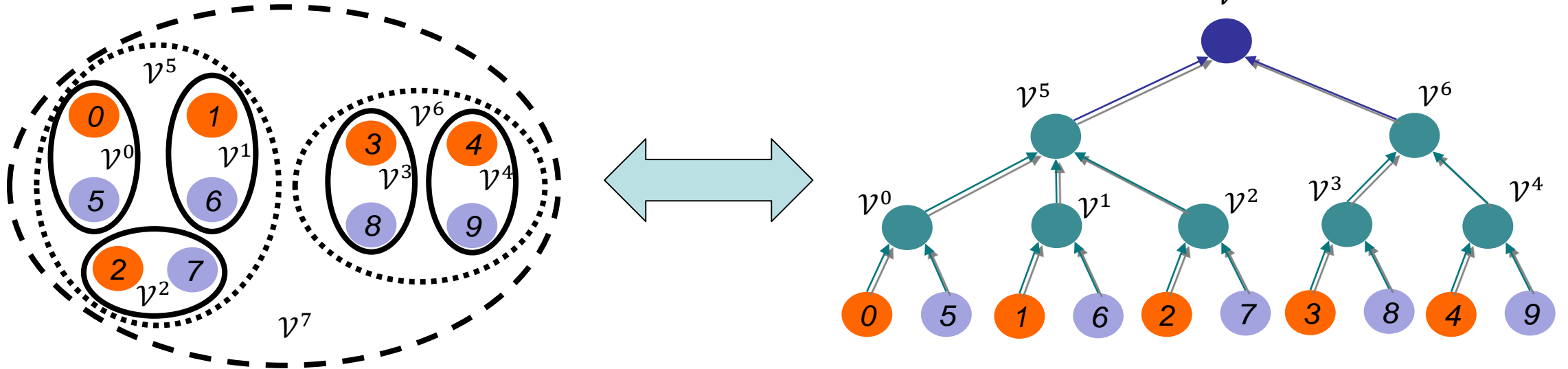
- **Trainable parameters:** $\mathcal{L} = [W_i, \alpha_{ij}, \mathbf{G}_j$ with $i = 0, \dots, N - 1, j = 0, \dots, M - 1]$

- satisfying

$$\sum_{i=0}^{N-1} W_i \alpha_{ij} = 0 \quad \forall j$$

- **How to define architecture?**

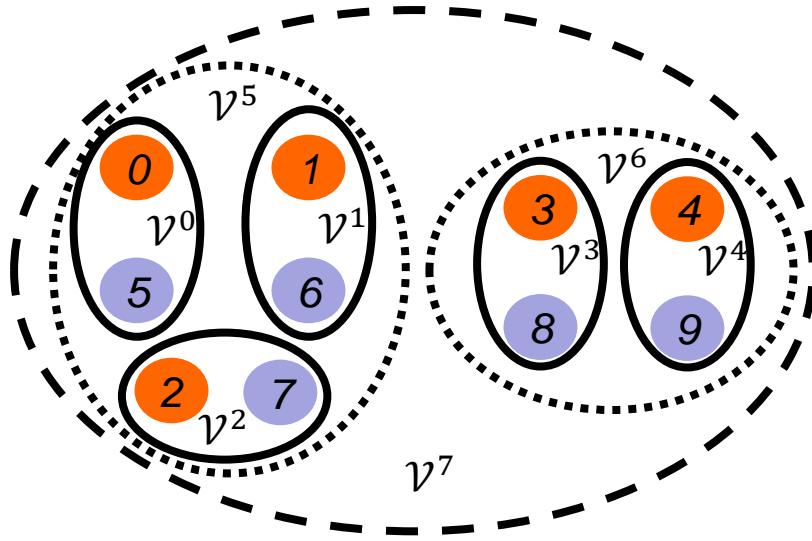
- Each interaction includes several nodes $\rightarrow \alpha_{ij} = 0$ if node i does not participate interaction j
- Hierarchical architecture



Example for a 2-phase material with 10 material nodes & 8 interactions

- Mechanistic building blocks: Laminate

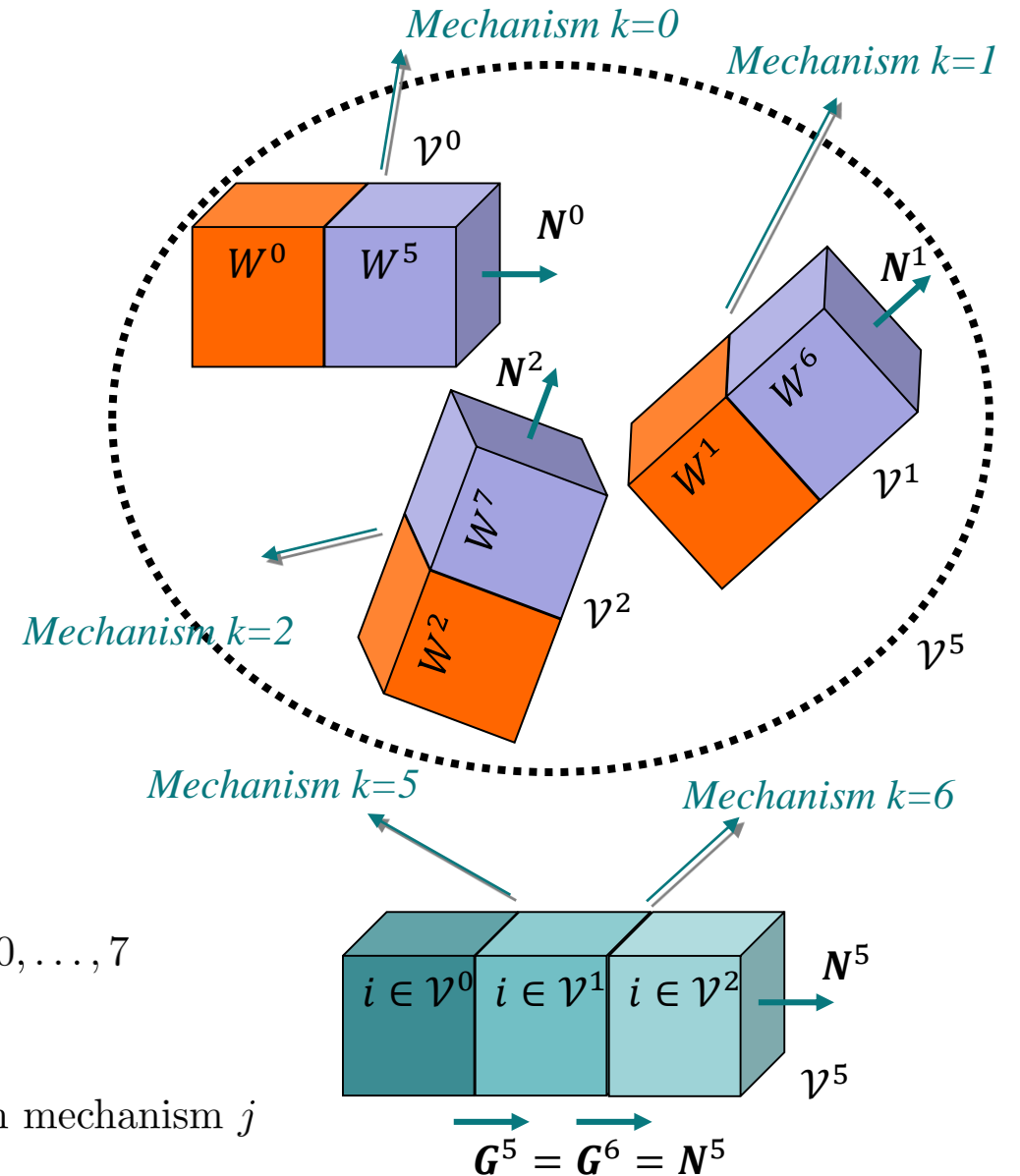
- Interaction \mathcal{V}^j as a laminate



- Tuning parameters

- Weight: W_i with $i = 0, \dots, 9$
 - Unique direction for an interaction \mathcal{V}^j : $\mathbf{G}_j \Rightarrow \mathbf{N}_j$ with $j = 0, \dots, 7$
 - Constraints:

$$\sum_{i=0}^{N-1} W_i \alpha_{ij} = 0 \quad \forall j \Rightarrow \alpha_{ij} \text{ from node weights in mechanism } j$$



- Mechanistic building blocks: Full interaction

- Interaction \mathcal{V}^j as a full interaction

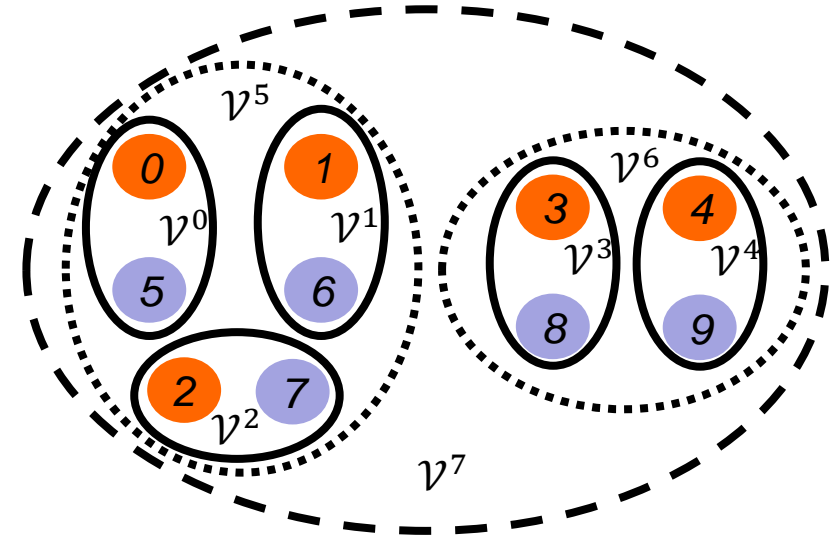
- Mechanism j is a full interaction if satisfying

$$\sum_{i=0}^{N-1} W_i \alpha_{ij} = 0$$

- Tuning parameters

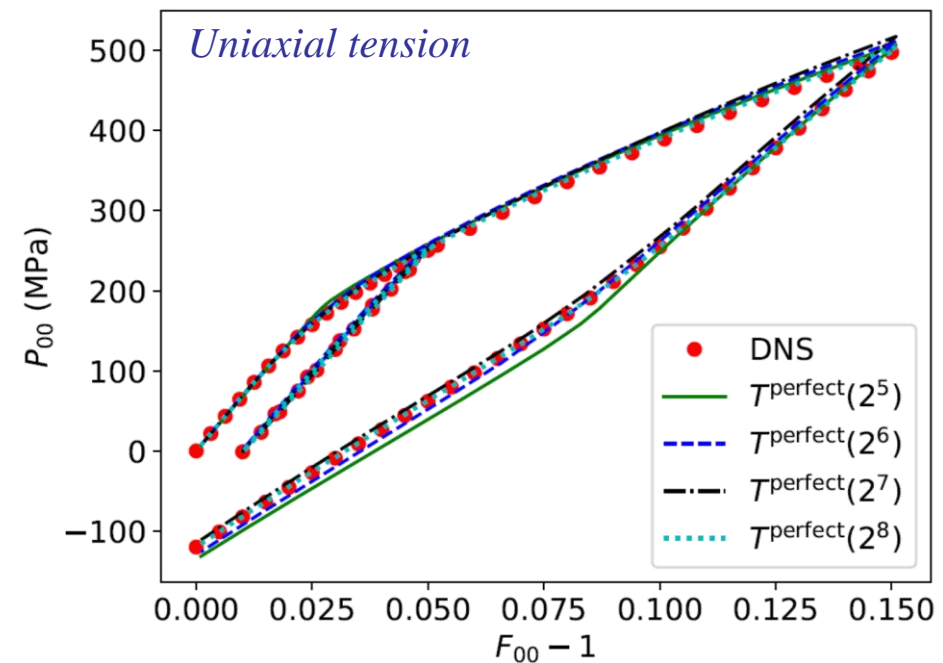
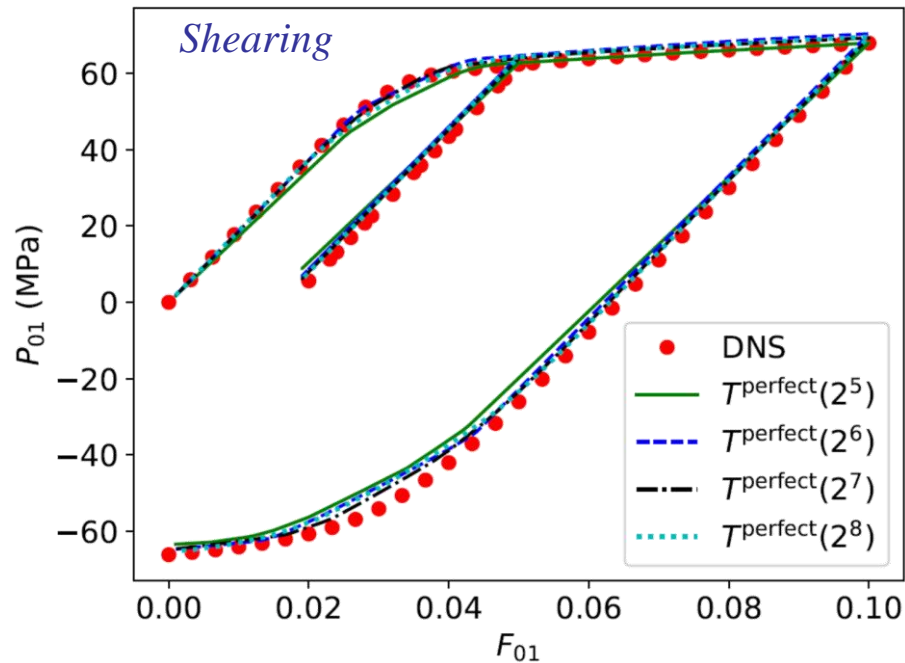
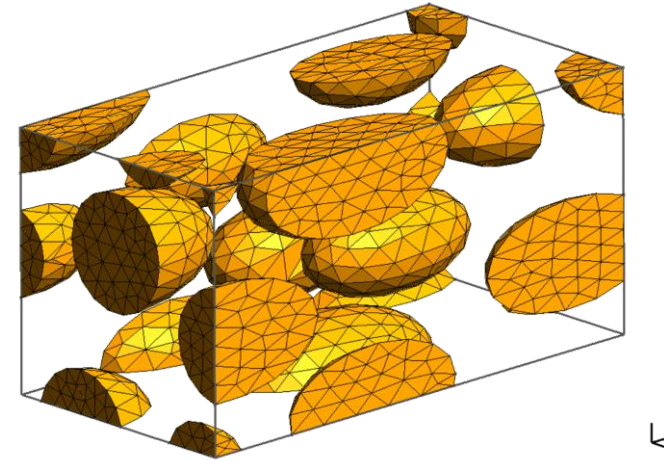
- **Weight:** W_i with $i = 0, \dots, 9$
- **Unique direction for an interaction \mathcal{V}^j :** $\mathbf{G}_j \rightarrow \mathbf{N}_j$ with $j = 0, \dots, 7$
- **Coefficients:** α_{ij} with $i \in \mathcal{V}^j$ and $j = 0, \dots, 7$

- **Constraints:** $\sum_{i=0}^{N-1} W_i \alpha_{ij} = 0 \forall j$ are enforced during training iterations



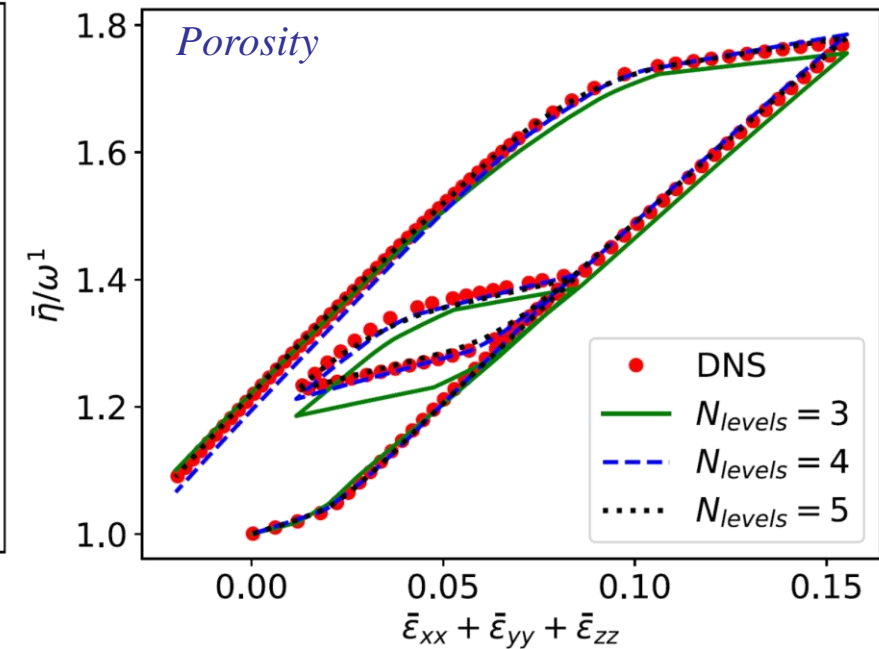
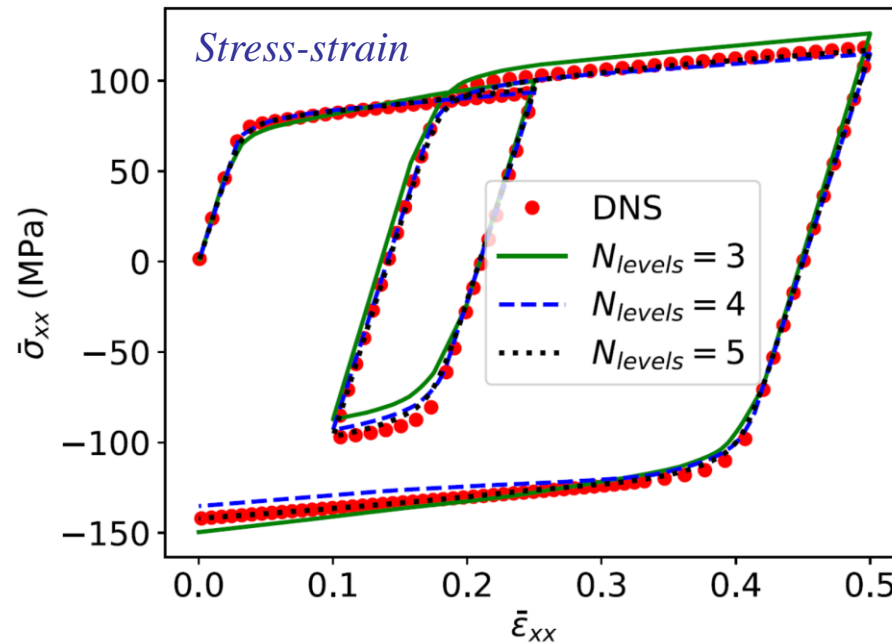
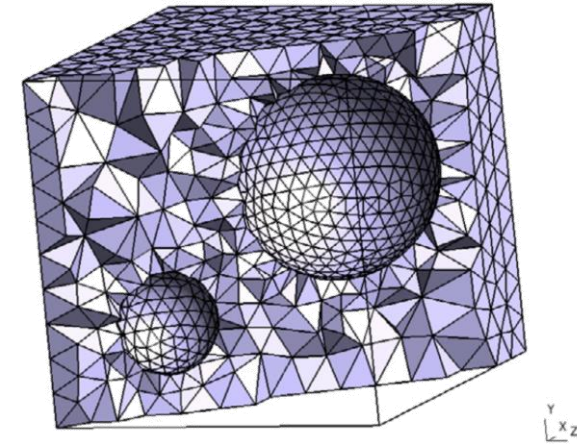
- Online stage on a particle-reinforced composite

- Properties
 - Elastic inclusions
 - Elasto-plastic matrix
- Laminate as mechanistic building blocks
- Linear elastic training



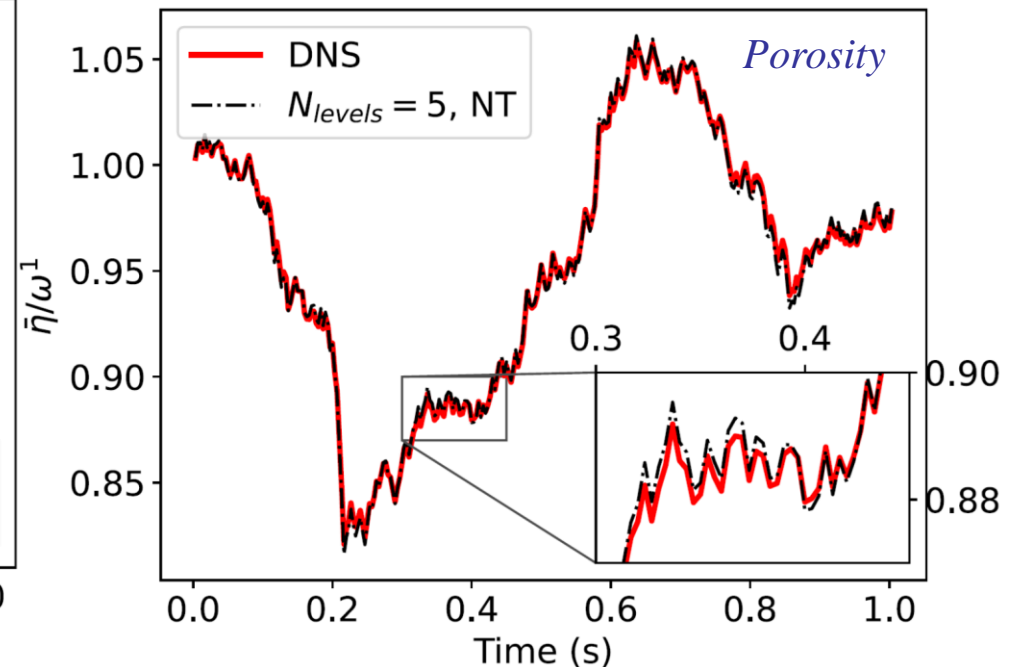
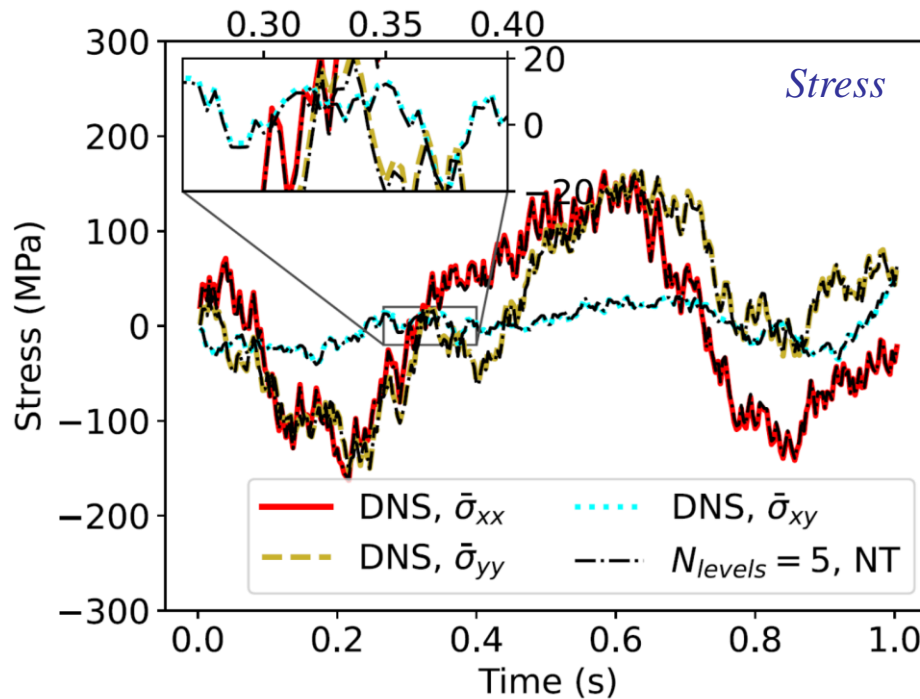
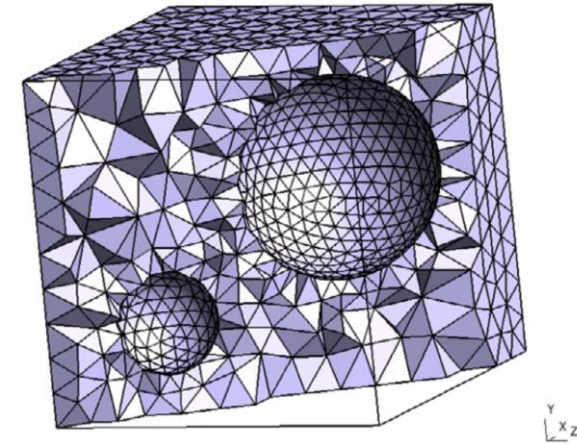
- Online stage on a porous material

- Properties
 - Elasto-plastic matrix
 - Small strain
- Full interactions as mechanistic building blocks
- Non-linear training
- Uniaxial tension



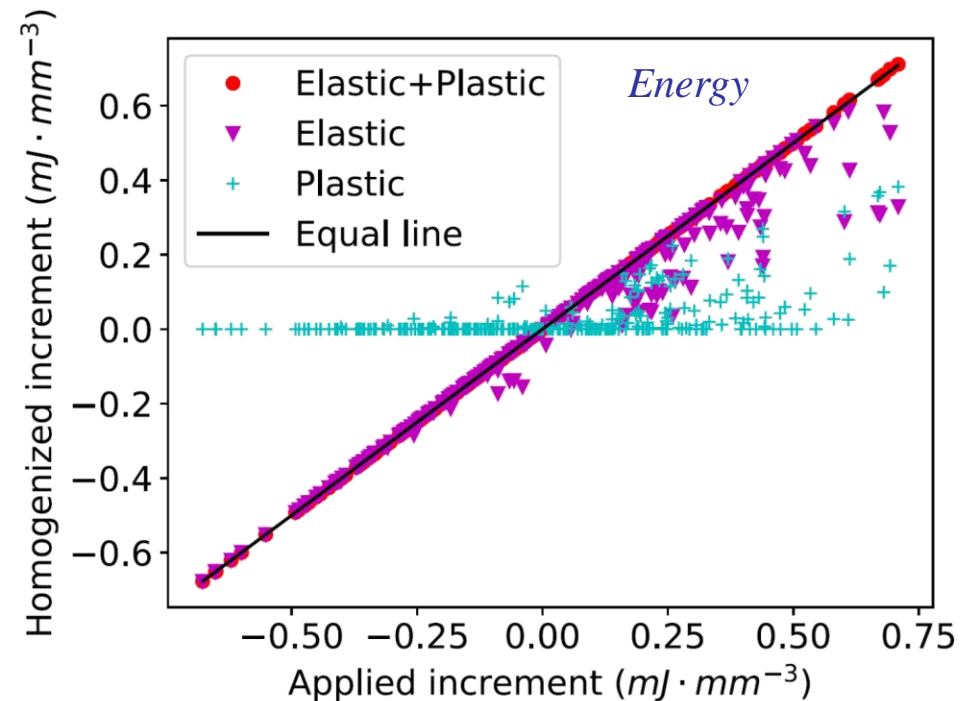
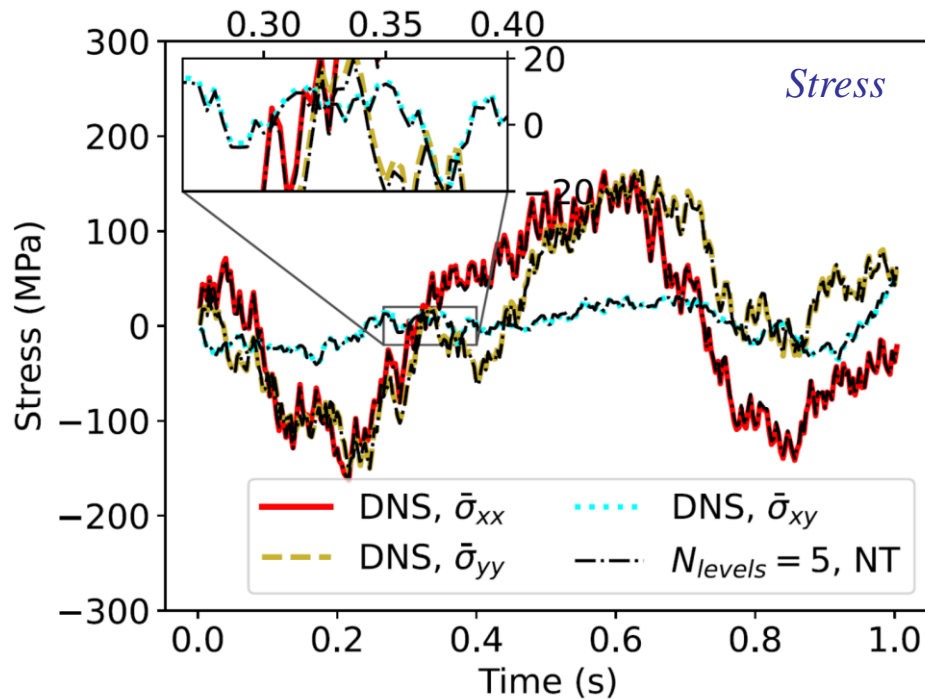
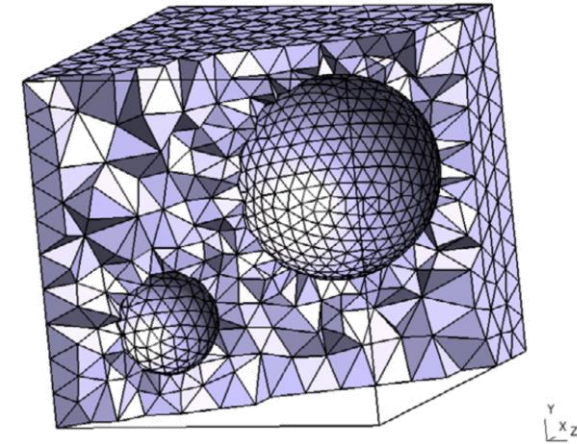
- Online stage on a porous material

- Properties
 - Elasto-plastic matrix
 - Small strain
- Full interactions as mechanistic building blocks
- Non-linear training with Material 1, on-line material 2
- Random loading



- Online stage on a porous material

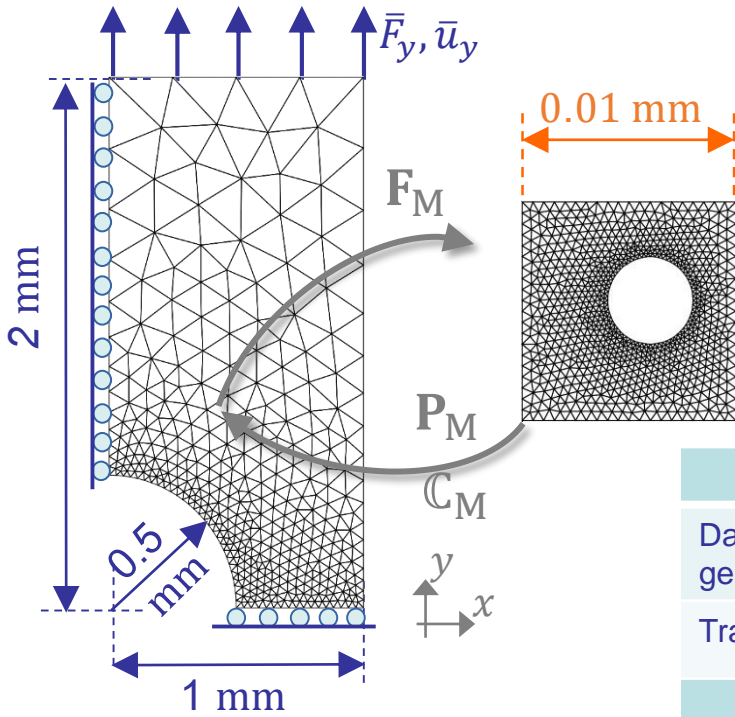
- Properties
 - Elasto-plastic matrix
 - Small strain
- Full interactions as mechanistic building blocks
- Non-linear training
- Thermodynamically consistent



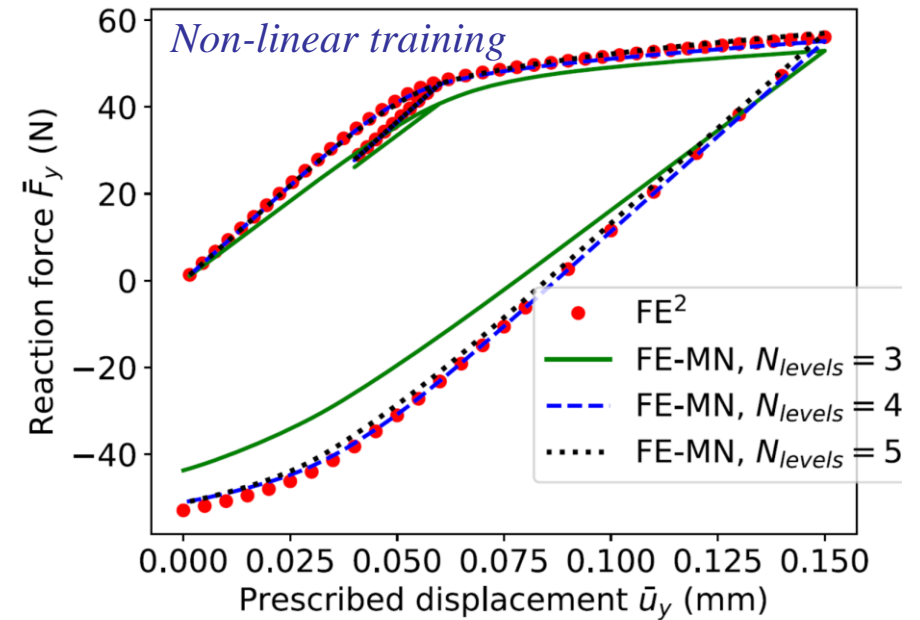
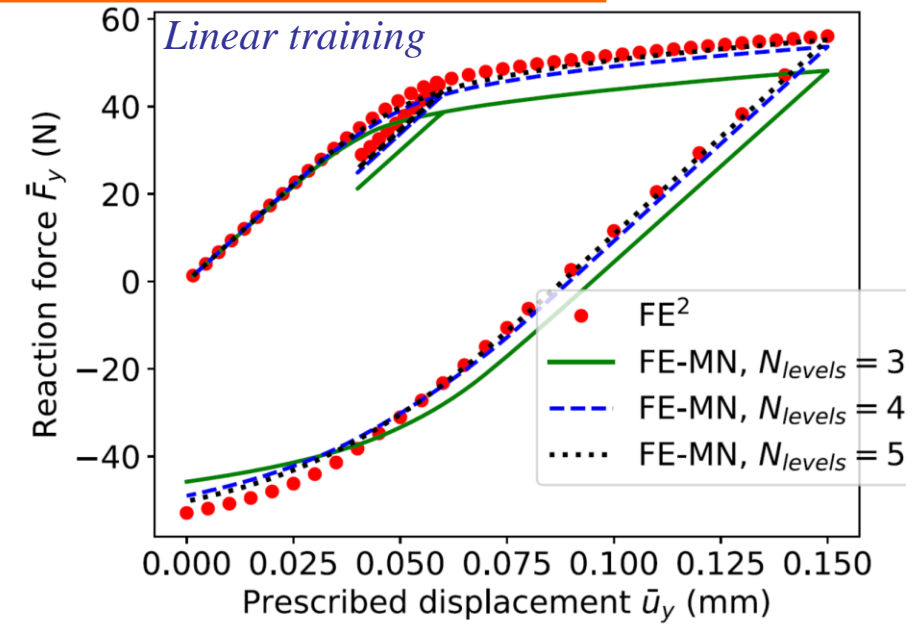
Interaction-based material network as surrogate model

- Multiscale simulation

- Comparison FE² vs. Material network-surrogate
- Full interactions as mechanistic building blocks
- Non-linear training

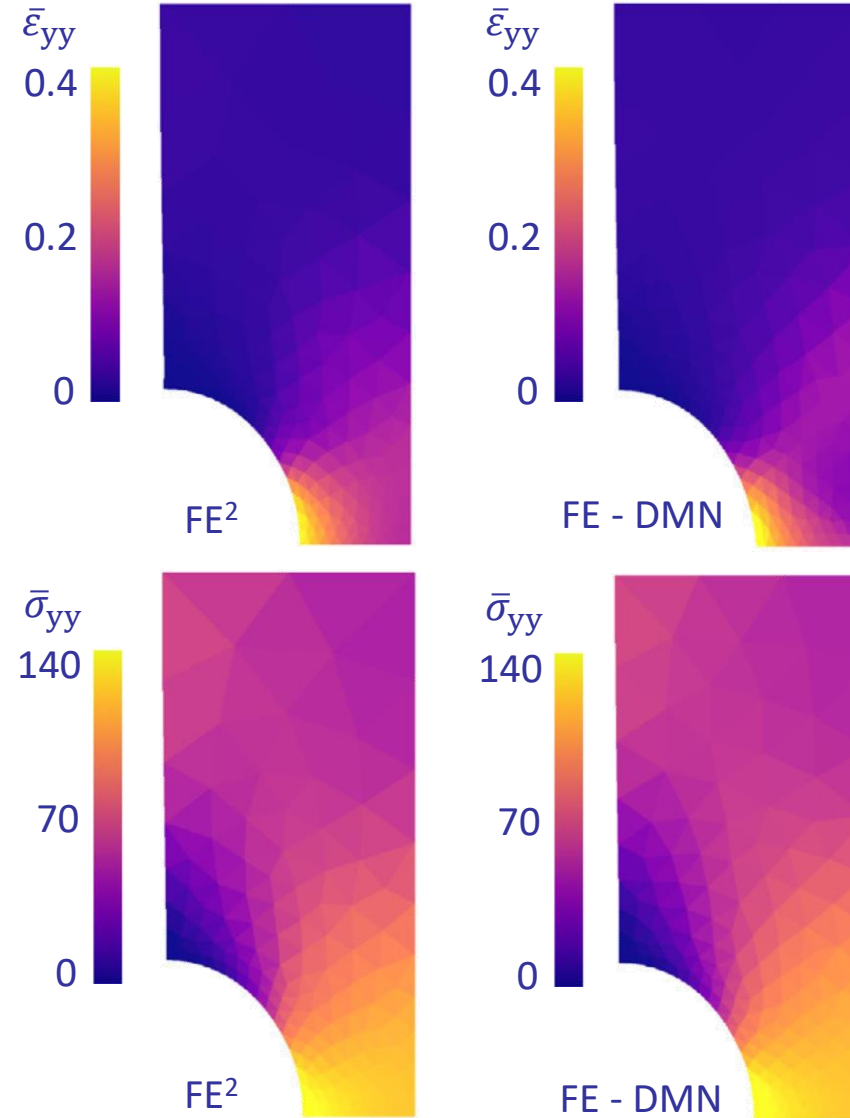
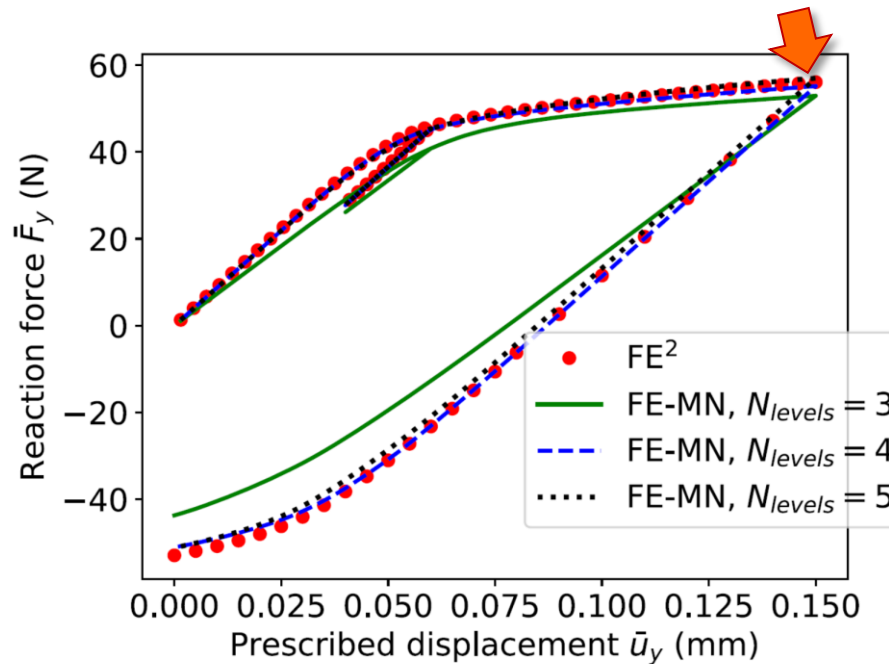


	Off-line	FE ²	FE-DMN
Data generation	-	-	0.04 (linear) – 3.5 (non-linear) hour.-cpu
Training	-	-	0.16-20 hours.-cpu
	On-line	FE ²	FE-DMN
Simulation	-	7200 h-cpu	0.1 to 1 h-cpu



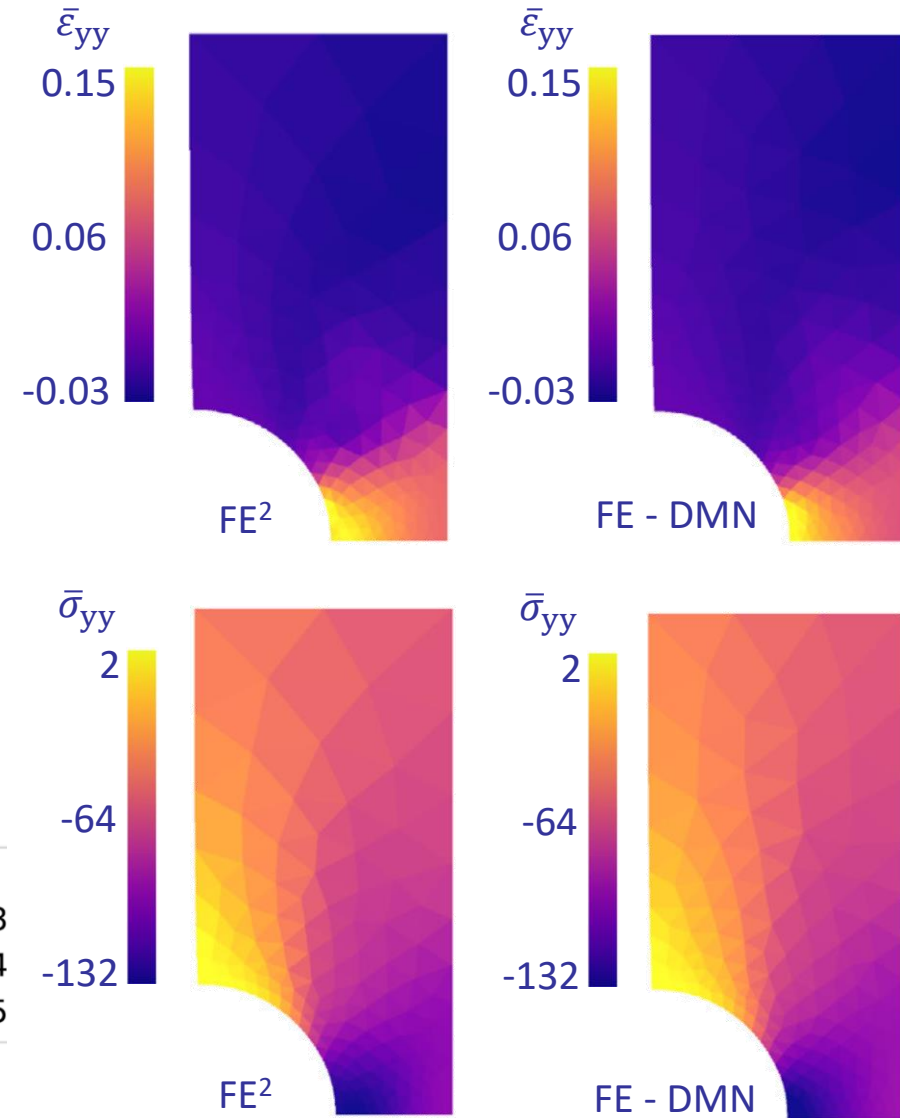
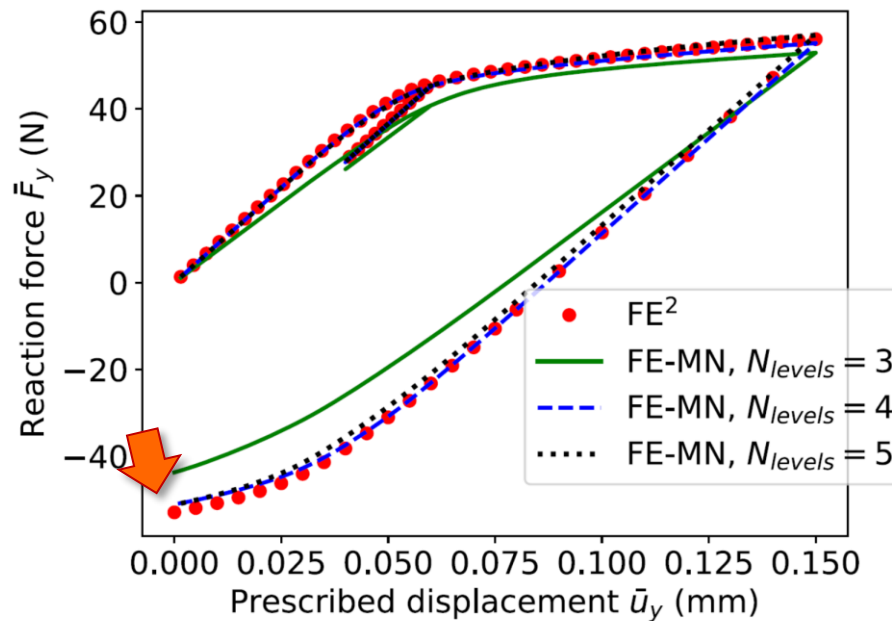
- Multiscale simulation

- Stress-strain distribution at point A
- For 2^5 material nodes
- Full interactions as mechanistic building blocks
- Non-linear training



- Multiscale simulation

- Stress-strain distribution at point B
- For 2^5 material nodes
- Full interactions as mechanistic building blocks
- Non-linear training



Conclusions and perspectives

- **Interaction-based material network**
 - A general framework to build surrogate models for micro-structured materials
 - Satisfy all requirements of a truly microscopic boundary value problem including the stress and strain averaging principles and the Hill–Mandel energetically consistent condition
 - Efficient training procedures
 - Trained material networks with the ones of the direct numerical simulations in both contexts of virtual testing and multiscale simulations.
- **Future works**
 - Interaction-based material network for damage and fracture

Thank you for your attention