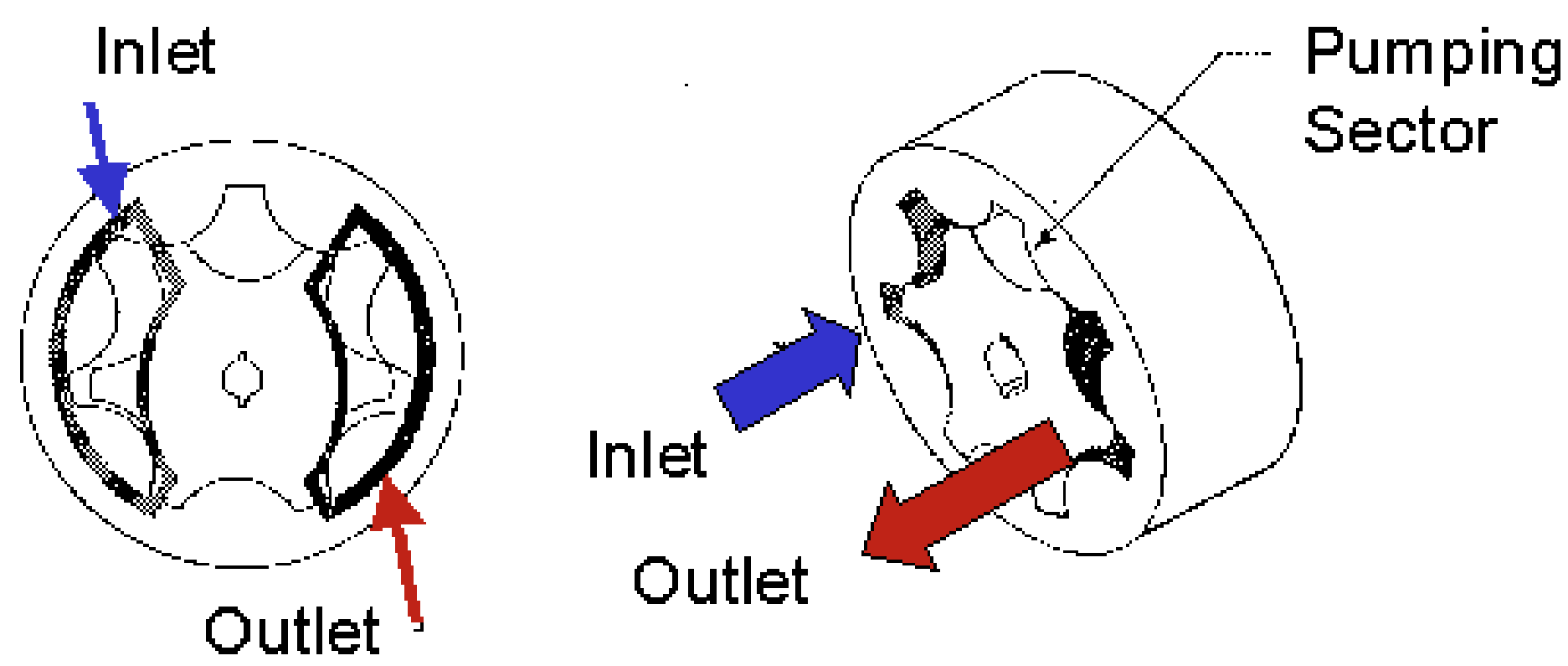


Computation of Weakly Compressible Flows Induced by Boundary Movements Parallel Finite Volumes Method on 3D Unstructured Moving Meshes

Didier Vigneron

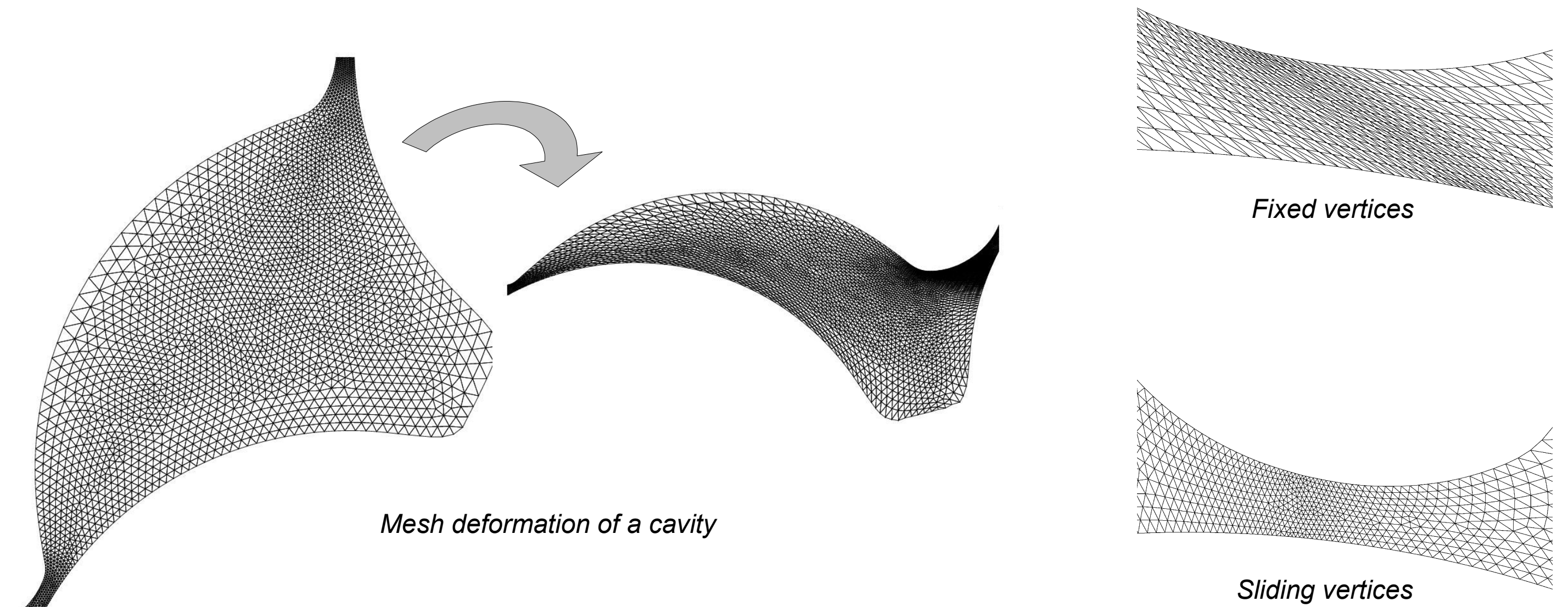
Simulation of flow through G-Rotor Pumps

- Weakly compressible Air/Oil mixture
- Detection of cavitation
- Pump efficiency analysis



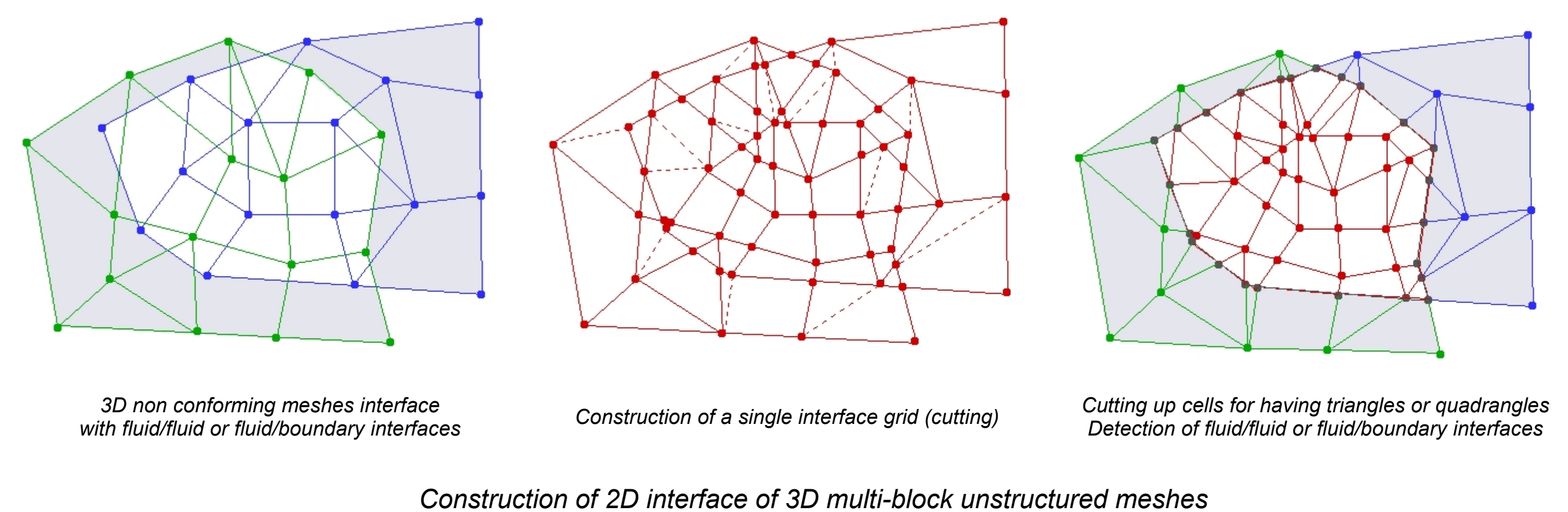
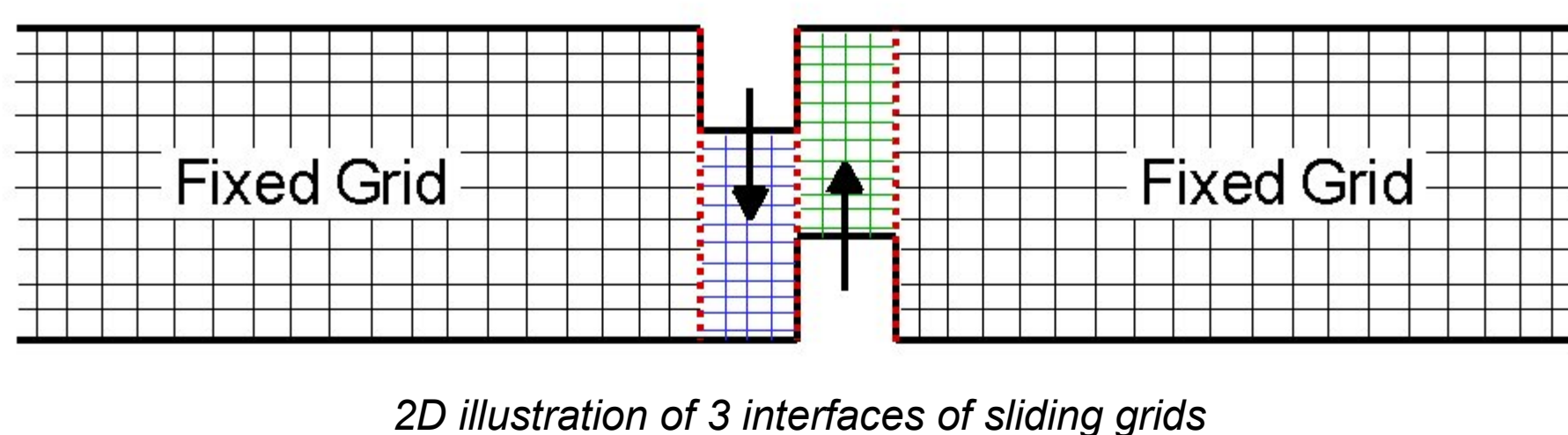
Mesh Deformation Technique

- Computation of vertices displacement as the solution of elasticity equations
- Sliding vertices on boundaries
- Analytical or numerical description of boundaries



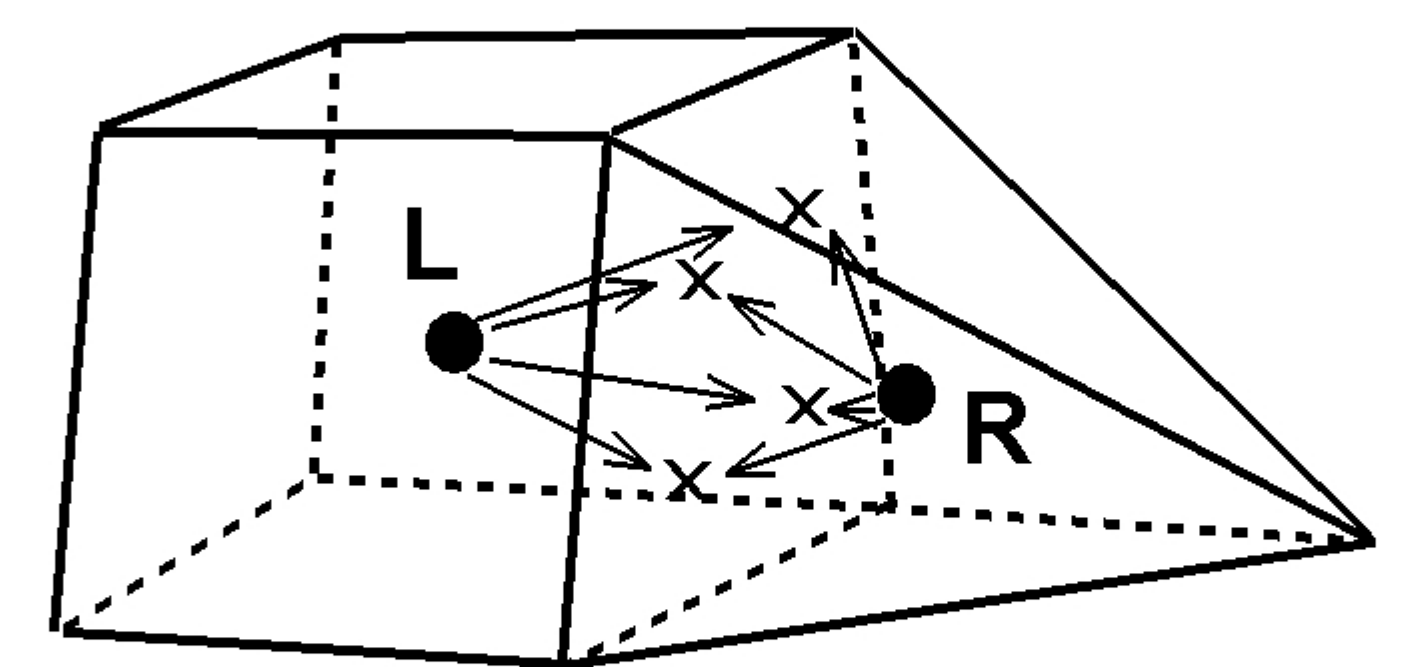
Sliding Multi-Block Meshes Interface

- Interface treatment between fixed and moving grids
- Use of multi-block sliding meshes
- Construction of a common interface grid using non conforming grid with hanging vertices



ALE Finite Volumes Discretization on 3D Unstructured Meshes (cell-centered approach)

- Implicit Crank-Nicolson temporal integration (second order of accuracy)
- Face by face conservative spatial integration
- Left and Right quadratic reconstruction of primitive variables
- Use ALE version of Van Leer, Roe or AUSM(+up) numerical flux functions taking grid velocity into account
- Exact preservation of a uniform and time independent flow on moving grids (DGCL condition)
- Modification of Coirier diamond path for viscous fluxes to obtain first order accuracy and preserve positivity property
- Parallel computing based on domain decomposition (Metis, MPI, PETSc)



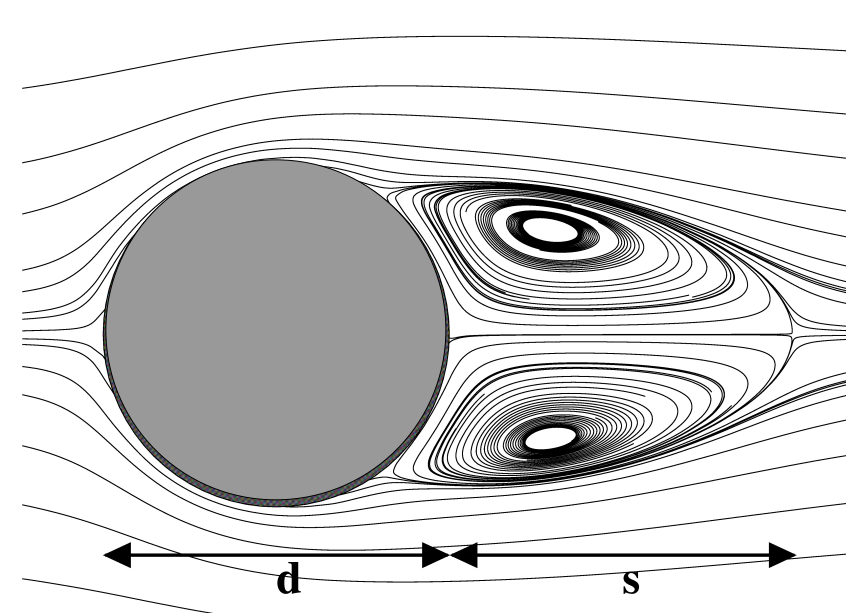
$$\frac{V^{l+1} s(\mathbf{w}^{l+1}) - V^l s(\mathbf{w}^l)}{V^{l+1} \Delta t^{l+1}} = \frac{1}{2} \frac{1}{V^{l+1}} \mathbf{Rhs}^{l+1} + \frac{1}{2} \frac{1}{V^l} \mathbf{Rhs}^l$$

$$\mathbf{Rhs} = \sum_i \int \int_{\Delta_i / \square_i} \left[\tilde{\mathbf{f}}_n^a(\tilde{\mathbf{w}}_L, \tilde{\mathbf{w}}_R, \tilde{v}_n^g) + \mathbf{f}_n^d(\tilde{\mathbf{w}}, \nabla \tilde{\mathbf{w}}) \right] dS_i$$

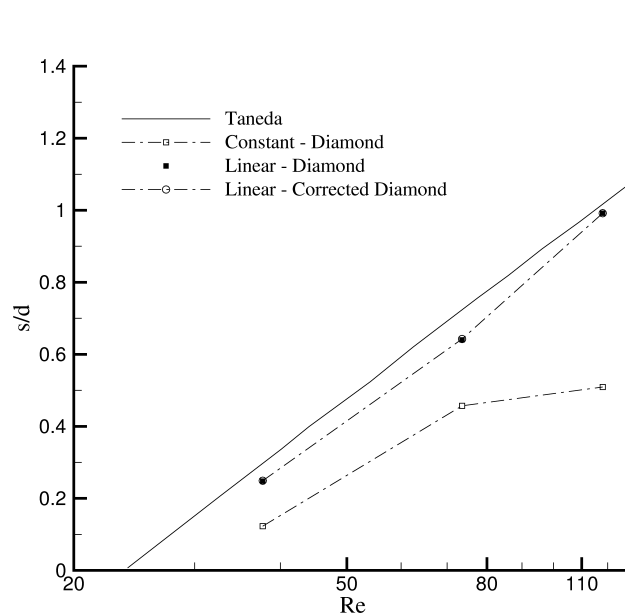
$$\tilde{\mathbf{f}}_n^a(\tilde{\mathbf{w}}_L, \tilde{\mathbf{w}}_R, \tilde{v}_n^g) \approx \mathbf{f}_n^a(\mathbf{w}) - \mathbf{s} v_n^g$$

$$\tilde{w}_{L/R} = w_{L/R} + (\mathbf{x} - \mathbf{x}_{L/R})^T \nabla(w) \Big|_{L/R} + \frac{1}{2} (\mathbf{x} - \mathbf{x}_{L/R})^T \mathbf{H}(w) \Big|_{L/R} (\mathbf{x} - \mathbf{x}_{L/R})$$

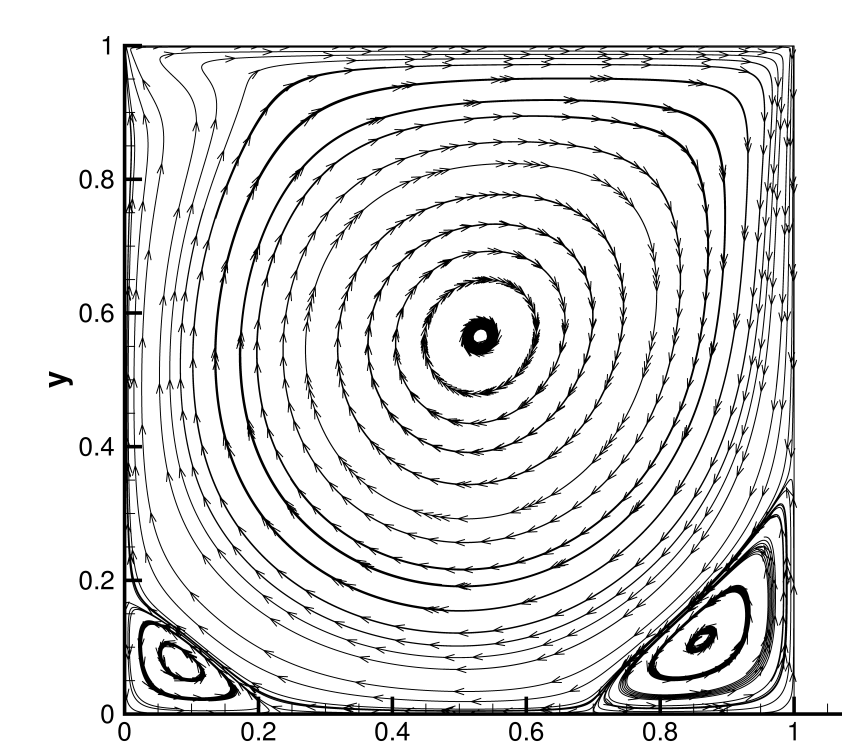
$$\tilde{v}_n^g = v_n^g \left(\frac{t^{l+1} + 1}{2} - \frac{\sqrt{3}}{3} \frac{\Delta t^{l+1}}{2} \right) \quad \tilde{v}_n^{g,l+1} = v_n^g \left(\frac{t^{l+1} + 1}{2} + \frac{\sqrt{3}}{3} \frac{\Delta t^{l+1}}{2} \right)$$



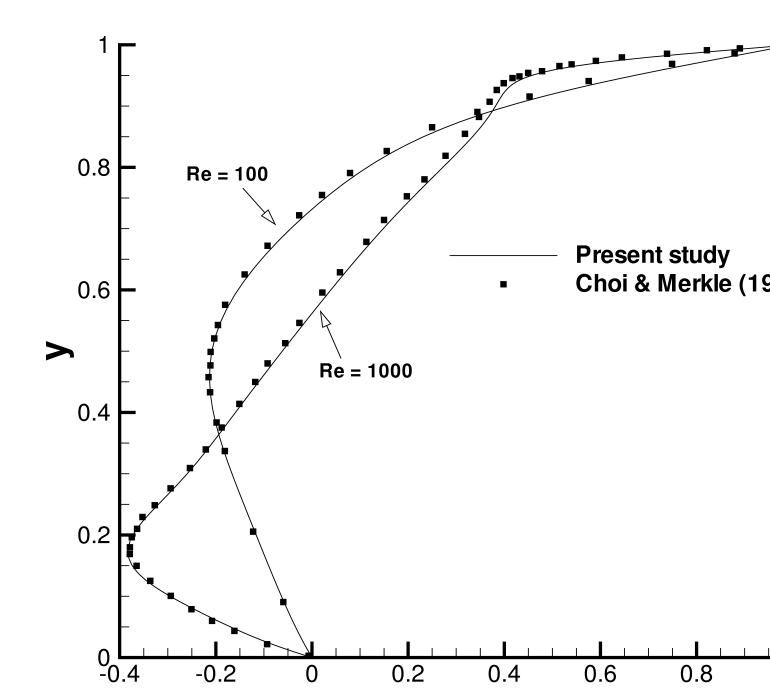
Steady flow past a sphere Re = 118



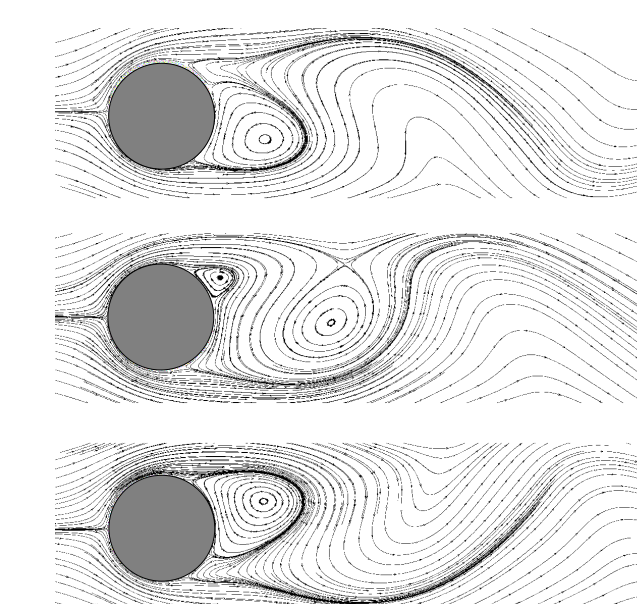
Steady flow past a sphere Scheme accuracy analysis



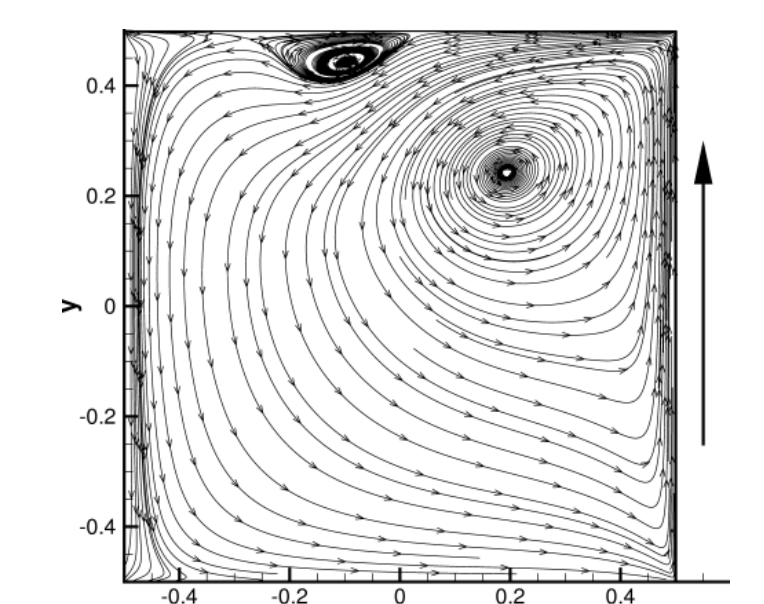
2D steady lid-driven cavity flow Re = 1000



2D lid driven flow x-velocity



Unsteady flow past a cylinder Re = 100



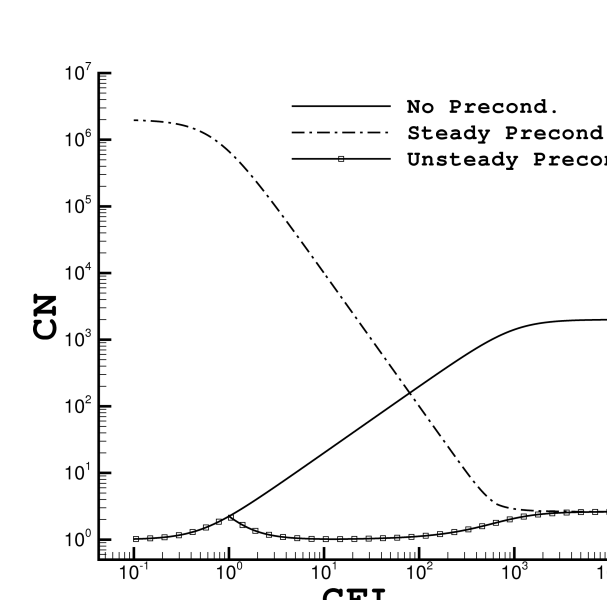
3D lid-driven cavity flow Re = 1000

Local Preconditioning Techniques

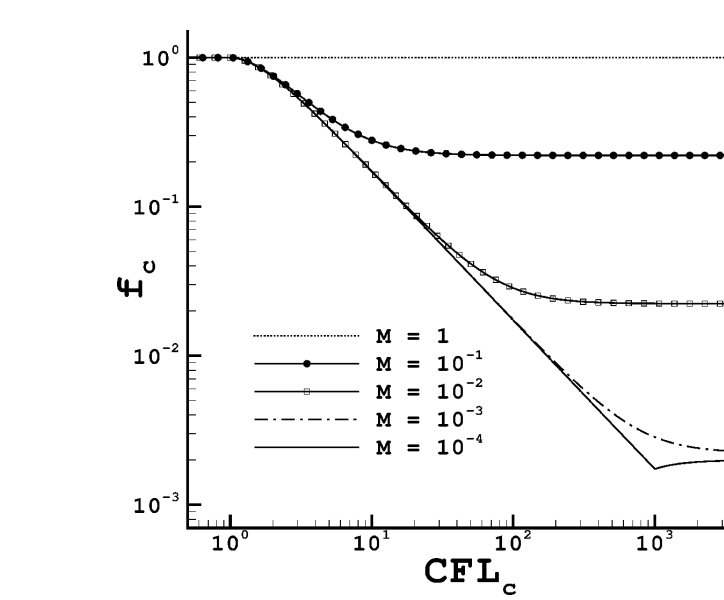
- Fully implicit dual time stepping
- Matrix free Newton-GMRes algorithm
- Introduction of an artificial speed of sound to improve the condition number for all Mach, Reynolds and Strouhal numbers
- New scaling of numerical flux dissipation for accuracy

$$M_* = \frac{c_*}{c} = \min \left[1, \max \left(\sqrt{M^2 + CFL_c^{-2}}, M_\epsilon \right) \right]$$

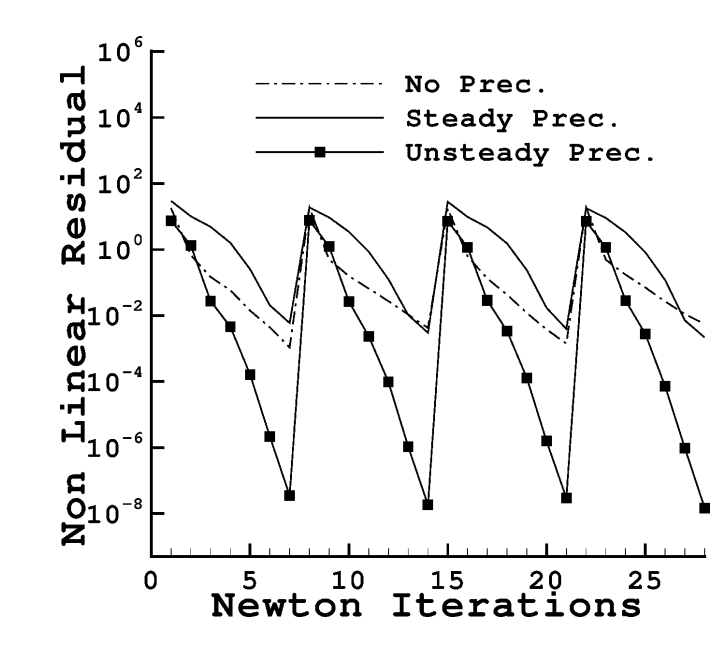
$$\left[\frac{\mathbf{P}^n}{\Delta \tau^n} + \frac{\mathbf{S}^n}{\Delta t^{l+1}} - \frac{1}{2} \mathbf{J}^n \right] (\mathbf{w}^{n+1} - \mathbf{w}^n) = - \frac{V^{l+1} s(\mathbf{w}^n) - V^l s(\mathbf{w}^l)}{V^{l+1} \Delta t^{l+1}} + \frac{1}{2} \frac{1}{V^{l+1}} [\mathbf{Rhs}(\mathbf{w}^n) + \mathbf{Rhs}(\mathbf{w}^l)]$$



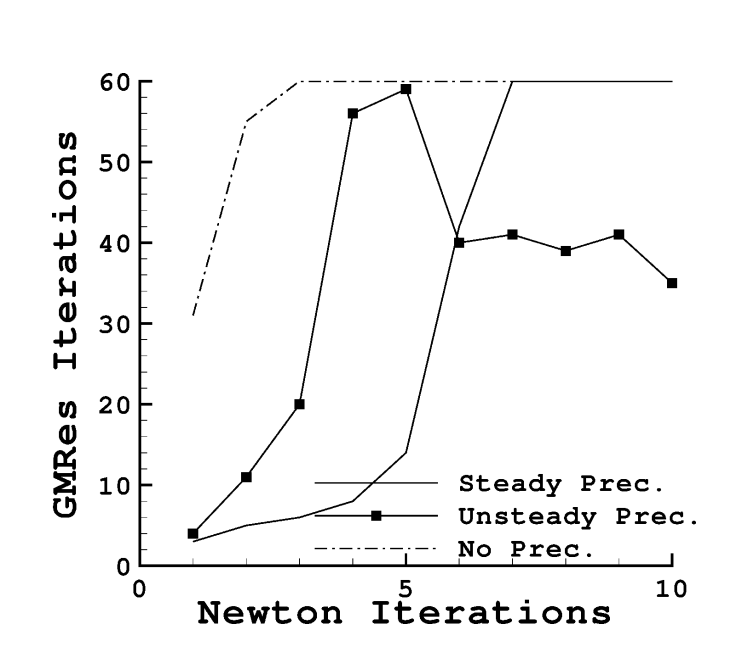
Condition number



Ausm+up dissipation scaling function



Newton convergence



GMRes convergence

University of Liège - Aerospace and Mechanical Engineering Department



Aerodynamics (Prof. J.-A. Essers)
Turbomachinery (Prof. O. Léonard)
Chemin des Chevreuils, 1 B52/3
B-4000 Liège (Belgium)

<http://www.ulg.ac.be/aerodyn>
Phone : +32 (0)4 366 94 39
Fax : +32 (0)4 366 91 36
Didier.Vigneron@ulg.ac.be

