



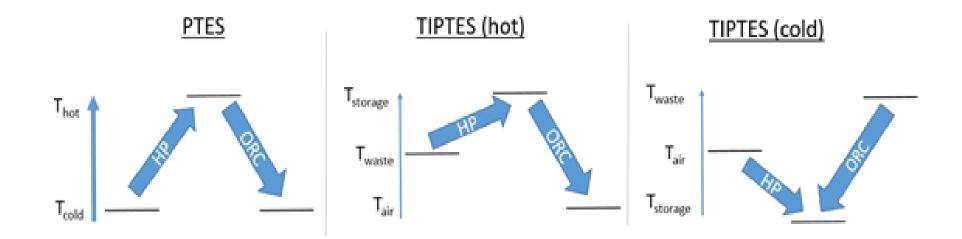
Investigation of a thermally integrated Carnot battery using a reversible heat pump/organic Rankine cycle

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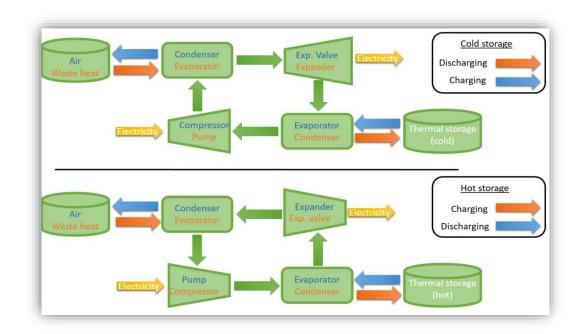
Why Rankine?

- Already available commercial products
- Thermal integration
- Low temperature
- Low costs



Reversible HP/ORC unit

- One unit able to work as HP and as ORC
- Cheap
- Constraints (Reynolds, efficiency)



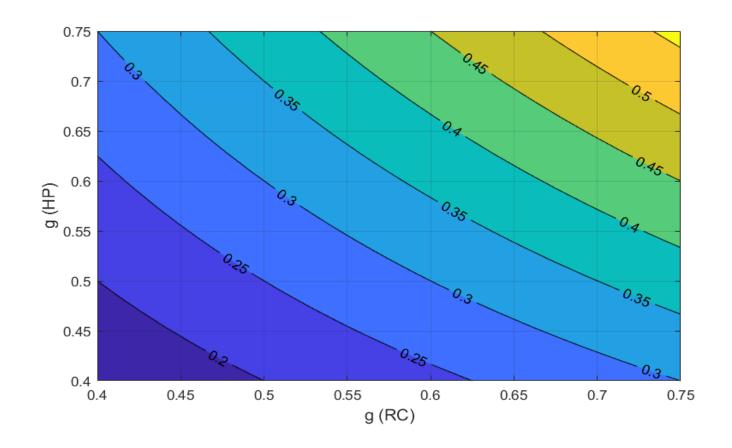


Mapping of performance

$$\varepsilon_{rt,hot} = \left(\frac{COP_{HP,hot}}{Q_{cd,HP}}\right) \cdot \left(\eta_{RC,hot}Q_{ev,RC}\right) = COP_{HP,hot} \cdot \eta_{RC,hot}$$

$$COP_{HP} = \frac{Q_{cd}}{E_{el}} = g_{HP} \frac{T_{hot}}{T_{hot} - T_{cold}}$$

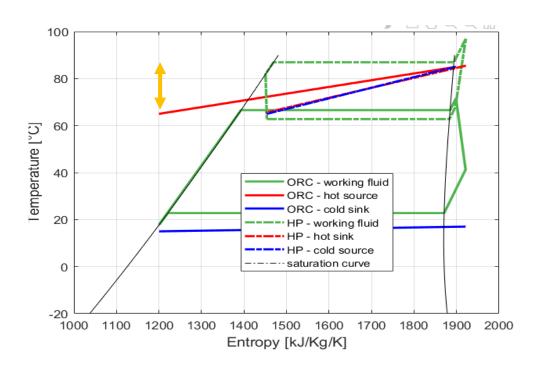
$$\eta_{RC} = \frac{E_{el}}{Q_{ev}} = g_{RC}(1 - \frac{T_{cold}}{T_{hot}})$$



Thermal integration

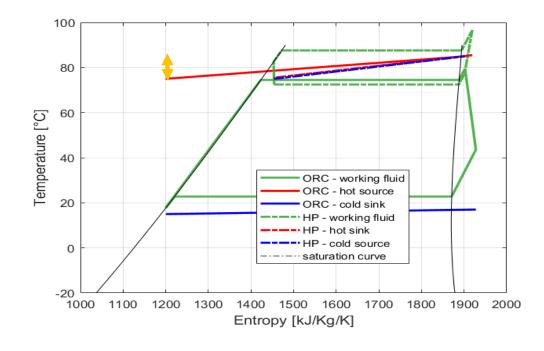
High lift

- High compactness
- High waste heat energy use

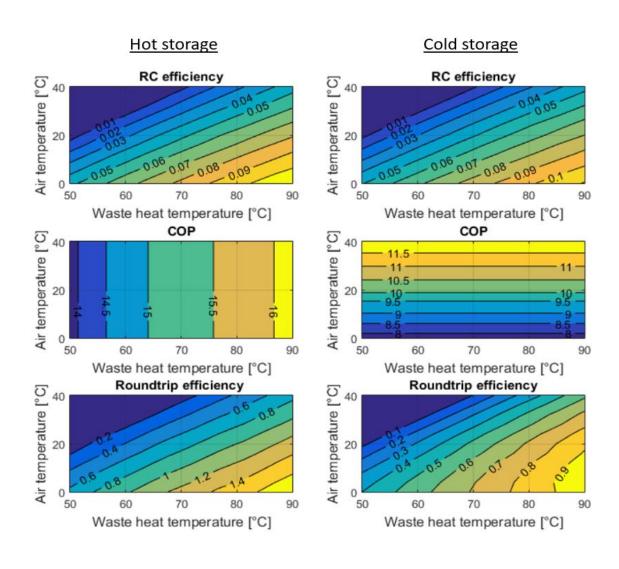


Low lift

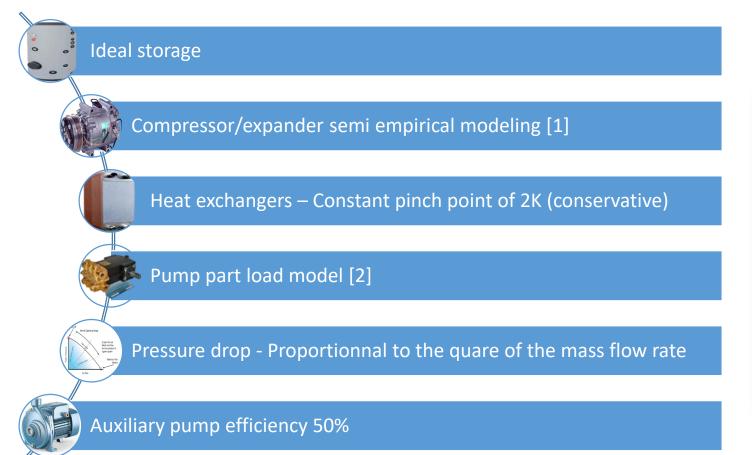
High roundtrip efficiency

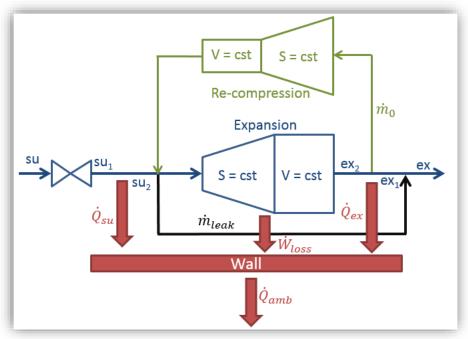


Mapping of performance (thermally integrated)



Modeling





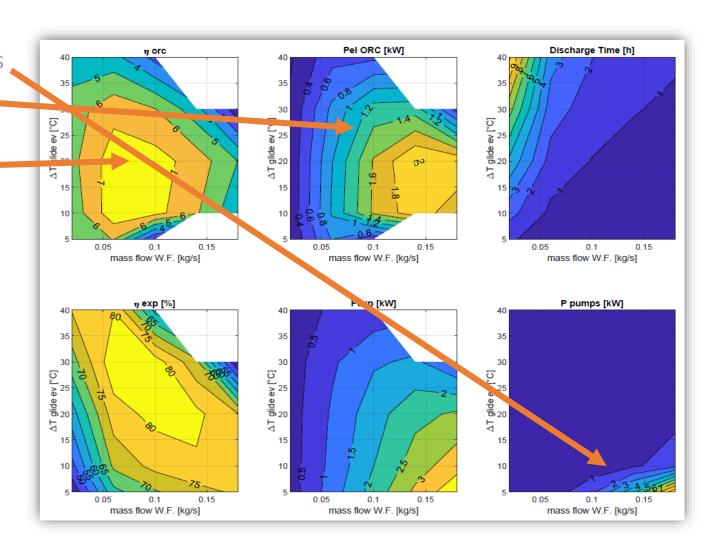
[1] Landelle, A., Tauveron, N., Revellin, R., Haberschill, P., Colasson, S., Roussel, V., 2017. Performance investigation of reciprocating pump running with organic fluid for organic Rankine cycle, Applied Thermal Engineering 113 (2017) 962–969 [2] Lemort, V., 2008. PhD thesis, Contribution to the characterization of scroll machines in compressor and expander modes, (Liege).



ORC Mappings



- For to temperature levels:
- Possibly strong influence of auxiliary pumps
- Optimization of the evaporator glide
- Necessary optimization of the mass flow rate

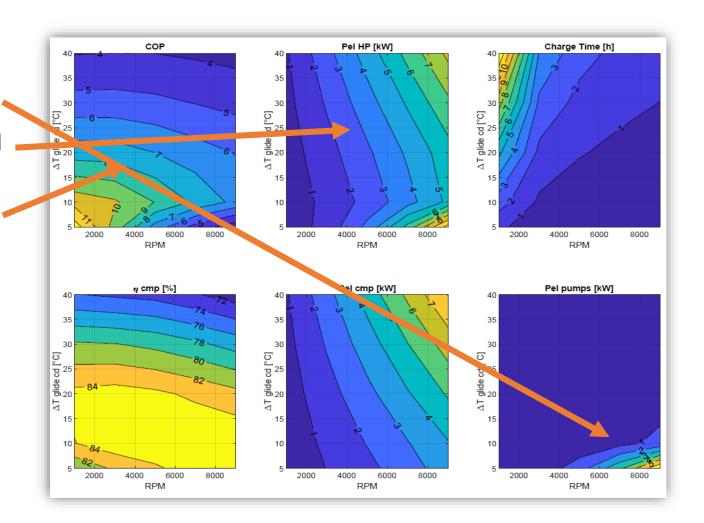




HP mappings



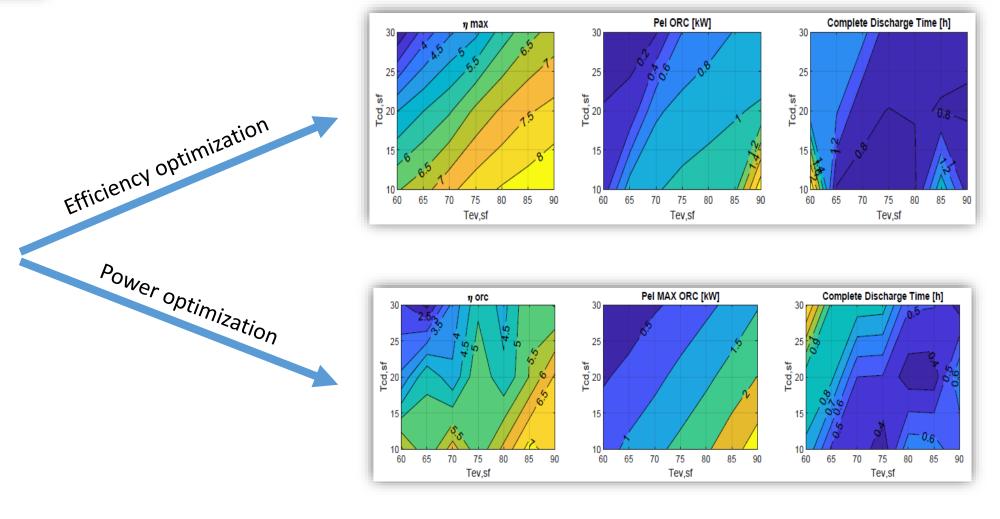
- For to temperature levels:
- Possibly strong influence of auxiliary pumps
- Increase of the thermal power with the RPM and with the glide (opposite for COP)
- Necessary optimization of the scroll speed





Optimization of ORC performance



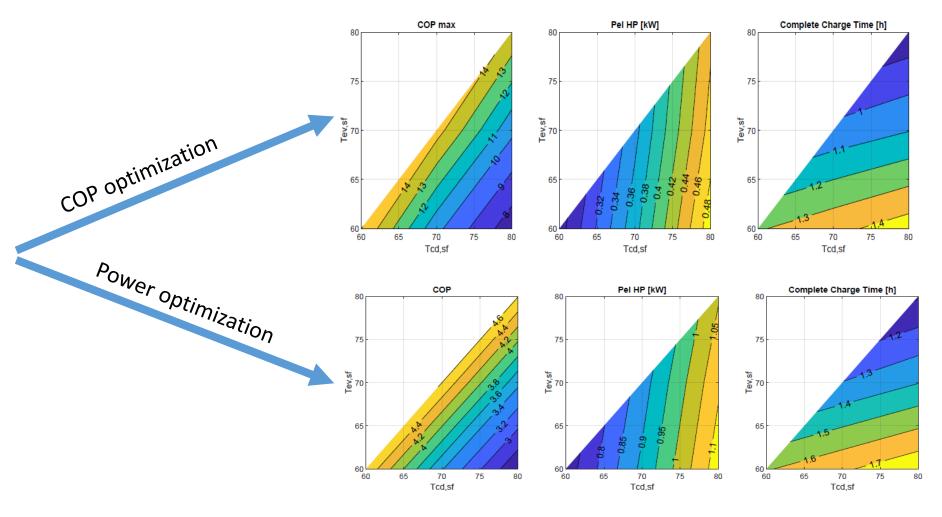


→ Power increased with glides and mass flow rate



Optimization of heat pump performance





- Power increased with glides and mass flow rate
- Strong influence on COP

Experimental setup

Heat Pump

- Cold source= Waste heat (75°C)
- Hot sink = storage (85°C)
- COP = 14

ORC

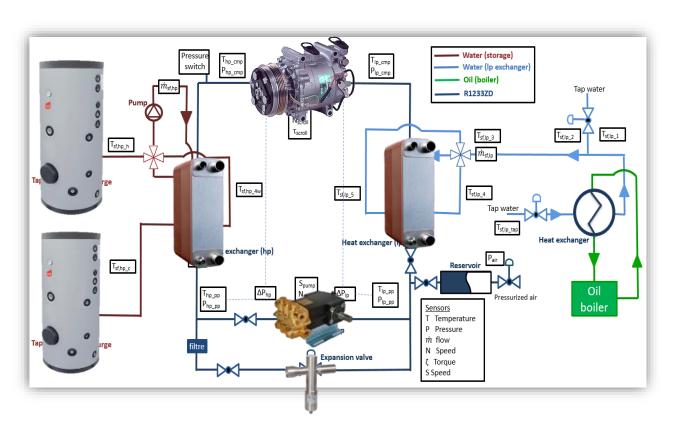
- Hot source = Storage (85°C)
- Cold sink = Air (15°C)
- Efficiency = 7%

→ Energy to energy ratio ~ 100%



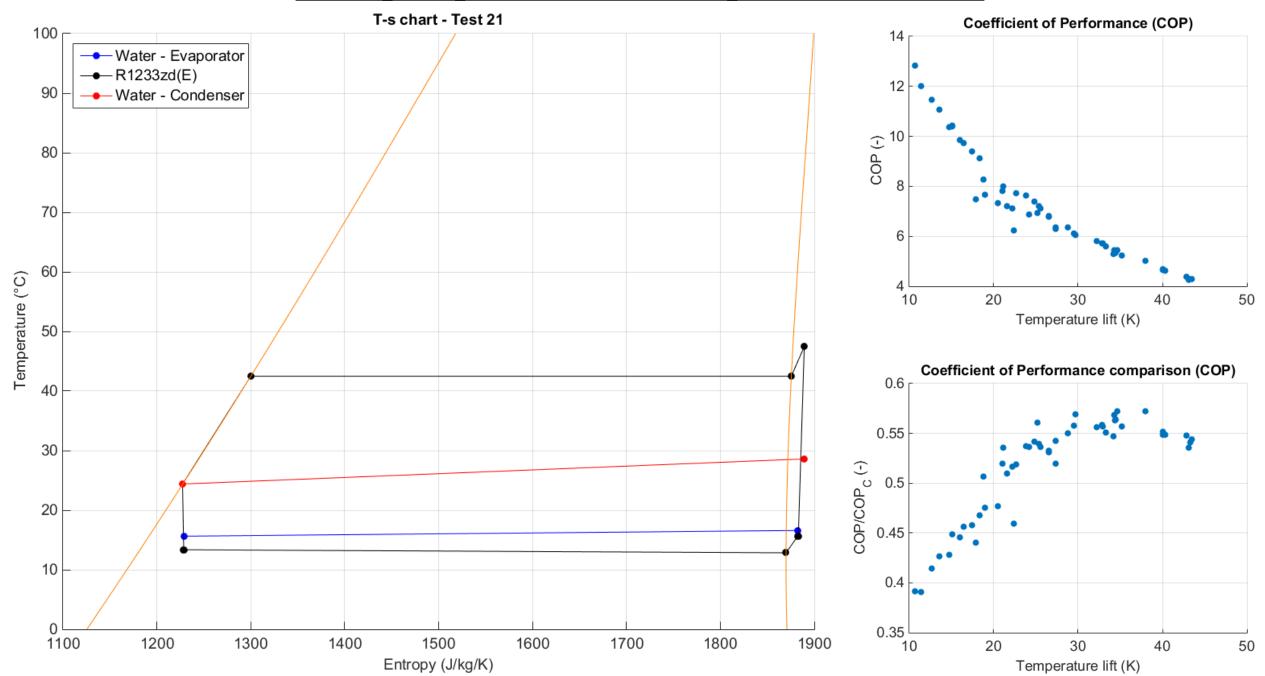
		ORC	HP
	Sub-cooling [K]	5	5
	Exchangers pinch points [K]	2	2
	Evaporator secondary fluid glide [K]	10	10
Parameters	Condenser secondary fluid glide [K]	2	10
Ĕ	Compressor volume ratio [-]	2.2	
Para	Compressor maximum efficiency [-]	0.75	
	Condenser secondary fluid temperature [°C]	15	85
	Evaporator secondary fluid temperature [°C]	80	75
	COP/eff [-]	0.076	12.9
	Condenser thermal power [W]	20985	24110
	Evaporator thermal power [W]	22844	21720
	Compressor power [W]	1942	1865
	Condenser pressure [bar]	1.25	8.27
Outputs	Evaporator pressure [bar]	5.45	5.17
	Working fluid flow rate [kg/s]	0.096	0.14
	Compressor speed [RPM]	5000	8000
	Auxiliary pump consumption	129	29
	Compressor efficiency [-]	0.70	0.72
	Volume ratio [-]	2.26	0.57
	Compressor swept volume [m³]	3e ⁻⁵	
	P2P [-]	1.01	
	Reynolds ratio [-]	0.76	
	Electrical ratio [-]	1.04	

Layout/components

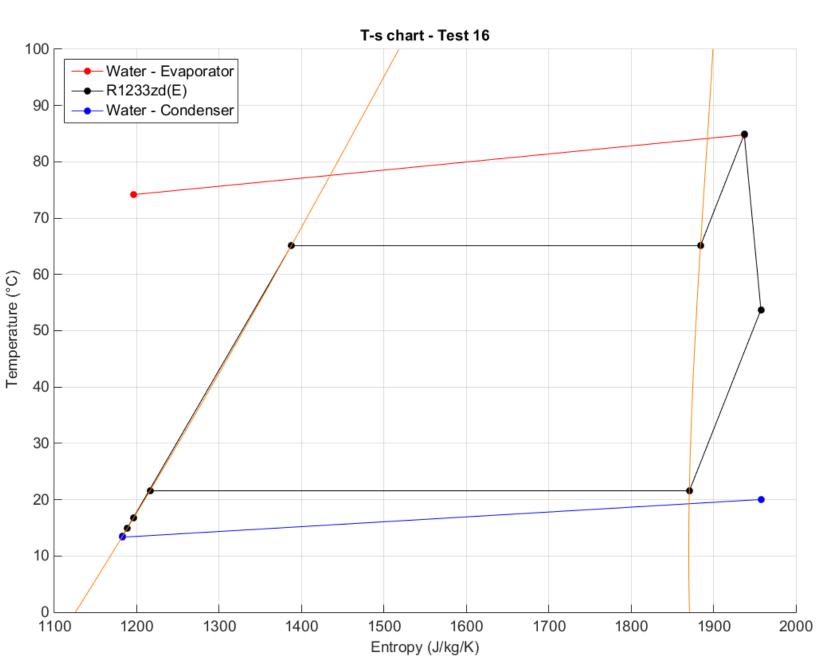


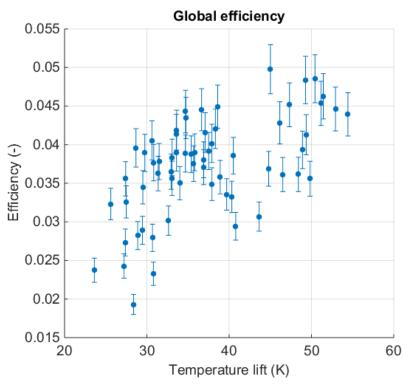
- Mechanical scroll
 Variable speed
 VR=2.2
 Swept volume = 121 cm³
- <u>Plate heat exchangers</u> 25 kW
- Hot and cold water storage
 Perfect stratification
 2X900 L
- Plunger pump 70 g/s
- Manual expansion valve

<u>Heat pump mode – Global performance (1)</u>

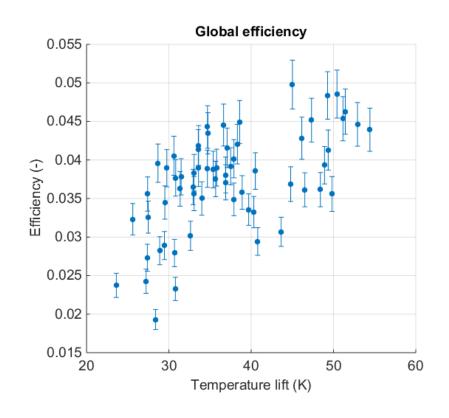


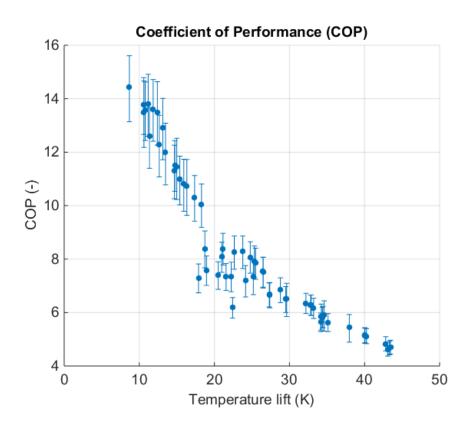
ORC mode – Global performance





First tests





- No optimal control (scroll speed, sub-cooling, over-heating)
- No optimization of the volumetric machine

Thank you!

Perspectives

- Control optimization
- Cycle optimization
- Business model



Open source papers → https://orbi.uliege.be/myorbi



