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**IDENTIFICATION OF THE ESSENTIAL FEATURES OF THE TRANSIENT
 AMPLIFICATION OF MISTUNED SYSTEMS**

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ABSTRACT

The dynamic behavior of bladed disks in resonance crossing has been intensively investigated in the community of turbomachinery, addressing the attention to (1) the transient-type response that appear when the resonance is crossed with a finite sweep rate and (2) the localization of the vibration in the disk due to the blade mistuning. In real conditions, the two mentioned effects coexist and can interact in a complex manner. This paper investigates the problem by means of analytic solutions obtained through asymptotic expansions, as well as numerical simulations. The mechanical system is assumed as simple as possible: a 2-dof linear system defined through the three parameters: damping ratio ξ , frequency mistuning Δ , rotor acceleration $\dot{\Omega}$. The analytic solutions are calculated through the multiple-scale method.

NOMENCLATURE

A response amplitude
 α angle of the mistuning pattern
 \mathbb{C} set of complex numbers
 δ_K, δ_M mistuning amplitude for \mathbf{K} and \mathbf{M}
 $\partial_i, \partial_\tau$ partial derivative with respect to t and τ
 Δ mistuning amplitude
 EO engine order
 f force complex amplitude
 \mathbf{f} force vector
 ϕ phase angle between TW responses
 $\phi_r^{(c)}, \phi_r^{(s)}$ standing-wave modes
 i imaginary unit
 \mathbf{I} identity matrix
 k blade stiffness
 k_c blade coupling stiffness
 \mathbf{K} stiffness matrix

κ reduced chirp rate
 λ_r system eigenvalues
 m complex mistuning parameter
 \mathbf{M} mass matrix
 N number of blades
 QS quasi steady
 r harmonic index
 \mathbb{R} set of real numbers
 Ψ_r traveling-wave modes
 SW standing wave
 t time
 τ slow time scale
 TW traveling wave
 \mathbf{u} blade displacement vector
 ω_r natural frequencies
 $\bar{\omega}$ average natural frequency of mistuned system
 Ω rotor speed
 x_1, x_2 SW coordinates
 ξ damping
 y_1, y_2 TW coordinates
 Y, Y_1, Y_2 TW amplitudes after time shift
Superscript
 \bullet temporal derivative
 T transpose
 $*$ Hermitian transpose
Subscript
 QS quantity related to QS regime
 $tuned$ quantity related to the tuned system

INTRODUCTION

The dynamic behavior of bladed disks in resonance crossing has been intensively investigated in the community of turbomachinery. In particular, the attention has been addressed towards two issues: (1) the transient-type response that appear when the resonance is crossed with a finite sweep rate and (2) the localization of the vibration in the disk due to the blade mistuning.

The transient effects produce a reduction of the maximum amplitude of the response and shift (upwards in run-up) the rotor speed at which the maximum response appears. Coherently with the common intuition, the reduction of the maximum amplitude of vibration is proportional to the rotor acceleration, e.g. [1-5].

Blade mistuning produces the increment of the dynamic response of some blades when the disk is excited with a resonant or quasi-resonant force. On this matter the literature is vast and a wide list of references can be found for example in [6] and in the recent monography [7]. Some analytical formulations developed in the quasi-steady regime, i.e. disregarding the transient effects due to the rotor acceleration, show that the increment of dynamic amplification compared to the tuned case is a function of the mistuning level and damping [8], as well as the number of active modes involved in the disk response [9].

In real conditions, the two mentioned effects coexist and can interact in a complex manner, e.g. [3]. In particular, it was observed that the reduction of the dynamic response that is expected in resonant crossing due to the transient effects may vanish when dealing with mistuned disks [10]. For some systems it was even observed a weak over-amplification compared to the quasi-steady prediction, which appears quite counterintuitive. This phenomenon has been called Transient Amplitude Amplification of Mistuned Systems (TAMS) and has been investigated both numerically as well as experimentally [11-13].

This paper investigates the TAMS by means of analytic solutions obtained through asymptotic expansions, as well as numerical simulations. The problem is studied working on the simplest possible bladed disk model able to produce TAMS, namely, a 2-dof linear system defined through the three parameters: damping ratio ξ , frequency mistuning Δ , rotor acceleration $\dot{\Omega}$. The dynamic response is calculated using the multiple-scale method. The differential equation governing the evolution of the complex envelope are derived both for the case of tuned and mistuned disks. The analytic solutions demonstrate that the problem is governed by two parameters $\dot{\Omega}/\xi^2$ and Δ/ξ .

IDEALIZED DISK MODEL

In order to analyze the nature of the TAMS, we consider a mechanical system that, remaining as simple as possible, retains the important features of a bladed disk. To this purpose, we start from an idealized bladed disc composed by N blades modeled as s -dof systems. The equation of motion has the form

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{f} \quad (1)$$

where \mathbf{M} and \mathbf{K} are the mass and stiffness matrices, respectively, $\mathbf{u} \in \mathbb{R}^N$ is the displacement vector and $\mathbf{f} \in \mathbb{R}^N$ is the external force. The damping term is assumed to be small and will be introduced later.

Tuned case

If the disk is cyclic symmetric, \mathbf{M} and \mathbf{K} are circulant matrices, i.e. they have the structure [7]

$$\mathbf{K} = \begin{bmatrix} k & k_c & & & k_c \\ k_c & k & k_c & & \\ & k_c & \ddots & \ddots & \\ & & \ddots & k & k_c \\ k_c & & & k_c & k \end{bmatrix} \quad (2)$$

Under this condition, the vibration modes have harmonic shape, i.e. their j^{th} components are in the form [7]

$$\begin{aligned} \phi_{r,j}^{(c)} &= \frac{1}{\sqrt{N}} \cos\left(2\pi r \frac{j}{N}\right) & \left(r = 0 \dots \text{floor}\left(\frac{N}{2}\right) \right) \\ \phi_{r,j}^{(s)} &= \frac{1}{\sqrt{N}} \sin\left(2\pi r \frac{j}{N}\right) & \left(j = 1 \dots N \right) \end{aligned} \quad (3)$$

where r is called harmonic index and $\text{floor}(\bullet)$ is the rounding towards $-\infty$. For the cases $r = 0$ and $r = N/2$ (if N is even), the eigenvector $\phi^{(s)}$ does not exist. In the other cases, the eigenvectors $\phi^{(c)}$ and $\phi^{(s)}$ share the same eigenvalue $\lambda_r = \omega_r^2$.

The force \mathbf{f} is assumed as a traveling wave (TW) excitation, whose frequency changes linearly in time. It represents an Engine Order component of a synchronous excitation during a constant-acceleration run-up or run-down. For reasons that will be clear afterwards, it is convenient to represent the force using the complex-valued notation

$$\mathbf{f} = \boldsymbol{\psi}_r f e^{\frac{1}{2} i r \Omega t^2} \quad (4)$$

where f is the force complex amplitude, the index r is here interpreted as EO, $\dot{\Omega}$ is the rotor acceleration, referred to as chirp rate, and $\boldsymbol{\psi}_r$ is a vector whose components $\psi_{r,j}$ are given as

$$\psi_{r,j} = \frac{1}{\sqrt{N}} e^{2\pi i r \frac{j}{N}} \quad (j = 1, \dots, N) \quad (5)$$

Comparing Eq. (3) and Eq. (5), it can be deduced from the Euler's identity that

$$\begin{aligned} \boldsymbol{\psi}_r &= \phi_r^{(c)} + i \phi_r^{(s)} \\ \boldsymbol{\psi}_{-r} &= \phi_r^{(c)} - i \phi_r^{(s)} \end{aligned} \quad (6)$$

Since the vectors $\boldsymbol{\psi}_r$ and $\boldsymbol{\psi}_{-r}$ are given by two independent linear combinations of eigenvectors sharing the same

eigenvalues, then they are eigenvectors as well. Due to their nature, $\phi_r^{(c)}$ and $\phi_r^{(s)}$ are called Standing Wave (SW) modes, while ψ_r and ψ_{-r} are called Traveling Wave (TW) modes.

Let us assume that the blade motion is entirely described by the mode pair with harmonic index r , i.e.:

$$\begin{aligned} \mathbf{u}(t) &= \text{Re}\left(\phi_r^{(c)}x_1(t) + \phi_r^{(s)}x_2(t)\right) \\ &= \text{Re}\left(\psi_r y_1(t) + \psi_{-r} y_2(t)\right) \end{aligned} \quad (7)$$

where the extraction of the real part is required due to the choice of using a complex-valued force in Eq. (4), thus x_j and y_j are complex valued as well.

The equations of motion projected on the SW modes read

$$\begin{aligned} \ddot{x}_1 + 2\xi\omega_r\dot{x}_1 + \omega_r^2 x_1 &= \phi_r^{(c)\text{T}} \mathbf{f} = f e^{\frac{1}{2}i r \Omega t^2} \\ \ddot{x}_2 + 2\xi\omega_r\dot{x}_2 + \omega_r^2 x_2 &= \phi_r^{(s)\text{T}} \mathbf{f} = f i e^{\frac{1}{2}i r \Omega t^2} \end{aligned} \quad (8)$$

in which a viscous dissipation has been added and parametrized by the modal damping ratio ξ , assumed equal for both the modes.

The two Eqs. (8) are identical and are excited by equal forces with 90-degree phase shift. Besides, also the real and imaginary parts of both x_1 and x_2 have the same amplitude and 90-degree phase shift.

If the equations of motion are projected on the TW modes, they assume the form

$$\begin{aligned} \ddot{y}_1 + 2\xi\omega_r\dot{y}_1 + \omega_r^2 y_1 &= \psi_r^* \mathbf{f} = f e^{\frac{1}{2}i r \Omega t^2} \\ \ddot{y}_2 + 2\xi\omega_r\dot{y}_2 + \omega_r^2 y_2 &= \psi_{-r}^* \mathbf{f} = 0 \end{aligned} \quad (9)$$

where the superscript $*$ represents the Hermitian transpose. Also in this case the two equation of motion are identical, however the force appears only in the first equation, corresponding to the mode having the same whirl direction of the considered force. The relationship between SW and TW coordinates can be deduced by substituting Eqs. (6) into Eqs. (7)

$$y_1 = \frac{x_1 - i x_2}{2}; \quad y_2 = \frac{x_1 + i x_2}{2} \quad (10)$$

The assumption of having only two active modes is obviously a simplification with respect to the general case. However, it represents the realistic situation in which mistuning is small and the natural frequencies are well isolated.

Mistuning

Blade mistuning modifies the shape of the matrices \mathbf{M} and \mathbf{K} and, as a consequence, destroys the regular structure of eigenvalues and eigenvectors that have been described above [7].

Since we are interested in exploring simple systems, we assume that the blade vibration can be still represented by two vibration modes that retain the harmonic structure of the tuned

disk. This happens rigorously if the two considered modes are isolated and the mistuning pattern has a harmonic shape with harmonic index $2r$, i.e. the system matrices are updated as [9]:

$$\begin{aligned} \mathbf{K} &\leftarrow \mathbf{K} + \text{diag}\left(\delta_K \psi_{2r} + \delta_K^* \psi_{-2r}\right) \\ \mathbf{M} &\leftarrow \mathbf{M} + \text{diag}\left(\delta_M \psi_{2r} + \delta_M^* \psi_{-2r}\right) \end{aligned} \quad (11)$$

where δ_K and δ_M are complex-valued constants representing the amplitude of the mistuning and $\text{diag}(\cdot)$ constructs a diagonal matrix from a vector. This result is actually obtained even when the mistuning pattern does not follow the mentioned condition, but, simply, when it is very small.

As an effect of the mistuning, the double eigenvalue λ_r splits into two separate eigenvalues $\lambda_{r,1} = \omega_{r,1}^2$ and $\lambda_{r,2} = \omega_{r,2}^2$. Due to this circumstance, the TW vectors ψ_r and ψ_{-r} are not vibration modes of the system. Besides, the SW modes defined by Eq. (3) are modified as [14]:

$$\begin{aligned} \phi_{r,j}^{(c)} &= \frac{1}{\sqrt{N}} \cos\left(2\pi r \frac{j}{N} + \frac{\alpha}{2}\right) \\ \phi_{r,j}^{(s)} &= \frac{1}{\sqrt{N}} \sin\left(2\pi r \frac{j}{N} + \frac{\alpha}{2}\right) \end{aligned} \quad \begin{cases} r = 0 \dots \text{floor}\left(\frac{N}{2}\right) \\ j = 1 \dots N \end{cases} \quad (12)$$

where the angle α depends on the constants δ_K and δ_M and is referred to as mode clocking.

The equations of motion in terms of SW coordinates are a simple update of Eqs. (8), i.e.,

$$\begin{aligned} \ddot{x}_1 + 2\xi(1-\Delta)\bar{\omega}\dot{x}_1 + (1-\Delta)^2 \bar{\omega}^2 x_1 &= f e^{\frac{1}{2}i r \Omega t^2} e^{-i\frac{\alpha}{2}} \\ \ddot{x}_2 + 2\xi(1+\Delta)\bar{\omega}\dot{x}_2 + (1+\Delta)^2 \bar{\omega}^2 x_2 &= f i e^{\frac{1}{2}i r \Omega t^2} e^{-i\frac{\alpha}{2}} \end{aligned} \quad (13)$$

where

$$\bar{\omega} = \frac{\omega_{r,1} + \omega_{r,2}}{2}; \quad \Delta = \frac{\omega_{r,2} - \omega_{r,1}}{\omega_{r,1} + \omega_{r,2}} \quad (14)$$

The relationship between the SW amplitudes and the TW amplitudes can be obtained by substituting Eqs. (12) into Eqs. (7). It yields:

$$y_1 = \frac{x_1 - i x_2}{2} e^{i\frac{\alpha}{2}}; \quad y_2 = \frac{x_1 + i x_2}{2} e^{-i\frac{\alpha}{2}} \quad (15)$$

The manipulation of Eqs. (13) according to Eqs. (15) provides the equations of motion in terms of TW coordinates as:

$$\begin{aligned} \begin{bmatrix} \ddot{y}_1 \\ \ddot{y}_2 \end{bmatrix} + 2\xi\bar{\omega} \begin{bmatrix} 1 & -\Delta e^{i\alpha} \\ -\Delta e^{-i\alpha} & 1 \end{bmatrix} \begin{bmatrix} \dot{y}_1 \\ \dot{y}_2 \end{bmatrix} + \bar{\omega}^2 \begin{bmatrix} 1+\Delta^2 & -2\Delta e^{i\alpha} \\ -2\Delta e^{-i\alpha} & 1+\Delta^2 \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} &= \begin{bmatrix} f e^{\frac{1}{2}i r \Omega t^2} \\ 0 \end{bmatrix} \end{aligned} \quad (16)$$

It can be observed that, while the equations in term of SW

coordinates remain decoupled, the equations in terms of TW coordinates become coupled due to terms that scale with the mistuning amplitude.

For a systematic analysis of the problem, Eqs. (16) are non-dimensionalized introducing the scaling

$$\begin{aligned} t &\leftarrow \bar{\omega}t; \quad \Omega \leftarrow \frac{\Omega}{\bar{\omega}}; \quad \dot{\Omega} \leftarrow \frac{\dot{\Omega}}{\bar{\omega}^2} \\ y_j &\leftarrow i \frac{2\xi}{f} y_j \quad (j=1,2) \end{aligned} \quad (17)$$

Besides, the harmonic index r is set equal to 1 without introducing any conceptual restriction. After these modifications, the equations of become:

$$\begin{aligned} \begin{bmatrix} \ddot{y}_1 \\ \ddot{y}_2 \end{bmatrix} + 2\xi \begin{bmatrix} 1 & -\Delta e^{i\alpha} \\ -\Delta e^{-i\alpha} & 1 \end{bmatrix} \begin{bmatrix} \dot{y}_1 \\ \dot{y}_2 \end{bmatrix} + \\ + \begin{bmatrix} 1 + \Delta^2 & -2\Delta e^{i\alpha} \\ -2\Delta e^{-i\alpha} & 1 + \Delta^2 \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = 2\xi i \begin{bmatrix} e^{\frac{1}{2}i\Omega t^2} \\ 0 \end{bmatrix} \end{aligned} \quad (18)$$

QUASI-STEADY RESPONSE OF A TUNED SYSTEM

If the system is tuned (i.e. $\Delta=0$) and if the chirp rate $\dot{\Omega}$ is very small (to be quantified next), the system response can be obtained as the steady-state response due to a harmonic load of frequency $\Omega = \dot{\Omega}t$, i.e.:

$$\begin{bmatrix} \ddot{y}_1 \\ \ddot{y}_2 \end{bmatrix} + 2\xi \begin{bmatrix} \dot{y}_1 \\ \dot{y}_2 \end{bmatrix} + \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = 2\xi i \begin{bmatrix} e^{i\Omega t} \\ 0 \end{bmatrix} \quad (19)$$

where only y_1 shows a resonance at $\Omega=1$, while y_2 remains $\sim \mathcal{O}(\xi)$ and can be neglected. The solution is readily available in the form:

$$y_1 = A e^{i\Omega t}; \quad A = \frac{2\xi i}{1 - \Omega^2 + 2i\xi\Omega} \quad (20)$$

showing that, for $\xi \ll 1$, the maximum amplitude appears at $t = 1/\dot{\Omega}$ and is equal to 1

$$A_{QS-tuned} = \max |A| = 1 \quad (21)$$

Figure 1 shows the response of a bladed disk with $N_b = 6$ blades and $\xi = 3 \cdot 10^{-3}$. The amplitude $|A|$ is reported together with the displacement u_j of the individual blades. It can be observed that all the blades share the same envelope, but vibrate with a different phase angle.

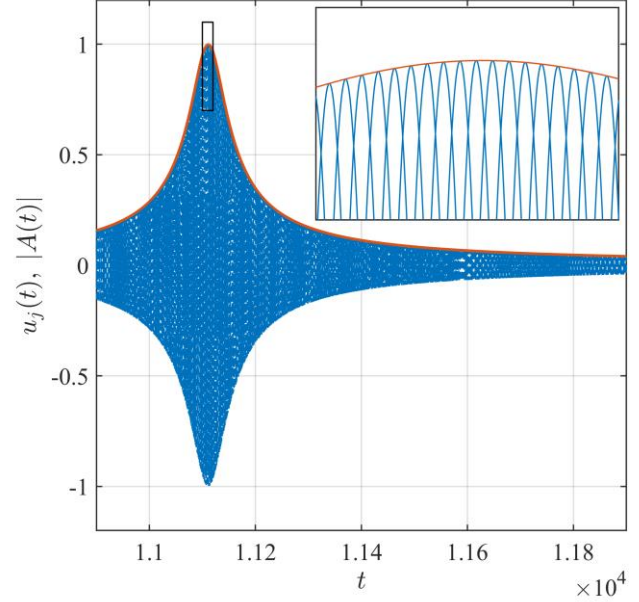


Figure 1. Quasi-steady response of a tuned disk.

TRANSIENT RESPONSE OF A TUNED SYSTEM

If the sweep velocity $\dot{\Omega}$ is not very small, transient effects during the resonance crossing appear. This situation is typical of the resonance crossing of rotors during run-up or run-down. The effects are (1) a shift of the amplification peak towards high frequencies for run-up and low frequencies for run-down; (2) reduction of the peak height; (3) increment of the peak width; (4) amplitude modulation after the resonance crossing due to the beating of the transient free-decaying response with the forced response (e.g. [1-5]).

The equation of motion is obtained from Eq. (18) by letting $\Delta=0$ and reads

$$\begin{bmatrix} \ddot{y}_1 \\ \ddot{y}_2 \end{bmatrix} + 2\xi \begin{bmatrix} \dot{y}_1 \\ \dot{y}_2 \end{bmatrix} + \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = 2\xi i \begin{bmatrix} e^{i\frac{1}{2}\Omega t^2} \\ 0 \end{bmatrix} \quad (22)$$

Likewise for Eq. (19), y_2 is not excited by the load and can be disregarded. Besides, it is convenient to first shift the time to the vicinity of the resonance as $t \leftarrow t - t_0$, with $t_0 = 1/\dot{\Omega}$. With this substitution, the equation of motion becomes:

$$\ddot{y}_1 + 2\xi \dot{y}_1 + y_1 = 2\xi i e^{\frac{1}{2}i\Omega t^2} e^{i\frac{1}{2}\Omega t^2} \quad (23)$$

The first exponential term in the forcing gives a constant phase change on the solution, and can be removed by introducing the variable $y_1 = Y e^{i/2\Omega t^2}$. After this substitution, the equation of motion becomes:

$$\ddot{Y} + 2\xi \dot{Y} + Y = 2\xi i e^{i/2\Omega t^2} \quad (24)$$

The small damping $\xi \ll 1$ and chirp rate $\dot{\Omega} \ll 1$ produce a slow time modulation of the solution that can be captured using a multiple scales method (see, e.g. [15-16]). To this purpose, it is necessary to formalize the relative smallness of the two parameters by letting, without loss of generality, $\xi = \varepsilon$ and $\dot{\Omega} = \kappa\varepsilon^q$ where $0 < \varepsilon \ll 1$, $\kappa \sim 1$ and $q > 0$.

$$\ddot{Y} + 2\varepsilon\dot{Y} + Y = 2\varepsilon i e^{i\tau} e^{\frac{1}{2}\kappa\varepsilon^q t^2} \quad (25)$$

The solution is expanded using two time scales $t \sim 1$ and $\tau = \varepsilon t$

$$Y = Y^0(t, \tau) + \varepsilon Y^1(t, \tau) + \dots \quad (26)$$

And, inserted into Eq. (25), equating terms with the same power of ε , gives:

$$\begin{aligned} \text{ord}(\varepsilon^0): \quad \partial_t^2 Y^0 + Y^0 &= 0 \\ \text{ord}(\varepsilon^1): \quad \partial_t^2 Y^1 + Y^1 + 2\partial_{t\tau} Y^0 + 2\partial_\tau Y^0 &= 2i e^{i\tau} e^{\frac{1}{2}\kappa\varepsilon^q t^2} \end{aligned} \quad (27)$$

The solution at the leading order is directly available and reads

$$Y^0 = A(\tau) e^{i\tau} \quad (28)$$

where the amplitude $A(\tau)$ is a function of the slow time scale and will be determined with a secularity condition. As far as the order ε^1 is concerned, it must be noted that the governing equation should not depend explicitly on the small parameter ε . It is therefore necessary to re-write the right-hand side of Eq. (27) by choosing $\varepsilon^q t^2 = t^\beta \tau^\gamma$ so that the parameter ε disappears. Substituting $\tau = \varepsilon t$ indicates that it is necessary to choose $\gamma = q$ and $\beta + \gamma = 2$, so that the governing equation at the order ε reads

$$\partial_\tau^2 Y^1 + Y^1 = -2i e^{i\tau} (\partial_\tau A + A) + 2i e^{i\tau} e^{\frac{1}{2}\kappa t^2 - q\tau^q} \quad (29)$$

To prevent the presence of secular terms, to assure that Y_1 is finite, it is necessary to force to zero the resonant terms present at the RHS. If $q \neq 2$ this condition leads to the equation

$$\partial_\tau A + A = 0 \quad (30)$$

which, with the initial condition $A \rightarrow 0$ at $\tau \rightarrow -\infty$, only admits the trivial solution $A = 0$. In order to find a non-trivial solution, it must be set $q = 2$, thus the secularity condition reads:

$$\frac{dA}{d\tau} + A = e^{\frac{1}{2}\kappa\tau^2} \quad (31)$$

The general solution of this linear problem can be written as

$$A(\tau) = C e^{-\tau} + \int_{-\infty}^{\tau} e^{\frac{1}{2}\kappa s^2 - (\tau-s)} ds \quad (32)$$

where the constant C can be set to zero to select the solution that verifies $A \rightarrow 0$ as $\tau \rightarrow -\infty$. Moreover, the Faddeeva

function [17]

$$w(z) = e^{-z^2} \left(1 + \frac{2i}{\sqrt{\pi}} \int_0^z e^{\zeta^2} d\zeta \right) \quad (33)$$

allows to finally express the envelope $A(\tau)$ in the form

$$A(\tau) = -\sqrt{\frac{\pi i}{2\kappa}} e^{-\frac{1}{2}\kappa\tau^2} w\left(\tau\sqrt{\frac{i\kappa}{2}} + \frac{1}{\sqrt{2i\kappa}}\right) \quad (34)$$

which gives a much more straightforward way to compute the response.

This result provides a method to calculate the transient response of the system, but also indicates that the right scaling for the chirp rate is obtained by choosing $\dot{\Omega} = \kappa\varepsilon^2$. This suggests that $\kappa = \dot{\Omega} / \xi^2$ is the correct parameter that should be employed to represent the chirp rate, as it was already deduced in [4] on the basis of different arguments.

Figure 2 shows the transient response of a tuned disk with $N_b = 6$, $\xi = 3 \cdot 10^{-3}$ and $\kappa = 10$. The blade response u_j and the TW coordinate y_1 are obtained by numerical integration of Eqs. (22) and (7), while the envelope A is calculated by the asymptotic solution (34). It can be observed that, likewise in the QS case, the vibration of all the blades share the same envelope, which is very well approximated by the asymptotic solution, even for the considered case with relatively high chirp rate. It can be appreciated that the maximum response amplitude is below the maximum QS response $A_{QS-tuned}$. This fact is general and can be proved analytically by multiplying Eq. (31) by A^* and adding the complex conjugate of the equation to obtain the energy equation

$$2 \frac{d|A|^2}{d\tau} + 2|A|^2 = A^* e^{\frac{1}{2}\kappa\tau^2} + A e^{-\frac{1}{2}\kappa\tau^2} \quad (35)$$

As the maximum amplitude appears for $d|A|/d\tau = 0$, therefore:

$$2|A|^2 = A^* e^{\frac{1}{2}\kappa\tau^2} + A e^{-\frac{1}{2}\kappa\tau^2} \quad (36)$$

Then, using the complex variable $B = A e^{-i\kappa\tau^2/2}$ and its real and imaginary parts $B = x + iy$, Eq. (36) simplifies to

$$x^2 + y^2 = x \quad (37)$$

which corresponds to a circumference in the complex plane with maximum distance to the origin equal to 1, and, thus

$$|A| = |B| = \sqrt{x^2 + y^2} \leq 1 \quad (38)$$

Figure 3 shows the maximum response u_j as a function of κ , calculated by numerical integration of Eq. (23) for different values of the damping ξ ranging between 10^{-3} , 10^{-2} , compared with the maximum amplitude provided by the asymptotic solution. The perfect matching of the results confirms that the asymptotic solution is accurate in a very wide range of κ and

that the system response does not depend on the $\dot{\Omega}$ and ξ separately, but only jointly through κ .

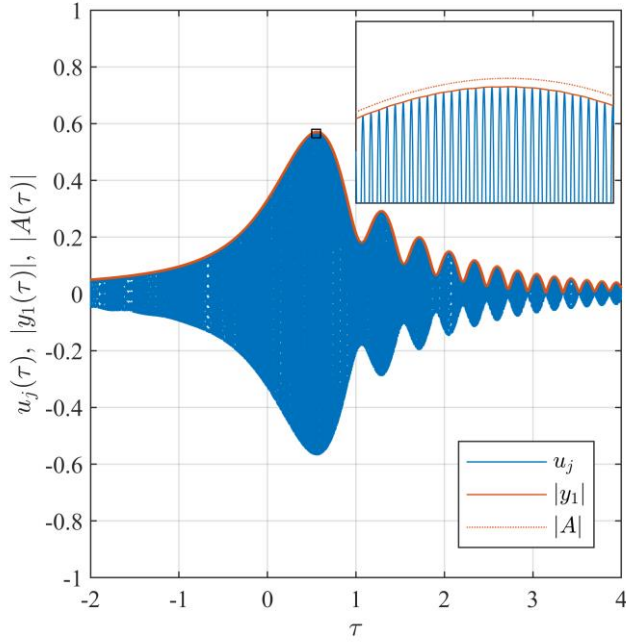


Figure 2. Transient response of a tuned system; u_j and y_1 calculated by numerical integration; A calculated by asymptotic expansion.

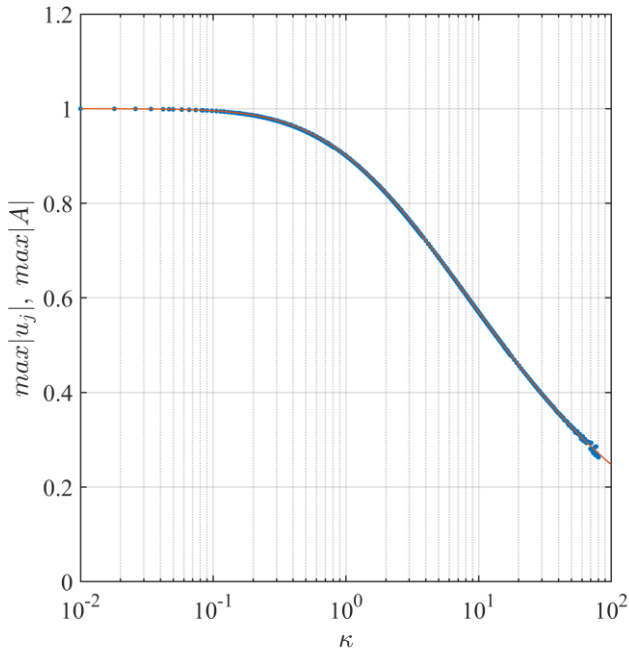


Figure 3. Maximum amplitude of vibration as a function of κ calculated by numerical integration (dots) with 8 values of ξ in the range $[10^{-3}, 10^{-2}]$ and asymptotic solution (solid line).

QUASI-STEADY RESPONSE OF A MISTUNED SYSTEM

When mistuning is present, the equations of motion in terms of TW coordinates become coupled and also y_2 , which is not directly forced, plays a role in the response. If the chirp rate is very small, the response of Eq. (18) approaches its steady-state and can be written in the form

$$\begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} A_1 \\ A_2 \end{bmatrix} e^{i\Omega t} \quad (39)$$

where $\Omega = \dot{\Omega}t$, and the amplitudes A_1 and A_2 can be obtained by manipulating the system FRF. For $\xi, \Delta \ll 1$, it yields

$$A_1 = \frac{-2\xi i(-\Omega^2 + 2i\xi\Omega + 1)}{-\Omega^4 + 4i\xi\Omega^3 + 2(1 + \Delta^2 + 2\xi^2)\Omega^2 - 4i\xi\Omega + 2\Delta^2 - 1} \quad (40)$$

$$A_2 = \frac{-4\Delta\xi i e^{-i\alpha}}{-\Omega^4 + 4i\xi\Omega^3 + 2(1 + \Delta^2 + 2\xi^2)\Omega^2 - 4i\xi\Omega + 2\Delta^2 - 1}$$

Due to the definition of the TW coordinates, the quantity $|A_1 + A_2|$ represents the vibration amplitude of the blade 0 and depends on the angle of the mistuning pattern α . Besides, the angle α also controls the relative phase angle between A_1 and A_2 , in such a way that it is always possible to select a value of α for which A_1 and A_2 are aligned in the complex plane. This condition provides the maximum of $|A_1 + A_2|$ and the envelope of the blade vibration

$$A_{qs} = \max_{\alpha} |A_1 + A_2| = |A_1| + |A_2|. \quad (41)$$

Figure 4 shows the QS response of a disk with $N_b=27$ blades, $\xi=3 \cdot 10^{-3}$, $\Delta=4.4 \cdot 10^{-3}$. The detail of the figure shows that the envelope is reached only by a few blades, while the others vibrates with a lower amplitude.

Figure 5 shows the maximum amplitude of vibration as a function of ξ and Δ . It can be noted that for $\Delta/\xi \rightarrow 0$ the maximum response tends to 1, the QS response of the tuned system. The tip of the curve is consistent with the Whitehead's limit $(1 + \sqrt{2})/2$. For small levels of mistuning the maximum response is determined only by the ratio Δ/ξ , while when $\Delta \sim \xi$ their separate influence is visible, though relatively small.

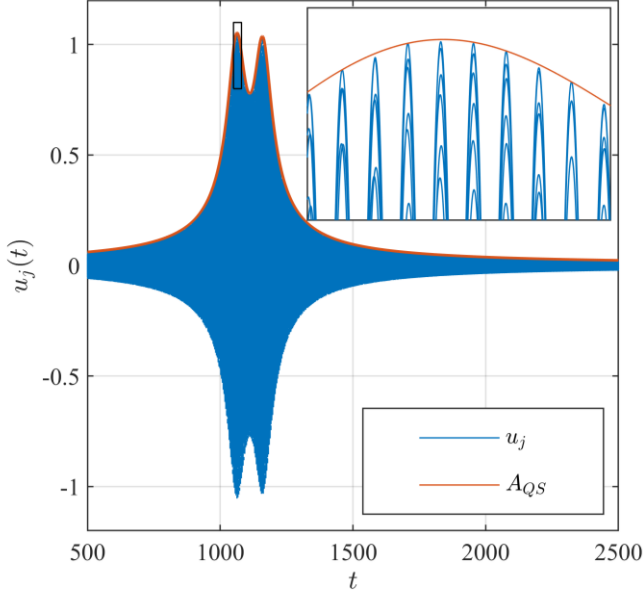


Figure 4. Quasi-steady response of a mistuned disk;
 $\xi = 3 \cdot 10^{-3}$, $\Delta = 4.4 \cdot 10^{-3}$.

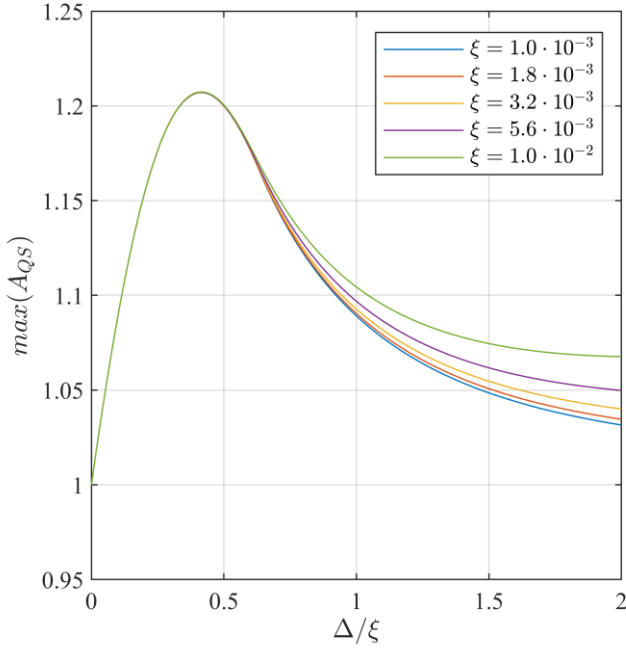


Figure 5. Maximum QS response of a mistuned disk.

TRANSIENT RESPONSE OF A MISTUNED SYSTEM

Eq. (18) contains the small parameter Δ , beside the two parameters ξ and $\tilde{\Omega}$ already discussed for the tuned case. Like in the previous section, we formalize the relative smallness of

this new parameter by setting $\Delta = m i e^{-i\alpha} \varepsilon^p$ where $|m| \sim 1$ and $p > 0$ is to be determined in order to obtain a distinguish limit. Besides, the chirp rate is set to $\tilde{\Omega} = \kappa \varepsilon^2$ according to the findings of the previous section, the time is shifted to the resonance condition $t \leftarrow t - t_0$, and the resulting constant phase is absorbed in the new variables $y_1 = Y_1 e^{i(2\tilde{\Omega})}$ and $y_2 = Y_2 e^{i(2\tilde{\Omega})}$ to obtain

$$\begin{aligned} \begin{bmatrix} \ddot{Y}_1 \\ \ddot{Y}_2 \end{bmatrix} + 2\varepsilon \begin{bmatrix} 1 & -i\varepsilon^p m \\ i\varepsilon^p m^* & 1 \end{bmatrix} \begin{bmatrix} \dot{Y}_1 \\ \dot{Y}_2 \end{bmatrix} + \\ + \begin{bmatrix} 1 + \varepsilon^{2p} |m|^2 & -2i\varepsilon m \\ 2i\varepsilon m^* & 1 + \varepsilon^{2p} |m|^2 \end{bmatrix} \begin{bmatrix} Y_1 \\ Y_2 \end{bmatrix} = 2\varepsilon i \begin{bmatrix} e^{i\tau} e^{i\frac{1}{2}\kappa\tau^2} \\ 0 \end{bmatrix} \end{aligned} \quad (42)$$

The solution is then expanded using the two time scales $t \sim 1$ and $\tau = \varepsilon t$.

$$\begin{bmatrix} Y_1 \\ Y_2 \end{bmatrix} = \begin{bmatrix} Y_1^0(t, \tau) \\ Y_2^0(t, \tau) \end{bmatrix} + \varepsilon \begin{bmatrix} Y_1^1(t, \tau) \\ Y_2^1(t, \tau) \end{bmatrix} + \dots \quad (43)$$

and inserted into Eq. (42) to obtain, equating the terms at the same power of ε :

$$\begin{aligned} \text{ord}(\varepsilon^0): \quad & \begin{bmatrix} \partial_t^2 Y_1^0 \\ \partial_t^2 Y_2^0 \end{bmatrix} + \begin{bmatrix} Y_1^0 \\ Y_2^0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \\ \text{ord}(\varepsilon^p): \quad & \begin{bmatrix} 0 & -2im \\ 2im^* & 0 \end{bmatrix} \begin{bmatrix} Y_1^0 \\ Y_2^0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \\ \text{ord}(\varepsilon^1): \quad & \begin{bmatrix} \partial_t^2 Y_1^1 \\ \partial_t^2 Y_2^1 \end{bmatrix} + \begin{bmatrix} Y_1^1 \\ Y_2^1 \end{bmatrix} + 2 \begin{bmatrix} \partial_{t\tau} Y_1^0 \\ \partial_{t\tau} Y_2^0 \end{bmatrix} + 2 \begin{bmatrix} \partial_t Y_1^0 \\ \partial_t Y_2^0 \end{bmatrix} = 2i \begin{bmatrix} e^{i\tau} e^{i\frac{1}{2}\kappa\tau^2} \\ 0 \end{bmatrix} \end{aligned} \quad (44)$$

with the following order being ε^{1+p} . Since $p > 0$, the governing equation at the leading order is the first of Eqs. (44), whose solution can be expressed as

$$\begin{bmatrix} Y_1^0 \\ Y_2^0 \end{bmatrix} = \begin{bmatrix} A_1(\tau) \\ A_2(\tau) \end{bmatrix} e^{i\tau} \quad (45)$$

The second of Eqs. (44) cannot be fulfilled unless by the trivial solution. For this reason its order ε^p , that is still to be defined, cannot be lower than ε^1 . In particular, the lowest value of p for which a non-trivial solution is possible is $p = 1$. Setting this value, the two equations in $\text{ord}(\varepsilon^p)$ and $\text{ord}(\varepsilon^1)$ combine and the next-order problem reads

$$\begin{bmatrix} \partial_t^2 Y_1^1 \\ \partial_t^2 Y_2^1 \end{bmatrix} + \begin{bmatrix} Y_1^1 \\ Y_2^1 \end{bmatrix} = 2i e^{i\tau} \left(\begin{bmatrix} e^{i\frac{1}{2}\kappa\tau^2} \\ 0 \end{bmatrix} - \begin{bmatrix} \partial_t A_1 \\ \partial_t A_2 \end{bmatrix} - \begin{bmatrix} 1 & -m \\ m^* & 1 \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \end{bmatrix} \right) \quad (46)$$

The cancellation of the terms proportional to $e^{i\tau}$ to impose the secularity condition gives the following system of equations for the slow time evolution of the amplitudes A_1 and A_2

$$\begin{bmatrix} \partial_\tau A_1 \\ \partial_\tau A_2 \end{bmatrix} + \begin{bmatrix} 1 & -m \\ m^* & 1 \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \end{bmatrix} = \begin{bmatrix} e^{\frac{i}{2}\kappa\tau^2} \\ 0 \end{bmatrix} \quad (47)$$

The solution of this linear system that verifies $A_1, A_2 \rightarrow 0$ at $\tau \rightarrow -\infty$ can be expressed in closed form using again the Faddeeva function as

$$\begin{bmatrix} A_1 \\ A_2 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 1 & 1 \\ ie^{-i\phi} & -ie^{-i\phi} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} \quad (48)$$

where

$$I_{1,2} = -\sqrt{\frac{\pi i}{2\kappa}} e^{-\frac{i}{2}\kappa\tau^2} w \left(\tau \sqrt{\frac{i\kappa}{2}} + (1 \mp i|m|) \frac{1}{\sqrt{2i\kappa}} \right) \quad (49)$$

and $m = |m|e^{i\phi}$. The displacement of the blade $j = 0$ is given by the quantity $|A_1 + A_2|$.

Figure 6 shows the transient response of a mistuned disk, as well as the analytic solution of the envelope. The blade displacement u_j and the TW coordinates are calculated by numerical integration. The envelope is obtained from the asymptotic solution, which is extremely accurate.

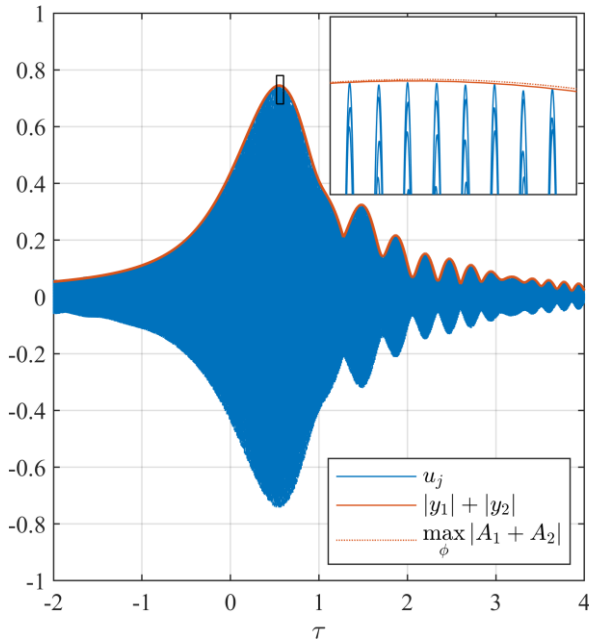


Figure 6. Transient response of a mistuned disk.

The computation of the maximum response requires to maximize the quantity

$$|A_1 + A_2| = \frac{1}{2} \left| (I_1 + I_2) + ie^{-i\phi} (I_1 - I_2) \right| \quad (50)$$

over $\tau, \kappa, |m|, \phi$. The maximization over ϕ can be easily performed as

$$A = \max_\phi |A_1 + A_2| = \frac{1}{2} |I_1 + I_2| + \frac{1}{2} |I_1 - I_2| \quad (51)$$

because the modulus of the sum of the two complex numbers $(I_1 + I_2)$ and $(I_1 - I_2)$ will reach its maximum when they are aligned. The maximization on the remaining 3 parameters $\tau, \kappa, |m|$, has been performed numerically and the results are shown in Figure 7 compared to $\max(|y_1| + |y_2|)$ computed by numerical integration of Eqs. (18) for 8 values of damping in the range $[10^{-3}, 10^{-2}]$. The maximum amplification of the transient response because of mistuning is always below the maximum mistuning amplification for the QS case (Whitehead limit), but, on the other hand, for a given chirp rate, κ -fixed, mistuning amplification with respect to the tuned transient response can be much larger than Withehead's limit.

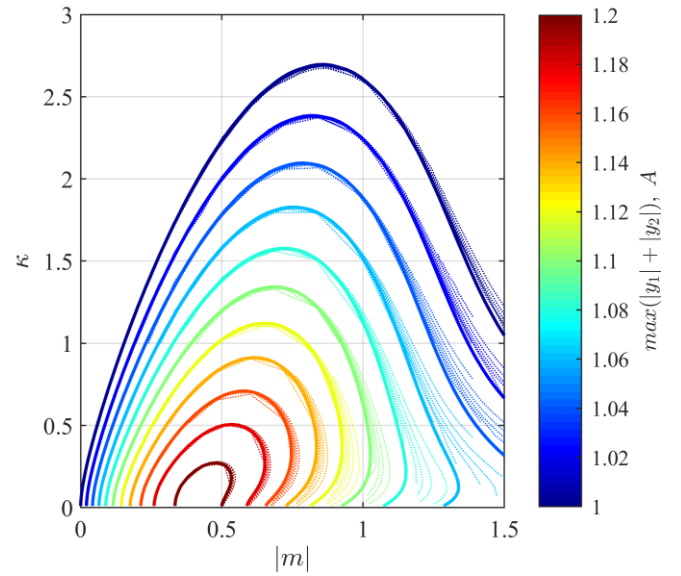


Figure 7. Maximum transient response; y_1 and y_2 are calculated by numerical integration for 8 values of $\xi \in [10^{-3}, 10^{-2}]$ (thin concour lines); A is obtained by the asymptotic solution (thick contour lines).

DISCUSSION

It has been observed that chirp rate and mistuning plays an opposite role on the response amplification in resonance crossing. Namely, while the transient effects due to a non-zero chirp rate lead to a reduction of the response, mistuning produces an increment of the amplitude. However, these two phenomena are not decoupled as the ability mistuning in over-amplifying the resonant response increases as the chirp rate increases. This circumstance can be observed in Figure 8 representing the ratio between the maximum transient response of a mistuned system (function of $|m|$ and κ) and the maximum transient response of tuned system driven with the same chirp

rate. It can be observed that the amplification due to mistuning is well above the Whitehead's limit in a very large region of the parameter space.

Figure 9 shows the ratio of the transient response of the mistuned system and its QS response. It can be observed that, in a relatively narrow region of the parameter space the ratio is above unity indicating that, for the same system, the transient response is larger than the QS response.

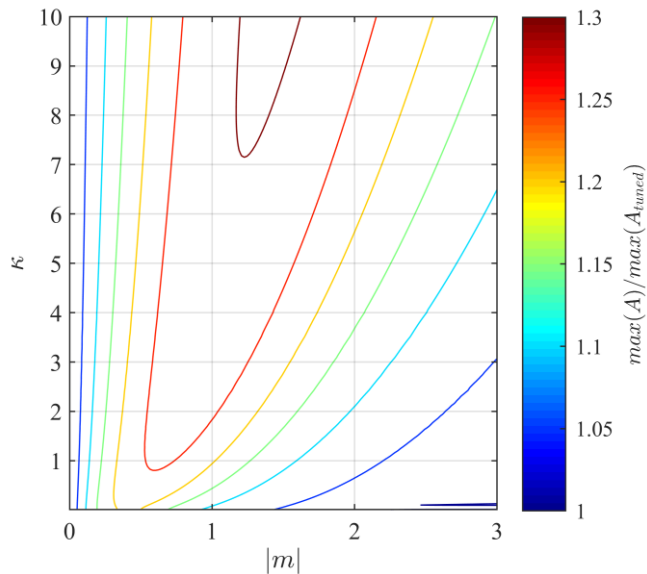


Figure 8. Transient amplification with respect to the tuned disk.

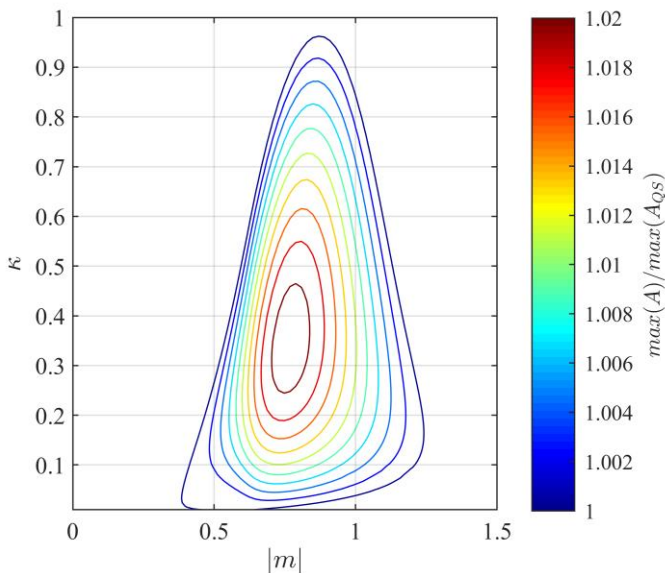


Figure 9. Transient amplification with respect to the QS response (TAMS).

CONCLUSIONS

When the vibration of a bladed disk is governed by a pair of isolated modes, the system can be represented as a 2-dof linear oscillator. For this system, we derived asymptotic solutions valid both for the tuned and the mistuned case. This result has consequences both for the quantitative and qualitative analysis of bladed disks in resonance crossing condition.

From a quantitative point of view, the asymptotic solutions enable a fast calculation of the transient response avoiding the numerical integration of the equations of motion.

From a qualitative point of view, the development demonstrated that the problem is governed by two non-dimensional parameters, namely, the reduces chirp rate $\kappa = \dot{\Omega} / \xi^2$ and the mistuning parameter $m = \Delta / \xi$. These two parameters provide a proper quantification of the importance of transient effects and mistuning, enabling the judgment and the comparison of systems under this point of view.

The asymptotic solutions, as well as the numerical simulation showed that the amplification due to mistuning is significantly more effective in transient conditions than in QS condition.

This circumstance has two consequences. First, the increment of amplitude due to mistuning should be evaluated using a transient formulation as the use of the QS increment is not on the safe side. Second, the design of mistuned disks in resonance crossing should not rely on the beneficial effects of a fast resonance crossing. In the most unfavorable case, the transient effects can even over-amplify the QS response producing an effect that is opposite to the usual one.

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