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Electromigration-induced resistance switching in indented Al microstrips

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Abstract

Non-volatile resistive memory cells are promising candidates to tremendously impact the further development of Boolean and neuromorphic computing. In particular, nanoscale memory-bit cells based on electromigration (EM)-induced resistive switching in monolithic metallic structures have been identified as an appealing and competitive alternative to achieve ultrahigh density while keeping straightforward manufacturing processes. In this work, we investigate the EM-induced resistance switching in indented Al microstrips. In order to guarantee a large switching endurance, we limited the on-to-off ratio to a minimum readable value. Two switching protocols were tested, (i) a variable current pulse amplitude adjusted to ensure a precise change of resistance, and (ii) a fixed current pulse amplitude. Both approaches exhibit an initial training period where the mean value of the device's resistance drifts in time, followed by a more stable behavior. Electron microscopy imaging of the devices show irreversible changes of the material properties from the early stages of the switching process. High and low resistance states show retention times of days and endurances of ~10³ switching cycles.

1. Introduction

The phenomenon of current-induced atomic migration, or electromigration (EM), is a widely known failure mechanism in semiconductor integrated circuits. It manifests itself as short circuits, through the development of extrusions and hillocks, or as open circuits, by the formation of voids and cracks [1]. With the years, researchers have first learnt to mitigate the wearout problem, and later on to master it. As of today, some degree of control of this inherently stochastic phenomenon has been achieved, permitting to create nanogaps for addressing nanoclusters or single molecules [2–4], locally modify the geometry or the material properties to fabricate point contacts [5–7], superconducting weak links [8–10], nanoheaters [11], plasmonic nanoantennas [12], etc. In addition, recent works also showed that the change of electrical resistance in random networks of conducting nanowires under electric bias can induce percolation in these materials, making them interesting transparent conducting materials suitable in a wide range of applications, as window electrodes, transparent heaters, antennas, etc [13, 14]. Besides this rich multipurpose nanofabrication toolbox, controlled EM benefits from the fact that it can be achieved through rather unsophisticated softwares and conventional electronics [6, 15–19].

One particularly appealing aspect that makes controlled EM to stand out, is the possibility to heal a previously electromigrated sample, by simply inverting the direction of the drive (anti-EM) [20–24]. This unique feature has naturally fostered the idea of fabricating monolithic memory devices based on switching between two resistance states. Johnson *et al* [25] introduced a two-terminal hysteretic switch (memristor [26–28]) in which the state variable of the resistance was the system's physical geometry. The case of a reversible resistance switching effect occurring across a nanogap between metal electrodes was described by Naitoh *et al* [29]. Later on, Schirm and co-authors [30] used EM to toggle the conductance of an aluminum atomic contact between two well-defined values in the range of a few conductance quanta. More recently, the concept of EM-stimulated resistance switching has been applied to cluster-assembled gold films by Minnai *et al* [31] and remains a

promising approach in current-controlled oxygen doping in YBa₂Cu₃O_{7- δ} [32, 33]. Interestingly, the threshold logic implemented by memristive devices permits to emulate synaptic actions in which the memristance of the device can be incrementally modified and a thresholding system governs the firing of the output [34, 35]. These artificial brain-inspired devices or neuromorphic systems have been the basis of the research on neural networks and their hardware implementation beyond CMOS can be achieved by using a multi-level resistance memristor leading to the programmable threshold gate.

There is however an important factor that may undermine this emerging technological niche, which is the fact that the EM/anti-EM process is not always fully reversible. Indeed, it has been shown that the degree of reversibility depends, among other things, on the toggle frequency, the choice of material, and the amplitude of resistance variations [24, 36, 37]. Even for the case of no resistance variation at all, i.e. when the system is driven at current densities much lower than the EM current, there is an inevitable thermal fatigue loading generated by the alternating current which may lead to a premature breakdown of the device [38–41].

In the present work we investigate and shed a critical light on the effects of resistance switchings in Al bridges with a predefined nanoconstriction. The memristive response arises naturally in this system in which solid-state electronic and ionic transport are coupled under an external bias voltage. Two distinct protocols are adopted to toggle between high and low resistance values. The first consists of a train of pulses of linearly increasing amplitude until achieving a resistance change not larger than ~1%, then the same approach is applied with reversed current polarity until the initial resistance value is recovered. The second method achieves the bipolar switching by alternating pulses of fixed amplitude. These cycles of EM/anti-EM are repeated about 10^3 times. Even though the final resistance of the device may remain within a few percents of the initial value, we observe that severe damage is induced at the constriction site. In situ scanning electron microscopy (SEM) imaging during the process shows that this damage appears already at early stages of the cyclic excitation. Our findings rise some concerns on the potential technological value of this kind of devices as competitive memristor candidates, particularly in the emerging electronics based on flexible substrates.

2. Experimental details

2.1. Sample fabrication

The samples are made of 25 nm thick Al films evaporated via electron-beam deposition technique onto a Si wafer with crystallographic orientation (100) and a native oxide layer on top. The wafers are p-doped and have a resistivity of 1.2 Ω cm. The Al films are patterned by conventional electron-beam lithography and lift-off procedure using a single 100 nm thick layer of PMMA 950 K resist as a mask. The final layout of the sample is shown in figure 1(a) and consists of a 8 μ m long and 1 μ m wide transport bridge with a border indentation at half length. Two types of indentation shapes have been investigated, a symmetric triangular indentation (figure 1(b)) and an asymmetric triangular indentation (figure 1(c)), both producing a constriction of 200 nm at the narrowest point along the bridge. SEM images show that the apex of the triangle has a radius smaller than 10 nm and that the Al films are polycrystalline with a log-normal grains' radius distribution maximizing at 20 nm (see supplementary material is available online at stacks.iop.org/NJP/21/113015/mmedia). Several identical samples of each type have been measured. Unless stated otherwise, all measurements are performed in ambient conditions.

2.2. Measurement protocol and criterion for EM breakdown

The samples are electrically excited by a train of $\delta t = 12$ ms long pulses and amplitude I_{max} starting at 500 μ A and increasing by steps of 200 μ A (see figure 1(d)). These pulses are intercalated by probe pulses $I_{\text{min}} = 500 \ \mu$ A delayed by 5 s from the excitation pulse. A resistance R_{max} is measured at the top of the excitation pulse starting 1 ms after the rising edge of the pulse, and a resistance R_{min} is recorded at the top of the probe pulse. A similar protocol has been used in [15, 33]. At low I_{max} values, $R_{\text{max}} \approx R_{\text{min}}$ (see figure 2). When I_{max} increases, R_{max} surpasses R_{min} as a result of Joule heating and a finite resistance temperature coefficient $\alpha \approx d(\ln R)/dT$. The EM current I_{EM} is defined as the point at which the R_{min} has changed by 0.25% of its initial value (see figure 2(b)). The train of pulses stops at the moment the increase of R_{min} has exceeded 1%. Then, the polarity of the excitation is inverted, and the same procedure is repeated.

2.3. Estimation of the local temperature at the constriction

Let us have a closer look at the current dependent R_{max} shown in figure 2(a). Since a linear increase of resistance of the device with temperature is observed (see inset in figure 2(a)), we can write $R(T) = R_{\text{bath}}[1 + \alpha(T - T_{\text{bath}})]$, where $R_{\text{bath}} = R(T_{\text{bath}})$ and T_{bath} is the temperature of the substrate.

Considering that at the stationary state the total power dissipated, $R(T)I^2$, is proportional to the induced change of the device average temperature, $T - T_{\text{bath}}$, we can write $R(T) = R_{\text{bath}}(1 + \gamma R(T)I^2)$, with γ a factor



Figure 1. (a) Scanning electron microscopy image of the transport bridge with an asymmetric constriction at its center. Zoom in showing the geometrical details of a symmetric (b) and asymmetric (c) constriction. The narrowest point along the bridge (the constriction) is 200 nm wide. (d) Schematic representation of the electrical pump-probe measurements.





depending on the thermal conductivity, specific heat, heat transfer to the substrate and sample geometry as well. From this expression, the following relation can be deduced [19]

$$R(T) = \frac{R_{\text{bath}}}{1 - \gamma R_{\text{bath}} I^2}.$$
(1)

In figure 2(a) we show R_{max} as a function of current I_{max} through the device along with the fitting (solid line) according to equation (1). This theoretical model seems to capture the overall trend of resistance increase due to Joule heating effects for currents below the onset of EM process ($I_{EM} = 11.8 \text{ mA}$ and current density $J_{EM} = 236 \text{ MA cm}^{-2}$). However, it should be noted that the resistance plotted in figure 2 results from the electrical potential difference between pads 4 μ m symmetrically away from the constriction and therefore, for a given applied current *I*, the temperature distribution is not uniform throughout the bridge. Under this circumstance, the application of equation (1), which has been deduced under the assumption of uniform temperature distribution, is uncertain. In order to properly address this problem, it is imperative to resort to numerical simulations of the coupled electric and thermal equations.

We have carried out finite element method (FEM) simulations using the commercial software COMSOL [42], using as input parameters the experimentally-determined resistance temperature coefficient $\alpha = 1.8 \times 10^3 \text{ K}^{-1}$, the thermal conductivity of the Al film [43] $k = 75 \text{ W mK}^{-1}$, specific heat [44] $C = 828 \text{ J kgK}^{-1}$ and adjusting the thermal transfer contact with the Si substrate. The FEM simulations confirm the general trend predicted by equation (1) as indicated by the solid square dots in figure 2(a). More details about the FEM simulations are presented in the supplementary material. The FEM simulations allow us to obtain the temperature distribution at the constriction during the current sweep and estimate a local increase of temperature up to ~420 K at the onset of EM. This local temperature will be even higher when the 1% increase of resistance is achieved. Considering that for Al, there is a relief of internal strain (decrease of dislocation density) when the softening temperature ~450 K is reached, it is expected that even before EM takes place, a change of material properties may occur [45]. Note that Au, previously tested in a monolithic memristive device [25], has even lower softening temperature (~390 K) than Al. Although recrystallization and grain growth in Al will develop at somewhat higher temperatures (~550 K), it has been shown that nonpassivated Al-1 at.% Si micron size lines under rapid thermal cycling induced by alternating electric current smaller than the EM current, undergo a rapid and significant growth of grains [38].

3. EM-induced resistive switching

3.1. Resistance as control variable

Figure 2(b) shows that the resistance of the proposed device can be progressively increased in a fully controllable fashion. In the case of Al (as for Pt, Au, Pd), the observed resistance increase is typically associated to a combined effect of effective reduction of cross section due to generation of voids at the constriction, and a relief of internal stress, as mentioned above. Note that an increase of resistance of 1% could be obtained by narrowing down the constriction by 15 nm (from 200 to 185 nm) whereas the experimental resistance resolution is about 8 m Ω which can be translated in a width change of about 0.4 nm.

The observed change in the material and geometric properties can, to some extent, be healed by reversing the polarity of the current, thus permitting to recover the initial resistance of the device. In other words, the associated resistive switching produced by the cycle EM/anti-EM on a single metal microstructure uses the resistance of the device as the control variable. In figure 3(a) we demonstrate that this memristive effect can be reproduced thousands of times. In this figure the color code corresponds to the polarity of the bias current. The evolution from low to high resistive state produced by direct EM corresponds to blue color, whereas the passage from high to low resistive state due to anti-EM appears in red.

After an initial training period of about ~30 cycles where the high and low resistive states drift up, the system enters a rather stable phase with high degree of predictibility. These long periods of reproducible switching are occasionally interrupted by a small resistance jump or a change of polarity (see supplementary material). The separation between the inital training and the subsequent stable regime is also seen in the time dependence of the maximum current needed to increase the resistance by 1% as shown in figure 3(b) in blue and red for positive and negative current polarity, respectively. By performing the EM process inside a SEM chamber, we are able to monitor *in situ* the evolution of the structure. Changes in the structure of the sample can be seen at as early stage as the very first half cycle. Images of the switching process consisting in void generation and void refilling have been reported previously in [24] for Al bow-tie constrictions. In that case a resistance ratio of 250% was used in order to make more apparent the change in geometry. In the present work we aim for a change of 0.25% (i.e. 1000 times smaller) which may be challenging to capture in a single hysteresis loop. In view of the fact that we are limited in the number of images during *in situ* inspection before the carbon contamination severely reduces the









contrast, we prioritize the imaging of accumulated damage after several cycles. As expected, the cumulated morphology changes occur in the vicinity of the narrowest point of the structure and take the form of voids. The functionality of a memristor as a two terminal hysteretic switch becomes more evident by combining the data in figures 3(a), (b) and plotting $\delta R_{\min}(t) = R_{\min}(t) - R_{\min}(0)$ as a function of current *I*(*t*), which is shown in figure 3(c).

The data in figure 3(b) allow us to build up the probability density function (PDF) of the EM current as shown in figure 4. The PDF exhibits a tail at high current values corresponding to the training period, and a sharp peak fingerprint of the more stable switching regime. The distribution in blue color corresponds to the current threshold needed to increase the sample resistance by 0.25% (EM process), whereas in red is the distribution of the threshold current to diminish the resistance by 0.25% (anti-EM process). The fact that the mean value (\overline{I}) of the anti-EM current distribution is shifted towards lower current values with respect to the





EM distribution could be attributed to the fact that the high resistance state corresponds to a narrower constriction and therefore needs a lower current to induce anti-EM. If this is the case, and assuming a constant density of current for EM $J_{\rm EM}$, we can deduce a change of width $\delta w \approx \delta I/J_{\rm EM}t \sim 17$ nm, which is in reasonable agreement with the 15 nm estimated from the increase in resistance.

Alternatively, the difference between the mean values of the distributions shown in figure 4, may result from concentration-gradient and stress assisted atom displacement acting in the same direction as the anti-EM current. Indeed, for the anti-EM to heal the sample, there should exist a memory effect guiding the atoms to refill the voids. Under this circumstance, the driving force produced by the gradient of vacancies concentration and stress gradient can lead to a relaxation effect which in turn limits the retention of the device. Previous investigations of damage relaxation after thermal [46] and electric [47] stress showed a relaxation time on the scale of days. In [47] it was pointed out that such decay behavior is not purely exponential, but is best described by a combination of several decay modes. We have performed several tests of the resistance decay after the devices has been set in the high resistance state. The upper inset of figure 4 shows the relative resistance change $\delta R_{\min}(t)$ corresponding to the fastest time relaxation that we have found in our devices. The same data is plotted in the lower inset of figure 4 with time in log scale, confirming a non exponential decay but rather a logarithmic decrease. The time lapse needed to reduce the excess resistance at half of its initial value (retention time) can be estimated to ~ 2 d. A logarithmic relaxation has been reported in a large diversity of physical systems [48] and has been the subject of significant theoretical work [49]. It is worth mentioning that, a healing process of electromigrated oxygen vacancies in YBa₂Cu₃O_{7- δ} films have shown a stretched-exponential functional form [50].

3.2. Switching current as control variable

Note that the standard deviation of the probability distribution shown in figure 4 is rather small, with $\sigma_I / \overline{I} \approx 3\%$. This fact suggests that the device could be driven by alternative bipolar current pulses of fixed amplitude rather than controlling the actual resistance of the device. In order to test this hypothesis, we submit a sample to high current pulses of $I = \pm 14$ mA for 'write-state', intercalated with low current amplitude pulse I = 0.5 mA for 'read-state'. Prior to these measurements, the initial value of the EM current was precisely defined following the procedure illustrated in figure 2. A clear advantage of this method with respect to the approach discussed in the previous section is the abillity to change the state with a single pulse and therefore reach higher toggle frequencies. Unfortunately, the representative results shown in figure 5 indicate a discouraging decrease of the separation between the high and low resistance state as a function of time. The reason for this behavior likely arises from the fact that the same pulse amplitude for the two opposite polarities has been used, even though the probability distribution shown in figure 4 indicates that the current needed for EM and that required for anti-EM differ by about $\delta I = 1$ mA. An initial training period of about 300 cycles is also observed in this case. Figure 6(a) shows a SEM image of the damage produced at the constriction after 2500 cycles.



Figure 6. Scanning electron microscopy images of the symmetric (a) and asymmetric (e) devices after several thousand switching cycles. The inhomogeneous current density distributions and the corresponding current crowding effects at the constrictions are shown in panels (b) and (f). The temperature distributions are shown in panels (c) and (g), whereas the temperature gradients, relevant for thermomigration effects, are depicted in panels (d) and (h).

3.3. Asymmetric structures

In 1998 Derenyi *et al* [51] theoretically predicted that the application of AC electric fields could favor the smoothing process during annealing thanks to a ratchet effect of surface EM. Some experimental evidence supporting this scenario was soon after shown by de Pablo *et al* [52] through scanning force microscopy in gold micro-stripes. More recently, lateral asymmetries in the nanostructures have shown to also produce an asymmetric EM current [53, 54] chiefly due to the resulting asymmetric temperature distribution. Motivated by these works we have compared the polarity dependence of the EM current for symmetric and asymmetric structures (see figures 1(b) and (c)), although we were unable to find a clear trend since the dispersion from one sample to another was more important that the differences observed between symmetric and asymmetric structures.

According to Black's law, the lifetime of the device is proportional to J^{-2} and depends exponentially on T^{-1} . In addition, if important temperature gradients develop, thermomigration (TM) may compete or reinforce the EM process. Figure 6 shows FEM of the temperature distribution, temperature gradient and current crowding for the symmetric (b)–(d) and asymmetric (f)–(h) constrictions for I = 10 mA. Although the current density seems to be rather insensitive to the symmetry of the constriction, the temperature landscape exhibits a clear asymmetry that could favor EM ratchet effect if TM would play an important role. The fact that we have not observed a clear ratchet signal seems to indicate that TM does not play a dominant role in our structures.

It would require a colossal experimental effort to quantify the relative importance of each mechanism due to the fact that EM, stress migration (SM), and TM are tightly interlinked. Indeed, current density increases the temperature through Joule heating and in turn, the temperature rise influences mechanical stress through differences in the expansion coefficients. In other words, the particular damage observed in the investigated sample (figure 7) cannot be attributed to a given migration type since all diffusion processes eventually lead to voids. There are, however, some indications concerning the location of the damage which could provide certain clues about the dominant mechanism at play.

Note first that for a symmetric structure, TM would lead to symmetric distribution of damage. In contrast to that, EM is driven by current and therefore the induced damage may not necessarily respect the symmetry of the structure as indeed observed. In addition, EM damage is most likely to be found in areas of high current density (current crowding effect) whereas the maximum temperature gradient should occur at about a thermal healing length (Δ) distance from that point. We estimate $\Delta \sim 0.5 \ \mu m$ in our sample. The fact that the first voids are seen exactly at the constriction seem to reinforce the idea that TM is less relevant than EM. Furthermore, it is believed that hillocks, as the ones observed in our samples, usually result from EM rather than TM.

The role of SM is more delicate to evaluate since SM is driven by mechanical stress which may be pre-existing due to deposition of Al onto SiO_2 . As temperature rises during EM, the huge difference (a factor of about 50) in thermal expansion coefficients of the metal and the insulator can result in substantial tensile stress. Even in absence of the above effects, EM will produce dislocation of metal atoms inducing mechanical stress and hence SM. The resulting SM acts in the opposite direction than EM flow and the damaging dislocation due to EM will



Figure 7. Sequence of scanning electron microscopy images of an asymmetric device during the alternating switching process. The time separation between two consecutive images corresponds to about 15 cycles high resistance-low resistance. Panel (a) shows the sample in the virgin state. In panel (b), an elongated void at the tip of the constriction is visible. In panel (c) an overgrowth of material develops at the constriction and a void appears in the internal side of the triangular constriction, where the current density is particularly weak. At later stages (d)–(h) the overgrowth increase in size at the same time that other voids develop along the lower border of the sample. The fact that the location of the voids do not coincide with the points of maximum temperature, gradient of temperature, or current density, indicates that SM is at play. The width of the bridge is 1 μ m.

be slowed down. A close inspection to the series of *in situ* images of an asymmetric device under EM/anti-EM cycles presented in figure 7 reveals the creation of voids along a border where neither current density nor temperature gradients are important. This observation leads us to conclude that SM should be invoked to understand the atomic migration in these memristive devices.

4. Conclusion

We have investigated the performance of monolithic metallic microwires with an indentation, as candidates for two-terminals resistance switching (memristors) induced by current-stimulated atomic migration. The controllability and reproducibility of the low-amplitude switching process between high and low resistance states has been tested during 10^3 cycles with a retention that is, at worst, of few days. The inconvenience of controlled resistance switching is the involved procedure and the consequent slowness. An attempt for faster switching with fixed current amplitude of alternating polarity, showed a poor performance in terms of stability and reproducibility. The fastest operation frequency is limited by the heat dissipation time constant of about 10 ns as estimated from FEM. For resistance values of \sim 35 Ω and current amplitudes \sim 15 mA, the power dissipated to switch the resistance from low to high (or viceversa) is $P = RI^2 \sim 8$ mW. Assuming that this switching can be achieved with a 10 ns pulse (lower bound imposed by the thermal evacuation time), the energy per bit amounts to 80 pJ. This is to compare with other memory devices as in [28]. For instance, USB flash drives allow reading, writing, and erasing of data, with endurance of 1 million write/erase cycles in each cell of memory. Although the concept of a memristive device based on EM seems to be viable, in order to comply with the milestones already set by competing alternative approaches, devices should be considerably scaled down. By doing so, based on geometrical considerations, one is led to conclude that less current will be needed to induce resistance switching and consequently less power consumption will be associated to this process. However, as dimension shrinks the heat evacuation towards the substrate improves and lower temperatures are achieved. Since EM is a thermally activated process, this means that the threshold current for triggering EM will not simply scale with the width of the constriction. EM at lower temperatures is highly desirable since other effects than material transport, such as crystallization or alloying, are reduced and thus healing effects obtained by reversing the current polarity may become more reversible. This would open the possibility to explore higher meltingpoint materials such as Cu. As an extra benefit of low dimensional devices we should mention the substantial

increase of the on-to-off ratio facilitating the reading process. As a last note, if the constriction width was smaller than the mean grain size (\sim 20–30 nm) the dynamics of the EM is expected to change due to the bamboo-like structure.

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