

# A simple torque magnetometer for magnetic moment measurement of large samples: application to permanent magnets and bulk superconductors

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The development of large size magnetic materials requires non-destructive measurement techniques to characterize their magnetic moment. In this work we report the design and construction of a torque magnetometer able to accommodate sizable magnetic samples ( $> 1 \text{ cm}^3$ ) both at room and cryogenic temperature. This device has an intermediate sensitivity between miniature torque magnetometers designed to work at cryogenic temperature and industrial torque meters poorly adapted to extreme conditions. We show that torque sensing in the range  $10^{-3} - 100 \text{ Nm}$  can be achieved with piezoresistive metallic strain gages cemented on a cylindrical aluminum shaft with external temperature control. An absolute calibration of the device, carried out with a coil fed by a DC current, shows that magnetic moments down to  $5 \times 10^{-3} \text{ Am}^2$  can be measured by this technique. The magnetometer is used to characterize a Nd-Fe-B permanent magnet and a permanently magnetized bulk, large grain superconductor at liquid nitrogen temperature (77 K). Results are in excellent agreement with data obtained with a flux extraction magnetometer for large samples. The device is able to measure magnetic moments in excess of  $1.5 \text{ Am}^2$ , i.e. two orders of magnitude above the maximum magnetic moment of commercial magnetometers. The sample can be inserted in the air-gap of an electromagnet to measure the decrease of magnetic moment in the presence of a transverse applied field. The device was used to characterize the magnetic moment of ‘quasi-bulk’ superconductors made of stacked coated conductor tapes (12 mm width) in such ‘crossed field’ conditions.

## I. INTRODUCTION

High temperature superconductors manufactured as bulk pellets are able to trap a significant magnetic flux density and can act as powerful permanent magnets able to generate several teslas<sup>1,2</sup>. This property makes them very attractive for various engineering applications where the best classic permanent magnets (Nd-Fe-B) are strongly limited by their saturation field. In particular bulk superconductors are used in applications involving rotating machines, portable magnets and magnetic bearings<sup>3</sup>. The typical size of a bulk superconductor is a disk of 10-50 mm in diameter and 10-20 mm in height<sup>3,4</sup> and can sometimes extend up to 100 mm in diameter<sup>5</sup>. In this context, the design of measurement systems devoted to the non-destructive magnetic characterization of such large-size superconducting samples is quite challenging. Well-established characterization methods consist in measuring the local magnetic flux distribution above the top surface of the sample using a miniature Hall probe<sup>6</sup> or magneto-optic imaging<sup>7</sup>. Such techniques can provide insights on their intrinsic physical characteristics like the critical current density but primarily in a small region located in the vicinity of the sample surface. In order to access properties that are representative of the whole volume of the sample, the determination of the magnetic moment is the most appropriate measurement because it is linked unambiguously to the critical current density<sup>8</sup>. Since magnetometers usually accommodate samples of small size ( $< 1 \text{ cm}^3$ ), however,

the standard procedure to obtain useful information on the magnetic properties of macroscopic samples consists in cutting the bulk single domain superconductors into small specimens and to characterize their magnetic properties as a function of temperature individually using AC susceptometry or DC magnetometry. This procedure is time-consuming and destructive which is particularly inconvenient. Examples of well known magnetometry techniques include Vibrating Sample Magnetometry (VSM)<sup>9-11</sup>, Alternating Gradient Magnetometry (AGM)<sup>12</sup> or Superconducting QUantum Interference Device (SQUID)<sup>13</sup>. Several efforts were made to develop AC susceptometers<sup>14,15</sup> or DC magnetometers<sup>16</sup> suited to large-size magnetic materials. These include a recent magnetometer based on a flux extraction device to measure the magnetic moment of large samples (a few  $\text{cm}^3$ ) in a non-destructive way<sup>17</sup>. In order to ensure that the electromagnetic force across the sensing coils is sensitive to the magnetic moment, however, these sensing coils should be dimensioned carefully and, in general, should be much larger than (at least twice) the sample size<sup>17,18</sup>, which becomes problematic for large geometric dimensions.

In this paper we design a torque magnetometer system working both at room and low temperature (typically at the liquid nitrogen temperature, i.e. 77 K) to measure the magnetic moment of large magnetic samples. Torque magnetometry has been widely used to characterize magnetic properties of various materials and has the key advantage that it does not require sensing coils. The working principle of torque magnetometers is rather straightforward: when an external magnetic field is applied along a non parallel direction with respect to the magnetization direction, the sample will experience a torque. This torque (called the

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magnetic torque) is given by  $\tau = \mathbf{m} \times \mu_0 \mathbf{H}$  where  $\mathbf{m}$  is the magnetic moment and  $\mathbf{H}$  is the applied external magnetic field. A non-zero torque can be measured only for hysteretic or anisotropic samples<sup>19</sup>. Typical examples include magnetic thin films, permanent magnets or superconducting materials previously magnetized under their critical temperature. It is worth mentioning that for a superconductor, the magnetization can either be already present within the material or it can be generated by the external magnetic field itself<sup>20</sup>. Several types of sensitive torque magnetometers were developed over the last decades to measure magnetic moments of metallic multilayers, high-temperature superconductors (in bulk or thin film form) and several classes of magnetic materials<sup>21</sup>. The first torque magnetometers that have been proposed are capacitive torque magnetometers<sup>22–26</sup> in which the magnetic torque produces the displacement of a moving part which is detected through a capacitance measurement. Capacitive torque magnetometers were successfully designed to measure the de Haas-van Alphen effect<sup>22</sup>, anisotropic magnetic properties<sup>23,24</sup> or the magnetic torque of very small superconducting samples ( $< 10 \mu\text{g}$ ) with a noise level of approximately  $10^{-12} \text{ Nm}^25$ . Several torque magnetometers using piezoresistive cantilevers were also designed to measure the magnetic moment of ultra low weight samples ( $\leq 1 \mu\text{g}$ )<sup>27–31</sup> achieving a sensitivity as small as  $10^{-14} \text{ Am}^2$ . This method can be applied at very high field (up to 36 T)<sup>32–35</sup> and can be used to characterize the anisotropy of superconducting crystals<sup>36</sup>. Other torque magnetometers based on different torque sensing systems have been proposed including a commercial viscosimeter<sup>37</sup>, an integrated force transducer<sup>38</sup> or optoelectronic sensors<sup>39–41</sup>. Optical detection systems present the advantage of excellent immunity against any unwanted electromagnetic interference signals. Let us mention that the early concept of torque magnetometry based on a torsion wire<sup>37,40,42–44</sup> is still a relevant technique. Usually this technique is based on capacitive or optical readout of the twist angle on a thin wire. An actuation system is then designed to deliver an opposite torque in order to fully compensate the twist angle. Finally, very recently, Takahashi *et al.*<sup>45</sup> demonstrated a new method for torque magnetometry based on a commercially available membrane-type surface stress sensor, while Blankenhorn *et al.*<sup>46</sup> constructed a torque magnetometer using an ultra-thin silicon nitride (SiN) membrane.

Together with commercial torque magnetometers<sup>47</sup>, the devices mentioned above are designed to accommodate samples of typically a few  $\text{mm}^3$ , giving rise to magnetic moments typically  $< 10^{-7} \text{ Am}^2$  and magnetic torques  $< 10^{-5} \text{ Nm}$ . In theory, torque magnetometers based on a torsion wire could possibly accommodate sizable samples<sup>42</sup>. However, in practice such devices have only been proposed for measurements of very small samples or magnetic thin films<sup>37,40,43,44</sup> and the measurement of torques exceeding  $10^{-5} \text{ Nm}$  has not been demonstrated yet. In this work, we show that commercial metallic strain gages can be used to design a robust and easy-to-use torque magnetometer system aiming at measuring torques up to  $\sim 1 \text{ Nm}$  and magnetic moment ( $0.005 <$

$m < 1.5 \text{ Am}^2$ ) of several sizable magnetic samples, both at room and cryogenic temperature. The targeted materials include permanent magnets or superconducting samples. In a magnetic torque measurement, the magnetic moment is often determined under the so-called ‘crossed’ magnetic fields regime, i.e. the sample is subjected to magnetic fields that have been applied along two orthogonal directions<sup>48</sup>. The magnetic torque generated by a superconducting sample under crossed fields can give important information on the applicability of such materials in rotating machines application, e.g. when a magnetized superconductor is placed in the rotor of a synchronous motor and subjected to the rotating field produced by the three-phase stator. In addition to providing a non-destructive characterization technique that nicely complements transport methods<sup>49–51</sup>, determining the volume magnetic properties using a torque magnetometer is therefore helpful in assessing the applicability of large size magnets for various engineering applications.

## II. DESCRIPTION OF THE EXPERIMENTAL SET UP

The torque sensing system consists of metallic strain gages (1-VY43-3/350 type from HBM) cemented on a mechanical transmission system that will be strained. The strain gages are mounted in a full Wheatstone bridge configuration in order to achieve high sensitivity, good intrinsic linearity as well as optimal temperature compensation. To measure a torque with the best accuracy, the mechanical transmission system should be designed with great care, so that the torque is transmitted at best from the sample to the gage system. Unlike what is usually done in the miniature torque meters mentioned in the introduction, the chosen geometry is not a cantilever based system but a torque transmission system based on a cylindrical shaft on which the gages are placed. A schematic illustration of the mechanical part is shown in the top part of Fig. 1. The cross-shaped top part of the shaft is designed to be clamped in an external frame (not shown in Fig. 1), allowing the sample to be possibly placed in four orthogonal positions. The bottom part consists of the sample holder subjected to the magnetic torque to be measured. The sample holder is placed in the homogeneous field zone of a water-cooled electromagnet with poles of 180 mm diameter and an air-gap of 46 mm between the poles. In the present design, the sample holder can accommodate samples up to  $17 \text{ mm} \times 18 \text{ mm} \times 8 \text{ mm}$ , a size which is currently limited by the available air gap and the wall thickness of the cryostat when low temperature measurements are carried out. By using a magnet with a larger bore or air gap, the extension to larger samples is straightforward, if needed.

Because the measurement of the torque is provided by the torsional strain of the shaft, an important point when designing the structure is to achieve the largest possible strain at the surface of the cylinder in order to obtain a measurable electric signal. For a given torsional moment, the deformation of the cylinder is inversely proportional to the shaft diameter. As a result, the diameter of the cylindrical shaft should be chosen

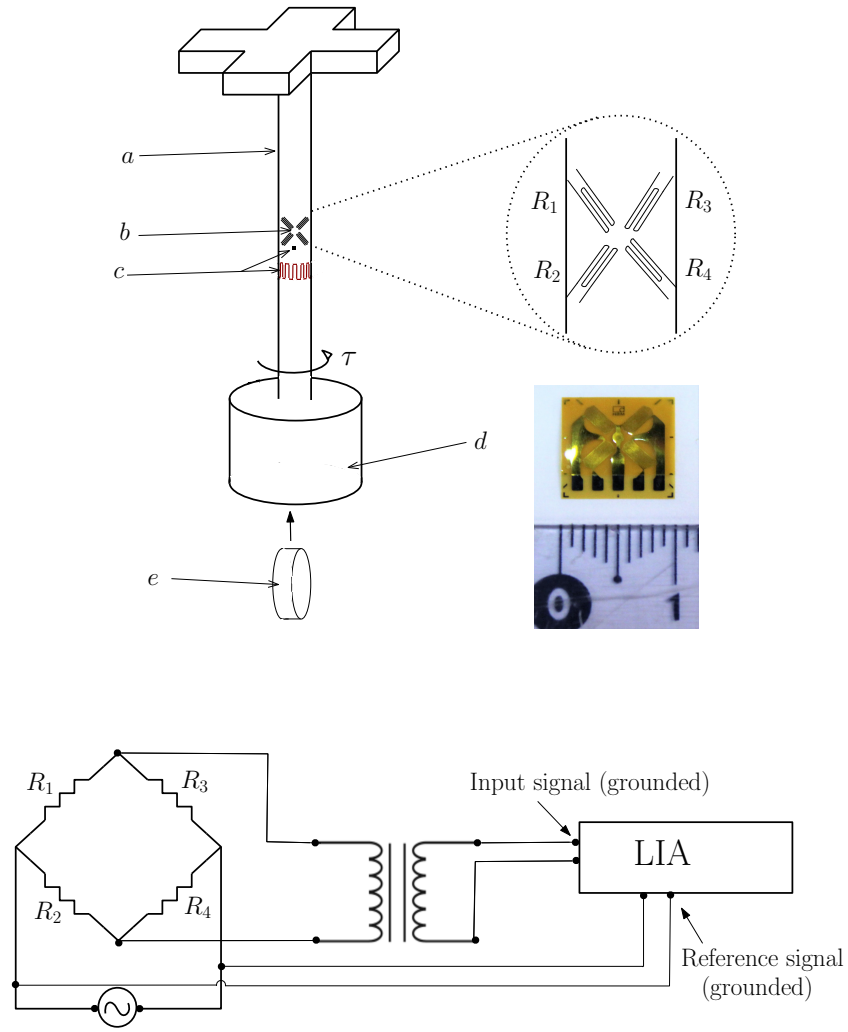


FIG. 1. Schematic representation of the torque transmission system and a picture of the full bridge mounted piezoresistive strain gages (upper part) as well as the electrical connections of the measurement system (bottom part). (a): cylindrical shaft, (b): strain gages mounted in a full bridge, (c): electrical heater and Pt100 temperature sensor, (d): sample holder, (e): magnetic sample.

as small as possible while ensuring that the gages can be attached without any difficulty. Typically, a reasonable diameter is 10 mm and is used in this work. The structure must be made of a non-ferromagnetic material with a sufficiently low stiffness. Moreover, a good temperature matching with the strain gages is required. For cryogenic full gage bridges, the commercially available configurations are temperature compensated for steel or aluminum. In the present system, aluminum (6082 AlMgSi1) is found to be well suited due to its relatively low stiffness compared to common steel, as well as the weak magnetic properties. Aluminum is paramagnetic with a room temperature magnetic susceptibility  $\chi \approx 2 \times 10^{-5}$  [-]<sup>52</sup> which is expected to have little effect on the magnetic properties of the ferromagnetic or superconducting materials to be investigated. The gage bridge used in this work is made of a constantan foil with an approximately 5  $\mu\text{m}$ -thickness. The carrier material is polyimide with a thickness of  $45 \pm 10 \mu\text{m}$  and the covering agent is also polyimide with a thickness of  $25 \pm 12 \mu\text{m}$ . The gages are already mounted on a full bridge

configuration and their nominal resistance at room temperature is 350  $\Omega$ . Gages are attached to the test material using a cold curing two components methyl methacrylate superglue, which is preferred to the usually recommended cyanoacrylate type glue due to its better mechanical behavior at low temperatures. For a full bridge placed on a cylindrical shaft at 45° from the longitudinal axis for torsion measurement, the torsional moment  $\tau$  is related to the deformation of the gages through the following relation<sup>53</sup>:

$$\tau = 2\varepsilon G S_p \quad (1)$$

where  $\varepsilon$  is the relative strain,  $G$  is the shear modulus and  $S_p$  is the polar surface modulus which depends on the cross sectional shape. For a cylindrical shaft of diameter  $d$ , one has  $S_p = \pi d^3 / 16$ . The strain gage bridge used has an operating temperature range above -70°C. For measurement of the magnetic torque of samples at cryogenic temperature, the sample holder is immersed in a small container filled with liquid nitrogen. A HK5295 electrical thermofoil heater from

MINCO and a Pt100 surface temperature sensor are both anchored thermally to the aluminum shaft and placed 13 mm below strain gage bridge (Fig. 1), so that it is maintained at a temperature of  $241.6 \pm 0.4$  K. The temperature control of the bridge is achieved through the PID feedback loop of a Model 325 LakeShore Cryotronics temperature controller. The system could possibly accommodate magnetic torque measurements at lower temperature (liquid helium temperature for instance). In this case, however, the cooling system should be modified. For instance, Patel *et al.*<sup>54</sup> used a sealed insert filled with helium gas. Then, the insert could be cooled directly with liquid helium. Strain gage bridges adapted to extreme temperature conditions should be used instead of the current gage bridge. Specific epoxy resin adhesives working down to  $-270^\circ\text{C}$  are also commercially available and could be used.

In order to increase the signal-to-noise ratio, the gage Wheatstone bridge circuit is excited by an AC voltage at a fixed frequency of 63 Hz. The bridge unbalance voltage is measured using a DSP lock-in amplifier (LIA) Model 7260 from EG&G Instruments. The bridge output signal is therefore almost unaffected by slowly-varying thermoelectric voltages occurring in the measurement circuit. The latter are reduced by thermally anchoring all junctions to the aluminum shaft and minimizing thermal gradients. The reference signal of the LIA is taken as the source signal of the Wheatstone bridge. The LIA is set in the  $X - Y$  mode where  $X$  and  $Y$  are the in-phase and the out-of-phase components of the output signal with respect to the reference. Since the voltage to be measured is related to the resistances of the circuit, the relevant signal is the in-phase signal ( $X$ ) and all out-of-phase contributions ( $Y$ ) should be ideally 0. In order to avoid ground loops, a 1:1 General Radio audio transformer is used as a galvanic isolation between the AC output voltage of the bridge and the lock-in amplifier. The electrical connections are illustrated in the bottom part of Fig. 1.

Once the full strain gage bridge is attached on the shaft and fed with an AC voltage (6.08 V RMS) without any applied torque, there is an unavoidable offset voltage of the order of  $\sim 1$  mV. This offset voltage results either from an initial mismatch between the piezoresistances of the bridge, or from a small mechanical stress caused by the cementing process. In the present case, further balancing of the bridge is achieved by connecting a precision resistor General Radio decade box, at room temperature, in parallel with one of the bridge legs. This procedure allows the zero-torque offset voltage to be decreased below  $1 \mu\text{V}$  and is performed prior to any measurement sequence.

### III. CALIBRATION

In this section, we first investigate the typical sensitivity that can be reached by the electrical measurement system and then, carry out an absolute calibration both at room and low temperature. In order to determine experimentally the sensi-

tivity of the electrical measurement system, we first balance the strain gage bridge using the procedure described above. Then we simulate a mechanical solicitation of the gages by connecting a variable General Radio precision resistor ( $R^*$ ) in parallel with one of the piezoresistive legs. In so doing, the resulting output voltage  $V$  of the bridge fed with a voltage  $V_{ac}$  is given by

$$\frac{V}{V_{ac}} \approx \frac{1}{4} \frac{\Delta R_{eq}}{R_{eq}}, \quad (2)$$

where  $R_{eq}$  is the equivalent resistance resulting from the parallel connection of the external resistor  $R^*$  and one of the piezoresistive gages. Changing  $R^*$  by small incremental amounts allows  $R_{eq}$  to be varied in a well-defined manner. Fig. 2 shows the variation of the output voltage measured by the lock-in amplifier when one of the resistances of the bridge  $R_{eq}$  varies, for three consecutive measurement runs. The theoretical result given by Eq.(2) is plotted for comparison (blue line). As can be seen in Fig. 2(b), the electrical circuit is sensitive to a relative change of one resistance of the bridge down to  $10^{-7}$ , which corresponds to detecting a  $(V/V_{ac})$  ratio of the order of  $\sim 2 \times 10^{-8}$ .

Absolute calibration of the torque measurement system can be performed using a small coil with well-defined characteristics and fed by a known current. In practice, we use a two-layered coil so that the magnetic moment can easily be computed and compared with experimental results. The reference magnetic moment of the coil is directly given by

$$m_{ref} = \pi I [R_{int}^2 n_1 + (R_{int} + d)^2 n_2], \quad (3)$$

where  $I$  is the DC current injected in the coil,  $R_{int} = 6$  mm is the radius of coil holder,  $d = 0.3$  mm is the diameter of the copper wire and  $n_1 = 18$  and  $n_2 = 17$  are respectively the number of turns of the first and the second layer. The coil is tested both at 300 K and at 77 K under an external magnetic field of 657 mT and inserted in the sample space. The orientation of the coil is such that the coil axis, and hence the direction of the magnetic moment, is perpendicular to the external magnetic field within  $0.5^\circ$  uncertainty. The resulting torque is given by  $\tau = m_{ref} B$ , where  $m_{ref}$  is the magnitude of the reference magnetic moment. The output voltage of the bridge is related to the magnetic moment through the following relation:

$$\frac{V}{V_{ac}} = \frac{8k}{\pi} \frac{B}{Gd^3} m, \quad (4)$$

and should therefore be a linear function of the injected current. Whereas Eq.(3) gives the reference magnetic moment directly calculated from the dimensions of the coil, Eq.(4) provides the value of the measured magnetic moment. Calibration is carried out by injecting increasing pulses of current of increasing amplitude, up to 2.5 A at 300 K and up to 8 A at 77 K, using a HP 6030A current source. Each pulse has a duration of 40 s, with a 20 s time interval between two pulses. The maximum current amplitude is chosen to minimize the risk of damaging the coil due to self-heating effect. Pulses duration of 40 s is used for two reasons. The first is that one has to

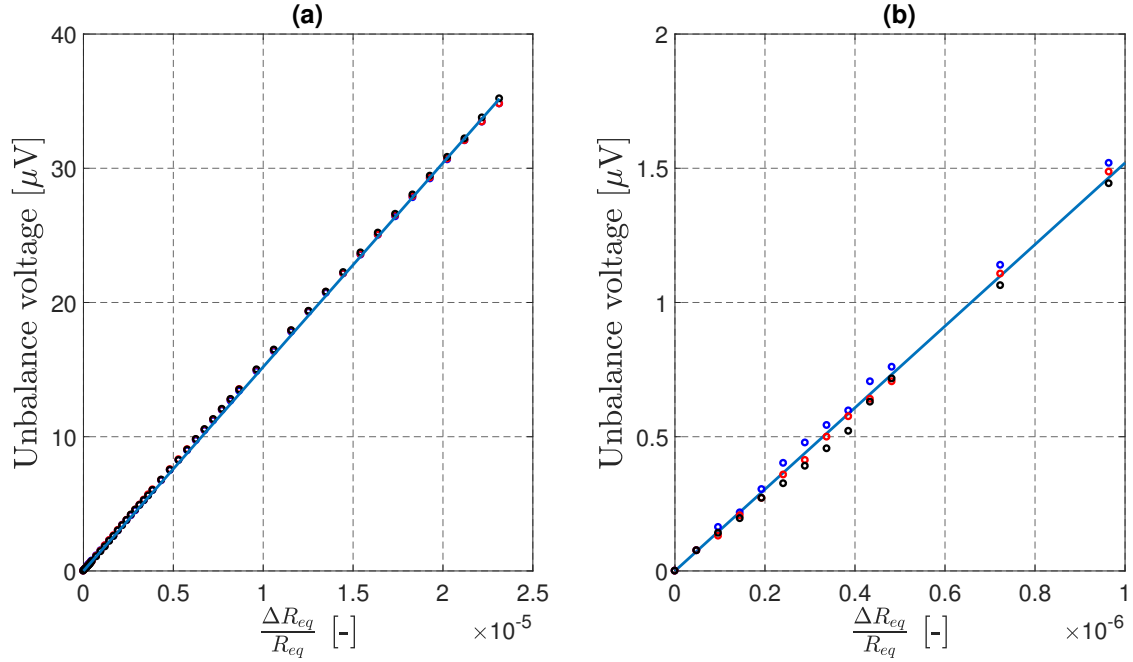


FIG. 2. (a): Unbalance voltage ( $X$ ) as a function of the relative change of equivalent resistance. (b): Zoom for small change of equivalent resistance. Three consecutive runs are shown with black, blue and red circles. The solid line is the theoretical value given by Eq.(2).

let the bridge output voltage stabilize for 20 s considering the time constant of the lock-in amplifier  $TC = 2$  s. The second reason is the offset signal that may change slightly over time. The offset signal, therefore, is recorded between two measurements and systematically subtracted from the bridge output voltage. The process of current injection and measurement recording is carried out automatically using the LabVIEW software from National Instruments. A comparison between the reference magnetic moment calculated by Eq.(3) and the measured magnetic moment deduced directly from Eq.(4) is plotted in Fig. 3. The vertical error bars represent the uncertainty on the measured magnetic moment where the main uncertainty sources come from the measured output voltage, the knowledge of the shear modulus  $G$ , and the applied transverse field. The horizontal error bars represent the uncertainty on the reference magnetic moment which results primarily from the uncertainty on the geometrical dimensions of the coil. Experimental data at room temperature are only showed up to  $0.01 \text{ Am}^2$  in Fig. 3 corresponding the injected current of  $2.5 \text{ A}$  mentioned previously. Let us mention that in principle, the torque measurements could be slightly affected by the liquid viscosity and bubbling of liquid nitrogen. Nevertheless, this effect is extremely small compared to the other uncertainty sources and will be neglected in this work. A remarkably close agreement is found between the magnetic moment determined through Eq.(4) and the reference magnetic moment, although Eq.(4) relies on the average shear modulus  $G$  determined from literature data. The data plotted in Fig. 3 show that the bridge output voltage is weakly influenced by the temperature at which calibration measurement points are taken. Possible errors that can arise from temperature variations are

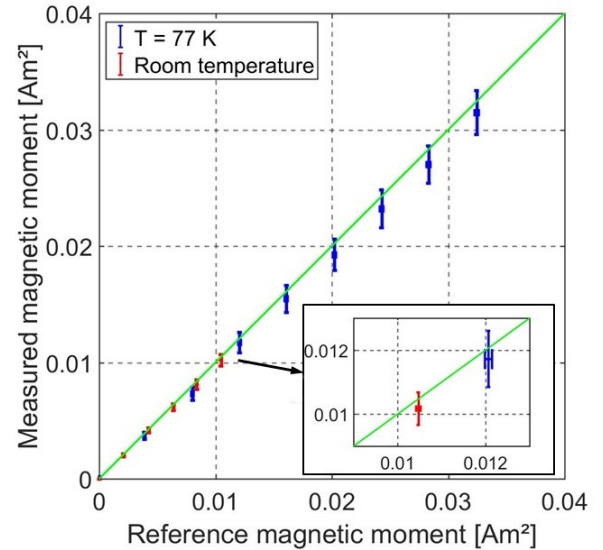


FIG. 3. Measured magnetic moment using the torque measurement system vs reference magnetic moment for each current step. The applied transverse field is  $657 \text{ mT}$ . The green line is the ideal relation. The uncertainty on the reference magnetic moment is represented by the horizontal error bars. The uncertainty on the measured magnetic moment is represented by the vertical error bars.

estimated as follows. A given temperature change affects the nominal resistances of the piezoresistors, the gage factor  $k$  and the differential thermal expansion with respect to the test ma-

terial, these effects being combined in the so-called ‘thermal output’ of the gage bridge. For the aluminum matched gage bridge used in this work, the thermal output is zero at 293 K and of the order of  $35 \mu\text{m/m}$  at 241 K (the stabilized temperature of the bridge when the sample holder is immersed in liquid nitrogen). Furthermore, the temperature itself has an impact on the output voltage for a given torque via the temperature dependence of the shear modulus  $G$ . This temperature dependence is typically  $< 0.2 \text{ } \%/^{\circ}\text{C}$  for most annealed Al alloys<sup>55</sup>. From the calibration results shown in Fig. 3, it can be concluded that the measurement system is suitable to measure reliably magnetic moments down to  $5 \times 10^{-3} \text{ Am}^2$ , both at room and at liquid nitrogen temperature. This corresponds to magnetic torques and relative strain in the range of  $\tau \sim 10^{-3} \text{ Nm}$  and  $\varepsilon \sim 10^{-7}$ , respectively. A linear fit of the calibration data shown in Fig. 3 can be used for determining the calibration constant  $K$  of the torque meter described in this work, without relying on the estimation of the shear modulus  $G$  literature data. This process yields to  $(V/V_{ac}) = K\tau$ , with  $K = (1.96 \pm 0.04) \times 10^{-4} \text{ (Nm)}^{-1}$ . This calibration value is then used for the measurements described in the next section. From this estimation one can deduce the value of the shear modulus  $G$  of the aluminum rod. From Eq.(4) and the knowledge of the calibration constant, we obtain  $G = 26.37 \pm 0.79 \text{ MPa}$ .

#### IV. RESULTS AND DISCUSSION

The torque magnetometer is used to determine the magnetic moment of three different materials: (i) a permanent magnet, (ii) a bulk superconductor and (iii) a composite ‘quasi-bulk’ superconductor made of stacked superconducting tapes.

First, the experimental system is tested on a cylindrical Nd-Fe-B permanent magnet of 15 mm in diameter and 8 mm in height. The experimental tests are carried out at room temperature and in liquid nitrogen. The sample is oriented such that its magnetization axis is perpendicular to the applied magnetic field. The experimental data can therefore be used (i) to estimate the sample initial magnetization by extrapolating the magnetic moment to zero field and (ii) to investigate how the magnetic moment is affected by the application of a transverse magnetic field, i.e. in ‘crossed-field’ conditions. The sample is submitted to increasing pulses of magnetic fields of approximately 40 s with 20 s between each pulses as described in sect. III. Fig. 4 shows the dipolar magnetic moment of the Nd-Fe-B magnet as a function of the applied magnetic field. A first observation is the fact that the magnetic moment is systematically higher at  $T = 77 \text{ K}$  than at room temperature. These data can be compared to the magnetic moment of the same magnet, measured at zero applied field using a flux extraction magnetometer developed for large samples up to 17 mm in diameter<sup>17</sup>:  $m = (1.40 \pm 0.01) \text{ Am}^2$  at 300 K and  $m = (1.47 \pm 0.01) \text{ Am}^2$  at 77 K. The magnetic moments obtained with the flux extraction magnetometer are therefore fully consistent with the results displayed in Fig. 4, and confirm the  $\sim 5\%$  increase of the magnetic moment between 300 K and 77 K. This

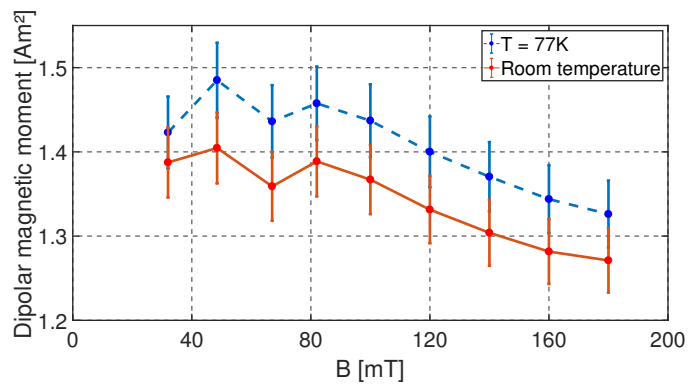


FIG. 4. Dipolar magnetic moment of the permanent magnet as a function of the applied transverse magnetic induction. The results at room temperature are compared with those at 77 K.

slight increase is in agreement with recent observations and elements of explanation about the evolution of the remnant field at low temperature in  $\text{Nd}_2\text{Fe}_{14}\text{B}$  permanent magnets that were studied by Dies-Jimenez *et al.*<sup>56</sup>. Starting from 300 K, the remnant magnetization first increases with decreasing temperature. Under a given temperature, the material experiences spin-reorientation transition and the magnetization then decreases with decreasing temperature. The spin-orientation transition is related to the fact that the easy magnetization direction, i.e. the direction which is the most energetically favorable for the magnetic moment, strongly depends on the temperature and thus, the magnetic moment can deviate from its initial orientation (up to  $30^\circ$  at 4 K). Nevertheless, the magnetic moment is always found to be higher at 77 K than it is at 300 K, in agreement with the results plotted in Fig. 4. Another direct observation from the measurement results obtained with the torque magnetometer is the overall decrease of the magnetic moment as the transverse field increases. Again, several phenomena may be responsible for the behavior of a permanent magnet under an applied transverse magnetic field. Demagnetization can happen due to a misalignment of microscopic domains when the material is submitted to a magnetic field. Because of its high coercive field, however it is not possible to demagnetize permanently the magnet at the magnetic induction levels involved in this work. Experimental data of permanent magnets in crossed fields are rather scarce. As an example, Katter<sup>57</sup> showed that in a direction perpendicular to the magnetic moment of the sample, a demagnetizing field higher than 2 T should be applied to observe irreversible demagnetization. The conclusions to be drawn from the data plotted in Fig. 4 are that (i) the torque measurement system is able to measure reliably the magnetic torque exceeding  $1 \text{ Am}^2$ , which is much higher than magnetization of the coil used in the calibration phase, (ii) the magnetization data are in agreement with those obtained using a flux extraction technique and (iii) the demagnetization effects can be studied directly. At the same time, the necessity of applying a transverse magnetic field to measure the magnetic moment of the permanent magnet is the main limitation of the technique because of the slight

demagnetization observed.

In a second experiment, the crossed-field torque measurements are carried out on a bulk, large grain  $\text{GdBa}_2\text{Cu}_3\text{O}_7$  (Gd-Ba-Cu-O) superconductor from Nippon Steel Corporation. The sample is a small cylinder of 9 mm in diameter and 5.16 mm in thickness. The torque magnetometer is used to evaluate the magnetic moment of the superconducting sample previously magnetized in a field cooled (FC) process. The sample is first placed with its easy magnetization direction (c-axis) parallel to the field direction (0.67 T) and cooled down to 77 K ( $T/T_c \approx 0.85$ )<sup>58</sup> so that a permanent magnetic moment is trapped. The holder is then rotated by 90° such that the magnetic moment is perpendicular to the applied field and can be measured by the magnetometer.

First, the magnetic moment is measured under increasing transverse magnetic field pulses. The magnetic moment as a function of the applied transverse magnetic induction is shown in Fig. 5(a). One can see a significant decrease of the magnetic moment when the applied transverse field increases. From the data plotted in Fig. 5(a), one can estimate the magnetic moment at zero applied transverse field by linear extrapolation from the three points measured at the lowest applied field. This procedure gives a magnetic moment at zero applied field equal to 0.092 Am<sup>2</sup>. This value is in very close agreement with the magnetic moment of the same sample determined using the flux extraction magnetometer developed by Egan *et al.*<sup>17</sup>, i.e.  $m = (0.089 \pm 0.01) \text{ Am}^2$ . Knowing the magnetic moment of the whole sample, the Bean model can be used to estimate the critical current density  $J_c$  if the sample is fully magnetized<sup>8,59,60</sup>. As a reminder this model ignores the flux creep and assumes a homogeneous, field-independent current density. Under these assumptions, the magnetic moment  $m$  of a cylindrical superconductor is given by<sup>60</sup>

$$m = \frac{2\pi}{3} J_c a^3 b, \quad (5)$$

where  $2a$  and  $2b$  denote the diameter and the height of the cylinder respectively.

This procedure gives an average critical current density of  $J_c \approx 2.10^4 \text{ A/cm}^2$  which is representative of the volume of the sample. Because the model does not take the flux creep into account and because the flux creep (in the absence of applied field) cannot be measured with a torque magnetometry technique, the initial magnetic moment, i.e. the moment just after the magnetization process, cannot be recovered in the scope of this work. As a result, the critical current density is likely to be underestimated. When submitted to crossed magnetic fields (i.e. magnetic fields in the  $ab$  plane after it has been magnetized in the  $c$  direction), the superconducting Gd-Ba-Cu-O sample is found to exhibit demagnetization effects. This is physically due to the creation of induced current density by the transverse field which cancels the existing current density flowing in the  $ab$  plane (induced by the magnetizing field). This results in a decrease in the current density previously induced by the magnetization

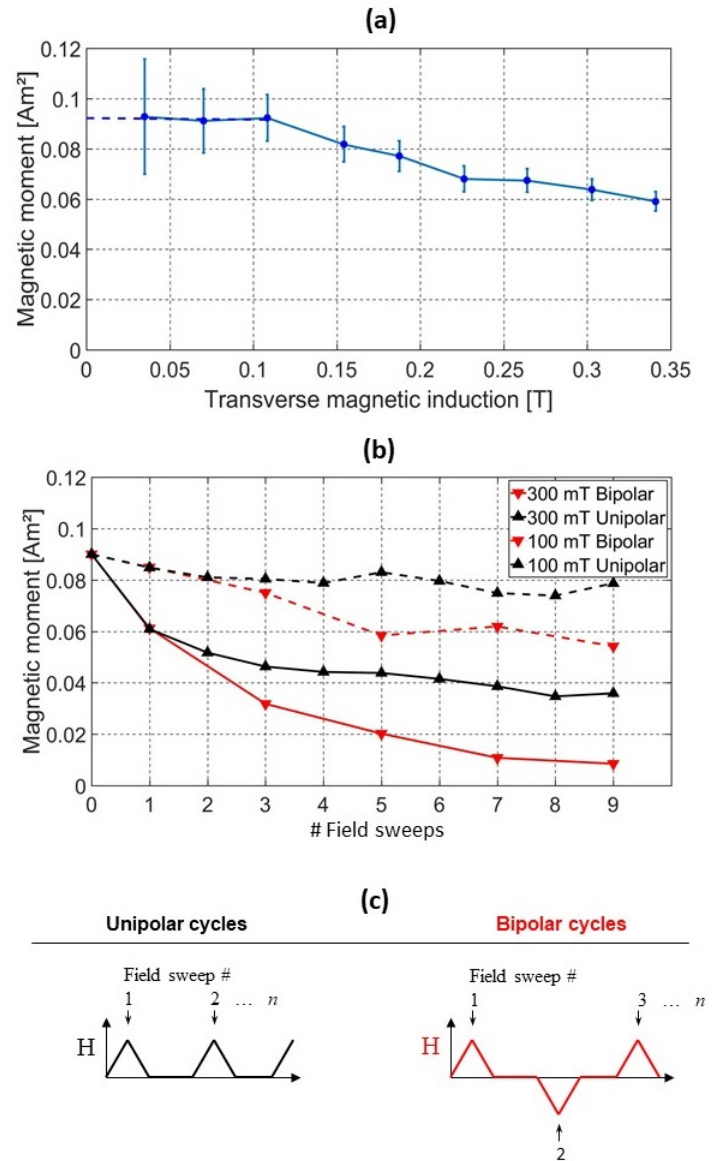


FIG. 5. Magnetic moment of the superconducting sample previously magnetized under 670 mT (FC) as a function of (a) the applied transverse magnetic field and (b) the number of field sweeps of 300 mT (6 mT/s) and 100 mT (2 mT/s). The field sweeps are illustrated in (c). The measurements are obtained 1020 s after the magnetization process.

process and thus, a decrease in the magnetization<sup>60</sup>.

The torque magnetometer developed in this work is also suited to test the crossed-field effects when the sample is submitted to triangular cycles of transverse magnetic field of larger amplitude (100 mT and 300 mT) in both bipolar and unipolar configurations. In this kind of experiments, the sample is subjected to linear increasing and decreasing variations of the applied transverse field. The measurements are then taken at each positive peak value of the applied field. Fig. 5(b) displays the magnetic moment as a function of the

number of field sweeps for the two amplitudes considered. The extrapolated value for zero applied field is also shown in this graph. Fig. 5(c) illustrates the applied transverse field as a function of time. As expected the demagnetization effect is more pronounced for an amplitude of 300 mT than for an amplitude of 100 mT. Furthermore Fig. 5(b) shows that the demagnetization is amplified by bipolar cycles. These results outline one of the key advantages of the torque magnetometer over magnetometers involving sensing coils: during the measurement, the sample can be inserted in the relatively narrow air-gap of the electromagnet, with the possibility of generating a transverse field of much higher amplitude than that ( $\sim 25$  mT) attainable in the flux extraction magnetometer with sensing coils<sup>60</sup>.

In a third set of experiments, the magnetic torque measurement system is tested on stacked second generation (2G)  $\text{YBa}_2\text{Cu}_3\text{O}_7$  (YBCO) superconducting tapes from SuperPower<sup>®</sup>. The sample consists of a stack of 42 superconducting tapes ( $12 \text{ mm} \times 12 \text{ mm}$ ) maintained together in an aluminum holder, as shown in the inset of Fig. 6(a). The tapes include a  $50 \mu\text{m}$  Hastelloy<sup>®</sup> substrate and a  $1 \mu\text{m}$  (RE)BCO superconducting layer deposited by metal-organic chemical vapor deposition (MOCVD). Such stack of tapes forms therefore a ‘quasi-bulk’ superconductor with the ability of trapping, at low temperature, high flux densities that are comparable to those of plain, bulk materials<sup>61,62</sup>. As shown by recent work demonstrating the suitability of using stacked tapes in high power density electric motors, e.g. in the next generation of electric aircrafts, understanding their behavior under crossed fields is needed to assess their long time stability and the reliability of the device<sup>63</sup>.

The stack of tapes is first magnetized permanently under 670 mT in a field cooling procedure and the magnetic moment is measured when this stack is submitted to increasing transverse fields (parallel to their  $ab$  plane) up to 300 mT. The measured magnetic moment as a function of the applied transverse field is shown in Fig. 6(a). A linear extrapolation based on the measurements at the three lowest applied fields (the dashed line) is used to find the value of the magnetic moment at zero applied field i.e.  $m \approx 0.022 \text{ Am}^2$ . Following a similar procedure than for the bulk Gd-B-C-O sample, it is possible to estimate the engineering critical current density, i.e. considering the whole stack of tapes including the substrates as one bulk superconductor. In the limit of the Bean model, the engineering critical current density estimation gives  $J_c \approx 212 \text{ A/cm}^2$ . This quite low value compared to the critical current density of the Gd-B-C-O sample can be explained by the fact that the superconducting layer in each tape is very thin compared to the substrate. The torque meter system is an efficient technique for engineering current density estimation as it gives a good estimation of the average current density on the sample volume. Using trapped field measurements could also give an estimation of the engineering current density but it would require some assumptions on the homogeneity of the sample. It would also depend on the distance between the sample and the active surface area of the Hall probe used to

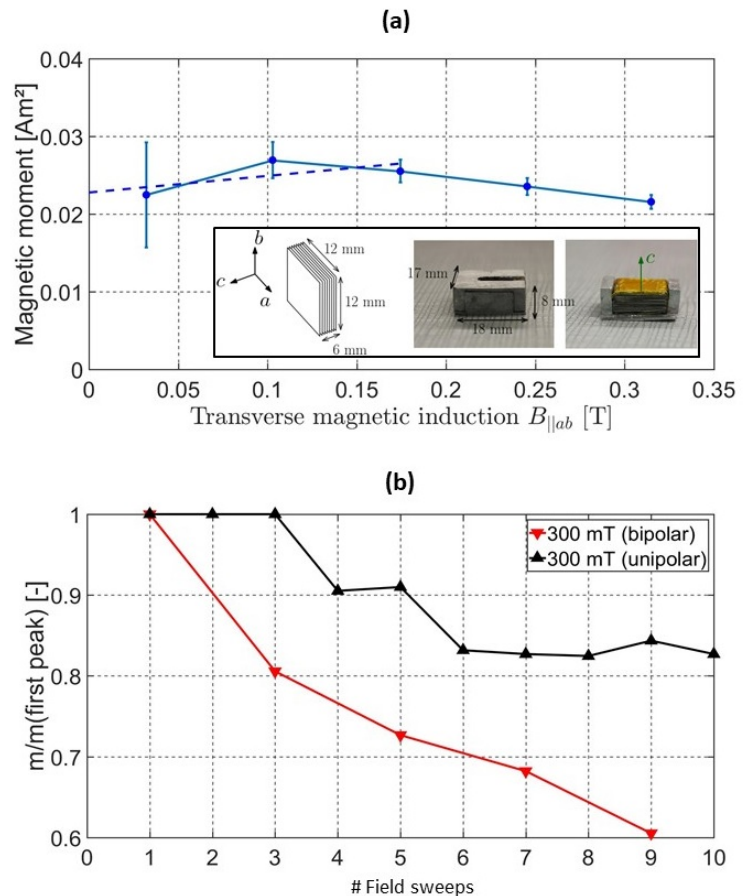


FIG. 6. Magnetic moment of the stacked tapes after a magnetization under 670 mT (FC) as a function of (a) the applied transverse magnetic field and (b) the number of field sweeps up to 300 mT (6 mT/s). The measurements are obtained 1080 s after the magnetization process. Pictures and schematic illustration of the stack are shown in the inset of (a).

perform such measurements. The results obtained for both the Gd-B-C-O bulk sample (cf. Fig. 5(a)) and the stacked tapes, show that the demagnetization is significantly reduced for the latter. In order to visualize this reduction of the demagnetizing factor, several unipolar and bipolar cycles of transverse fields are applied to the stack of tapes after a magnetization under 670 mT. Fig. 6(b) shows the magnetic moment normalized with respect to the value measured for the first peak of transverse magnetic field. Once again, results show a significant reduction of the demagnetization effect when working with stacked tapes. This result is in qualitative agreement with previous experimental data obtained by measuring the trapped flux density by one or several Hall probes attached to the surface of the sample<sup>63,64</sup>. In this latter case, however, the signal is strongly dependent of the exact distance between the Hall sensor and the surface of the stacked tape. This issue disappears for the magnetic moment obtained with the torque magnetometer in the present work since no Hall sensor is used and the useful signal depends on the average prop-



erties of the whole, quasi-bulk sample. The characterization of stacked tapes structures by the torque magnetometer could be extended directly to much larger samples (e.g. tapes of width  $> 40$  mm, once they will become commercially available) with no substantial modification of the current design.

## V. CONCLUSION

An experimental magnetic torque measurement system for the non-destructive measurement of the magnetic moment of sizable samples (up to 17 mm in diameter and 8 mm in thickness) has been designed, constructed and calibrated. The system was shown to work at both room and cryogenic (77 K) temperatures. The torque measurement system was used to measure the magnetic torque of various permanently magnetized samples under ‘crossed field’ configuration. The device consists of an aluminum cylindrical shaft of 10 mm in diameter which transmits the torque acting on the sample from the sample holder to the strain gages attached on the cylinder. In order to achieve a good sensitivity, linearity and temperature compensation, the strain gages are mounted in a full Wheatstone bridge configuration and supplied with an AC voltage at 63 Hz. It is worth mentioning that the sensing system based on piezoresistive gages is much easier to implement compared to an optical or a capacitive detection system, the latter requiring an appropriate electrostatic shield. The system has been shown to be perfectly able to detect relative changes of resistance down to  $10^{-7}$  and to measure magnetic moment down to  $5 \times 10^{-3}$  Am<sup>2</sup>, corresponding to magnetic torques in the range of  $\sim 10^{-3}$  Nm and relative strain of  $\sim 10^{-7}$ . The device was experimentally shown to be able to probe magnetic moments exceeding 1.5 Am<sup>2</sup> (1500 emu) and magnetic torques in the range of  $\sim 1$  Nm. Such magnetic moments are two orders of magnitude above the maximum magnetic moment of commercial magnetometers. The method is ultimately limited by the maximum strain of the metallic strain gages ( $\sim 10^{-2}$ ) corresponding to torques of  $\sim 10^2$  Nm and magnetic moments of a few  $\sim 10^2$  Am<sup>2</sup>. One characteristic of the system is the ability to record the magnetic moment of permanently magnetized samples when applying simultaneously a transverse field of several hundreds of mT which is necessary to characterize their demagnetization effect. The magnetic moment of a Nd-Fe-B magnet and a bulk superconducting GdBa<sub>2</sub>Cu<sub>3</sub>O<sub>7</sub> (GdBCO) sample were successfully measured. The results were shown to be in excellent agreement with experimental data obtained with a flux extraction magnetometer. Another advantage of the technique described in this work is that there is no requirement on the size of the sample and no limitation on the sample volume provided it can be inserted in the bore or air-gap of the magnet. Finally, this system allowed, for the first time, measurements of the decrease of the magnetic moment of stacked second generation (2G) YBCO superconducting tapes.

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