

# Experimental and Theoretical Radiative Lifetimes, Branching Fractions, Transition Probabilities, and Oscillator Strengths of Some Highly Excited Odd-parity Levels in Ir I

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### Abstract

Radiative lifetimes of 62 odd-parity levels of Ir I in the energy range between 32513.43 and 58625.10 cm<sup>-1</sup> were measured using the time-resolved laser-induced fluorescence technique. The lifetime values obtained are in the range from 3.2 to 345 ns. To our best knowledge, 59 results are reported for the first time. These are compared to computed data deduced from a pseudo-relativistic Hartree–Fock model including core-polarization contributions. From the combination of the experimental lifetime measurements and branching fraction calculations, a new set of transition probabilities and oscillator strengths is derived for 134 Ir I spectral lines of astrophysical interest in the wavelength region from 205 to 418 nm.

Key words: atomic data - methods: data analysis - techniques: spectroscopic

### 1. Introduction

Atomic radiative parameters such as oscillator strengths and transition probabilities are very important in astrophysics, plasma diagnostics, analytical chemistry, etc. In astrophysics, the accuracy of stellar chemical abundances largely depends on the adequacy and accuracy of atomic radiative and structure data. For neutral iridium (Ir I, Z = 77), there are two stable isotopes, <sup>191</sup>Ir and <sup>193</sup>Ir, with relative abundances of 37.3% and 62.7% on the earth and a common nuclear spin of 3/2. Its ionization limit was estimated to be 72323.9 cm<sup>-1</sup> (Colarusso et al. 1997). Ir abundances in stars are of great significance not only in radioactive cosmochronology, but also in the structure and nucleosynthetic evolution of supernovae originating from the first stellar generation (Ivarsson et al. 2003).

Ramanujam & Andersen (1978) reported the lifetimes of  $z^6D_{9/2}^{\circ}$  and  $z^6F_{7/2,11/2}^{\circ}$  levels using the beam-sputtering technique. Gough et al. (1983) derived oscillator strengths for 27 transitions in Ir I by combination of the lifetimes of 25 odd-parity levels obtained by the technique of laser-excited fluorescence from sputtered metal vapor and the branching fractions (BFs) by a hollow cathode lamp. Ivarsson et al. (2003) used the time-resolved laser-induced fluorescence (TR-LIF) technique to measure the lifetime of  $5d^76p z^6F_{11/2}^{\circ}$  (28452.32 cm<sup>-1</sup>) and derived four transition probabilities for two levels by combination with BFs from Fourier transform spectroscopic measurement. Xu et al. (2007) measured lifetimes of nine odd-parity Ir I levels and four odd-parity Ir II levels using the TR-LIF method and performed corresponding calculations.

As far as we know, the experimental lifetimes of a total of 29 levels in the energy range  $26307.49-41118.75 \text{ cm}^{-1}$  in Ir I have been published so far. However, the lifetimes of high-lying levels above  $42,000 \text{ cm}^{-1}$  are still unknown. In the present work, we measured the lifetimes for 62 Ir I levels, including 56 levels above  $42,000 \text{ cm}^{-1}$ , with the TR-LIF technique. These new data were combined with BFs obtained from pseudo-relativistic Hartree–Fock calculations, including core-polarization effects, to deduce semi-empirical transition probabilities and oscillator

strengths for 134 IrI spectral lines involving upper levels ranging from 32513.43 to 49823.54 cm<sup>-1</sup>.

### 2. Experimental Setup

The TR-LIF method for radiative lifetime measurements has been fully proven to be very reliable and has been used by many researchers over the past few years (see e.g., Ivarsson et al. 2004; Xu et al. 2007; Den Hartog et al. 2011). The experimental setup used for lifetime measurements in the present work is the same as that recently used by Tian et al. (2016), so only a brief description is given here.

A 532 nm Q-switched Nd:YAG laser with 8 ns pulse duration, 10 Hz repetition rate, and pulse energy of 5-10 mJ was used as an ablation beam to generate Ir laser plasma. A dye laser (Sirah Cobra-stretch) using DCM or Rhodamine 6G dyes, which was pumped by another Nd:YAG laser with the same performance parameters as the former, except for pulse energy, produced a tunable laser at 604-658 nm or 558-588 nm. In order to achieve excitations of higher lying levels, this dye laser needed to be converted into the second or the third harmonic lights through one or two  $\beta$ -barium borate (BBO) type-I crystals, and sometimes the converted harmonic lights were extended as different orders of Stokes and anti-Stokes components by stimulated Raman scattering in a H<sub>2</sub> gas cell. The excitation wavelength range for the levels studied in this paper is 204.404-381.832 nm. The ablation laser was focused vertically on the Ir target in the vacuum chamber, where the excitation light passed horizontally through the Ir plasma at a distance of about 8 mm above the target to excite a level of interest. The laser-induced fluorescence from an excited level was collected by a fused silica lens into a grating monochromator and detected by a photomultiplier tube (PMT, Hamamatsu R3896). A 2.5 GHz digital oscilloscope (Tektronix DPO7254) registered and averaged the transient signals from the PMT. A digital delay generator (SRS Model 535) was used to change the delay time between the excitation and ablation pulses. In this work, the lifetime measurements were performed at the delay times



**Figure 1.** Convolution fitting to a typical fluorescence decay curve of the  $52051.75 \text{ cm}^{-1}$  level of Ir I from using a excitation pulse and an exponential function.



Figure 2. Exponential fitting to a typical fluorescence decay curve of the 35540.34 cm<sup>-1</sup> level of Ir I.

from 4 to 45  $\mu$ s. In order to wipe off Zeeman quantum beats induced by the Earth's magnetic field, a 100 G produced by a pair of Helmholtz coils in horizontal direction was employed to produce high-frequency Zeeman beats, which were out of the detection range of the PMT.

#### 3. Lifetime Measurements

In the measurements, the single-step excitation scheme was employed. The target levels were populated from the ground state or some metastable states like those listed in Table 3. To ensure that only the studied level was excited, the excitation wavelength was carefully chosen from available excitation paths and monitored by a wavemeter (HighFinesse WS6). Moreover, the excited level under study was confirmed by



**Figure 3.** Comparison between the branching fractions calculated in the present work ( $BF_{calc}$ ) using the HFR+CPOL approach and the experimental values ( $BF_{exp}$ ) measured by Gough et al. (1983) and Ivarsson et al. (2003).

verifying that the observed fluorescence wavelengths were related to this level and their decay behaviors were the same.

All possible systematic effects influencing lifetime results were carefully checked, such as the radiation trapping, the collision deexcitation, and the flight-out-of-view effect. These effects can be eliminated by choosing appropriate experimental conditions through changing the excitation laser energy, the entrance slit of the monochromator and its position along the direction of atomic motion, and the delay time of the excitation pulse relative to the ablation one. More details on the elimination of systematic effects were described in our previous paper (Feng et al. 2011). In order to achieve a good signal-to-noise ratio in the time-resolved fluorescence decay curve, fluorescence signals induced by excitations of over 1000 pulses were acquired and averaged for each decay curve. For each level, more than 10 curves were registered under different experimental conditions, and the level's lifetime is the average of the lifetime values from these curves. Each curve gave two lifetime values. In an exponential fit, the two values were determined with two starting points of fit, respectively. One was a position with the intensity as strong as possible and out of the influence of stray light of the excitation laser, and the other was at half of the intensity of the former point. When using a convolutional fit, two lifetime values were evaluated by means of two excitation-pulse shapes recorded respectively before and after the fluorescence curve registration. The two lifetime values from a decay curve are in good agreement, and their mean value and its deviation from the two values were taken as the lifetime revealed by this curve and its systematic error, respectively. The uncertainty of the final lifetime result for a level is the standard deviations composited from the systematic errors and the statistical errors of different curve measurements.

From experience, when the lifetime value is shorter than 5 times the excitation-pulse width, a convolution fit to the

		Table 1				
Calculated Energy	Levels Compared	to Experimentally	Known Values	for Even	Parity in	Ir I

$\overline{E_{exp}}^{a}$	$E_{calc}^{\mathbf{b}}$	$\Delta E$	J	LS Composition <sup>b,c</sup>
$(\mathrm{cm}^{-1})$	$(\mathrm{cm}^{-1})$	$(\mathrm{cm}^{-1})$		(%)
0.00	-51	51	9/2	$80  5d^76s^2  {}^4F + 13  5d^76s^2  {}^2G$
2834.98	2833	2	9/2	94 5d <sup>8</sup> ( <sup>3</sup> F)6s <sup>4</sup> F
4078.94	4153	-74	3/2	$32  5d^76s^2  {}^{2}P + 16  5d^8({}^{3}P)6s  {}^{2}P + 13  5d^8({}^{1}D)6s  {}^{2}D$
5784.62	5842	-57	5/2	23 $5d^{8}(^{1}D)6s ^{2}D + 21 5d^{7}6s^{2} ^{4}F + 8 5d^{9} ^{2}D$
6323.91	6130	194	7/2	54 $5d^8({}^3F)6s {}^4F + 26 5d^8({}^3F)6s {}^2F$
7106.61	7055	52	7/2	79 $5d^76s^2 {}^4F + 11 5d^8 ({}^3F)6s {}^4F$
9877.54	9893	-15	5/2	$32  5d^76s^2  {}^4F + 24  5d^8({}^3F)6s  {}^4F + 19  5d^8({}^3P)6s  {}^4P$
10578.68	10697	-118	3/2	22 $5d^8({}^3F)6s {}^4F + 22 5d^76s^2 {}^4P + 19 5d^8({}^1D)6s {}^2D$
11831.09	11893	-62	3/2	53 $5d^{7}6s^{2} {}^{4}F + 19 5d^{8} ({}^{3}F)6s {}^{4}F + 10 5d^{8} ({}^{1}D)6s {}^{2}D$
12218.47	12301	-83	5/2	58 $5d^8({}^3F)6s {}^4F + 16 5d^8({}^3P)6s {}^4P + 12 5d^8({}^3F)6s {}^2F$
12505.68	12467	39	1/2	$45  5d^{7}6s^{2}  {}^{2}P + 28  5d^{8}({}^{3}P)6s  {}^{2}P + 22  5d^{7}6s^{2}  {}^{4}P$
12951.67	13071	-119	5/2	$69  5d^76s^2  {}^{4}P + 17  5d^76s^2  {}^{4}F$
13087.90	13132	-44	7/2	58 $5d^8({}^3F)6s {}^2F + 32 5d^8({}^3F)6s {}^4F$
13939.80	13900	40	9/2	$54  5d^76s^2  {}^2G + 20  5d^76s^2  {}^2H + 13  5d^76s^2  {}^4F$
16103.32	16098	5	5/2	40 $5d^8(^3P)6s \ ^4P + 5d^9 \ ^2D + 12 \ 5d^8(^3F)6s \ ^2F$
16565.35	16553	12	3/2	$60  5d^8(^3P)6s  {}^4P + 23  5d^8(^3F)6s  {}^4F$
16681.20	16693	-12	1/2	87 $5d^8(^3P)6s \ ^4P + 8 \ 5d^8(^1S)6s \ ^2S$
17779.24	17772	7	7/2	58 $5d^76s^2 {}^2G + 29 5d^8({}^1G)6s {}^2G + 6 5d^76s^2 {}^2F$
18547.04	18539	8	3/2	$34  5d^76s^2  {}^4P + 29  5d^8({}^3P)6s  {}^4P + 13  5d^8({}^3P)6s  {}^2P$
19060.62	19149	-88	5/2	43 $5d^{8}({}^{3}F)6s {}^{2}F + 30 5d^{9} {}^{2}D + 12 5d^{7}6s^{2} {}^{2}F$
19593.25	19541	53	11/2	95 5d <sup>7</sup> 6s <sup>2</sup> <sup>2</sup> H
20236.70	20135	102	1/2	$68  5d^76s^2  {}^{4}P + 20  5d^8({}^{3}P)6s  {}^{2}P$
22110.24	22028	82	3/2	25 $5d^{8}(^{1}D)6s ^{2}D + 21 5d^{9} ^{2}D + 18 5d^{8}(^{3}F)6s ^{4}F$
23310.36	23218	92	5/2	$38  5d^76s^2  {}^{2}D + 34  5d^9  {}^{2}D + 7  5d^8({}^{1}D)6s  {}^{2}D$
23505.91	23509	-3	9/2	$66  5d^8({}^1G)6s  {}^2G + 29  5d^76s^2  {}^2H$
26229.48	26252	-23	3/2	43 $5d^{7}6s^{2}$ <sup>2</sup> D + 26 $5d^{8}(^{3}P)6s$ <sup>2</sup> P + 13 $5d^{7}6s^{2}$ <sup>4</sup> F
26365.16	26330	35	7/2	63 $5d^8({}^1G)6s {}^2G + 25 5d^76s^2 {}^2G + 6 5d^8({}^3F)6s {}^2F$
26404.17	26293	111	5/2	29 $5d^{8}(^{1}D)6s \ ^{2}D + 27 \ 5d^{7}6s^{2} \ ^{2}F + 15 \ 5d^{7}6s^{2} \ ^{2}D$
27913.84	28076	-162	9/2	$46  5d^76s^2  ^2H + 28  5d^76s^2  ^2G + 20  5d^8(^1G)6s  ^2G$
27970.05	27994	-24	3/2	$56  5d^9  {}^2D + 17  5d^8 ({}^1D) 6s  {}^2D + 9  5d^7 6s^2  {}^2D$

Notes.

<sup>a</sup> From Kramida et al. (2018).

<sup>b</sup> This work.

<sup>c</sup> Only the first three eigenvector components are given, provided they are greater than or equal to 5%.

fluorescence decay curve by combining the recorded excitation pulse with an exponential function is necessary for extracting more reliable lifetime value from the decay curve (Li et al. 1999). A typical decay curve observed at 237.040 nm from the 52051.75 to 9877.54 cm<sup>-1</sup> levels and fitted by convolution of a excitation-pulse shape and an exponential with 13.5 ns decay constant is shown in Figure 1. For the decay curves of longer lifetimes, exponential fits to the portions where the exciting pulse and its stray light ceased can give accurate decay constants. A typical decay curve observed at 351.594 nm from the 35540.34 to 7106.61  $\text{cm}^{-1}$  levels fitted by an exponential function, giving rise to a lifetime value of 281 ns, is shown in Figure 2. It can be seen from Figures 1 and 2 that the fit curves are in good agreement with the measured fluorescence curves, which benefit from the latter having a good signal-to-noise ratio. The lifetime results measured in the present work are shown in Table 3.

### 4. Theoretical Calculations

The theoretical approach used in the present work for computing the radiative parameters in Ir I was the pseudorelativistic Hartree–Fork (HFR) method of Cowan (1981) modified for taking core-polarization effects into account (HFR+CPOL), as described by Quinet et al. (1999, 2002). Since we considered the same model as the one used in our previous theoretical study of the iridium atom (Xu et al. 2007), just including more transitions in the calculations, only a brief summary is provided here. Twelve evenparity and nine odd-parity configurations were explicitly included in the calculations, namely 5d<sup>7</sup>6s<sup>2</sup>, 5d<sup>7</sup>6p<sup>2</sup>, 5d<sup>7</sup>6d<sup>2</sup>,  $5d^{7}6s7s$ ,  $5d^{7}6s6d$ ,  $5d^{6}6s^{2}7s$ ,  $5d^{6}6s^{2}6d$ ,  $5d^{6}6s6p^{2}$ ,  $5d^{8}6s$ , 5d<sup>8</sup>7s, 5d<sup>8</sup>6d, 5d<sup>9</sup>, and 5d<sup>7</sup>6s6p, 5d<sup>7</sup>6s7p, 5d<sup>7</sup>6s5f, 5d<sup>7</sup>6s6f,  $5d^{6}6s^{2}6p$ ,  $5d^{8}6p$ ,  $5d^{8}7p$ ,  $5d^{8}5f$ ,  $5d^{8}6f$ , respectively. The corepolarization effects were estimated using the dipole polarizability reported by Fraga et al. (1976) for an Ir IV ionic core, i.e.,  $\alpha_d = 6.48 a_0^3$ , and a cutoff radius  $r_c = 1.60 a_0$ , corresponding to the expectation value of  $\langle r \rangle$  for the outermost core orbital (5d), as obtained with the HFR method. Moreover, a semi-empirical fitting procedure was applied to the radial parameters related to the  $5d^{7}6s^{2}$ ,  $5d^{8}6s$ ,  $5d^9$ ,  $5d^76s6p$ ,  $5d^66s^26p$ , and  $5d^86p$  configurations. The details of this semi-empirical process can be found in Xu et al. (2007). It is important to note that the energy levels

Table 2
Calculated Energy Levels Compared to Experimentally Known Values for Odd Parity in Ir I up to 50,000 cm <sup>-</sup>

$E_{exp}^{a}$	$E_{\rm calc}^{\ b}$	$\Delta E$	J	LS Composition <sup>b,c</sup>
$(\mathrm{cm}^{-1})$	$(\mathrm{cm}^{-1})$	$(cm^{-1})$		(%)
26307 50	26600	203	0/2	52 5 $d^{7}({}^{4}E)6c6n {}^{6}D + 23 5d^{7}({}^{4}E)6c6n {}^{6}E + 8 5d^{7}({}^{2}C)6c6n {}^{4}E$
20307.30	20000	-293	9/2	52 5d (F)osop D + 25 5d (F)osop F + 8 5d (G)osop F 62 5d <sup>7</sup> ( <sup>4</sup> E)6c6p $^{6}C$ + 10 5d <sup>7</sup> ( <sup>4</sup> E)6c6p $^{6}C$ + 7 5d <sup>7</sup> ( <sup>4</sup> E)6c6p $^{4}C$
20432.32	20290	102	7/2	$55 \text{ sd}$ (F) (sop F + 19 sd (F) (sop O + 7 sd (F) (sop O + 27 sd <sup>7</sup> ( <sup>4</sup> E))(sop O + 28 sd <sup>7</sup> ( <sup>4</sup> E)(sop $^{6}\text{E} + 6 sd7(^{2}\text{C}))(sop A + 28 sd7(^{4}\text{E})(sop A + 28 sd7))$
22462 59	22524	-1/3	2/2	57.5d (F)osop D + 28.5d (F)osop F + 0.5d (G)osop F 24.5d <sup>7</sup> ( <sup>2</sup> D)6c6p <sup>4</sup> D + 0.5d <sup>8</sup> ( <sup>3</sup> D)6p <sup>4</sup> D + 8.5d <sup>7</sup> ( <sup>4</sup> D)6c6p <sup>6</sup> D
32403.30	32324	-00	$\frac{3}{2}$	24 5d (F) osop F + 9 5d (F) op F + 8 5d (F) osop D 27 5d <sup>7</sup> ( $^{4}$ E) 6c6p $^{6}$ C + 22 5d <sup>7</sup> ( $^{4}$ E) 6c6p $^{6}$ E + 18 5d <sup>7</sup> ( $^{4}$ E) 6c6p $^{6}$ D
32313.43	32372	61	9/2	27 50 (F)050p O + 25 50 (F)050p F + 18 50 (F)050p D 88 $5d^{7/4}$ E)666p ${}^{6}$ C + 11 $5d^{7/2}$ C)666p ${}^{4}$ H
32830.78	32692	-01	15/2	88 50 (F)050p O + 11 50 (G)050p H 16 $5d^{7}(2D)666p$ $^{4}D$ + 12 $5d^{7}(4D)666p$ $^{6}S$ + 11 $5d^{7}(2D)666p$ $^{4}D$
22974 42	32909	90	3/2	10 50 ( P)0sop P + 15 50 ( P)0sop S + 11 50 ( P)0sop D 28 $54^{8/3}E(x, 4D) + 054^{7/4}E(x, 4D) + 8 54^{7/4}E(x, 6D)$
24190 49	24062	-80	1/2	58 50 (F)0p D + 950 (F)050p D + 8 50 (F)050p F 28 $5d^{7}(4E)6c6n^{6}C$ + 25 $5d^{7}(4E)6c6n^{6}E$ + 22 $5d^{7}(4E)6c6n^{4}C$
34100.40 24010.92	34003	20	5/2	28 5d (F)0sop G + 25 5d (F)0sop F + 25 5d (F)0sop G 45 $5d^{7}(4E)C_{0}C_{0} = \frac{12}{5} 5d^{7}(4E)C_{0}C_{0} = \frac{6}{5}$
34919.85	34939	-39	5/2	45 5d (F)0sop F + 12 5d (F)0sop D 16 $54^{8/3}$ EVG $^{4}$ E + 14 $54^{7/4}$ EVG (G $^{4}$ E + 0.5 $4^{7/4}$ E)G (G $^{6}$ E
35080.80	35031	50	9/2	10 5d (F)op F + 14 5d (F)osop F + 9 5d (F)osop F 21.5174 F ( $60 + 14.5174$ F) ( $67 + 11.5174$ F) ( $67$
35410.05	25(00	220	1/2 5/2	21 Su (F) OSOP U + 14 Su (F) OSOP F + 11 Su (F) OSOP D 22 $54^{7}(4p)(-(p^{6}Q) + 15 54^{7}(4p)(-(p^{6}Q) + 10 54^{7}(4p)(-(p^{6}Q) + 10 54^{7}))$
35540.54	35600	-60	5/2	25 5d (P)0sop S + 15 5d (P)0sop D + 10 5d (P)0sop D 20 $54^{7/2}$ P)(-(- $4^{9}$ P) + 20 $54^{7/4}$ P)(-(- $6^{6}$ P) + 10 $54^{7/2}$ P)(-(- $4^{9}$ P)
35647.94	35629	19	1/2	20 Sd (P)osop P + 20 Sd (F)osop F + 10 Sd (D)osop D 51 $547(4E)(-(E + 7.547(2D))(-(E + 4D) + 5.547(4E))(-(E + 4D))$
30390.15	30430	-46	3/2	51 5d (F)osop F + / 5d (D)osop D + 5 5d (F)osop D 20.517(4T) ( $6C + 10.517(4T)$ ( $6T + 0.517(4T)$ ( $6T$ )
3/446.13	37408	38	5/2	$38 \text{ 5d}^{-}(\text{ F})\text{6sop }^{*}\text{G} + 19 \text{ 5d}^{-}(\text{ P})\text{6sop }^{*}\text{S} + 9 \text{ 5d}^{-}(\text{ F})\text{6sop }^{*}\text{D}$
3/515.31	3/516	-1	1/2	$1/5d^{-}(17)6sop^{-3}G + 15.5d^{-}(17)6sop^{-3}D + 12.5d^{-}(17)6sop^{-3}D$
37692.75	37580	113	3/2	25 5d (F) 050p 'G + 13 5d (P) 050p 'D + 12 5d (D) 050p 'F
3/8/1.69	3/838	34	9/2	21 $5d^{2}(F)$ 5p $F + 21 5d^{2}(F)$ 5s 5p $F + 18 5d^{2}(F)$ 5s 5p $F$
38120.94	38082	39	1/2	$35 \text{ Sd}^{-}(\mathbf{F})6\text{s6p}^{-}\mathbf{F} + 8 \text{ Sd}^{-}(\mathbf{F})6\text{s6p}^{-}\mathbf{P} + 7 \text{ Sd}^{-}(\mathbf{F})6\text{s6p}^{-}\mathbf{D}$
38158.24	38182	-24	7/2	$1/5d^{2}(F)6s6p^{2}G + 14.5d^{2}(F)6s6p^{2}F + 9.5d^{2}(D)6s^{2}6p^{2}D$
38229.75	38255	-25	9/2	29 $5d^{\circ}(^{\circ}F)bp^{\circ}G + 19 5d^{\circ}(^{\circ}F)bp^{\circ}G + 15 5d^{\circ}(^{\circ}F)bsbp^{\circ}G$
38358.13	38370	-12	5/2	$22 \text{ Sd}^{-}(\mathbf{P})6\text{ Sb}^{-}\text{S} + 10 \text{ Sd}^{-}(\mathbf{F})6\text{ p} \cdot \mathbf{D} + 10 \text{ Sd}^{-}(\mathbf{P})6\text{ sb}^{-}\text{G}$
38484.74	38582	-97	3/2	$32 \text{ 5d}^{-}(\text{ F})656p ^{\circ}\text{D} + 18 \text{ 5d}^{-}(\text{ F})656p ^{\circ}\text{D} + 16 \text{ 5d}^{-}(\text{ F})656p ^{\circ}\text{G}$
38568.05	38537	31	7/2	$13 \text{ 5d}'(\text{F})6\text{s6p }^{\circ}\text{D} + 10 \text{ 5d}'(\text{F})6\text{s6p }^{\circ}\text{D} + 9 \text{ 5d}'(\text{F})6\text{s6p }^{\circ}\text{F}$
39289.28	39384	-95	1/2	$15 \text{ Sd}^{7}(^{7}\text{F})6\text{s6p} ^{\circ}\text{D} + 15 \text{ Sd}^{7}(^{7}\text{P})6\text{s6p} ^{\circ}\text{D} + 10 \text{ Sd}^{6}(^{7}\text{D})6\text{p} ^{\circ}\text{P}$
39324.57	39312	13	5/2	$\frac{11}{50} \frac{50}{(7)} \frac{50}{50} \frac{50}{50} + \frac{9}{50} \frac{50}{(10)} \frac{50}{50} \frac{27}{7} + \frac{8}{50} \frac{50}{(7)} \frac{50}{50} \frac{50}{50}$
39805.97	39864	-58	5/2	$165d^{\circ}({}^{\circ}F)6p^{\circ}D + 85d^{\circ}({}^{\circ}P)6s6p^{\circ}P + 55d^{\circ}({}^{\circ}F)6s6p^{\circ}F$
39940.27	39821	119	11/2	$36 5d^{\circ}({}^{\circ}F)6p {}^{\circ}G + 29 5d^{\circ}({}^{\circ}F)6s6p {}^{\circ}G + 18 5d^{\circ}({}^{\circ}F)6s6p {}^{\circ}G$
40291.19	40343	-52	7/2	$15 5d^{\circ}({}^{\circ}F)6p {}^{\circ}F + 13 5d^{\circ}({}^{\circ}F)6p {}^{\circ}F$
40389.83	40270	120	9/2	$22 \text{ 5d}'(\text{TF})6\text{s6p} ^{\circ}\text{G} + 18 \text{ 5d}'(\text{TF})6\text{s6p} ^{\circ}\text{F}$
40524.73	40640	-115	3/2	23 $5d^{2}(F)6s6p^{2}G + 11 5d^{2}(P)6s6p^{2}D + 9 5d^{2}(D)6s^{2}6p^{2}D$
40710.78	40766	-55	7/2	$27 \text{ Sd}^{-}(\text{TP})6866 \text{ s}^{-}\text{D} + 14 \text{ Sd}^{-}(\text{SD})68^{-}66 \text{ s}^{-}\text{D}$
41118.71	41076	43	9/2	$27 \text{ Sd}^{\circ}(2\text{ D})6\text{s}^{2}6\text{p}^{\circ}\text{D} + 25 \text{ Sd}^{\circ}(2\text{ P})6\text{s6p}^{\circ}\text{D} + 6 \text{ Sd}^{\circ}(2\text{ P})6\text{s6p}^{\circ}\text{F}$
41210.33	41217	-7	1/2	$32 \text{ 5d}'(\text{F})6\text{s6p }^{\circ}\text{D} + 21 \text{ 5d}'(\text{D})6\text{s}^{\circ}\text{6p }^{\circ}\text{D} + 8 \text{ 5d}'(\text{P})6\text{s6p }^{\circ}\text{D}$
41522.22	41640	-118	5/2	$175d^{2}(^{2}P)6s6p^{9}D + 115d^{2}(^{2}D)6s^{2}6p^{9}D + 85d^{9}(^{2}F)6p^{9}D$
42014.44	42099	-85	1/2	$29 \text{ Sd}'(^2\text{P})6\text{s6p }^2\text{D} + 16 \text{ Sd}'(^2\text{P})6\text{p }^2\text{D} + 9 \text{ Sd}'(^2\text{P})6\text{s6p }^2\text{P}$
42029.14	41896	133	3/2	$14 5d^{\circ}(^{\circ}D)6p ^{\circ}D + 9 5d^{\circ}(^{\circ}F)6s6p ^{\circ}F + 7 5d^{\circ}(^{\circ}D)6s6p ^{\circ}D$
42131.82	42279	-147	11/2	$36 5d^{\circ}({}^{\circ}F)6p {}^{\circ}G + 20 5d'({}^{\circ}F)6s6p {}^{\circ}G$
42267.86	42382	-114	5/2	14 5d°( $^{\circ}$ D)6s <sup>2</sup> 6p $^{\circ}$ D + 11 5d′( $^{\circ}$ F)6s6p $^{\circ}$ F + 7 5d′( $^{\circ}$ P)6s6p $^{\circ}$ D
42279.28	42068	211	9/2	$15 5d^{\circ}(^{\circ}D)6s^{\circ}6p^{\circ}D + 14 5d^{\circ}(^{\circ}F)6s6p^{\circ}F$
43071.78	43021	51	5/2	$85d^{\circ}(^{\circ}F)6p^{\circ}G + 85d^{\circ}(^{\circ}F)6p^{\circ}F + 65d^{\circ}(^{\circ}F)6p^{\circ}D$
43176.15	42973	203	7/2	20 5d°( <sup>3</sup> F)6p <sup>4</sup> G + 8 5d′( <sup>2</sup> F)6s6p <sup>4</sup> G + 7 5d′( <sup>4</sup> F)6s6p <sup>4</sup> G
43200.89	43160	41	3/2	$13 5d^{\circ}({}^{3}F)6p^{+}D + 12 5d'({}^{4}F)6s6p^{+}D + 10 5d'({}^{4}F)6s6p^{+}F$
43592.21	43487	105	7/2	$\frac{19}{50} \frac{50}{(4P)656p} \frac{6P}{P} + \frac{17}{50} \frac{50}{(5D)65} \frac{6P}{P} + \frac{14}{50} \frac{50}{(4P)656p} \frac{6D}{D}$
44569.85	44474	96	3/2	$12 \text{ Sd}'(\text{P})6\text{s6p }^{\circ}\text{D} + 8 \text{ Sd}'(\text{P})6\text{s6p }^{\circ}\text{S}$
44596.77	44567	30	5/2	$14 5d'(^{2}P)6s6p ^{6}P + 12 5d'(^{3}F)6p ^{4}F + 8 5d'(^{2}P)6s6p ^{4}D$
44642.67	44883	-240	7/2	$15  \text{5d}^{7}(\text{*F})6\text{s6p}  \text{*D} + 13  \text{5d}^{6}(\text{*D})6\text{s}^{2}6\text{p}  \text{*D} + 10  \text{5d}^{7}(\text{*G})6\text{s6p}  \text{*G}$
44652.43	44734	-82	9/2	21 5d'( $^{\text{F}}$ )6s6p $^{\text{G}}$ + 8 5d'( $^{\text{C}}$ )6s6p $^{\text{2}}$ H + 7 5d'( $^{\text{F}}$ )6s6p $^{\text{O}}$ D
44785.44	44782	3	3/2	$16  5d'({}^{\circ}P)6s6p  {}^{\circ}D + 9  5d'({}^{\circ}D)6s^{2}6p  {}^{\circ}D + 8  5d'({}^{\circ}P)6s6p  {}^{\circ}P$
45111.68	45400	-288	7/2	13 5d'('F)6s6p 'G + 12 5d'('F)6s6p 'G + 11 5d'('F)6p 'G
45185.95	45210	-24	5/2	15 5d°(3F)6p $^{+}D$ + 10 5d'(3F)6s6p $^{+}D$ + 6 5d°(3F)6p $^{2}F$
45259.14	45186	73	3/2	13 5d'("P)6s6p "P + 12 5d"("F)6p "F + 8 5d'("F)6s6p "F
45415.26	45392	23	1/2	13 5d'("P)6s6p "D + 12 5d"("F)6p "D 12 5d"("F)6p = 2772
45503.15	45760	-256	1/2	11 $5d'({}^{4}P)6s6p {}^{6}D + 8 5d'({}^{2}P)6s6p {}^{2}S + 6 5d^{8}({}^{3}P)6p {}^{4}P$
45570.89	45638	-67	5/2	11 $5d'({}^{4}F)6s6p {}^{4}G + 9 5d'({}^{4}F)6s6p {}^{2}D$
45895.85	46030	-134	7/2	28 5d°( $^{3}F$ )6p $^{4}F$ + 12 5d′( $^{4}F$ )6s6p $^{4}F$ + 10 5d′( $^{4}F$ )6s6p $^{2}F$
45957.33	45502	455	11/2	$34  5d'({}^{2}G)6s6p  {}^{4}H + 20  5d'({}^{2}H)6s6p  {}^{4}I + 12  5d'({}^{2}G)6s6p  {}^{4}G$
46093.84	46259	-165	5/2	13 $5d'({}^{4}F)6s6p {}^{4}G + 8 5d'({}^{4}F)6s6p {}^{4}G + 7 5d'({}^{4}F)6s6p {}^{2}D$
46220.32	46011	209	9/2	19 5d'( ${}^{4}$ F)6s6p ${}^{4}$ F + 11 5d'( ${}^{2}$ G)6s6p ${}^{4}$ H + 11 5d ${}^{6}$ ( ${}^{5}$ D)6s ${}^{2}$ 6p ${}^{4}$ F

			(Continued)	
$\overline{E_{\exp}^{a}}_{(\mathrm{cm}^{-1})}$	$E_{ m calc}^{\ \ b}_{( m cm^{-1})}$	$\Delta E \over (\mathrm{cm}^{-1})$	J	LS Composition <sup>b,c</sup> (%)
46371.64	46371	1	9/2	$335d^7(^4P)6s6p^6D+125d^7(^4F)6s6p^4G+105d^7(^2G)6s6p^4F$
46471.84	46433	39	3/2	14 $5d^{7}(^{2}P)6s6p \ ^{2}D + 12 \ 5d^{7}(^{4}P)6s6p \ ^{4}D + 9 \ 5d^{7}(^{4}P)6s6p \ ^{4}S$
46618.13	46696	-78	3/2	19 $5d^8({}^3F)6p {}^4D + 9 5d^7({}^4F)6s6p^4F + 7 5d^7({}^4F)6s6p {}^4D$
46979.02	46984	-5	7/2	11 $5d^{6}({}^{5}D)6s^{2}6p {}^{4}D + 9 5d^{8}({}^{3}F)6p {}^{2}G + 9 5d^{8}({}^{3}F)6p {}^{4}F$
47011.09	47005	6	5/2	15 $5d^8(^3F)6p \ ^4G + 11 \ 5d^7(^2F)6s6p \ ^4G + 5 \ 5d^7(^2H)6s6p \ ^4G$
47165.12	47349	-184	7/2	13 $5d^{6}(^{5}D)6s^{2}6p \ ^{6}F + 10 \ 5d^{7}(^{4}P)6s6p \ ^{4}D + 6 \ 5d^{8}(^{1}D)6p \ ^{2}F$
47203.81	47141	63	1/2	23 $5d^{6}(^{5}D)6s^{2}6p \ ^{6}D + 18 \ 5d^{7}(^{4}P)6s6p \ ^{6}D + 16 \ 5d^{7}(^{2}P)6s6p \ ^{2}S$
47205.57	46930	276	9/2	21 $5d^{7}({}^{4}F)6s6p {}^{2}G + 8 5d^{7}({}^{2}H)6s6p {}^{4}I + 8 5d^{7}({}^{2}G)6s6p {}^{4}F$
47537.29	47608	-71	5/2	14 5d <sup>6</sup> ( <sup>5</sup> D)6s <sup>2</sup> 6p <sup>6</sup> F + 9 5d <sup>6</sup> ( <sup>5</sup> D)6s <sup>2</sup> 6p <sup>6</sup> D
47548.69	47685	-136	7/2	9 $5d^{7}(^{4}F)6s6p \ ^{4}F + 7 \ 5d^{7}(^{4}P)6s6p \ ^{6}P + 5 \ 5d^{7}(^{4}F)6s6p \ ^{4}D$
47824.93	47744	81	3/2	9 $5d^{7}(^{4}P)6s6p \ ^{4}S + 9 \ 5d^{6}(^{5}D)6s^{2}6p \ ^{6}D$
47858.47	47889	-31	11/2	47 $5d^{6}(^{5}D)6s^{2}6p \ ^{6}F + 17 \ 5d^{7}(^{4}F)6s6p \ ^{4}G + 9 \ 5d^{6}(^{3}F)6s^{2}6p \ ^{4}G$
48206.57	48468	-261	5/2	9 $5d^{7}(^{4}F)6s6p \ ^{4}F + 7 \ 5d^{8}(^{3}P)6p \ ^{4}P + 6 \ 5d^{7}(^{4}P)6s6p \ ^{6}D$
48299.24	48147	152	9/2	23 $5d^{8}({}^{3}F)6p^{4}G + 9 5d^{7}({}^{2}F)6s6p {}^{4}G + 8 5d^{8}({}^{3}F)6p {}^{2}G$
48440.83	48440	1	3/2	14 $5d^{6}(^{5}D)6s^{2}6p \ ^{6}F + 9 \ 5d^{6}(^{5}D)6s^{2}6p \ ^{6}D + 8 \ 5d^{7}(^{4}F)6s6p \ ^{2}D$
48448.65	48598	-149	7/2	39 $5d^{7}(^{2}G)6s6p \ ^{4}H + 6 \ 5d^{7}(^{4}F)6s6p \ ^{2}F + 5 \ 5d^{8}(^{3}F)6p \ ^{4}G$
48629.22	48690	-61	7/2	$17  5d^{7}({}^{4}F)6s6p  {}^{4}D + 13  5d^{6}({}^{5}D)6s^{2}6p  {}^{6}F + 7  5d^{6}({}^{5}D)6s^{2}6p  {}^{4}D$
48801.91	49027	-225	3/2	9 $5d^{7}(^{4}F)6s6p \ ^{4}F + 8 \ 5d^{8}(^{3}F)6p \ ^{4}F + 7 \ 5d^{7}(^{4}F)6s6p \ ^{4}D$
49146.44	49234	-88	5/2	11 $5d^{7}(^{4}P)6s6p \ ^{6}P + 8 \ 5d^{7}(^{4}F)6s6p \ ^{4}D + 9 \ 5d^{7}(^{4}F)6s6p \ ^{6}D$
49158.61	49570	-411	9/2	21 $5d^{6}(^{5}D)6s^{2}6p \ ^{6}D + 12 \ 5d^{6}(^{5}D)6s^{2}6p \ ^{4}F + 11 \ 5d^{6}(^{5}D)6s^{2}6p \ ^{6}F$
49342.51	49466	-123	3/2	19 $5d^{7}(^{4}P)6s6p \ ^{4}S + 12 \ 5d^{7}(^{4}P)6s6p \ ^{6}P + 6 \ 5d^{8}(^{3}P)6p \ ^{4}P$
49446.25	49353	93	1/2	$15  5d^{7}(^{4}P)6s6p  ^{4}D + 13  5d^{7}(^{4}P)6s6p  ^{4}P + 10  5d^{7}(^{4}F)6s6p  ^{4}D$
49719.17	48977	742	11/2	33 $5d^{6}(^{5}D)6s^{2}6p \ ^{6}F + 18 \ 5d^{7}(^{2}G)6s6p \ ^{4}G + 15 \ 5d^{7}(^{4}F)6s6p \ ^{4}G$
49779.37	49895	-116	5/2	$12 5d^{7}(^{4}P)6s6p {}^{4}P + 75d^{8}(^{3}P)6p {}^{4}D + 6 5d^{7}(^{4}F)6s6p {}^{4}D$
49823.54	49765	59	7/2	$11  5d^8(^3F) 6p  ^2G + 11  5d^6(^5D) 6s^2 6p  ^6F + 11  5d^7(^2G) 6s 6p  ^4F$

Table 2

#### Notes.

<sup>a</sup> From Kramida et al. (2018).

<sup>b</sup> This work.

<sup>c</sup> Only the first three eigenvector components are given, provided they are greater than or equal to 5%.

above  $50,000 \text{ cm}^{-1}$  were not included in the fit because many of them were found to be strongly mixed with unknown levels, which made very doubtful the correspondence between the calculated energies and the available experimental values. For this reason, our HFR+CPOL calculations of the atomic structure and radiative parameters in Ir I were limited to the energy levels situated below  $50,000 \text{ cm}^{-1}$ . The energy levels computed in our work are compared to the available experimental values in Tables 1 and 2 for even and odd parities, respectively. As seen from these tables, a good agreement is obtained between both sets of results, the average deviations being found to be equal to  $59 \text{ cm}^{-1}$  (even parity) and  $112 \text{ cm}^{-1}$  (odd parity). We can also note that the levels considered in the present study are extremely mixed, in particular for the odd parity for which very strong intermediate coupling and configuration interaction among  $5d^86p$ ,  $5d^76s6p$ , and  $5d^66s^26p$  are observed, as shown in Table 2. This HFR+CPOL approach was then used to compute the radiative decay rates for the transitions depopulating the IrI odd energy levels located below  $50,000 \text{ cm}^{-1}$ . All the line strengths were calculated in the length form.

### 5. Results and Discussion

The lifetimes measured in the present work for 62 odd-parity levels of Ir I in the region of  $32513.43-58625.10 \text{ cm}^{-1}$  are

listed in Table 3. Among them, three levels were also studied in the literature through experiments and calculations, thus their previous results are presented for comparison. For the three levels previously reported, it is seen that our results are in rather good agreement with the values measured by Gough et al. (1983) and Xu et al. (2007) using the TR-LIF technique. For the 33874.43 cm<sup>-1</sup> level, the result reported by Ramanujam & Andersen (1978) is  $34 \pm 3$  ns, which shows a slightly larger difference with our value of  $28.4 \pm 0.6$  ns and the other two results in the literature. Considering that the former was measured by the beam-sputtering excitation method, which might involve a cascade population for the studied level and hence prolonging its decay time if cascade correction is not performed well, it is reasonable to believe that our result is more reliable.

In Table 3, except for the three energy levels with previous results, to our best knowledge the other 59 levels are experimentally measured for the first time. The measured lifetime values are in the range from 3.2 to 345 ns, and their uncertainties are smaller than 10% (except 10.5% for the level at  $43529.31 \text{ cm}^{-1}$ ) and more than half of them are within 5%.

Our HFR+CPOL theoretical lifetimes are also given in Table 3. The general agreement between theory and experiment can be judged as rather satisfactory (within a factor of 2), if we discount the two J = 3/2 levels at 44785.44 and 48440.83 cm<sup>-1</sup> for which the calculated lifetimes are respectively a factor of about 4 and 7 longer than the experimental

	Table 3	
Measured and Calculated	Lifetimes for Ir I Levels and Comparison	with Previous Results

Upper Level	a	Lower Lev	/el <sup>a</sup>	$\lambda_{\text{Exc}}$	loha	Lifetime (ns)				Lifetime (ns)				Lifetime (ns)	
Assignment	$E ({\rm cm}^{-1})$	Assignment	$E ({\rm cm}^{-1})$	(nm)	(nm)	Exper	iment	Calcul	lation						
	2 (011 )	1.0018	2 (**** )	()	()	This work	Previous	This work	Previous						
5d <sup>7</sup> 6s( <sup>5</sup> F)6p z <sup>6</sup> F° <sub>9/2</sub>	32513.43	$5d^76s^2 \ a \ ^4F_{9/2}$	0	307.565	381.832	345(11)	335(10) <sup>b</sup>	430	303 <sup>°</sup>						
54 <sup>7</sup> 60( <sup>5</sup> E)6n = <sup>6</sup> E <sup>0</sup>	22071 12	5d <sup>8</sup> (3E)6a h 4E	2024 00	222 171	262.07	28 4(6)	27.5(10) <sup>b</sup>	21.2	430 <sup>c</sup>						
So $os(T)$ op Z $T_{7/2}$	338/4.43	$50^{\circ}(^{\circ}F)08^{\circ}D^{\circ}F_{9/2}$	2854.98	322.171	362.97	28.4(6)	$27.5(10)^{\circ}$ 29.6(20) <sup>°</sup>	21.2	15.9° 21.2°						
							$34(3)^{d}$		21.2						
5d <sup>7</sup> 6s( <sup>5</sup> F)6p z <sup>6</sup> G° <sub>5/2</sub>	35540.34	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>3/2</sub>	4078.94	317.85	351.695	281(15)		205							
$5d^{7}6s(^{5}F)6p \ z \ ^{4}D^{\circ}_{5/2}$	37446.13	$5d^76s^2 \ a \ ^4F_{5/2}$	5784.62	315.841	362.732	194(15)	180(10) <sup>b</sup>	128	94.0 <sup>c</sup>						
4052°	40524 72	$5d^{7}6c^{2} \circ {}^{4}F$	5781 67	207 052	256.0	20.4(14)		42.1	128						
4032 3/2 4152°- 4	40324.73	$5d^8({}^3F)6s h {}^4F_{-4}$	3784.02 9877 54	287.832	267.071	20.4(14) 16.8(5)		43.1							
4226°5/2	42267.86	$5d^{8}({}^{3}F)6s b {}^{4}F_{5/2}$	9877.54	308.734	261.856	23.3(13)		28.7							
4227°9/2	42279.28	$5d^{8}({}^{3}F)6s b {}^{4}F_{7/2}$	7106.61	284.312	253.522	74.0(27)		57.7							
4317° <sub>7/2</sub>	43176.15	$5d^76s^2 a {}^4F_{9/2}$	0	231.609	300.313	19.7(9)		26.7							
4359° <sub>7/2</sub>	43529.21	$5d^76s^2 a {}^4F_{9/2}$	0	229.399	264.497	53.2(56)		50.4							
4459° <sub>5/2</sub>	44596.77	5d8(3F)6s b 4F5/2	9877.54	288.025	356.743	17.5(14)		20.5							
4464° <sub>7/2</sub>	44642.67	$5d^8(^3F)6s a {}^2F_{5/2}$	12218.47	308.412	224.001	7.7(5)		15.6							
4465° <sub>9/2</sub>	44652.43	$5d^{7}6s^{2} a {}^{4}F_{9/2}$	0	223.952	266.341	12.2(8)		27.5							
4478° <sub>3/2</sub>	44785.44	$5d^{8}(^{3}F)6s b {}^{4}F_{5/2}$	9877.54	286.468	354.357	7.1(4)		28.0							
4511° <sub>7/2</sub>	45111.68	$5d^{\circ}({}^{3}F)6s b {}^{4}F_{5/2}$	9877.54	283.816	304.014	17.9(8)		29.0							
4518° <sub>5/2</sub>	45185.95	$5d^{\circ}({}^{3}F)6s a {}^{2}F_{7/2}$	13087.90	311.545	243.268	10.4(3)		10.0							
4525 <sup>-</sup> 3/2	45259.14	$5d^{8}(^{3}F)6s = b^{4}F$	9877.54	282.633	305.311	16.8(5)		20.2							
4557 5/2 4580°- 4	45370.89	$5d^{7}6s^{2} a^{4}F_{1}u$	9877.54	280.104	312.03	15.1(4)		0.8							
$4622^{\circ}$	46220 32	$5d^{7}6s^{2} a {}^{4}F_{2}a$	0	217.885	250 649	11 4(6)		26.1							
4637° <sub>0/2</sub>	46371.64	$5d^{7}6s^{2}a^{4}F_{0/2}$	0	215.649	254.68	22.6(8)		20.1							
4716° <sub>7/2</sub>	47165.12	$5d^8({}^3F)6s b {}^4F_{9/2}$	2834.98	225.58	249.635	14.3(8)		16.8							
4720° <sub>9/2</sub>	47205.57	$5d^76s^2 a {}^4F_{9/2}$	0	211.839	249.383	31.7(11)		24.8							
4754° <sub>7/2</sub>	47548.69	$5d^76s^2 a {}^4F_{9/2}$	0	210.311	247.267	21.7(7)		29.8							
4785° <sub>11/2</sub>	47858.47	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>9/2</sub>	0	208.949	410.634	3.7(3)		6.5							
4820° <sub>5/2</sub>	48206.57	$5d^{7}6s^{2} b {}^{4}P_{5/2}$	16103.32	311.495	260.899	8.3(7)		13.8							
4844° <sub>3/2</sub>	48440.83	$5d^{7}6s^{2} a {}^{4}F_{3/2}$	4078.94	225.419	264.116	6.2(2)		40.7							
4844° <sub>7/2</sub>	48448.65	$5d^{7}6s^{2} a {}^{4}F_{9/2}$	0	206.404	241.855	8.5(3)		15.3							
4862° <sub>7/2</sub>	48629.22	$5d'6s^2 a {}^4F_{9/2}$	0	205.638	218.368	6.3(3)		6.6							
4977° <sub>5/2</sub>	49//9.3/	50'65' a $F_{3/2}$	4078.94	218.816	255.098	11.0(6)		23.5							
4982 7/2 5016°	49823.34	5d (F)0S D $F_{9/2}$	2834.98	212.818	250.558	10.2(5)		12.4							
5056°a/a	50564.12	$5d^{7}6s^{2} + {}^{4}F_{2}a$	4078.94	210.902	232.381	0.8(3)									
5058° <sub>7/2</sub>	50580 39	$5d^8({}^3F)6s h {}^4F_{0/2}$	2834 98	209.444	230.024	8.5(6)									
5116°3/2	51166.54	$5d^{7}6s^{2}a^{4}F_{3/2}$	4078.94	212.37	246.379	27.6(4)									
5142° <sub>5/2</sub>	51427.15	$5d^76s^2 a {}^4F_{3/2}$	4078.94	211.201	252.55	11.9(5)									
5147° <sub>9/2</sub>	51470.74	$5d^8({}^3F)6s b {}^4F_{9/2}$	2834.98	205.61	225.407	7.8(4)									
5181° <sub>5/2</sub>	51814.75	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>3/2</sub>	4078.94	209.486	238.452	15.5(4)									
5198° 1/2	51983.92	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>3/2</sub>	4078.94	208.747	241.515	13.6(5)									
5205° <sub>5/2</sub>	52051.75	$5d^76s^2 a {}^4F_{3/2}$	4078.94	208.451	237.112	13.5(4)									
5213° <sub>7/2</sub>	52134.11	$5d^{7}6s^{2} a {}^{4}F_{5/2}$	5784.62	215.752	250.528	10.2(2)									
5222° <sub>7/2</sub>	52224.37	$5d'6s^2 a {}^4F_{5/2}$	5784.62	215.333	249.963	7.1(3)									
5230° <sub>3/2</sub>	52303.65	$5d^76s^2 a^{-7}F_{3/2}$	4078.94	207.363	239.665	8.2(3)									
5232°5/2	52327.33	$5d^{7}6s^{2} a F_{3/2}$	4078.94	207.261	235.572	7.9(5)									
5258 1/2 5260°	52605 16	5d <sup>7</sup> 6s <sup>2</sup> a ${}^{4}$ F	4078.94	206.999	240.303	0.8(4)									
5280° 5/2	52806.57	$5d^{7}6s^{2}a^{4}F_{2/2}$	4078.94	205.222	236.81	11.7(9)									
5355°572	53552.93	$5d^{7}6s^{2} a^{4}F_{5/2}$	5784.62	209.344	241.929	5.9(4)									
5364°9/2	53642.06	$5d^76s^2 a {}^4F_{7/2}$	6323.91	211.335	246.584	5.0(3)									
5368° <sub>7/2</sub>	53686.99	$5d^76s^2 a {}^4F_{7/2}$	6323.91	211.135	241.147	6.4(3)									
5411° <sub>5/2</sub>	54119.23	$5d^{7}6s^{2} a {}^{4}F_{5/2}$	5784.62	206.891	229.671	9.0(5)									
5414° <sub>7/2</sub>	54140.83	5d <sup>8</sup> ( <sup>3</sup> F)6s b <sup>4</sup> F <sub>7/2</sub>	7106.61	212.611	248.75	5.7(3)									
5426° <sub>9/2</sub>	54263.79	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>7/2</sub>	6323.91	208.595	242.861	20.3(7)									
5456° <sub>7/2</sub>	54566.06	$5d'6s^2 a {}^4F_{7/2}$	6323.91	207.288	236.141	6.4(4)									
5463° <sub>5/2</sub>	54639.31	$5d'6s^2 a {}^4F_{7/2}$	6323.91	206.973	233.6	5.8(4)									
5466° <sub>9/2</sub>	54667.54	$5d'6s^2 a {}^4F_{7/2}$	6323.91	206.852	320.907	21.0(17)									
54/1 <sup>-</sup> 7/2	54711.10	$5d^{-}(-F)6s b^{-}F_{7/2}$	/106.61	210.064	259.015	7.7(5)									
3489 7/2	54894.82	50 68 a $F_{5/2}$	5/84.62	203.624	257.788	11.8(6)									

			(0	Continued)						
Upper Level <sup>a</sup>		Lower Level <sup>a</sup>		$\lambda_{\text{Exc}}$	$\lambda_{Obs}$	Lifetime (ns)				
Assignment	$E ({\rm cm}^{-1})$	Assignment	$E ({\rm cm}^{-1})$	(nm)	(nm)	Experiment		Calculation		
	_ ( )	10019	_ ( )	· · ·		This work	Previous	This work	Previous	
5503° <sub>9/2</sub>	55035.94	5d <sup>8</sup> ( <sup>3</sup> F)6s b <sup>4</sup> F <sub>7/2</sub>	7106.61	208.641	238.39	3.2(3)				
5769° <sub>7/2</sub>	57697.46	5d <sup>8</sup> ( <sup>3</sup> F)6s b <sup>4</sup> F <sub>5/2</sub>	9877.54	209.118	250.512	7.2(4)				
5811° <sub>5/2</sub>	58117.84	5d <sup>8</sup> ( <sup>3</sup> F)6s b <sup>4</sup> F <sub>5/2</sub>	9877.54	207.296	238.031	8.8(3)				
5862° <sub>7/2</sub>	58625.10	$5d^8(^3F)6s b {}^4F_{5/2}$	9877.54	205.138	235.174	5.1(3)				

Table 3Continued)

Notes. The number in parentheses is the uncertainty in the last one or two digits of the reported result.

<sup>a</sup> Kramida et al. (2018).

<sup>b</sup> Gough et al. (1983).

<sup>c</sup> Xu et al. (2007).

<sup>d</sup> Ramanujam & Anderson (1978).

values. It is worth noting that, according to our calculations, most of the highly excited levels considered in the present work were found to be extremely mixed with, on average, a main LS component as low as 20% for all the levels listed in Table 3, and this main component not exceeding even 15% for the levels located between 40,000 and 50,000 cm<sup>-1</sup>.

Using the theoretical BFs and the experimental lifetimes, we deduced the transition probabilities and oscillator strengths for all the lines depopulating the odd-parity levels below  $50,000 \text{ cm}^{-1}$ . The results obtained are reported in Table 4. These correspond to 134 Ir I spectral lines appearing in the wavelength range from 205 to 418 nm. Note that concerning the BFs, only the values larger than 0.05 have been retained in the table. To our knowledge, transition probabilities were experimentally measured by Gough et al. (1983) for only two transitions among those considered in the present work. These are found to be in good agreement (within 20%) with our values.

The estimated uncertainties of the transition probabilities and oscillator strengths obtained in our work are also reported in Table 4, using the letter coding as the one usually employed in the NIST database (Kramida et al. 2018). They were evaluated as follows. First, an uncertainty was assigned to all our calculated HFR+CPOL BF values by comparing the latter to those deduced from experimental measurements by Gough et al. (1983) and Ivarsson et al. (2003) for some transitions depopulating Ir I levels up to 40,710 cm<sup>-1</sup>. Such a comparison is reported in Table 7 of Xu et al. (2007) and illustrated in Figure 3 of the present paper where the relative differences

 $(BF_{calc}-BF_{exp})/BF_{calc}$  are reported against  $BF_{calc}$ . When looking at this figure, one can clearly note a rather regular pattern of increasingly deviating weak branches, the average uncertainties on calculated BF-values being found to be about 10%, for  $0.8 < BF_{calc} < 1.0$ , 20% for  $0.6 < BF_{calc} < 0.8$ , 30% for  $0.4 < BF_{calc} < 0.6, 40\%$  for  $0.2 < BF_{calc} < 0.4$  and 100% for  $0.0 < BF_{calc} < 0.2$ . These uncertainties were then combined in quadrature with the experimental lifetime uncertainties derived from our measurements to yield the uncertainties of gA- and gf -values. As a final result, out of the 134 transitions listed in Table 4, 46 have an estimated decay rate accuracy that is better than 50%, which illustrates the fact that many of the highly excited levels considered in the present work are depopulated by quite a number of weak transitions. Moreover, a few transitions reported in Table 4 with an asterisk were found to be affected by strong cancellation effects in our HFR+CPOL calculations. More precisely, for such transitions, the cancellation factor (CF), as defined by Cowan (1981), was estimated to be smaller than 0.01, indicating that the corresponding line strength, and thus the BF or transition probability, might be expected to show a larger percentage uncertainty.

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Upp	er Level <sup>a</sup>	Lower Lev	vel <sup>a</sup>	$\lambda_{air}$ (nm)	BF <sup>b</sup>	$gA(10^6 s^{-1})$		Log(gf)		
Assign.	$E (\text{cm}^{-1})$ Lifetime (ns)	Assign.	$E ({\rm cm}^{-1})$			This work <sup>b</sup>	Previous	This work <sup>c</sup>	Previ	ious
	_ ( ) ()	8	_ ( )				Exp.		Exp.	Calc.
$5d^{7}6s(^{5}F)6p \ z \ ^{6}F^{\circ}_{9/2}$	32513.43	$5d^76s^2 a {}^4F_{9/2}$	0.00	307.476	0.10*	2.89 (E)		-2.38(E)		-2.34 <sup>d</sup>
	$\tau = 345(11)$	$5d^8({}^3F)6s b {}^4F_{9/2}$	2834.98	336.848	0.21	6.09 (D+)		-1.98 (D+)		$-1.98^{d}$
		$5d^76s^2 a {}^4F_{7/2}$	6323.91	381.724	0.17	4.93 (E)		-1.97 (E)		-1.96 <sup>d</sup>
		5d8(3F)6s b 4F7/2	7106.61	393.484	0.51	14.7 (D+)		-1.47 (D+)		$-1.45^{d}$
$5d^{7}6s(^{5}F)6p \ge {}^{6}F^{\circ}_{7/2}$	33874.43	$5d^8({}^3F)6s b {}^4F_{9/2}$	2834.98	322.078	0.80	225 (B)	192.9 <sup>e</sup>	-0.46(B)	$-0.523^{d}$	$-0.47^{d}$
· · · · · · · · · · · · · · · · · · ·	au = 28.4(6)	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>7/2</sub>	6323.91	362.867	0.06	16.9 (E)	22.7 <sup>e</sup>	-1.48 (E)	-1.35 <sup>d</sup>	$-1.51^{d}$
5d <sup>7</sup> 6s( <sup>5</sup> F)6p z <sup>6</sup> G° <sub>5/2</sub>	35540.34	$5d^{7}6s^{2} a {}^{4}F_{3/2}$	4078.94	317.758	0.60	12.8 (D+)		-1.71 (D+)		
( ) I 5/2	$\tau = 281(15)$	$5d^8({}^3F)6s b {}^4F_{7/2}$	7106.61	351.594	0.23	4.91 (D+)		-2.05 (D+)		
$5 \sqrt{7} (-\sqrt{5} E) ( 4 D^{\circ})$	2744(12	$5 1^{7} (-2) - 4 \Gamma$	4078.04	200 (00	0.44	12((D))		1.74(D+)		1 70 <sup>d</sup>
$d^{-}6s(^{-}F)6p^{-}z^{-}D^{-}_{5/2}$	3/446.13	50 68 a $F_{3/2}$	4078.94	299.609	0.44	13.6 (D+)		-1.74(D+)		-1./0
	au = 194(15)	50 68 a $F_{5/2}$	5784.62	315.750	0.11	3.40(E)		-2.29(E)		-2.28 2.20
		50 68 a $F_{7/2}$	0323.91	321.221	0.11	3.40(E)		-2.28(E)		-2.30 1.05
		5d (F) 6s b $F_{5/2}$	9877.54	362.629	0.22	6.80(D+)		-1.87(D+)		-1.85
		$5d^{\circ}(^{\circ}F)6s \ b \ F_{3/2}$	11831.09	390.285	0.09	2.78(E)		-2.20(E)		-2.16
$4052^{\circ}_{3/2}$	40524.73	$5d^{7}6s^{2} a {}^{4}F_{5/2}$	5784.62	287.768	0.30	58.8 (D+)		-1.14 (D+)		
-,-	$\tau = 20.4(14)$	$5d^8({}^3F)6s b {}^4F_{5/2}$	9877.54	326.200	0.15	29.4 (E)		-1.33(E)		
		$5d^8(^{3}P)6s a {}^{2}P_{3/2}$	10578.68	333.838	0.19	37.3 (E)		-1.21(E)		
		$5d^8(^{3}P)6s a {}^{2}P_{1/2}$	12505.68	356.798	0.07	13.7 (E)		-1.58 (E)		
		$5d^8(^{3}P)6s a {}^{4}P_{5/2}$	12951.67	362.570	0.10	19.6 (E)		-1.41(E)		
		$5d^8(^{3}P)6s a {}^{4}P_{3/2}$	16565.35	417.255	0.14	27.4 (E)		-1.14 (E)		
4152°5 (2	41522.22	$5d^{7}6s^{2}a^{4}F_{2/2}$	4078 94	266 992	0.16	57.1(E)		-1.21(E)		
5/2	$\tau = 16.8(5)$	$5d^{7}6s^{2}a^{4}F_{5/2}$	5784.62	279.735	0.24	85.7 (D+)		-1.00(D+)		
	1 1010(0)	$5d^{7}6s^{2} a {}^{4}F_{7/2}$	6324.91	284 021	0.25	89.3 (D+)		-0.97 (D+)		
		$5d^8({}^3F)6s h {}^4F_{7/2}$	7106.61	290 481	0.14	50.0(E)		-1.20(E)		
		$5d^8({}^3F)6s h {}^4F_{5/2}$	9877.54	315 918	0.06	21.4(E)		-1.49(E)		
		$5d^8(^3P)6s a {}^2P_{3/2}$	10578.68	323.076	0.11	39.3 (E)		-1.21 (E)		
4226° = 12	42267 86	$5d^{7}6s^{2}a^{4}F_{2/2}$	4078 94	261.778	0.50	129 (D+)		-0.88(D+)		
3/2	$\tau = 23.3(13)$	$5d^{7}6s^{2} a {}^{4}F_{7/2}$	6323.91	278.129	0.33	85.0 (D+)		-1.01 (D+)		
	()	$5d^8(^3F)6s b {}^4F_{5/2}$	9877.54	308.644	0.09	23.2 (E)		-1.48 (E)		
4227° <sub>9/2</sub>	42279.28 $\tau = 74.0(27)$	$5d^8(^3F)6s b \ ^4F_{9/2}$	2834.98	253.446	0.89	120 (C+)		-0.94 ( <i>C</i> +)		
4317° <sub>7/2</sub>	43176.15	$5d^{7}6s^{2} a {}^{4}F_{9/2}$	0.00	231.538	0.09	36.5 (E)		-1.53 (E)		
·/ -	$\tau = 19.7(9)$	$5d^{7}6s^{2} a {}^{4}F_{5/2}$	5784.62	267.361	0.15	60.9 (E)		-1.19 (E)		
		$5d^{7}6s^{2} a {}^{4}F_{7/2}$	6323.91	271.274	0.14	56.8 (E)		-1.20 (E)		
		$5d^8({}^3F)6s b {}^4F_{5/2}$	9877.54	300.225	0.14	56.8 (E)		-1.11 (E)		
		$5d^8({}^3F)6s a {}^2F_{5/2}$	12218.47	322.929	0.18	73.1 (E)		-0.94 (E)		
		$5d^{8}({}^{3}F)6s = 2F_{7/2}$	13087 90	332 260	0.20	81.2(D+)		-0.87 (D+)		

 $\infty$ 

Table 4

			(	Table 4 (Continued)						
	Upper Level <sup>a</sup>	Lower Lev	/el <sup>a</sup>	$\lambda_{\rm oir}$ (nm)	BF <sup>b</sup>	gA(10	$(6s^{-1})$		Log(gf)	
Assign.	$E (\mathrm{cm}^{-1})$ Lifetime (ns)	Assign.	$E (\mathrm{cm}^{-1})$			This work <sup>b</sup>	Previous	This work <sup>c</sup>	Prev	ious
12500	10700.01	5 18 (3m) (c 1 4m)	2024.00	215 201	0.07	0.04 (5)	Exp.	2.04 (5)	Exp.	Calc.
4359° <sub>7/2</sub>	43529.21	$5d^{\circ}({}^{3}F)6s b {}^{4}F_{9/2}$	2834.98	245.281	0.07	9.96 $(E)$		-2.04(E)		
	$\tau = 56.2(56)$	$50^{\circ}6s^{\circ}a^{\circ}F_{5/2}$	5/84.62	264.418	0.10	14.2(E)		-1.82(E)		
		$5d^{\circ}(^{\circ}F)6s b F_{7/2}$	7106.61	274.000	0.07	9.96(E)		-1.95(E)		
		$5d^{\circ}(^{\circ}F)$ bs b $^{\circ}F_{5/2}$	9877.54	296.520	0.05	7.12(E)		-2.02(E)		
		$5d^{-}(F)$ bs a $F_{7/2}$	13087.90	327.729	0.17	24.2(E)		-1.41(E)		
		$50^{\circ}68^{\circ} a^{\circ}G_{9/2}$	13939.80	337.144	0.09	12.8(E)		-1.00(E)		
4459° <sub>5/2</sub>	44596.77	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>3/2</sub>	4078.94	246.730	0.31	106 (D+)		-1.01 (D+)		
,	$\tau = 17.5(14)$	5d8(3F)6s b 4F5/2	9877.54	287.941	0.36	123 (D+)		-0.82 (D+)		
		$5d^8(^{3}P)6s a {}^{4}P_{5/2}$	12951.67	315.914	0.09	30.9 (E)		-1.34 (E)		
		5d <sup>8</sup> ( <sup>3</sup> F)6s a <sup>2</sup> F <sub>7/2</sub>	13087.90	317.279	0.06	20.6 (E)		-1.51 (E)		
4464° <sub>7/2</sub>	44642 67	$5d^8({}^3F)6s h {}^4F_{0/2}$	2834.98	239,117	0.51	530 (D+)		-0.34 (D+)		
1101 1/2	$\tau = 7.7(5)$	$5d^8({}^{3}F)6s a {}^{2}F_{5/2}$	12218 47	308.322	0.11	114(E)		-0.79(E)		
	, ,,,(0)	$5d^8({}^{3}P)6s a {}^{4}P_{5/2}$	12951.67	315 456	0.07	72.7(E)		-0.97(E)		
		$5d^{8}({}^{3}F)6s a {}^{2}F_{7/2}$	13087.90	316.817	0.14	145 (E)		-0.66(E)		
1165°	44652 42	$5d^{7}6s^{2} \circ {}^{4}F$	0.00	222 662	0.15	122 (E)		1.02(E)		
4405 9/2	= -12.2(8)	$5d^8(^3E)6ab^4E$	2824.08	223.062	0.15	125(L)		-1.05(L)		
	T = 12.2(8)	$5d^76s^2 + {}^{4}F$	2034.90	259.002	0.51	234 (D+)		-0.00 (D+) 1.04 (F)		
		$5d^8(^3E)6ab^4E$	7106.61	200.824	0.11	90.2(E)		-1.04(E)		
		$5d^{8}({}^{3}F)6s a {}^{2}F_{7/2}$	13087.90	316.719	0.34	57.4 (E)		-0.33(D+) -1.06(E)		
		0.2								
4478° <sub>3/2</sub>	44785.44	$5d^8({}^3F)6s b {}^4F_{5/2}$	9877.54	286.384	0.17	95.8 (E)		-0.93 (E)		
	au = 7.1(4)	$5d^8({}^3F)6s a {}^2F_{5/2}$	12218.47	306.971	0.27	152 (D+)		-0.67 (D+)		
		$5d^{8}(^{3}P)6s a {}^{4}P_{5/2}$	12951.67	314.041	0.10	56.3 (E)		-1.08 (E)		
		$5d^{7}6s^{2} b {}^{4}P_{5/2}$	16103.32	348.549	0.14	78.9 (E)		-0.84 (E)		
		$5d^8(^{3}P)6s a {}^{4}P_{1/2}$	16681.20	355.716	0.15	84.5 (E)		-0.79 (E)		
4511° <sub>7/2</sub>	45111.68	$5d^{7}6s^{2} a {}^{4}F_{5/2}$	5784.62	254.202	0.07	31.3 (E)		-1.51 (E)		
.,	au = 17.9(8)	$5d^8({}^3F)6s b {}^4F_{7/2}$	7106.61	263.051	0.08	35.8 (E)		-1.43 (E)		
		$5d^8({}^3F)6s b {}^4F_{5/2}$	9877.54	283.739	0.25	112 (D+)		-0.87 (D+)		
		$5d^8({}^3F)6s a {}^2F_{5/2}$	12218.47	303.932	0.42	188 (D+)		-0.58 (D+)		
		5d <sup>8</sup> ( <sup>3</sup> F)6s a <sup>2</sup> F <sub>7/2</sub>	13087.90	312.180	0.07	31.3 (E)		-1.34 (E)		
4518° - 10	45185 95	$5d^8({}^3F)6s h {}^4F_{7/2}$	7106 61	262 532	0.51	294 (D+)		-0.52 (D+)		
1010 3/2	$\tau = 10.4(3)$	$5d^{8}({}^{3}F)6s h {}^{4}F_{2/2}$	11831.09	299 719	0.07	40.4(E)		-1.26(E)		
	$\gamma = 10.1(3)$	$5d^{8}({}^{3}F)6s = a^{2}F_{c/2}$	12218 47	303 241	0.16	92.3(E)		-0.89(E)		
		$5d^{8}(^{3}F)6s a {}^{2}F_{7/2}$	13087.90	311.455	0.07	40.4 (E)		-1.23 (E)		
4525°	45250 14	$5d^{7}6c^{2} \circ {}^{4}E$	1079 04	212 761	0.16	20 1 (E)		1.47 (E)		
+323 3/2	43239.14 $\pi = 16.9(5)$	5d <sup>7</sup> 6c <sup>2</sup> a ${}^{4}\mathbf{F}$	4078747 578762	242.701	0.10	50.1(E)		-1.4/(L)		
	y = 10.0(3)	$5d^8(^3E)6c h^{4E}$	0877 54	233.232	0.25	$J_{+.0}(D+)$		-1.26 (D+) 1.64 (F)		
		$5d^{8}(^{3}E)6c h^{4}E$	7077.34 11821.00	202.330	0.00	19.0(E)		-1.04(E)		
		$JU(\Gamma)OSDF_{3/2}$	11631.09	299.003	0.34	00.9 ( <i>D</i> +)		-0.90 (D+)		

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			(	Table 4       (Continued)						
	Upper Level <sup>a</sup>	Lower Lev	/el <sup>a</sup>	$\lambda_{\rm oir}$ (nm)	BF <sup>b</sup>	gA(10	$^{6}s^{-1}$ )		Log(gf)	
Assign.	E (cm <sup>-1</sup> ) Lifetime (ns)	Assign.	$E ({\rm cm}^{-1})$	, van (min)	51	This work <sup>b</sup>	Previous	This work <sup>c</sup>	Prev	vious
8		8	_ ( )				Exp.		Exp.	Calc.
4557° <sub>5/2</sub>	45570.89	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>3/2</sub>	4078.94	240.938	0.63	289 (C)		-0.61 ( <i>C</i> )		
	au = 13.1(4)	$5d^76s^2 a {}^4F_{5/2}$	5784.62	251.267	0.06	27.5 (E)		-1.59 (E)		
		5d <sup>8</sup> ( <sup>3</sup> F)6s b <sup>4</sup> F <sub>5/2</sub>	9877.54	280.081	0.15	68.7 (E)		-1.10(E)		
4589° <sub>7/2</sub>	45895.85	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>9/2</sub>	0.00	217.817	0.23	242 (D+)		-0.76 (D+)		
,	au = 7.6(2)	5d <sup>8</sup> ( <sup>3</sup> F)6s b <sup>4</sup> F <sub>7/2</sub>	7106.61	257.726	0.27	284 (D+)		-0.55 (D+)		
		5d <sup>8</sup> ( <sup>3</sup> F)6s a <sup>2</sup> F <sub>7/2</sub>	13087.90	304.715	0.28	295 (D+)		-0.39 (D+)		
		$5d^76s^2 \ a \ ^2G_{9/2}$	13939.80	312.839	0.11	116 (E)		-0.77 (E)		
4622° <sub>9/2</sub>	46220.32	$5d^{7}6s^{2} a {}^{4}F_{9/2}$	0.00	216.287	0.36	316 (D+)		-0.65 (D+)		
>/2	$\tau = 11.4(6)$	$5d^8({}^3F)6s b {}^{4}F_{9/2}$	2834.98	230.422	0.28	246 $(D+)$		-0.71 (D+)		
		$5d^76s^2 a {}^4F_{7/2}$	6323.91	250.574	0.05	43.9 (E)		-1.38(E)		
		$5d^8(^3F)6s \ a \ ^2F_{7/2}$	13087.90	301.731	0.26	228 (D+)		-0.51 (D+)		
4637°o/2	46371 64	$5d^{7}6s^{2}a^{4}F_{0/2}$	0.00	215,581	0.45	199 (D+)		-0.86(D+)		
9/2	$\tau = 22.6(8)$	$5d^8({}^{3}F)6s h {}^{4}F_{0/2}$	2834.98	229.620	0.08	35.4(E)		-1.55(E)		
		$5d^76s^2 a {}^4F_{7/2}$	6323.91	249.627	0.14	61.9(E)		-1.24(E)		
		$5d^8({}^3F)6s b {}^4F_{7/2}$	7106.61	254.604	0.20	88.5 (D+)		-1.06 (D+)		
		$5d^8(^3F)6s \ a \ ^2F_{7/2}$	13087.90	300.359	0.09	39.8 (E)		-1.27 (E)		
4716° <sub>7/2</sub>	47165.12	$5d^{7}6s^{2}a^{4}F_{5/2}$	5784.62	241.587	0.06	33.6(E)		-1.53 (E)		
1/2	$\tau = 14.3(8)$	$5d^76s^2 a {}^4F_{7/2}$	6323.91	244.777	0.24	134 (D+)		-0.92(D+)		
		$5d^8({}^3F)6s b {}^4F_{7/2}$	7106.61	249.560	0.11	61.5 (E)		-1.24 (E)		
		$5d^{8}(^{3}F)6s a {}^{2}F_{5/2}$	12218.47	286.066	0.36	201 (D+)		-0.61 (D+)		
		5d <sup>8</sup> ( <sup>3</sup> F)6s a <sup>2</sup> F <sub>7/2</sub>	13087.90	293.365	0.07	39.2 (E)		-1.30 (E)		
4720°°° /2	47205.57	$5d^{7}6s^{2} a^{4}F_{0/2}$	0.00	211.772	0.09	28.4(E)		-1.72(E)		
5/2	$\tau = 31.7(11)$	$5d^{8}(^{3}F)6s b {}^{4}F_{9/2}$	2834.98	225.305	0.05	15.8 (E)		-1.92(E)		
		$5d^76s^2 a {}^4F_{7/2}$	6323.91	244.534	0.12	37.9 (E)		-1.47 (E)		
		$5d^8({}^3F)6s b {}^{4}F_{7/2}$	7106.61	249.308	0.64	202 (E)		-0.73 (E)		
		$5d^76s^2 a {}^2G_{9/2}$	13939.80	300.521	0.06	18.9 (E)		-1.59 (E)		
4754° <sub>7/2</sub>	47548 69	$5d^{7}6s^{2}a^{4}F_{0/2}$	0.00	210 244	0.17	62.7(E)		-1.38(E)		
1101 1/2	$\tau = 21.7(7)$	$5d^8({}^3F)6s b {}^4F_{0/2}$	2834.98	223.576	0.23	84.8 (D+)		-1.20 (D+)		
		$5d^8({}^3F)6s b {}^4F_{5/2}$	9877.54	265.376	0.07*	25.8 (E)		-1.56(E)		
		$5d^8({}^3F)6s a {}^2F_{5/2}$	12218.47	282.961	0.13	47.9 (E)		-1.24 (E)		
		$5d^76s^2 b {}^4P_{5/2}$	16103.32	317.920	0.19	70.0 (E)		-0.97 (E)		
4785°	47858 47	$5d^{7}6s^{2} a {}^{4}F_{0}c$	0.00	208 883	0.89	2886 $(C+)$		0.28(C+)		
1705 11/2	$\tau = 3.7(3)$	$5d^8({}^{3}E)6s h {}^{4}E_{0/2}$	2834 98	222.037	0.11	357(E)		-0.58(E)		
	. 5.(5)		200 1.90		0.11	227 (E)		0.00 (E)		
4820° <sub>5/2</sub>	48206.57	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>3/2</sub>	4078.94	226.545	0.16	116 (E)		-1.05 (E)		
	au = 8.3(7)	$5d'6s^2 a {}^4F_{7/2}$	6323.91	238.689	0.30	217 (D+)		-0.73 (D+)		
		$5d^{8}({}^{3}F)6s b {}^{4}F_{5/2}$	9877.54	260.821	0.15	108 (E)		-0.96 (E)		
		5d°(°P)6s a <sup>2</sup> P <sub>3/2</sub>	10578.68	265.681	0.16	116 (E)		-0.91 (E)		

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	(Continued)										
	Upper Level <sup>a</sup>	Lower Lev	/el <sup>a</sup>	$\lambda_{\rm oir}$ (nm)	BF <sup>b</sup>	$gA(10^6 \text{s}^{-1})$		Log(gf)			
Assign.	$E (\text{cm}^{-1})$ Lifetime (ns)	Assign.	$E (\mathrm{cm}^{-1})$	, an ()		This work <sup>b</sup>	Previous	This work <sup>c</sup>	Prev	vious	
							Exp.		Exp.	Calc.	
		5d <sup>8</sup> ( <sup>3</sup> P)6s a <sup>4</sup> P <sub>5/2</sub>	12951.67	283.566	$0.09^{*}$	65.1 (E)		-1.11(E)			
		$5d^{7}6s^{2} b {}^{4}P_{3/2}$	18547.04	337.063	0.05	36.1 (E)		-1.21 (E)			
4844° <sub>3/2</sub>	48440.83	5d <sup>8</sup> ( <sup>3</sup> P)6s a <sup>2</sup> P <sub>3/2</sub>	10578.68	264.037	$0.07^{*}$	45.2 (E)		-1.32 (E)			
-,-	au = 6.2(2)	$5d^8({}^3F)6s b {}^4F_{3/2}$	11831.09	273.070	0.62	400 (C)		-0.35(C)			
		5d <sup>8</sup> ( <sup>3</sup> P)6s a <sup>2</sup> P <sub>1/2</sub>	12505.68	278.197	0.10	64.5 (D)		-1.13 (D)			
4844° <sub>7/2</sub>	48448.65	$5d^{7}6s^{2} a {}^{4}F_{5/2}$	5784.62	234.317	0.09	84.7 (E)		-1.16 (E)			
,,	au = 8.5(3)	$5d^76s^2 a {}^4F_{7/2}$	6323.91	237.318	0.55	517 (D+)		-0.36 (D+)			
		5d <sup>8</sup> ( <sup>3</sup> F)6s b <sup>4</sup> F <sub>7/2</sub>	7106.61	241.812	0.14	132 (E)		-0.94(E)			
		$5d^8(^3F)6s a {}^2F_{5/2}$	12218.47	275.931	0.10	94.1 (E)		-0.97 (E)			
4862° <sub>7/2</sub>	48629.22	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>9/2</sub>	0.00	205.572	0.06	76.2 (E)		-1.32 (E)			
	$\tau = 6.3(3)$	$5d^8(^3F)6s b {}^4F_{9/2}$	2834.98	218.300	0.45	571 (D+)		-0.39 (D+)			
		5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>5/2</sub>	5784.62	233.330	0.24	305 (D+)		-0.60 (D+)			
		5d <sup>8</sup> ( <sup>3</sup> F)6s b <sup>4</sup> F <sub>7/2</sub>	7106.61	240.760	0.09	114 (E)		-1.00 (E)			
		$5d^8(^3F)6s b {}^4F_{5/2}$	9877.54	257.976	0.05	63.5 (E)		-1.20 (E)			
4977° <sub>5/2</sub>	49779.37	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>3/2</sub>	4078.94	218.748	0.15	81.8 (E)		-1.23 (E)			
,	$\tau = 11.0(6)$	5d <sup>7</sup> 6s <sup>2</sup> a <sup>4</sup> F <sub>7/2</sub>	6323.91	230.050	0.10	54.5 (E)		-1.36 (E)			
		5d <sup>8</sup> ( <sup>3</sup> F)6s b <sup>4</sup> F <sub>7/2</sub>	7106.61	234.270	0.18	98.2 (E)		-1.09 (E)			
		$5d^8(^{3}P)6s a {}^2P_{3/2}$	10578.68	255.021	0.12	65.5 (E)		-1.20 (E)			
		$5d^8(^3F)6s a^2F_{7/2}$	13087.90	272.462	0.16	87.3 (E)		-1.01 (E)			
		$5d^{8}(^{3}P)6s a {}^{4}P_{3/2}$	16565.35	300.990	0.08	43.6 (E)		-1.23 (E)			
		5d'6s <sup>2</sup> b <sup>4</sup> P <sub>3/2</sub>	18547.04	320.089	0.08	43.6 (E)		-1.17 (E)			
4982° <sub>7/2</sub>	49823.54	$5d^76s^2$ a ${}^4F_{5/2}$	5784.62	227.002	0.29	143 (D+)		-0.96 (D+)			
	$\tau = 16.2(5)$	$5d^76s^2 a {}^4F_{7/2}$	6323.91	229.816	0.31	153 (D+)		-0.92 (D+)			
		$5d^8({}^3F)6s b {}^4F_{5/2}$	9877.54	250.263	0.15	74.1 (E)		-1.16 (E)			
		5d <sup>8</sup> ( <sup>1</sup> D)6s a <sup>2</sup> D <sub>5/2</sub>	19060.62	324.973	0.09	44.4 (E)		-1.15 (E)			

Notes.

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<sup>a</sup> Kramida et al. (2018).

<sup>b</sup> Calculated branching fractions with \* are characterized by cancellation factors smaller than 0.01 (see text).

<sup>c</sup> gA- and log gf -values obtained in this work were deduced from the combination of HFR+CPOL branching fractions with experimental lifetimes. The estimated uncertainties are given in parentheses. They are indicated by the same letter coding one used in the NIST database (Kramida et al. 2018), i.e.,  $B + (\leq 7\%)$ ,  $B (\leq 10\%)$ ,  $C + (\leq 18\%)$ ,  $C (\leq 25\%)$ ,  $D + (\leq 40\%)$ ,  $D (\leq 50\%)$ , and E (>50%) (see the text).

<sup>e</sup> Gough et al. (1983).

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