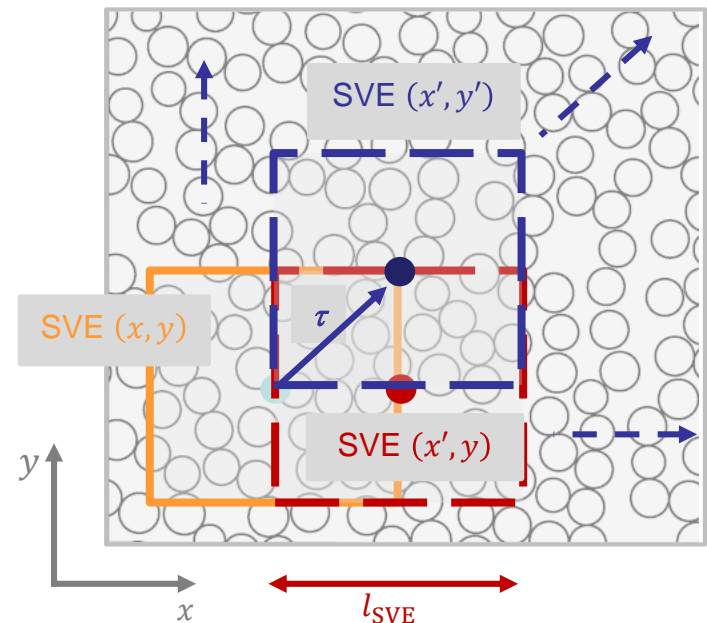
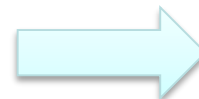
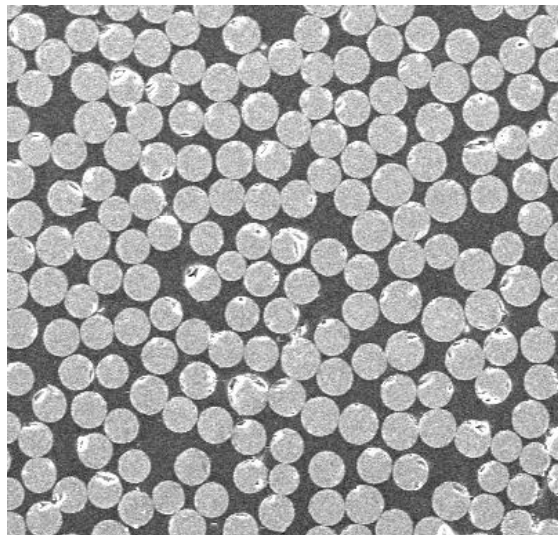


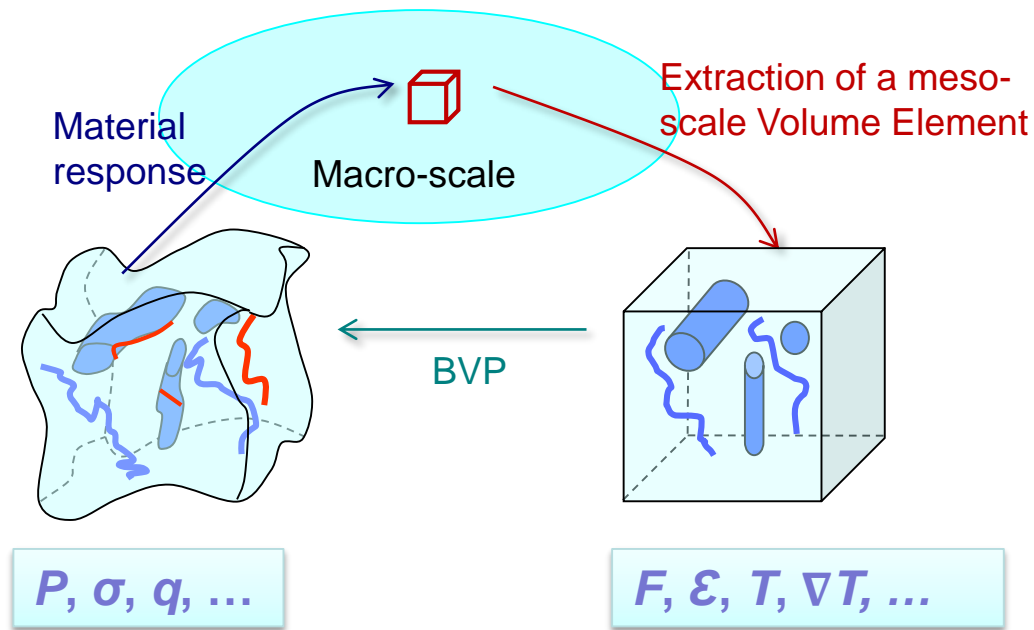
# A stochastic Mean-Field Reduced Order Model of Unidirectional Composites

*Wu Ling, Noels Ludovic*



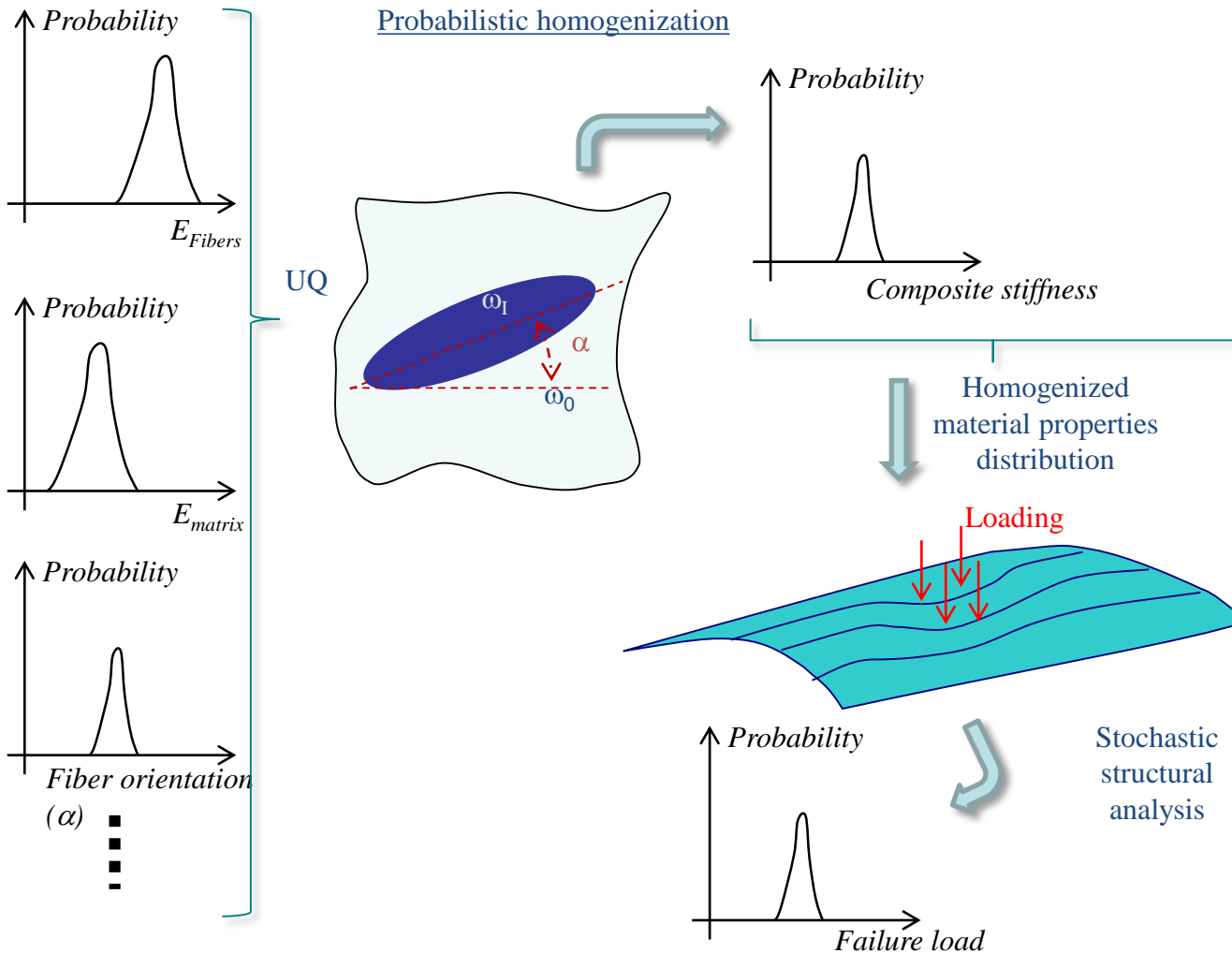
The research has been funded by the Walloon Region under the agreement no 1410246-STOMMMAC (CT-INT 2013-03-28) in the context of the M-ERA.NET Joint Call 2014. SEM images by Major Zoltan, Nghia Chnug Chi, JKU, Austria

- Two-scale modelling
  - One method: homogenization
  - 2 problems are solved (concurrently)
    - The macro-scale problem
    - The meso-scale problem (on a meso-scale Volume Element)



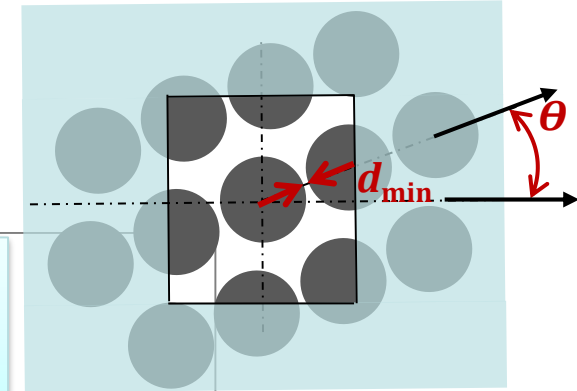
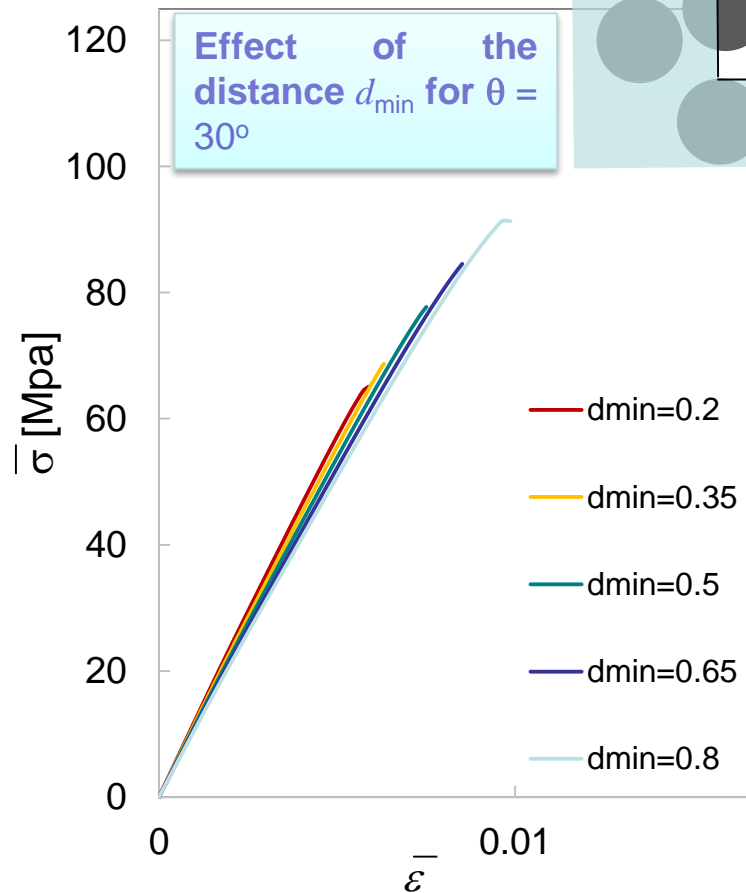
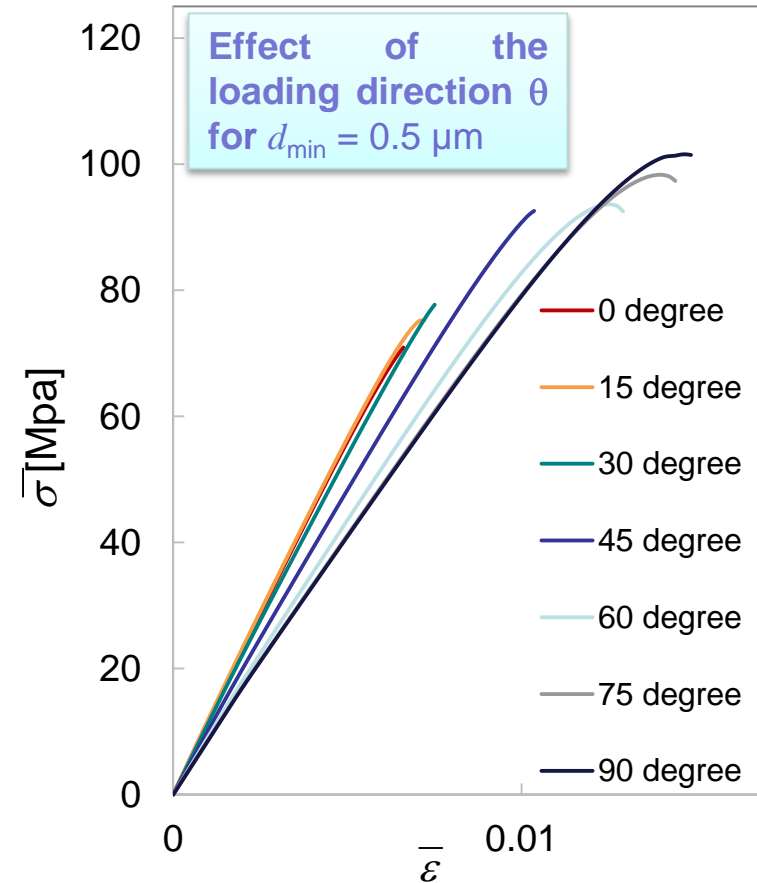
# The problem

- Material uncertainties affect structural behaviors



# The problem

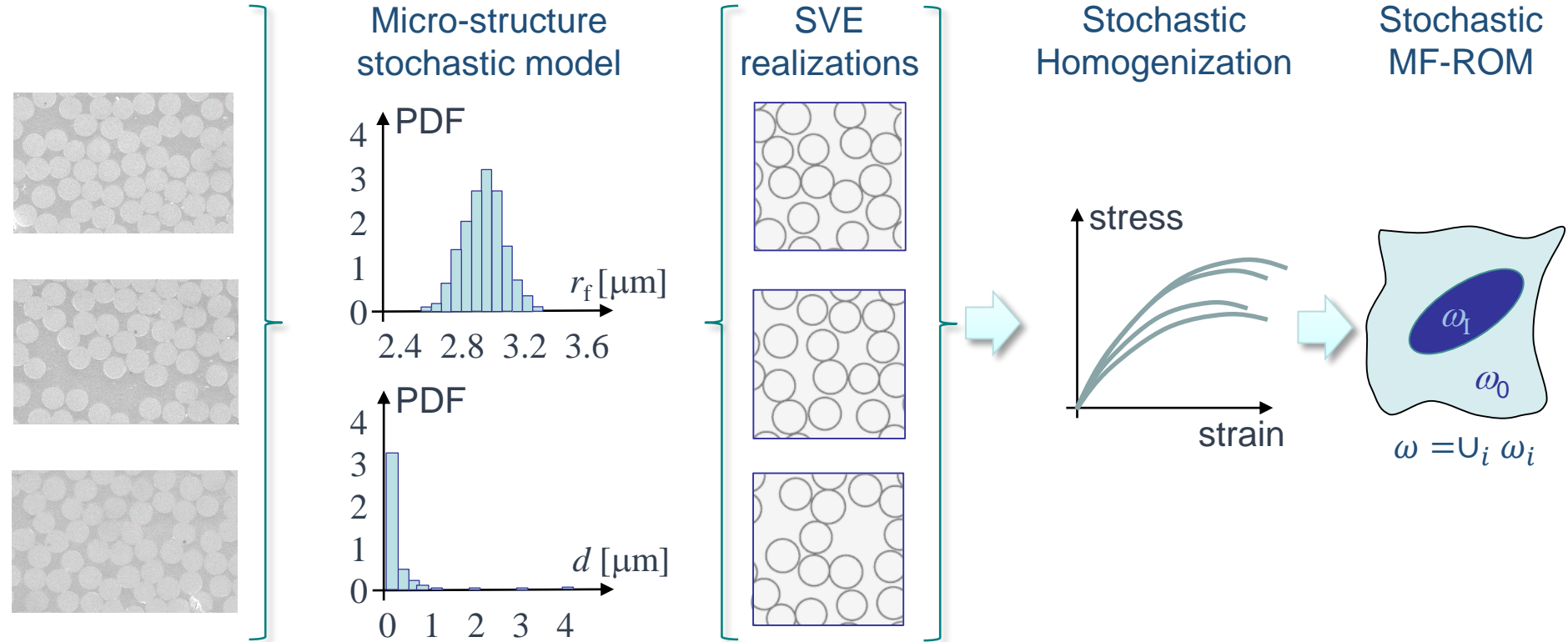
- Illustration assuming a regular stacking
  - 60%-UD fibers
  - Damage-enhanced matrix behavior



- Question: what does happen for a realistic fiber stacking?

# The problem

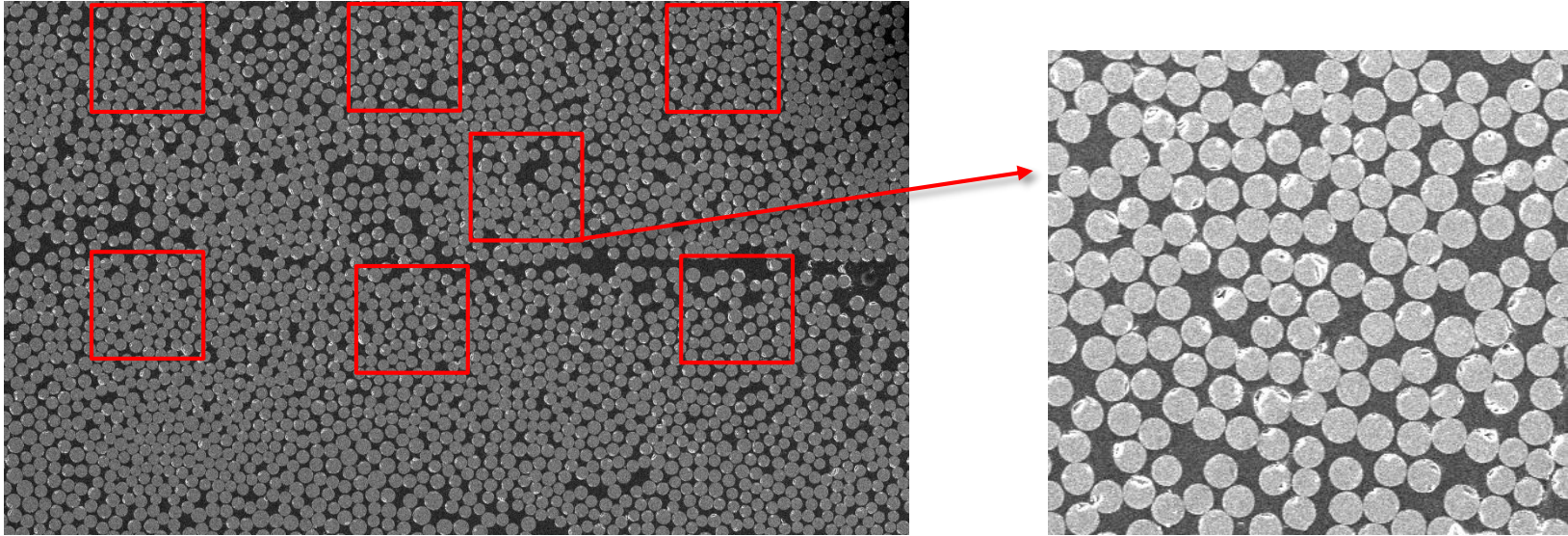
- Proposed methodology:



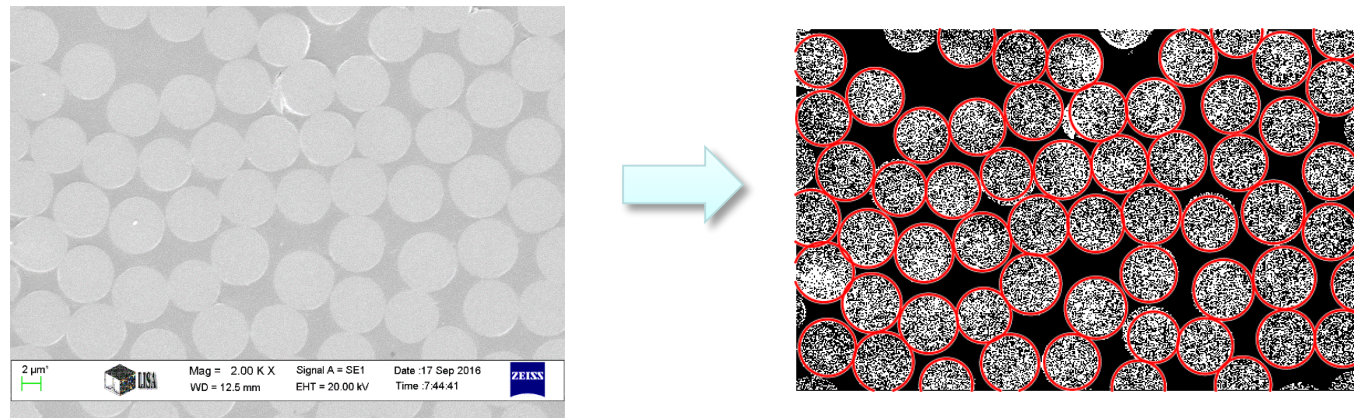


# Experimental measurements

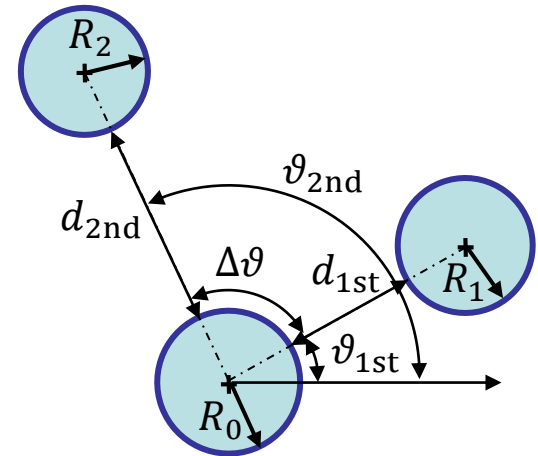
- 2000x and 3000x SEM images



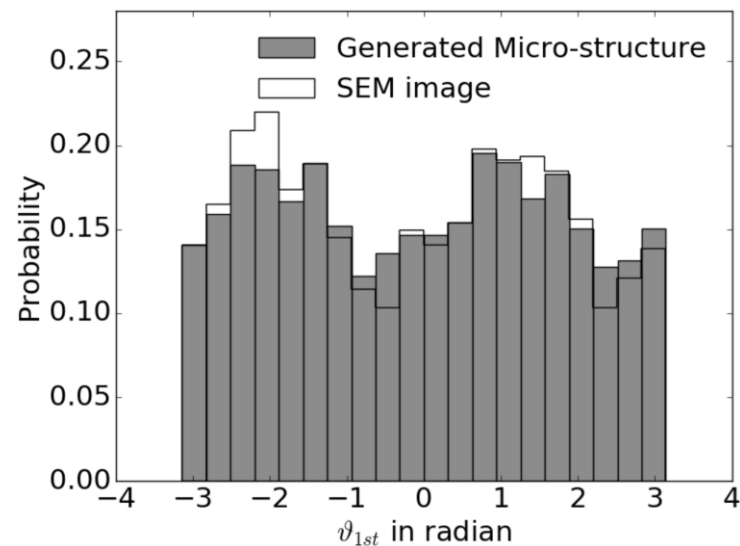
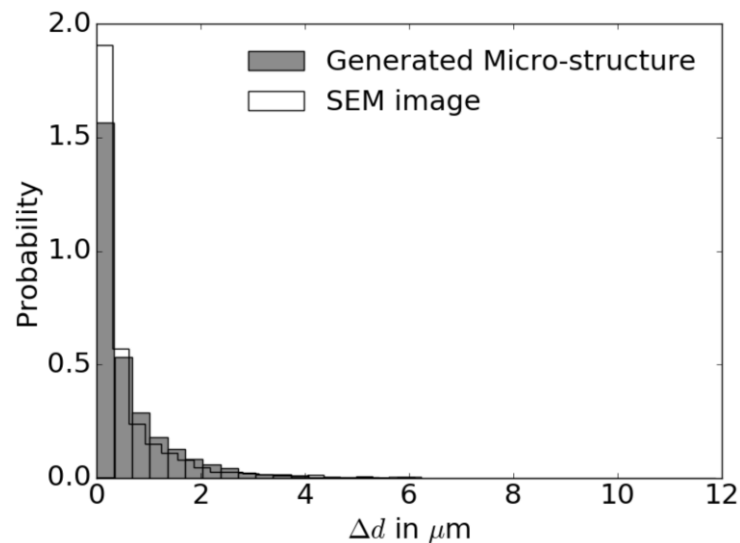
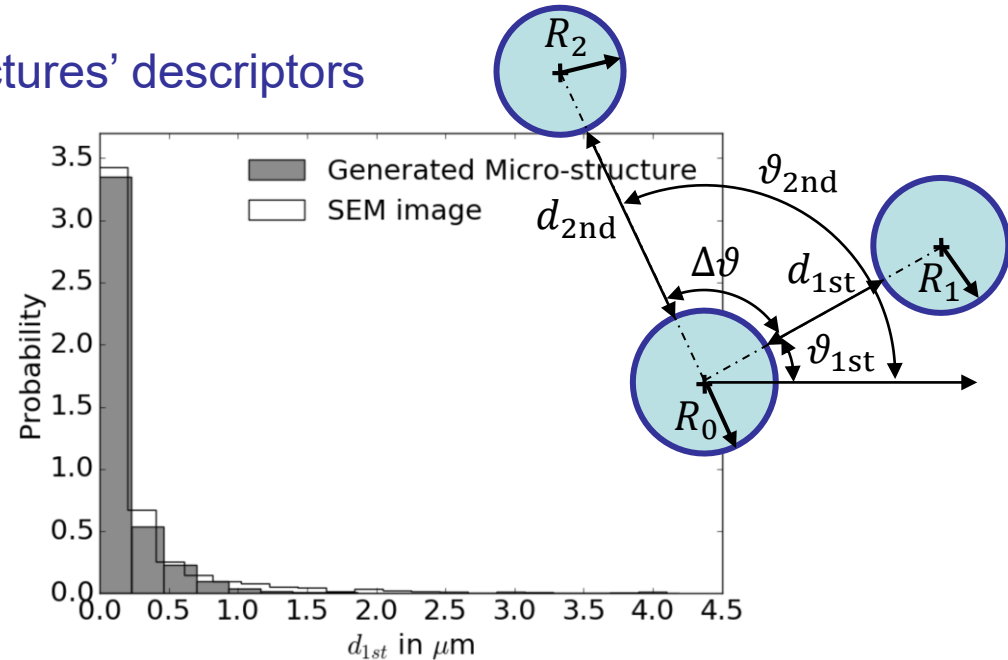
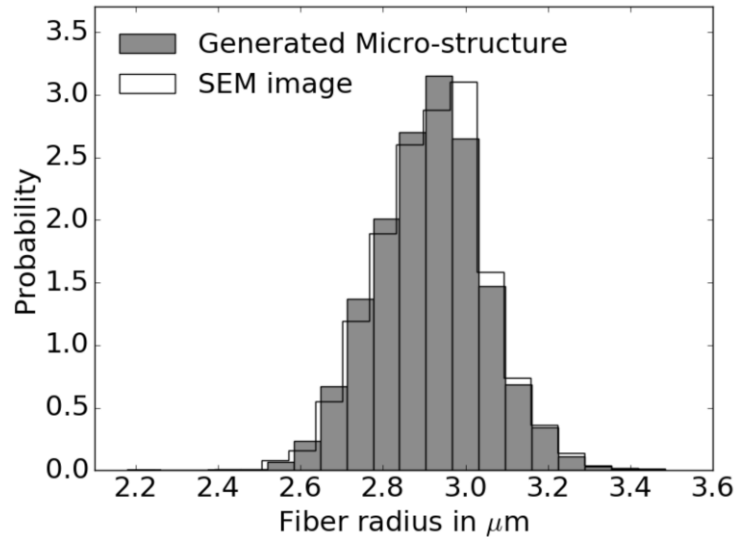
- Fibers detection



- Basic geometric information of fibers' cross sections
  - Fiber radius distribution  $p_R(r)$
- Basic spatial information of fibers
  - The distribution of the nearest-neighbor net distance function  $p_{d_{1st}}(d)$
  - The distribution of the orientation of the undirected line connecting the center points of a fiber to its nearest neighbor  $p_{\vartheta_{1st}}(\theta)$
  - The distribution of the difference between the net distance to the second and the first nearest-neighbor  $p_{\Delta d}(d)$  with  $\Delta d = d_{2nd} - d_{1st}$
  - The distribution of the second nearest-neighbor's location referring to the first nearest-neighbor  $p_{\Delta\vartheta}(\theta)$  with  $\Delta\vartheta = \vartheta_{2nd} - \vartheta_{1st}$

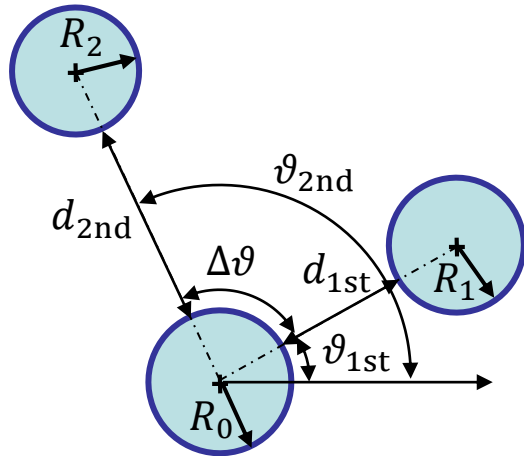


- Histograms of random micro-structures' descriptors





- Dependency of the four random variables  $d_{1st}$ ,  $\Delta d$ ,  $\vartheta_{1st}$ ,  $\Delta\vartheta$
- Correlation matrix



	$d_{1st}$	$\Delta d$	$\vartheta_{1st}$	$\Delta\vartheta$
$d_{1st}$	1.0	0.21	0.01	0.02
$\Delta d$		1.0	0.002	-0.005
$\vartheta_{1st}$			1.0	0.02
$\Delta\vartheta$				1.0

- Distances correlation matrix

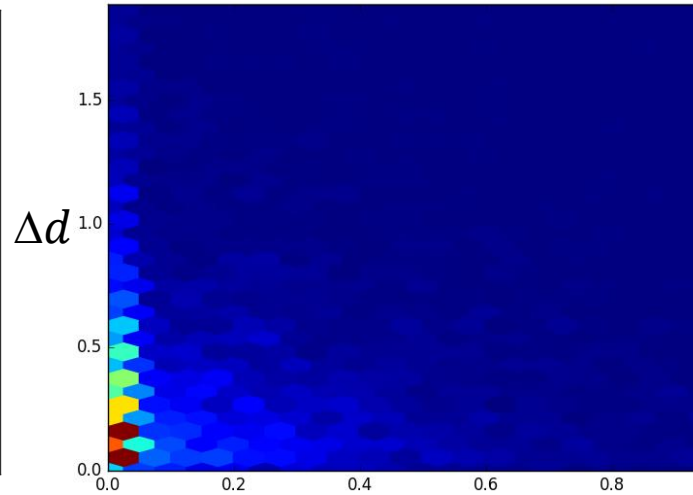
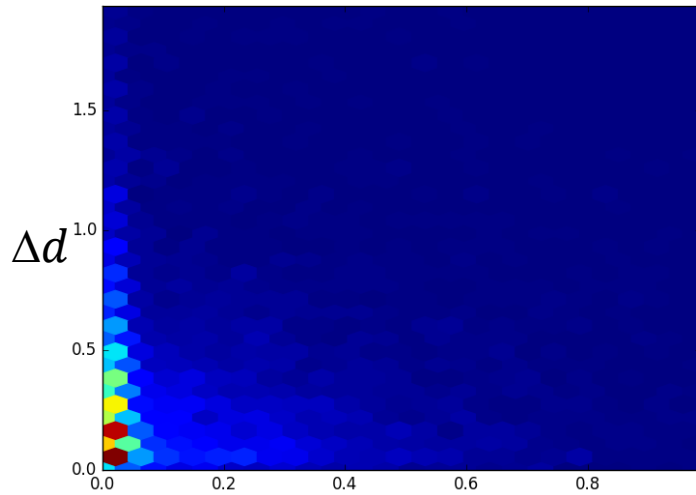
$d_{1st}$  and  $\Delta d$  are dependent  
 ➡ they will have to be generated  
 from their empirical copula

	$d_{1st}$	$\Delta d$	$\vartheta_{1st}$	$\Delta\vartheta$
$d_{1st}$	1.0	0.27	0.04	0.08
$\Delta d$		1.0	0.05	0.06
$\vartheta_{1st}$			1.0	0.05
$\Delta\vartheta$				1.0

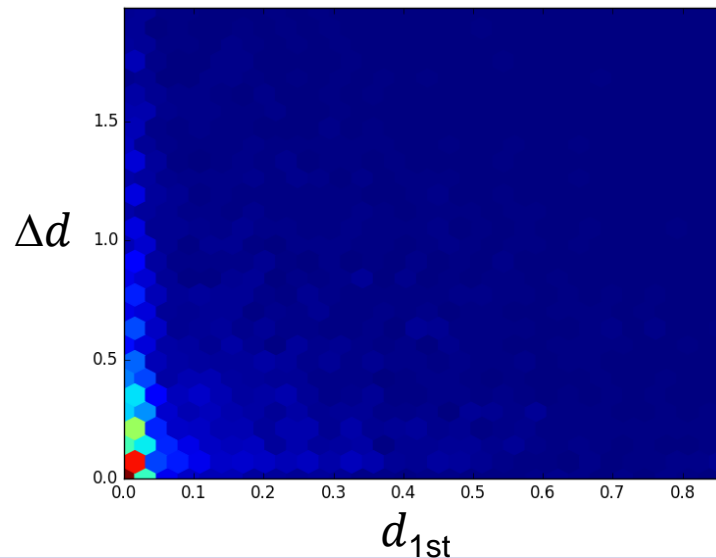
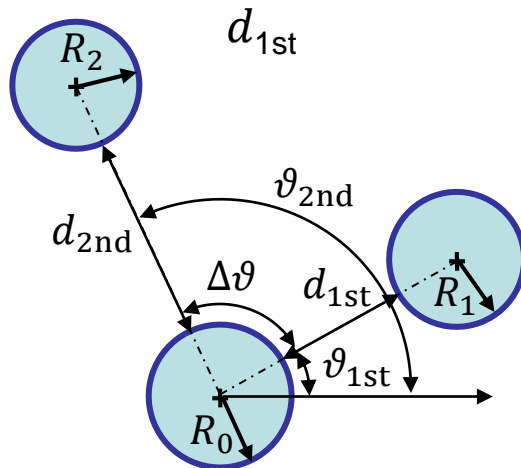
- $d_{1st}$  and  $\Delta d$  should be generated using their empirical copula

SEM sample

Generated sample



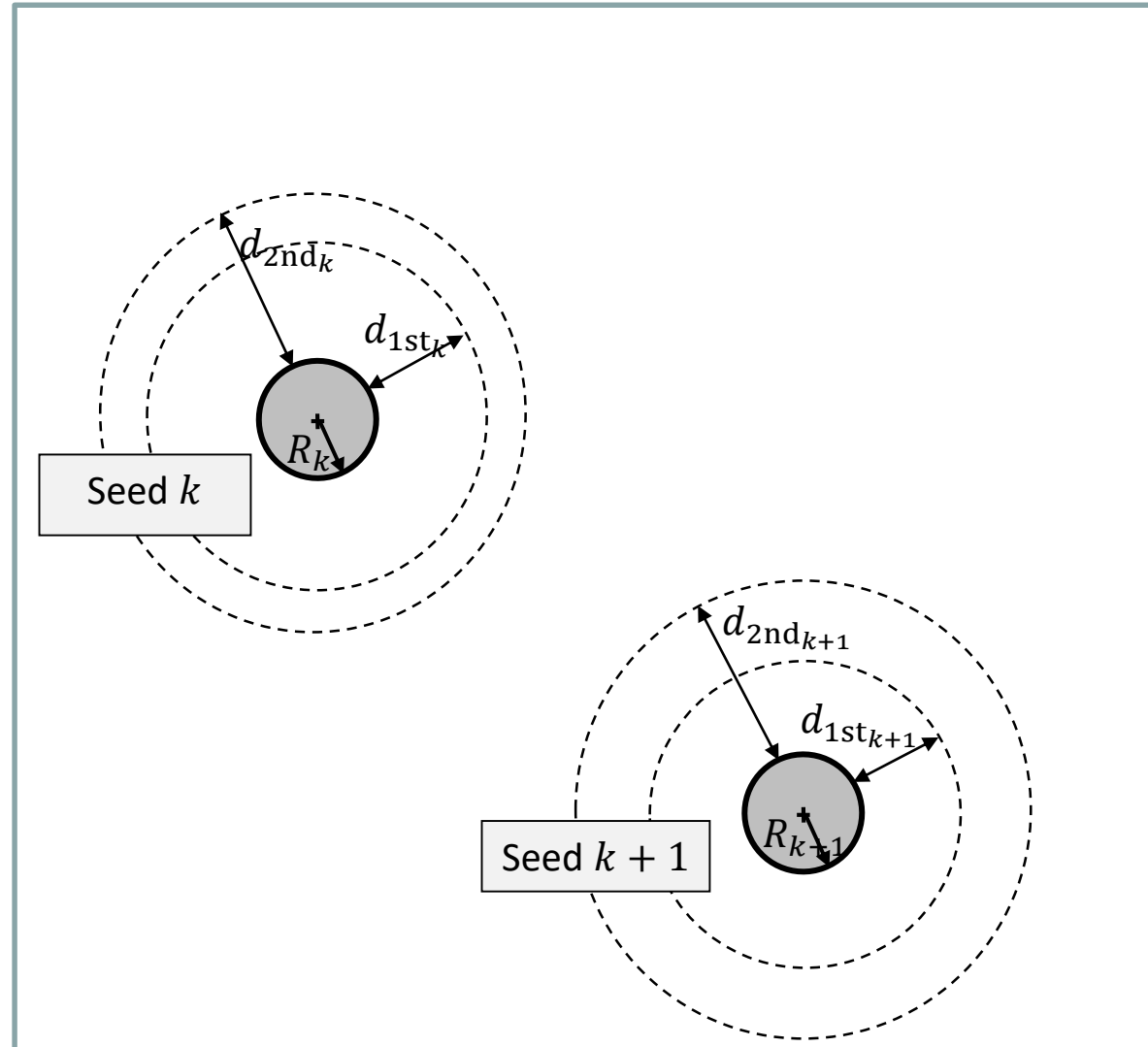
Directly from  
copula generator



Statistic result from  
generated SVE

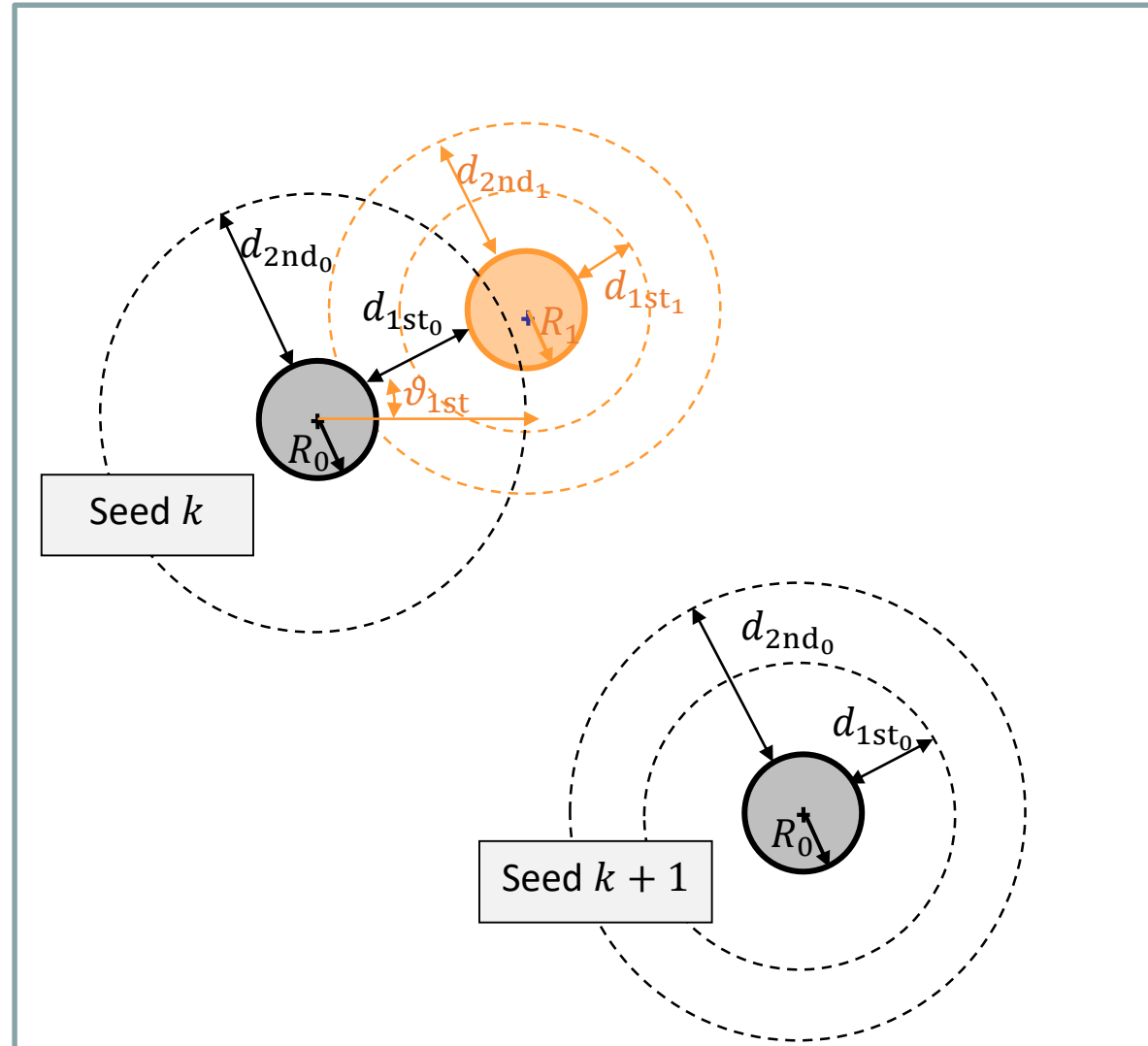
- The numerical micro-structure is generated by a fiber additive process

1) Define  $N$  seeds with first and second neighbors distances



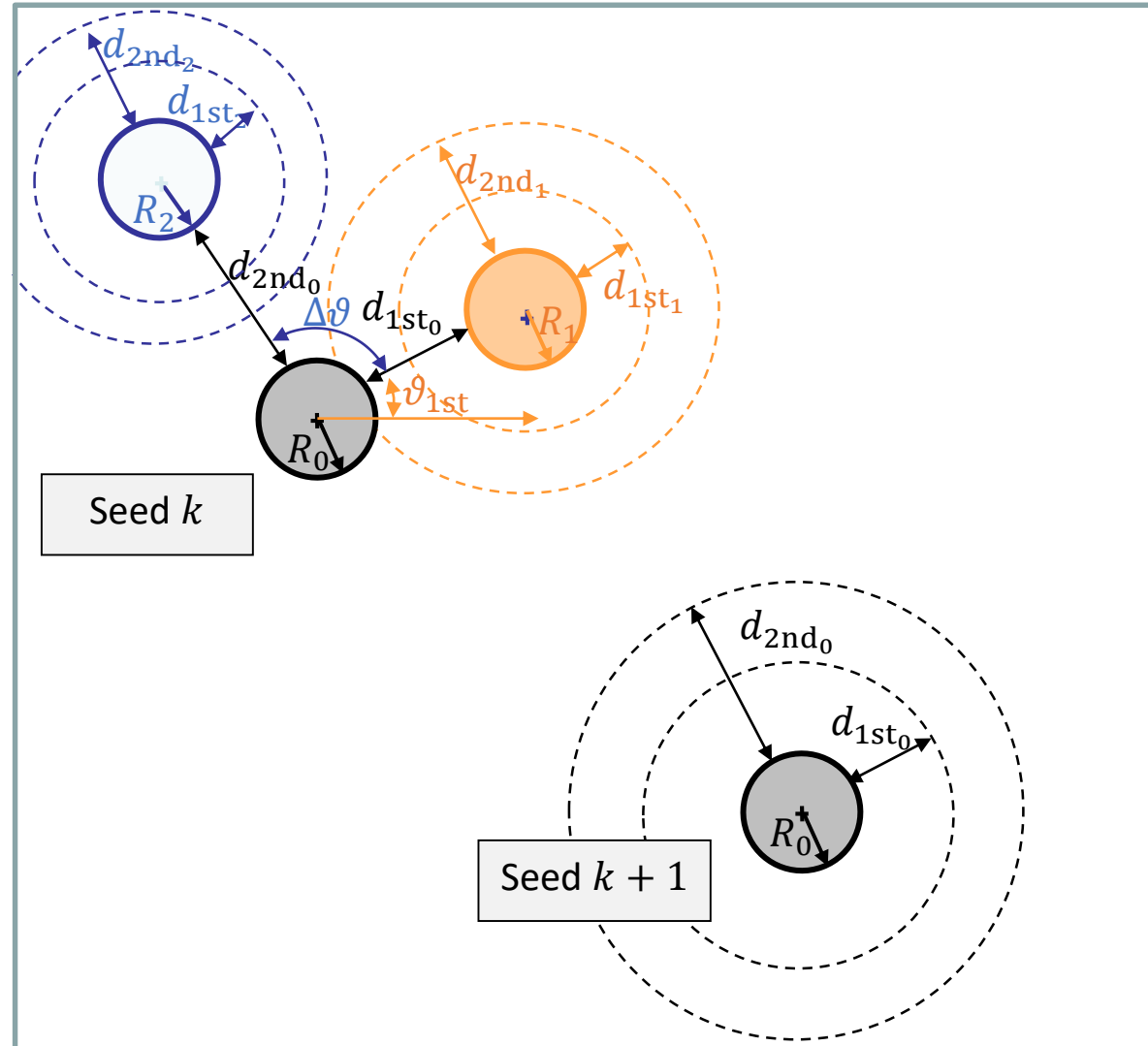
- The numerical micro-structure is generated by a fiber additive process

- 1) Define  $N$  seeds with first and second neighbors distances
- 2) Generate first neighbor with its own first and second neighbors distances



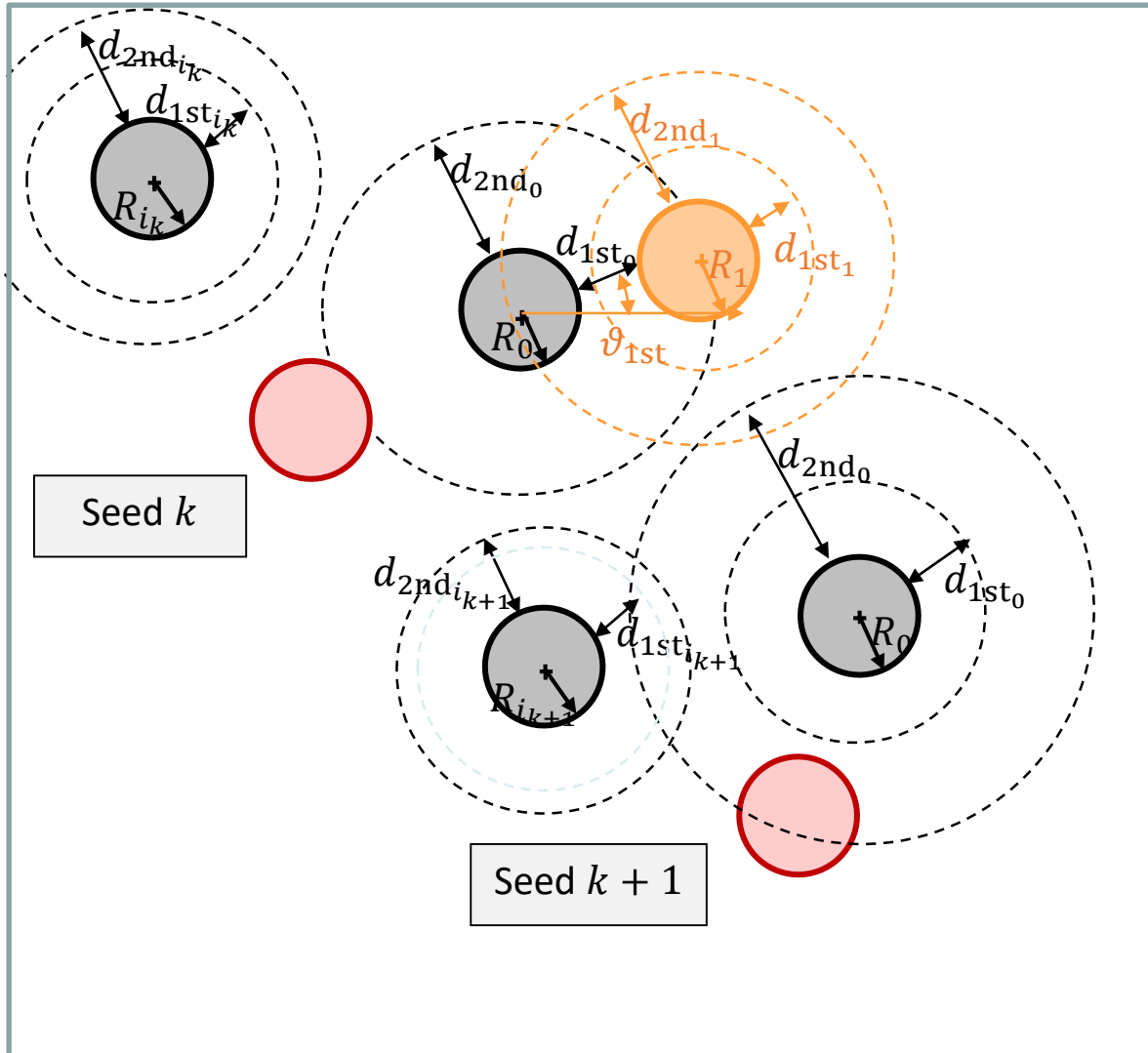
- The numerical micro-structure is generated by a fiber additive process

- 1) Define  $N$  seeds with first and second neighbors distances
- 2) Generate first neighbor with its own first and second neighbors distances
- 3) Generate second neighbor with its own first and second neighbors distances



- The numerical micro-structure is generated by a fiber additive process

- 1) Define  $N$  seeds with first and second neighbors distances
- 2) Generate first neighbor with its own first and second neighbors distances
- 3) Generate second neighbor with its own first and second neighbors distances
- 4) Change seeds & then change central fiber of the seeds

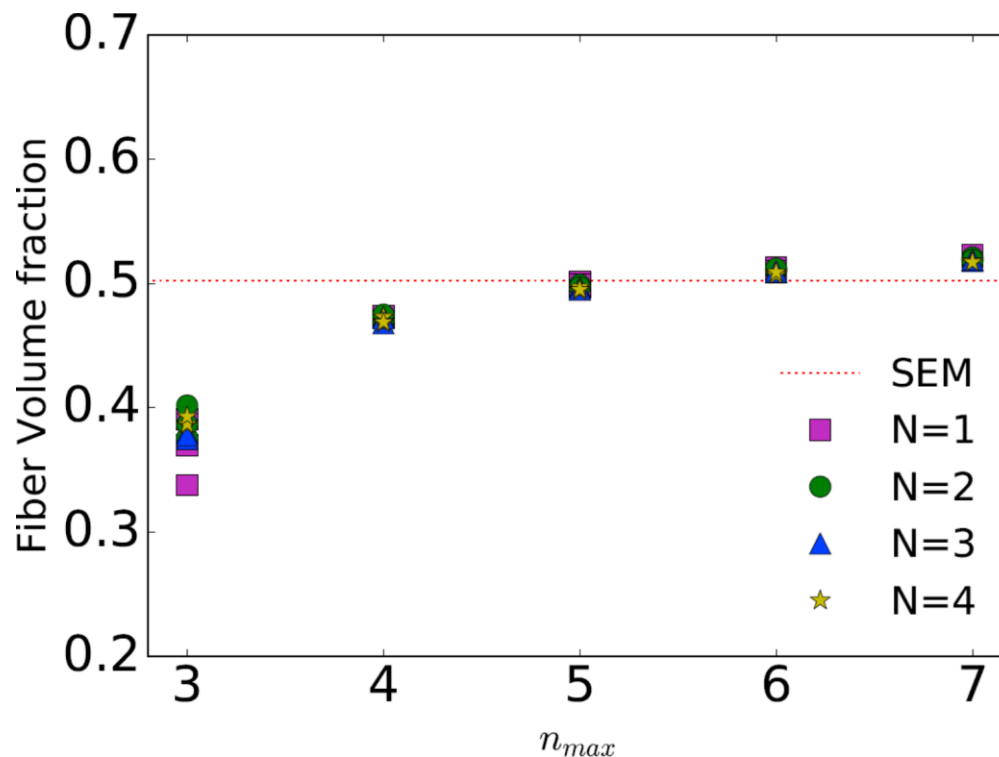




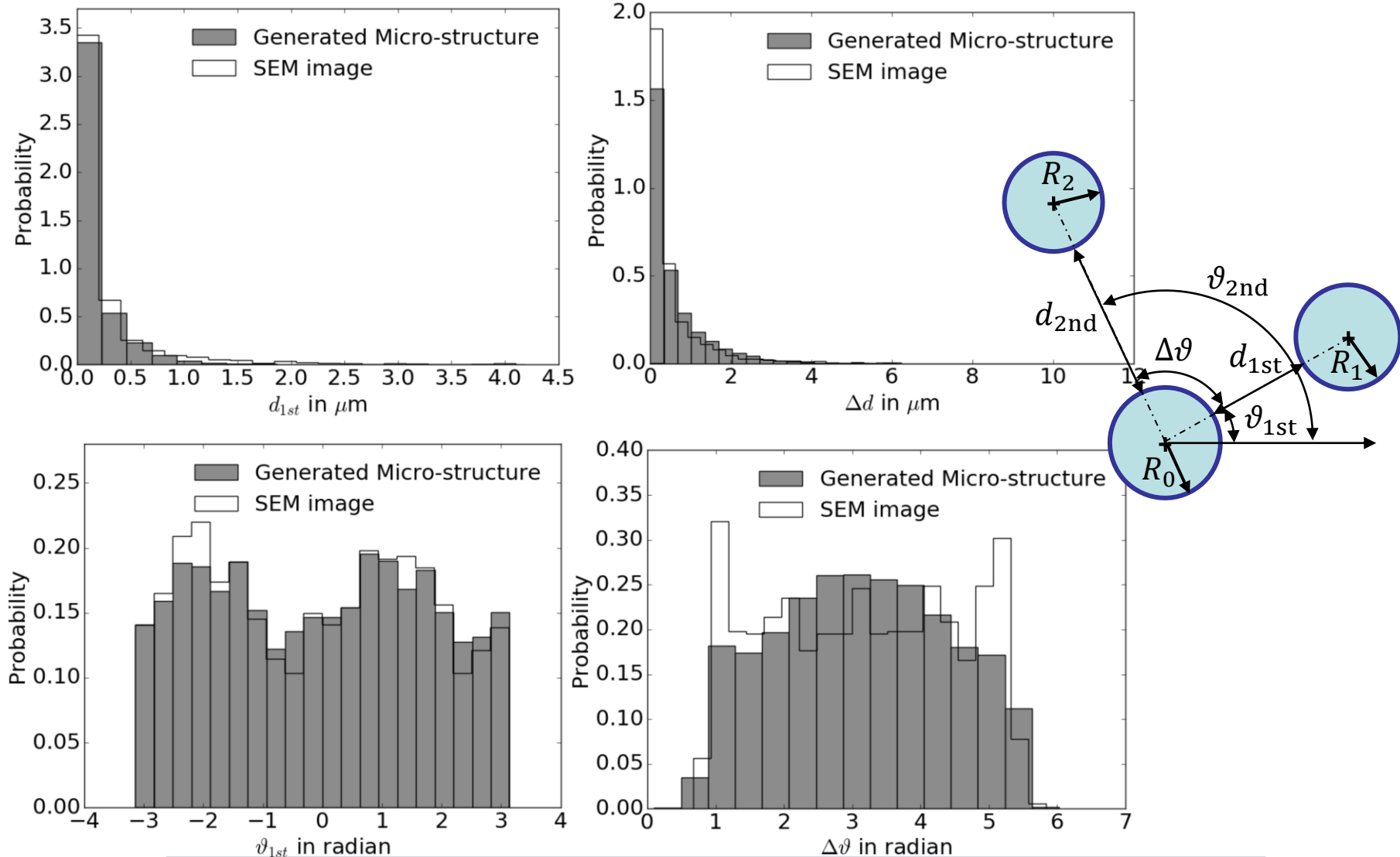
- The numerical micro-structure is generated by a fiber additive process
  - The effect of the initial number of seeds  $N$  and
  - The effect of the maximum regenerating times  $n_{\max}$  after rejecting a fiber due to overlap

SEM: Average  $V_f$  of 103 windows;

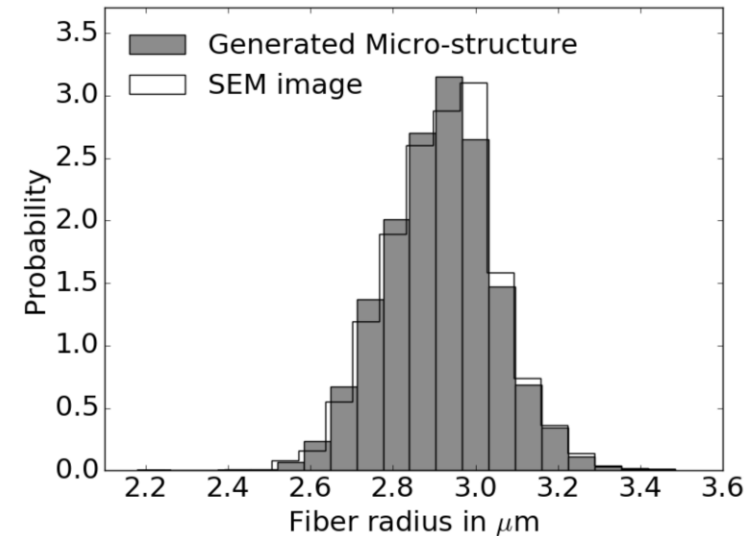
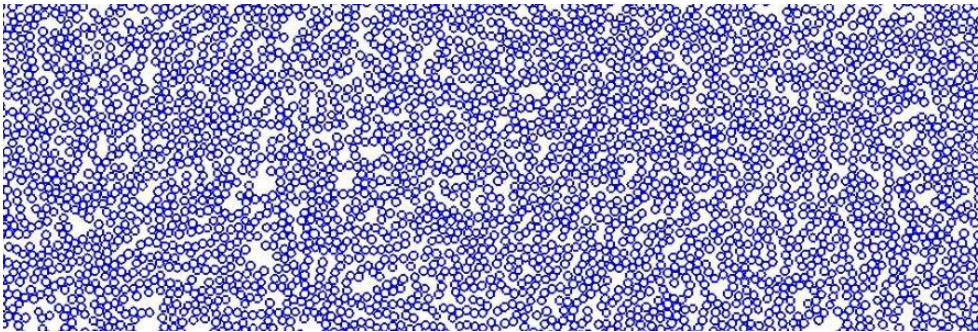
Numerical micro-structures: Average  $V_f$  of 104 windows.



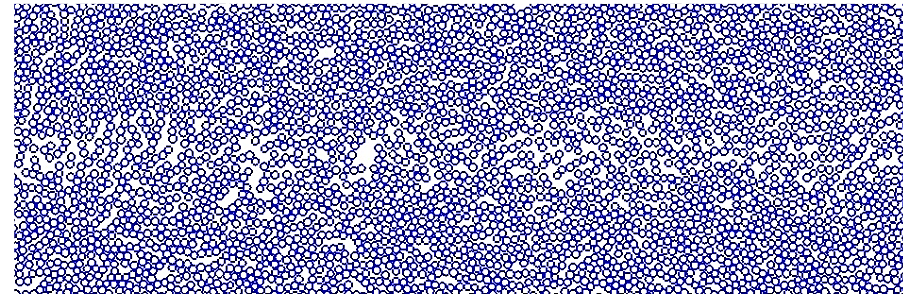
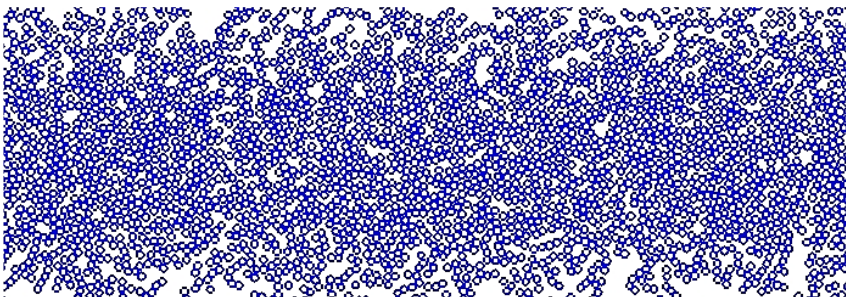
- Comparisons of fibers spatial information



- Numerical micro-structures are generated by a fiber additive process
  - Arbitrary size
  - Arbitrary number



- Possibility to generate non-homogenous distributions



- Stochastic homogenization

- Extraction of Stochastic Volume Elements

- 2 sizes considered:  $l_{\text{SVE}} = 10 \mu\text{m}$  &  $l_{\text{SVE}} = 25 \mu\text{m}$
- Window technique to capture correlation

$$R_{rs}(\tau) = \frac{\mathbb{E}[(r(\mathbf{x}) - \mathbb{E}(r))(s(\mathbf{x} + \boldsymbol{\tau}) - \mathbb{E}(s))]}{\sqrt{\mathbb{E}[(r - \mathbb{E}(r))^2]} \sqrt{\mathbb{E}[(s - \mathbb{E}(s))^2]}}$$

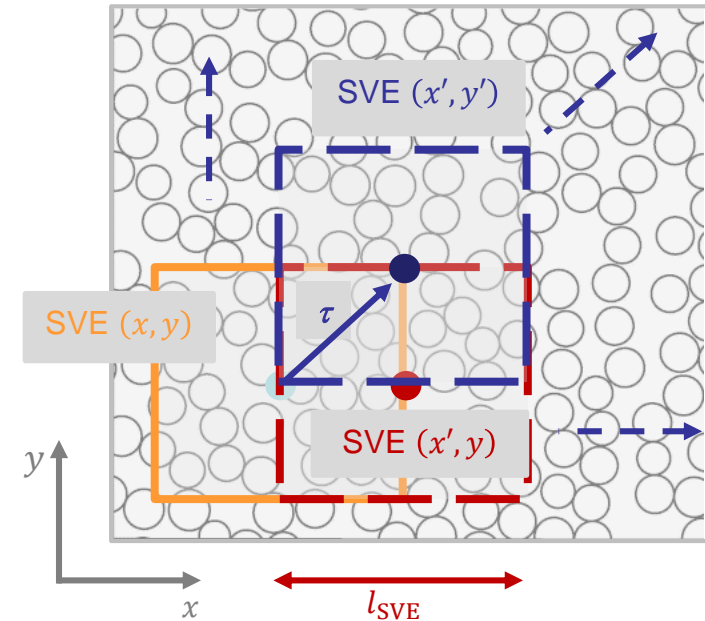
- For each SVE

- Extract apparent homogenized material tensor  $\mathbb{C}_M$

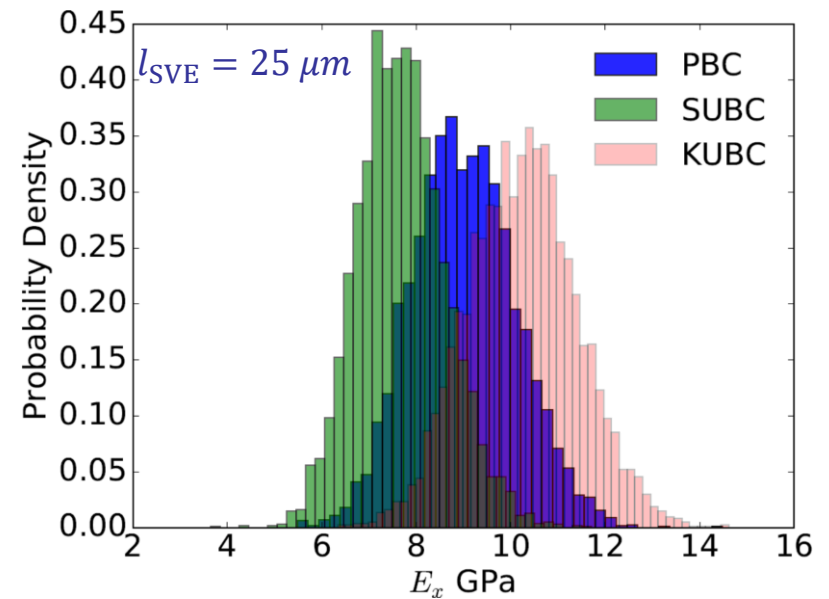
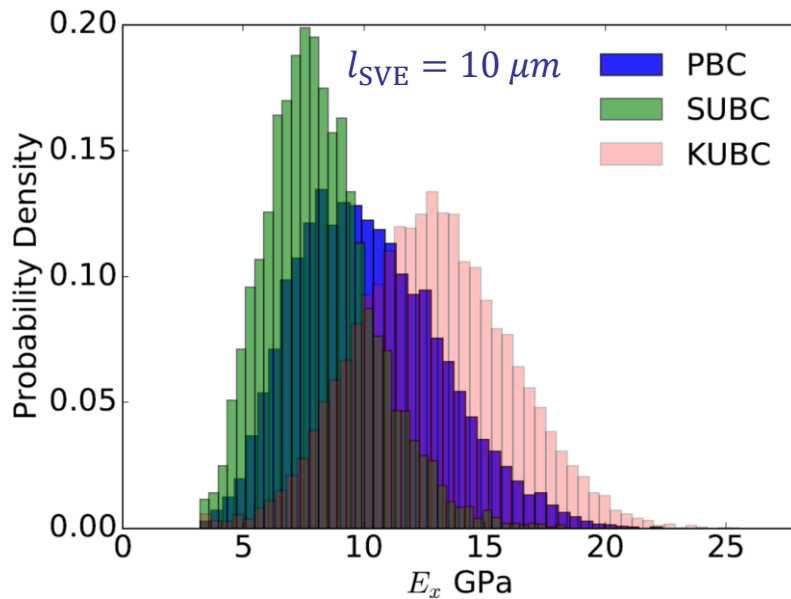
$$\begin{cases} \boldsymbol{\varepsilon}_M = \frac{1}{V(\omega)} \int_{\omega} \boldsymbol{\varepsilon}_m d\omega \\ \boldsymbol{\sigma}_M = \frac{1}{V(\omega)} \int_{\omega} \boldsymbol{\sigma}_m d\omega \\ \mathbb{C}_M = \frac{\partial \boldsymbol{\sigma}_M}{\partial \mathbf{u}_M \otimes \nabla_M} \end{cases}$$

- Consistent boundary conditions:

- Periodic (PBC)
- Minimum kinematics (SUBC)
- Kinematic (KUBC)



- Apparent properties



Increasing  $l_{SVE}$

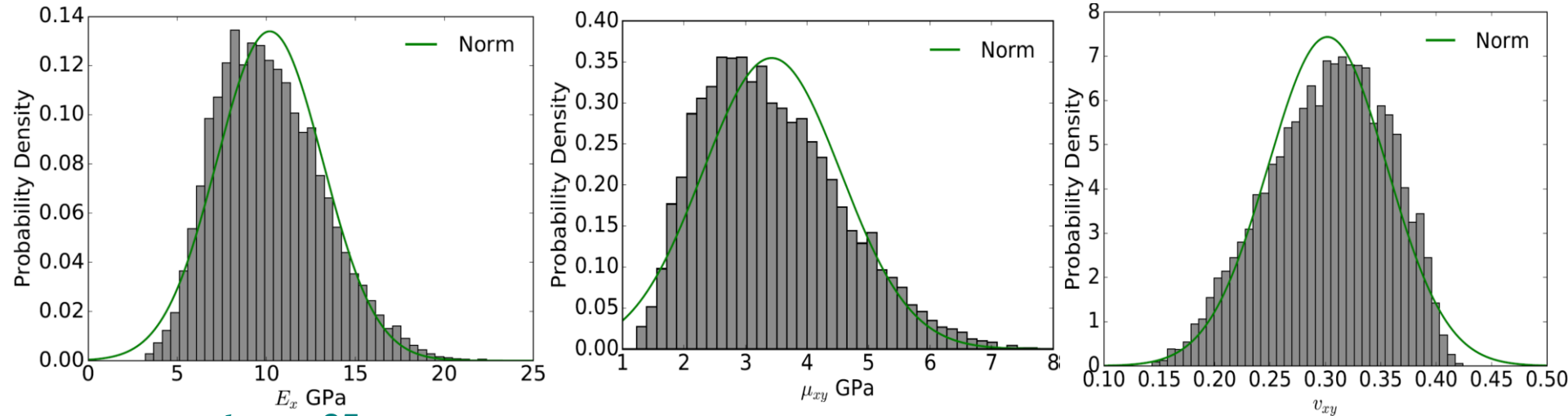
When  $l_{SVE}$  increases

- Average values for different BCs get closer (to PBC one)
- Distributions narrow
- Distributions get closer to normal

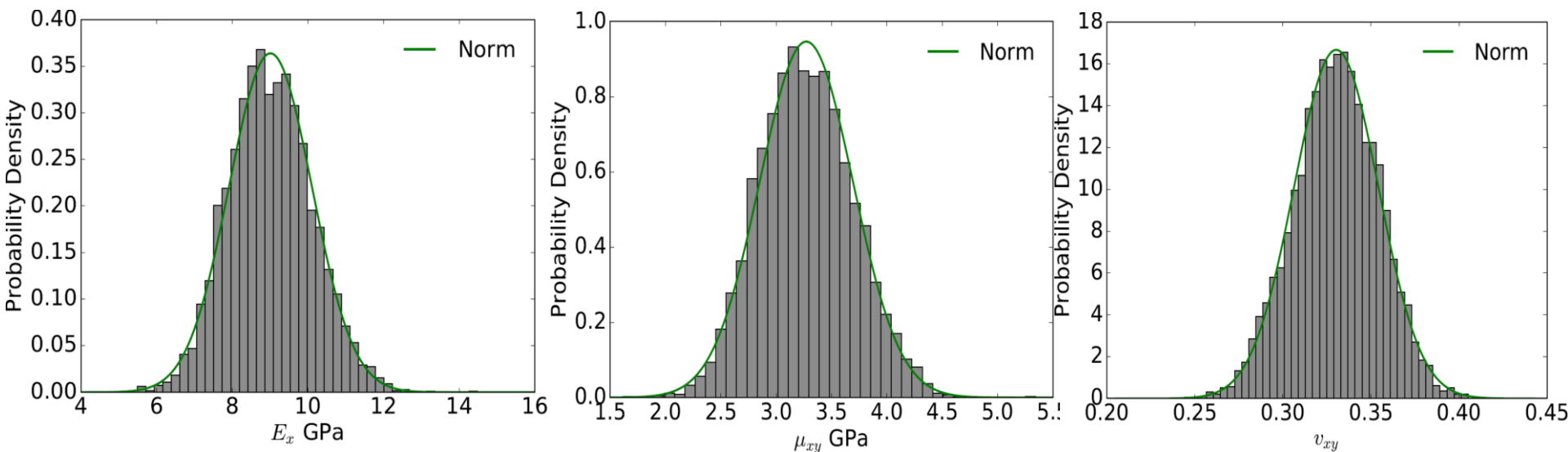
# Stochastic homogenization on the SVEs

- When  $l_{\text{SVE}}$  increases: marginal distributions of random properties closer to normal

–  $l_{\text{SVE}} = 10 \mu\text{m}$

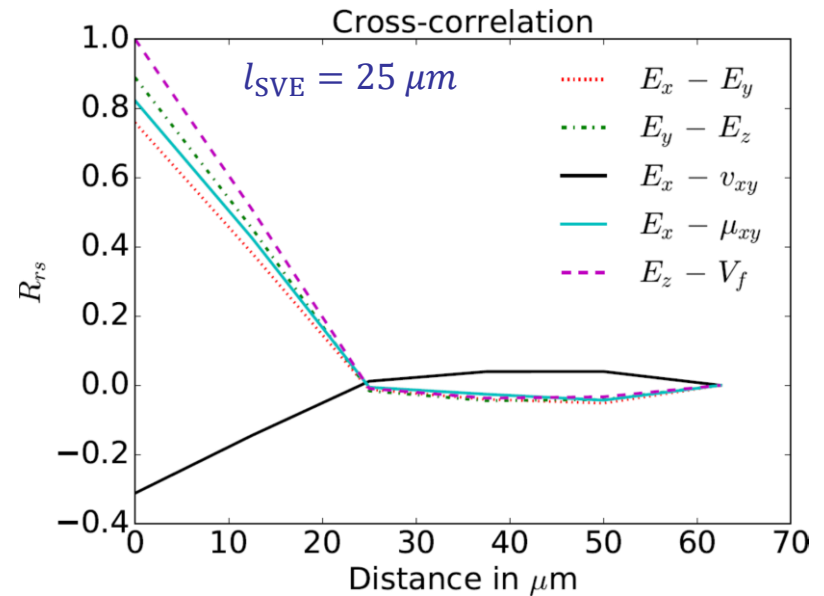
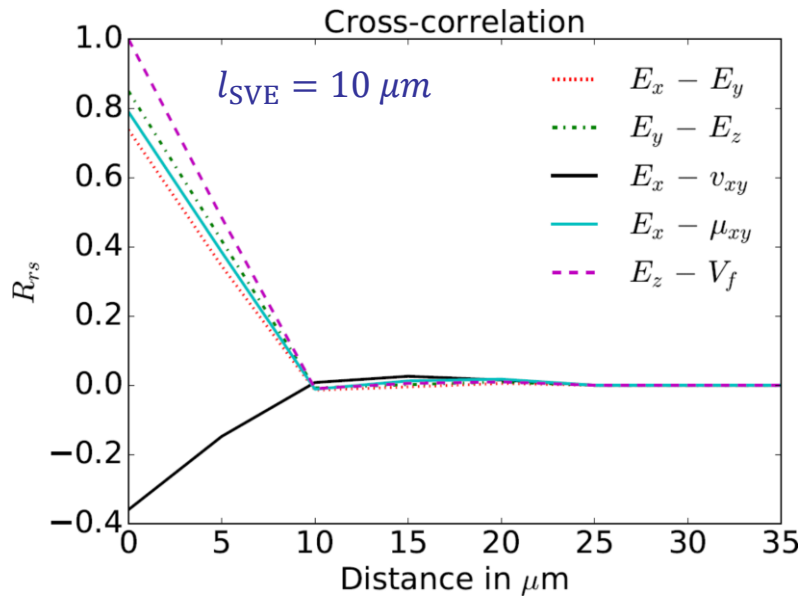


–  $l_{\text{SVE}} = 25 \mu\text{m}$





## Correlation



Increasing  $l_{\text{SVE}}$

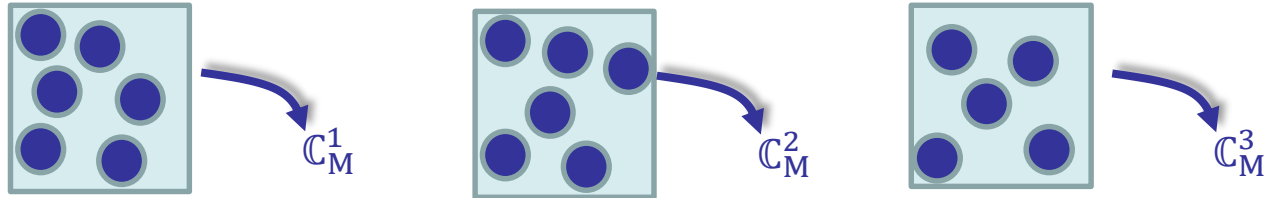
- (1) Auto/cross correlation vanishes at  $\tau = l_{\text{SVE}}$
- (2) When  $l_{\text{SVE}}$  increases, distributions get closer to normal

(1)+(2) Apparent properties are independent random variables  
However the distribution depend on

- $l_{\text{SVE}}$
- The boundary conditions

- Stochastic model of the anisotropic elasticity tensor

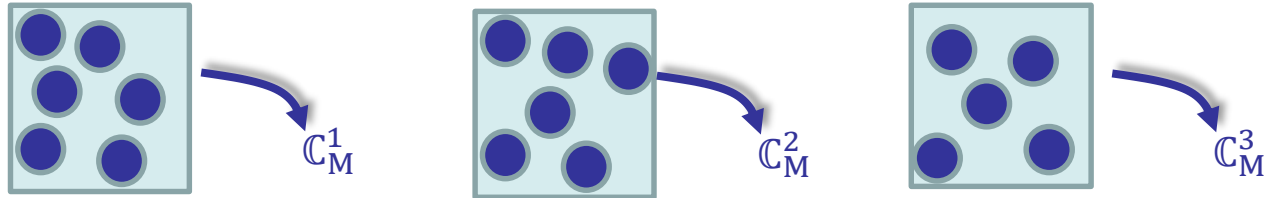
- Extract (uncorrelated) tensor realizations  $\mathbb{C}_M^i$



- Represent each realization  $\mathbb{C}_M^i$  by a vector  $\mathcal{V}$  of 9 (dependent)  $\mathcal{V}^{(r)}$  variables
- Generate random vectors  $\mathcal{V}$  using the Copula method

- Stochastic model of the anisotropic elasticity tensor

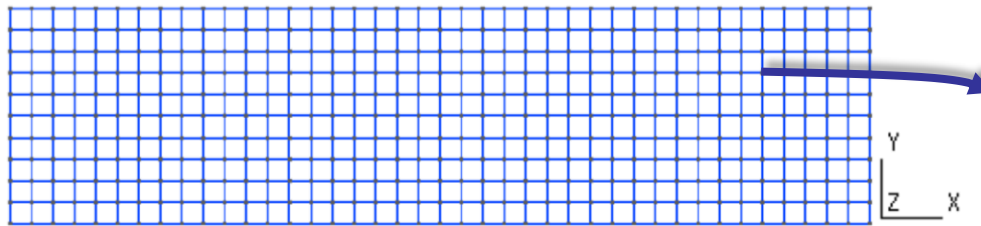
- Extract (uncorrelated) tensor realizations  $\mathbb{C}_M^i$



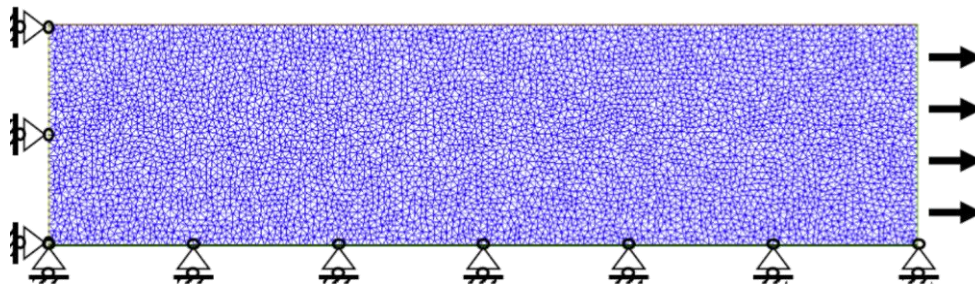
- Represent each realization  $\mathbb{C}_M^i$  by a vector  $\mathcal{V}$  of 9 (dependent)  $\mathcal{V}^{(r)}$  variables
- Generate random vectors  $\mathcal{V}$  using the Copula method

- Simulations require two discretizations

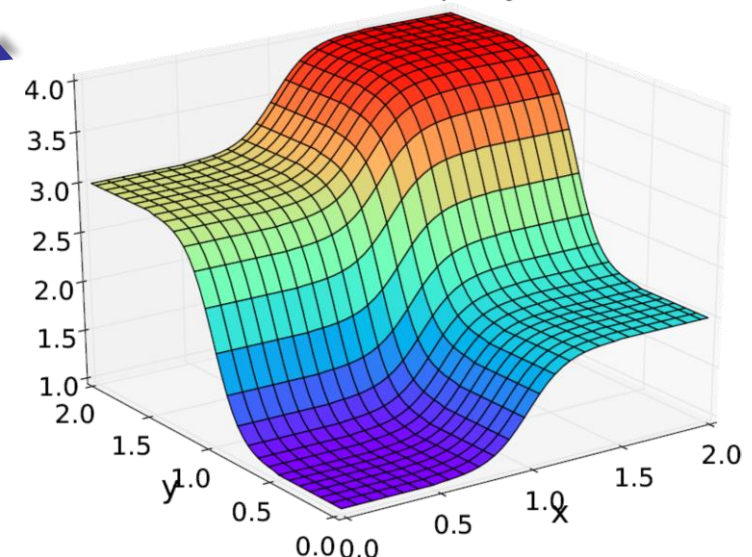
- Random vector field discretization



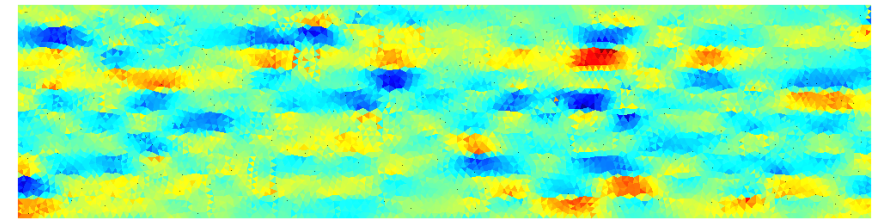
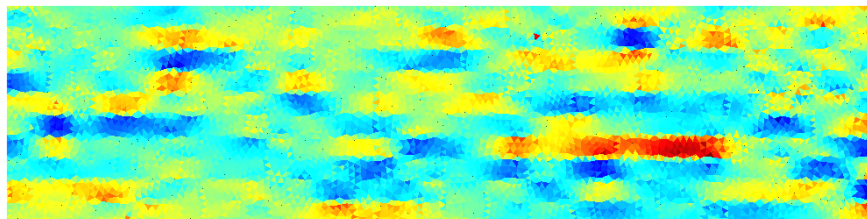
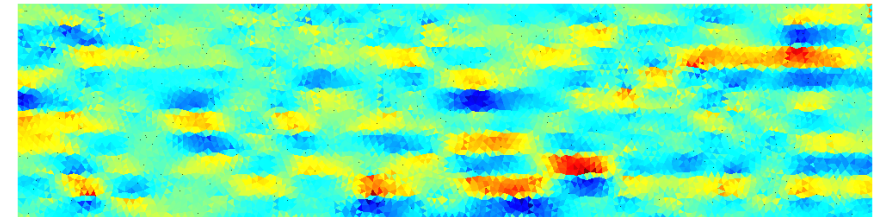
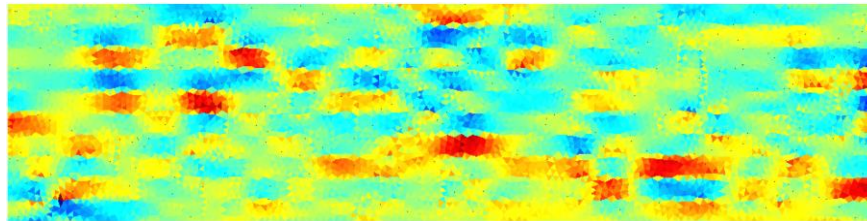
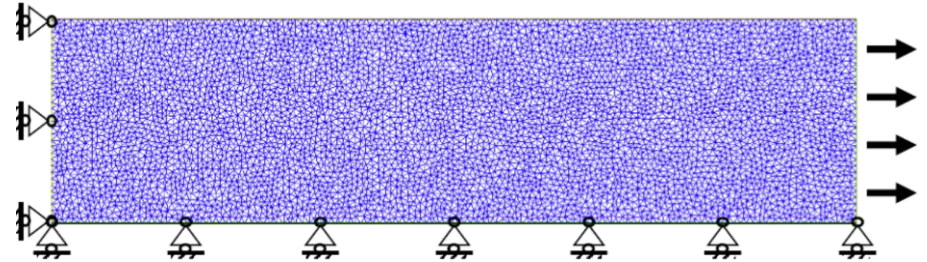
- Finite element discretization



Material Property



- Ply loading realizations
  - Non-uniform homogenized stress distributions
  - Different realizations yield different solutions



- Mean-Field-homogenization (MFH)

- Linear composites

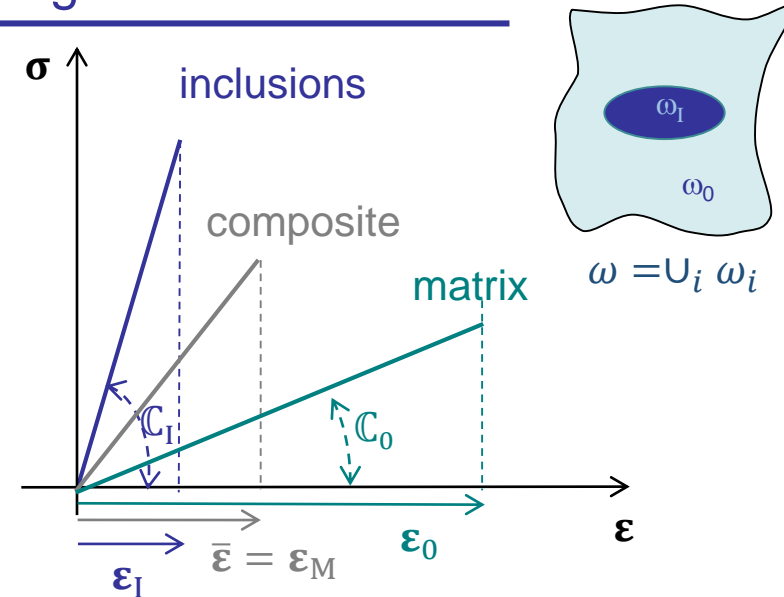
$$\left\{ \begin{array}{l} \boldsymbol{\sigma}_M = \bar{\boldsymbol{\sigma}} = v_0 \boldsymbol{\sigma}_0 + v_I \boldsymbol{\sigma}_I \\ \boldsymbol{\varepsilon}_M = \bar{\boldsymbol{\varepsilon}} = v_0 \boldsymbol{\varepsilon}_0 + v_I \boldsymbol{\varepsilon}_I \\ \boldsymbol{\varepsilon}_I = \mathbf{B}^\varepsilon(I, \mathbb{C}_0, \mathbb{C}_I) : \boldsymbol{\varepsilon}_0 \end{array} \right.$$

→  $\hat{\mathbb{C}}_M = \hat{\mathbb{C}}_M(I, \mathbb{C}_0, \mathbb{C}_I, v_I)$

- We use Mori-Tanaka assumption for  $\mathbf{B}^\varepsilon(I, \mathbb{C}_0, \mathbb{C}_I)$

- Stochastic MFH

- How to define random vectors  $\mathcal{V}_{MT}$  of  $I, \mathbb{C}_0, \mathbb{C}_I, v_I$  ?





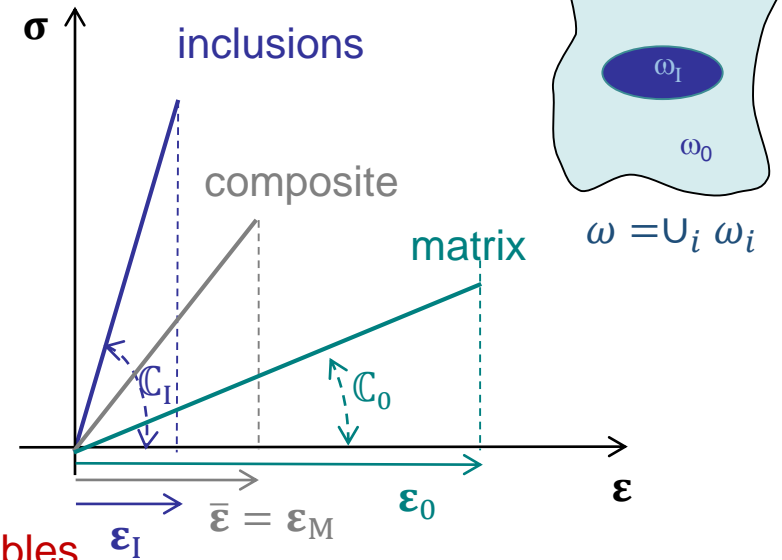
- Mean-Field-homogenization (MFH)

- Linear composites

$$\begin{cases} \sigma_M = \bar{\sigma} = v_0 \sigma_0 + v_I \sigma_I \\ \varepsilon_M = \bar{\varepsilon} = v_0 \varepsilon_0 + v_I \varepsilon_I \\ \varepsilon_I = \mathbf{B}^\varepsilon(I, \mathbb{C}_0, \mathbb{C}_I) : \varepsilon_0 \end{cases}$$

$$\hat{\mathbb{C}}_M = \hat{\mathbb{C}}_M(I, \mathbb{C}_0, \mathbb{C}_I, v_I)$$

Defined as random variables



- Consider an equivalent system

- For each SVE realization  $i$ :

$\mathbb{C}_M$  and  $v_I$  known

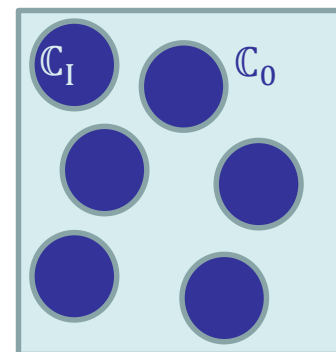
- Anisotropy from  $\mathbb{C}_M^i$

$\theta$  is evaluated

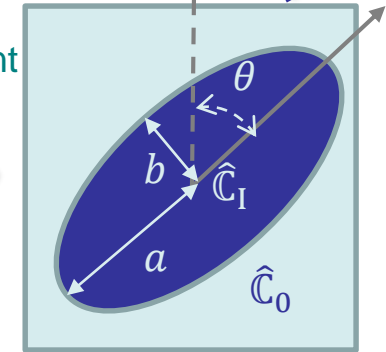
- Fiber behavior uniform

$\hat{\mathbb{C}}_I$  for one SVE

$$\mathbb{C}_M \simeq \hat{\mathbb{C}}_M(\hat{I}, \hat{\mathbb{C}}_0, \hat{\mathbb{C}}_I, v_I, \theta)$$



Equivalent inclusion



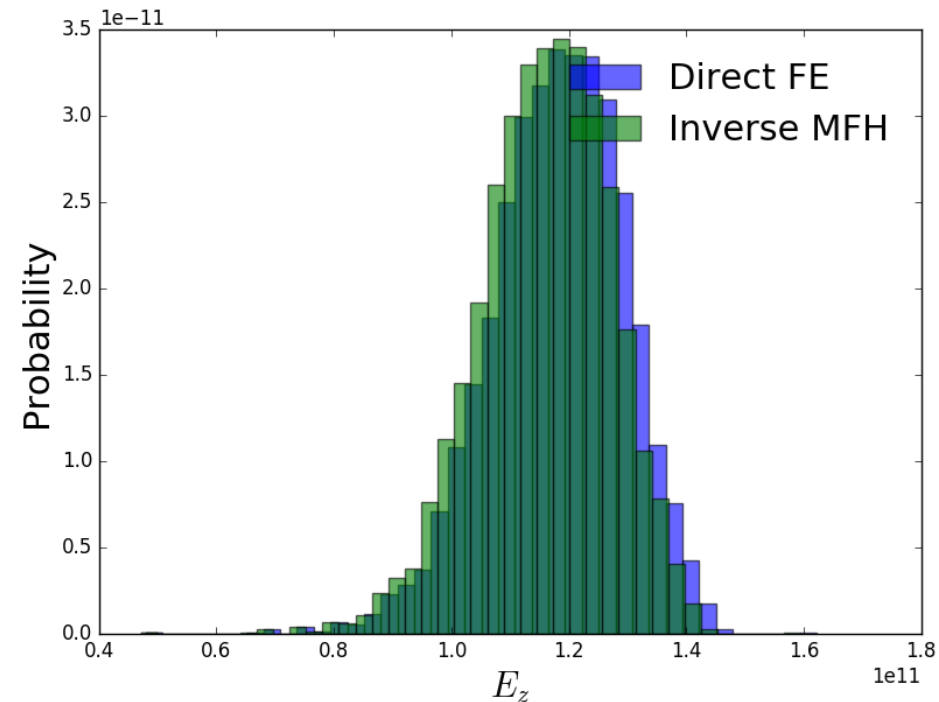
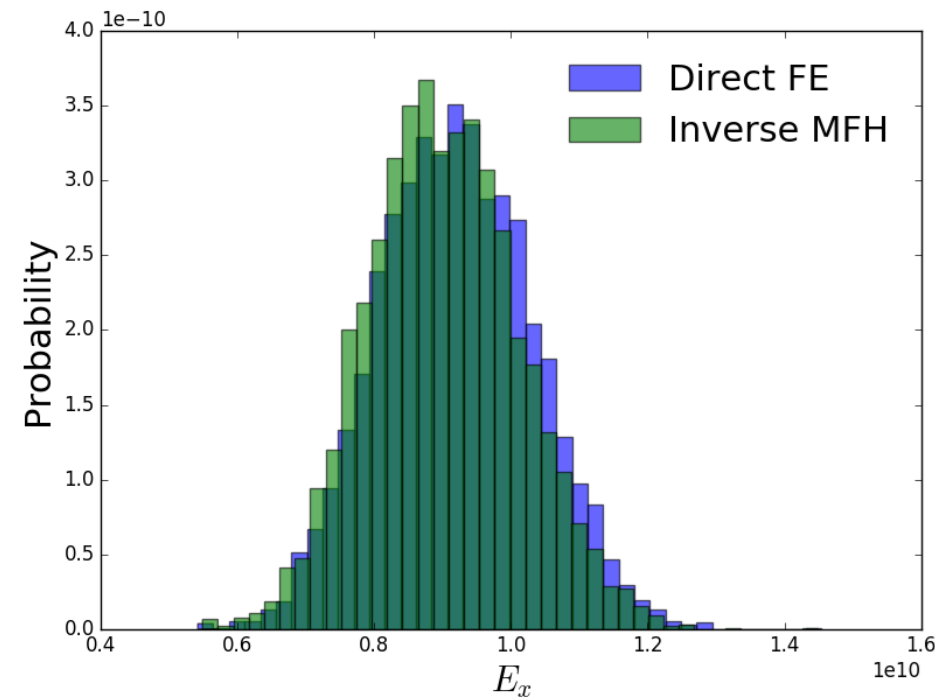
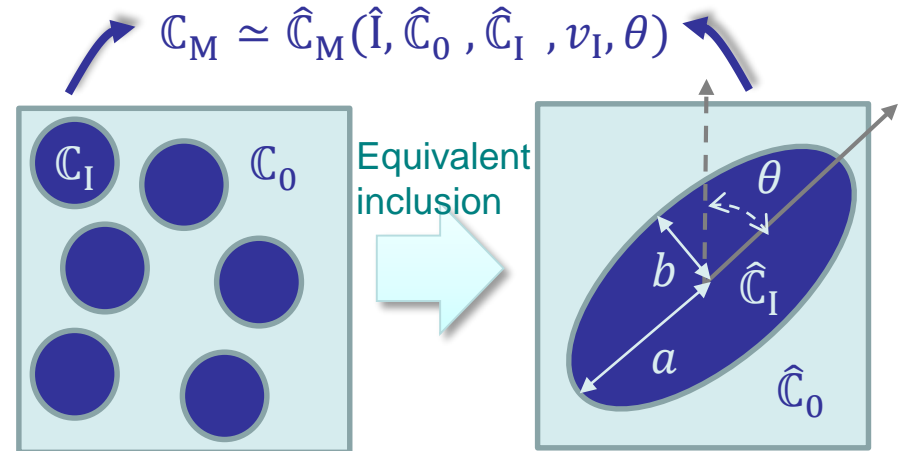
- Remaining optimization problem:

$$\min_{\frac{a}{b}, \hat{E}_0, \hat{\nu}_0} \left\| \mathbb{C}_M - \hat{\mathbb{C}}_M\left(\frac{a}{b}, \hat{E}_0, \hat{\nu}_0; v_I, \theta, \hat{\mathbb{C}}_I\right) \right\|$$



# Stochastic Mean-Field Homogenization

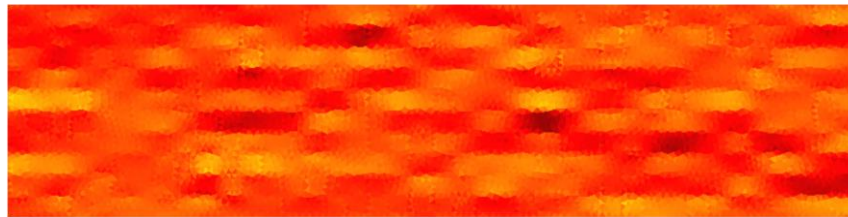
- Inverse stochastic identification
  - Comparison of homogenized properties from SVE realizations and stochastic MFH



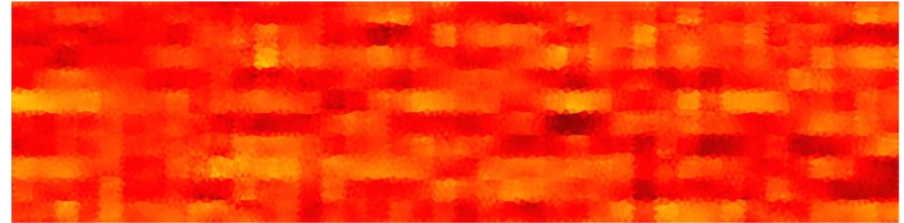
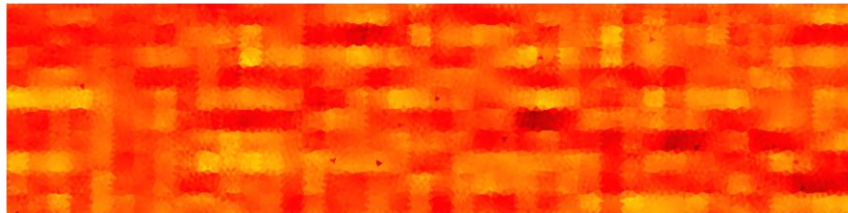
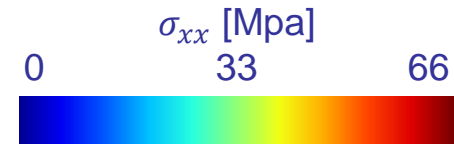
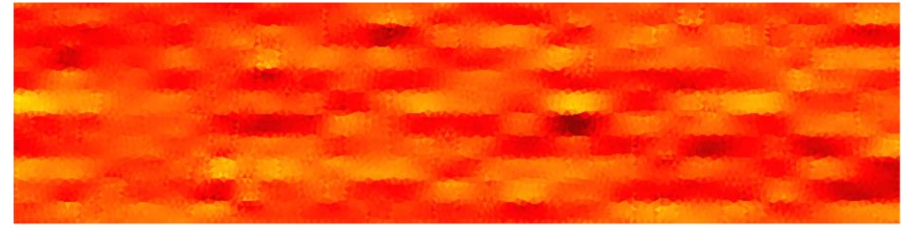
# Stochastic Mean-Field Homogenization

- Comparison Random fields vs. Stochastic elastic MFH

Random anisotropic material tensor



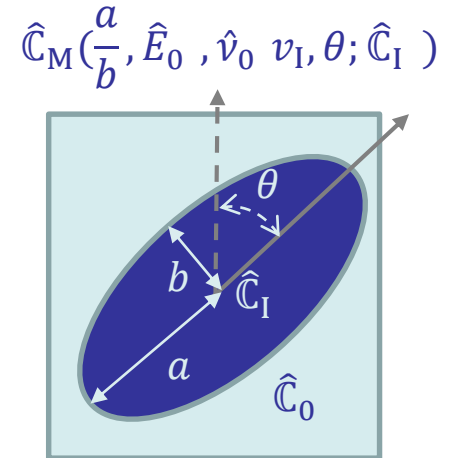
Stochastic MFH



# Stochastic Mean-Field Homogenization

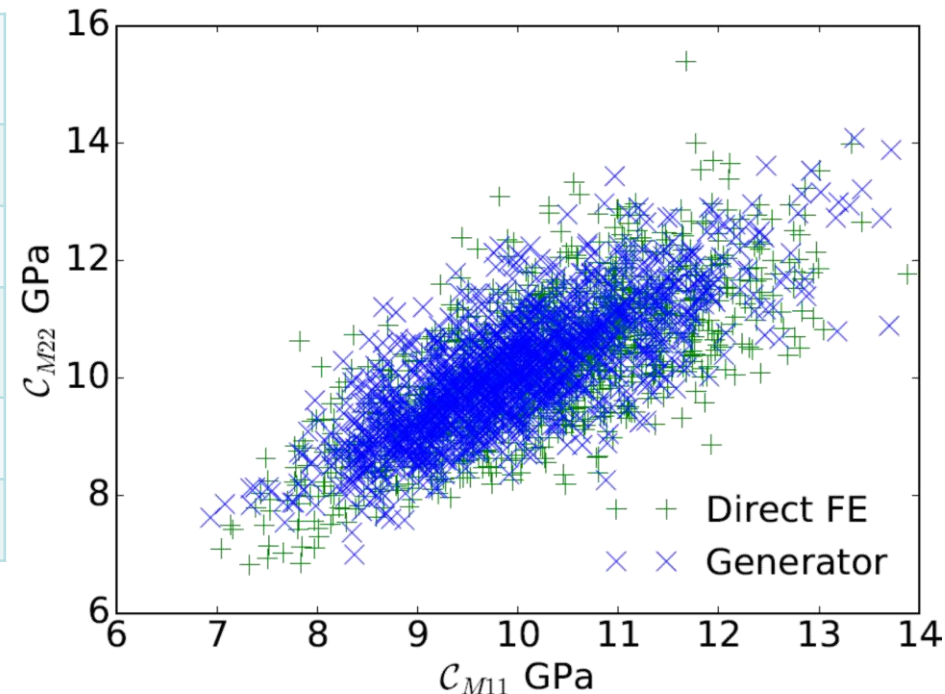
- Stochastic MFH model:

- Homogenized properties  $\hat{\mathbb{C}}_M(\frac{a}{b}, \hat{E}_0, \hat{\nu}_0, v_I, \theta; \hat{\mathbb{C}}_I)$
- Random vectors  $\mathcal{V}_{MT}$ 
  - Realizations  $v_{MT} = \{\frac{a}{b}, \hat{E}_0, \hat{\nu}_0, v_I, \theta\}$
  - Characterized by the distance correlation matrix
  - Generator using the copula method



	$v_I$	$\theta$	$\frac{a}{b}$	$\hat{E}_0$	$\hat{\nu}_0$
$v_I$	1.0	0.015	0.114	0.523	0.499
$\theta$		1.0	0.092	0.016	0.014
$\frac{a}{b}$			1.0	0.080	0.076
$\hat{E}_0$				1.0	0.661
$\hat{\nu}_0$					1.0

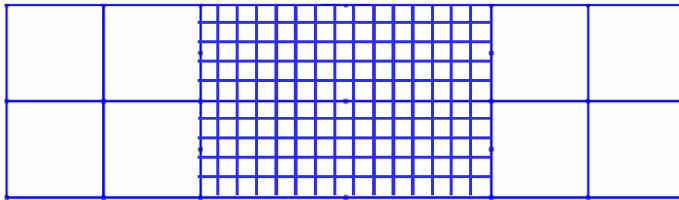
Distances correlation matrix



# Stochastic Mean-Field Homogenization

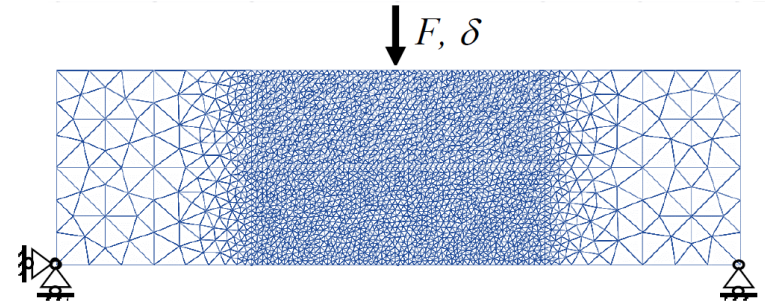
- Stochastic simulations

- 2 discretization: Random field  $\mathcal{V}_{MT}$

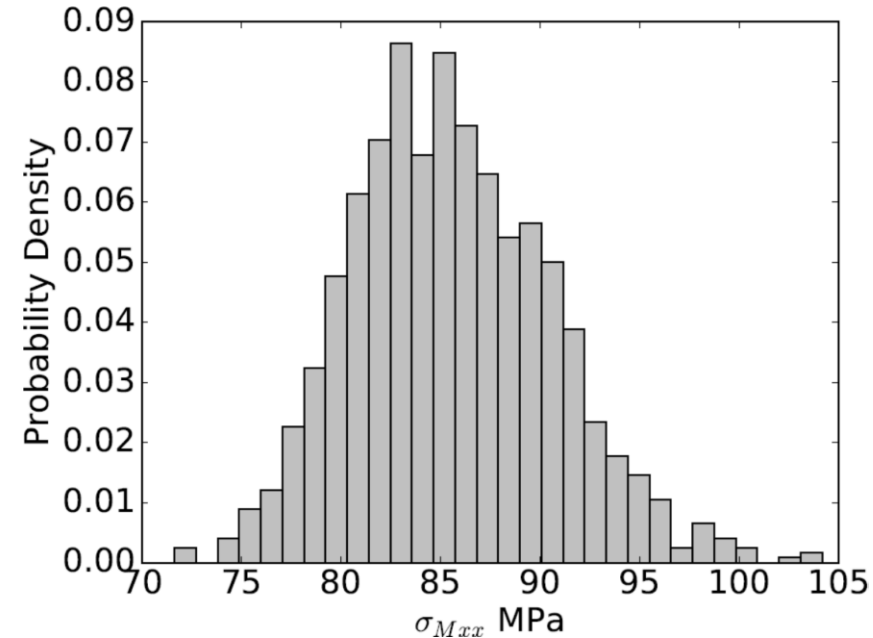
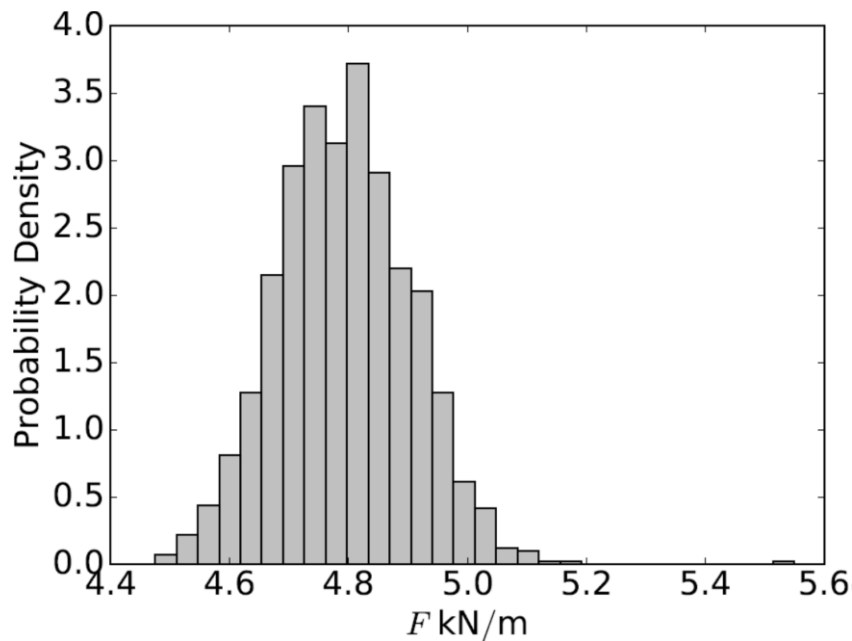


&

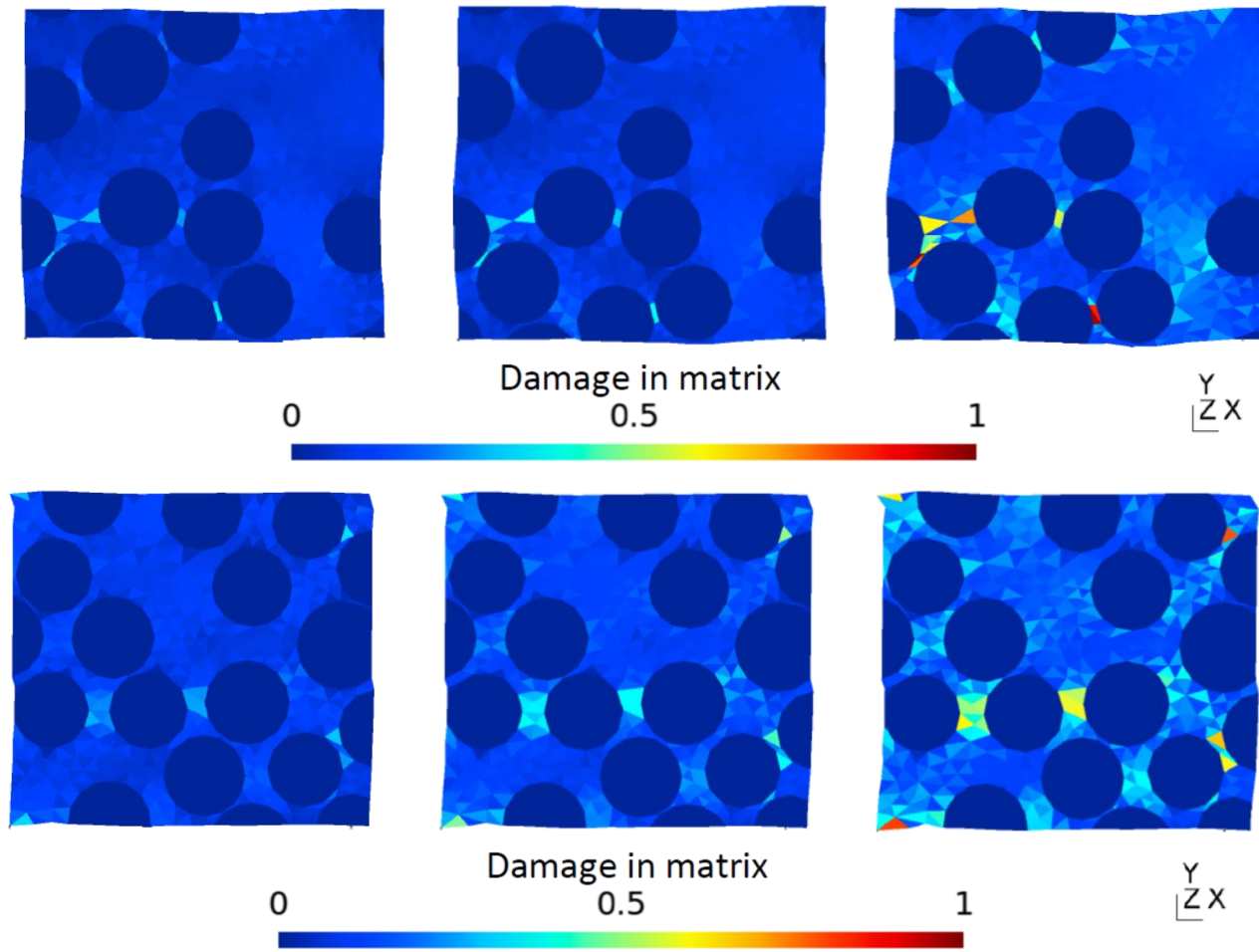
Stochastic finite-elements



- Realizations to reach a given deflection  $\delta$



- Non-linear SVE simulations



# Non-linear stochastic Mean-Field Homogenization

- Non-linear Mean-Field-homogenization

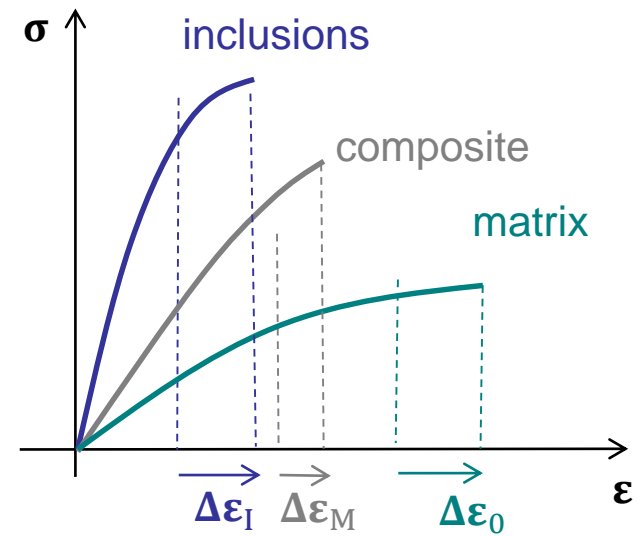
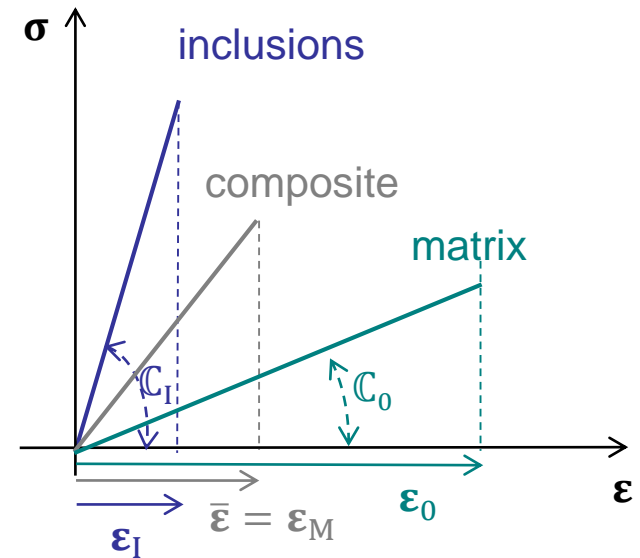
- Linear composites

$$\left\{ \begin{array}{l} \sigma_M = \bar{\sigma} = v_0 \sigma_0 + v_I \sigma_I \\ \varepsilon_M = \bar{\varepsilon} = v_0 \varepsilon_0 + v_I \varepsilon_I \\ \varepsilon_I = \mathbf{B}^\varepsilon(I, \mathbb{C}_0, \mathbb{C}_I) : \varepsilon_0 \end{array} \right.$$

- Non-linear composites

$$\left\{ \begin{array}{l} \sigma_M = \bar{\sigma} = v_0 \sigma_0 + v_I \sigma_I \\ \Delta \varepsilon_M = \bar{\Delta \varepsilon} = v_0 \Delta \varepsilon_0 + v_I \Delta \varepsilon_I \\ \Delta \varepsilon_I = \mathbf{B}^\varepsilon(I, \mathbb{C}_0^{LCC}, \mathbb{C}_I^{LCC}) : \Delta \varepsilon_0 \end{array} \right.$$

Define a linear comparison composite material

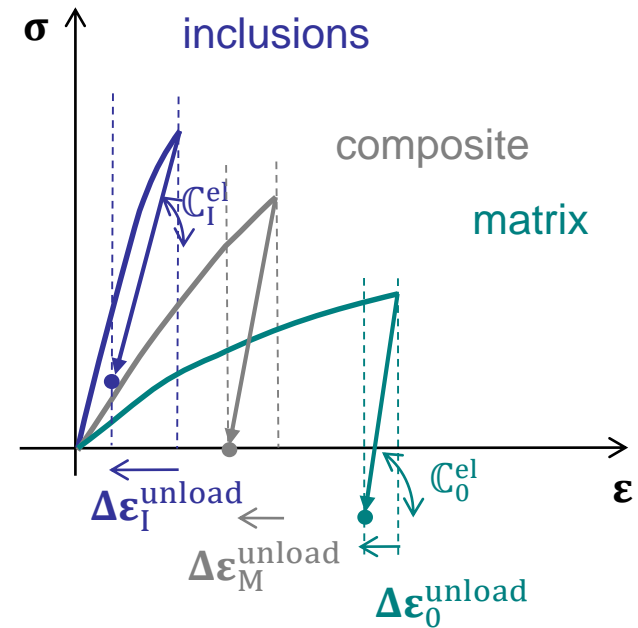




# Non-linear stochastic Mean-Field Homogenization

- Incremental-secant Mean-Field-homogenization

- Virtual elastic unloading from previous state
  - Composite material unloaded to reach the stress-free state
  - Residual stress in components



# Non-linear stochastic Mean-Field Homogenization

- Incremental-secant Mean-Field-homogenization

- Virtual elastic unloading from previous state
  - Composite material unloaded to reach the stress-free state
  - Residual stress in components

- Define Linear Comparison Composite

- From unloaded state

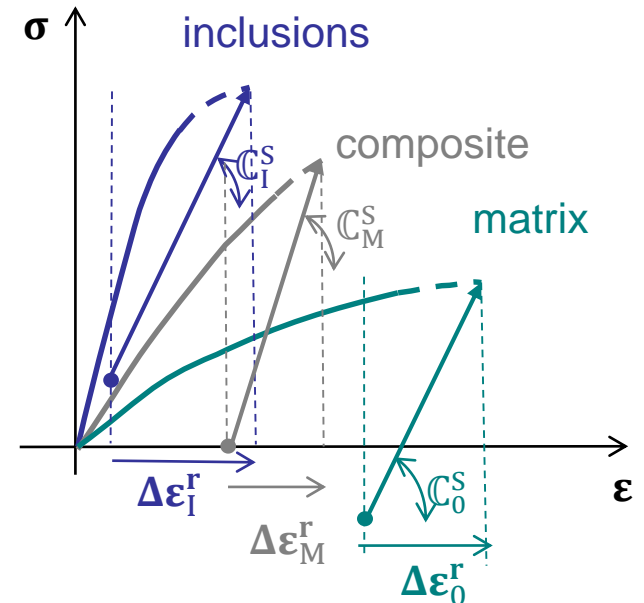
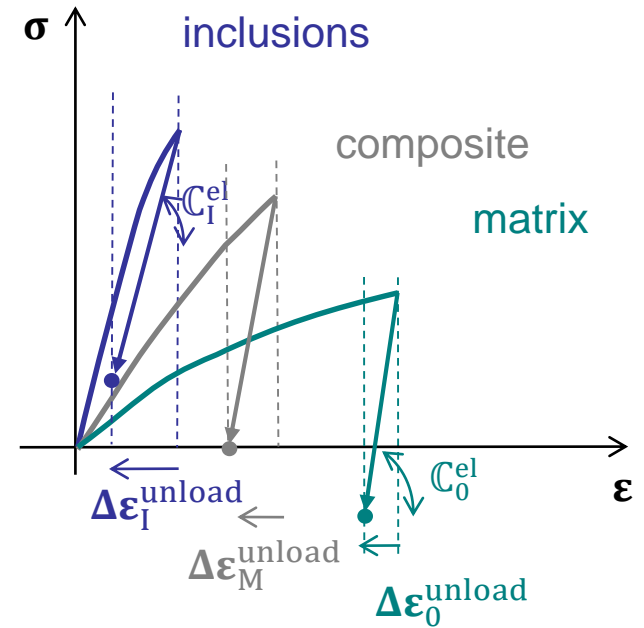
$$\Delta \boldsymbol{\varepsilon}_{I/0}^r = \Delta \boldsymbol{\varepsilon}_{I/0} + \Delta \boldsymbol{\varepsilon}_{I/0}^{\text{unload}}$$

- Incremental-secant loading

$$\left\{ \begin{array}{l} \boldsymbol{\sigma}_M = \bar{\boldsymbol{\sigma}} = v_0 \boldsymbol{\sigma}_0 + v_I \boldsymbol{\sigma}_I \\ \Delta \boldsymbol{\varepsilon}_M^r = \bar{\Delta \boldsymbol{\varepsilon}} = v_0 \Delta \boldsymbol{\varepsilon}_0^r + v_I \Delta \boldsymbol{\varepsilon}_I^r \\ \Delta \boldsymbol{\varepsilon}_I^r = \mathbf{B}^\varepsilon(I, \mathbb{C}_0^S, \mathbb{C}_I^S) : \Delta \boldsymbol{\varepsilon}_0^r \end{array} \right.$$

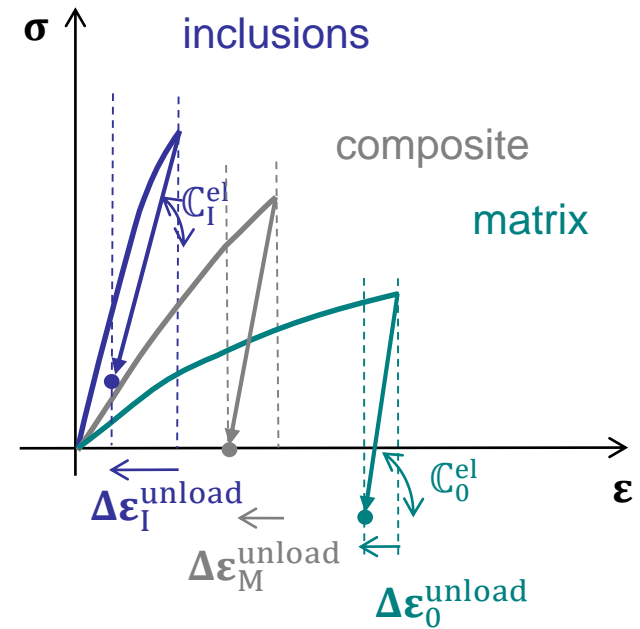
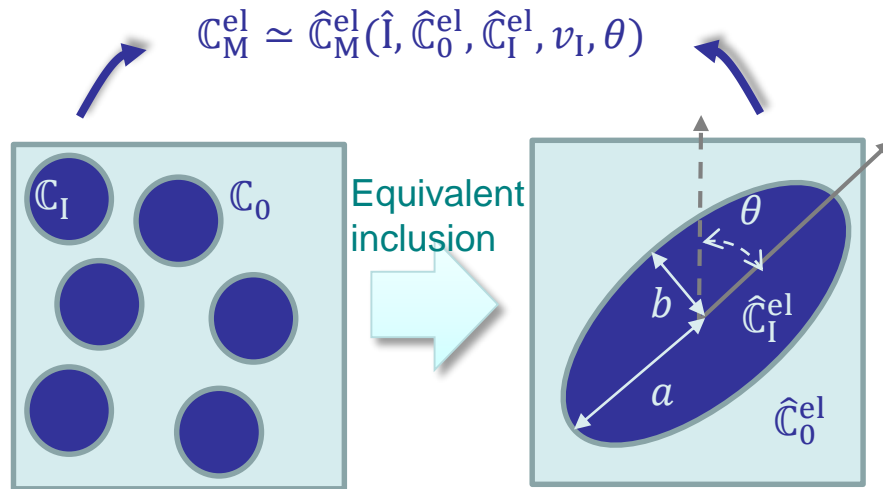
- Incremental secant operator

$$\Rightarrow \Delta \boldsymbol{\sigma}_M = \mathbb{C}_M^S(I, \mathbb{C}_0^S, \mathbb{C}_I^S, v_I) : \Delta \boldsymbol{\varepsilon}_M^r$$



# Non-linear stochastic Mean-Field Homogenization

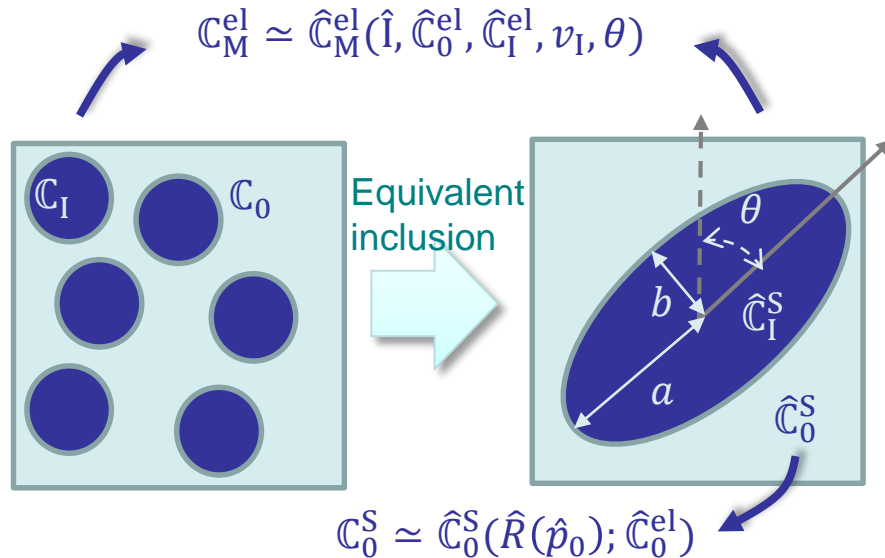
- Non-linear inverse identification
  - First step from elastic response



# Non-linear stochastic Mean-Field Homogenization

- Non-linear inverse identification

- First step from elastic response



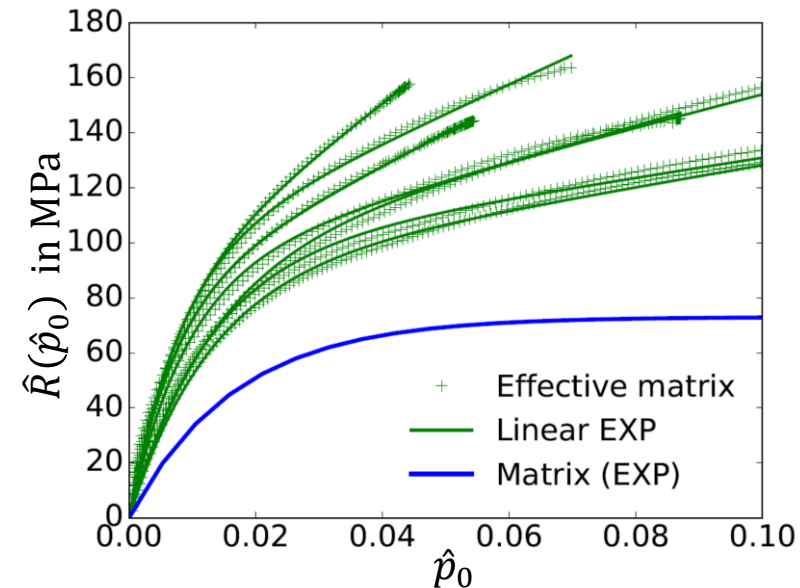
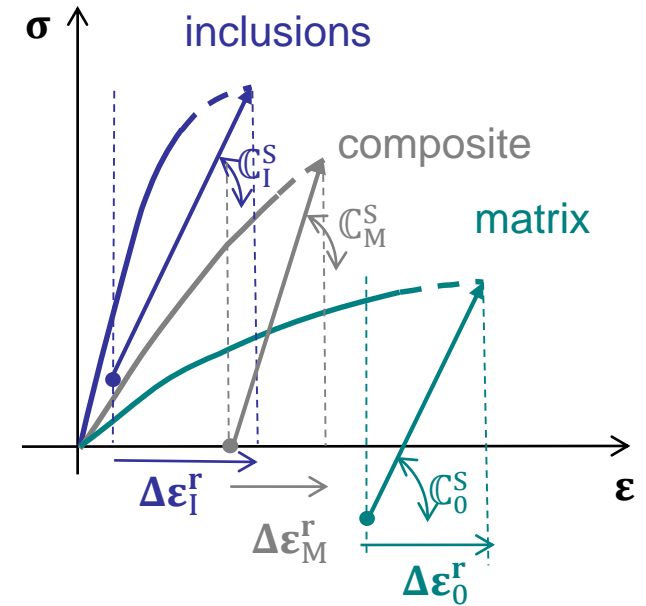
- Second step from the LCC

- New optimization problem

$$\Delta \sigma_M \simeq \hat{\mathbb{C}}_M^S(\hat{\mathbf{I}}, \hat{\mathbb{C}}_0^S, \mathbb{C}_I^S, v_I, \theta) : \Delta \epsilon_M^r$$

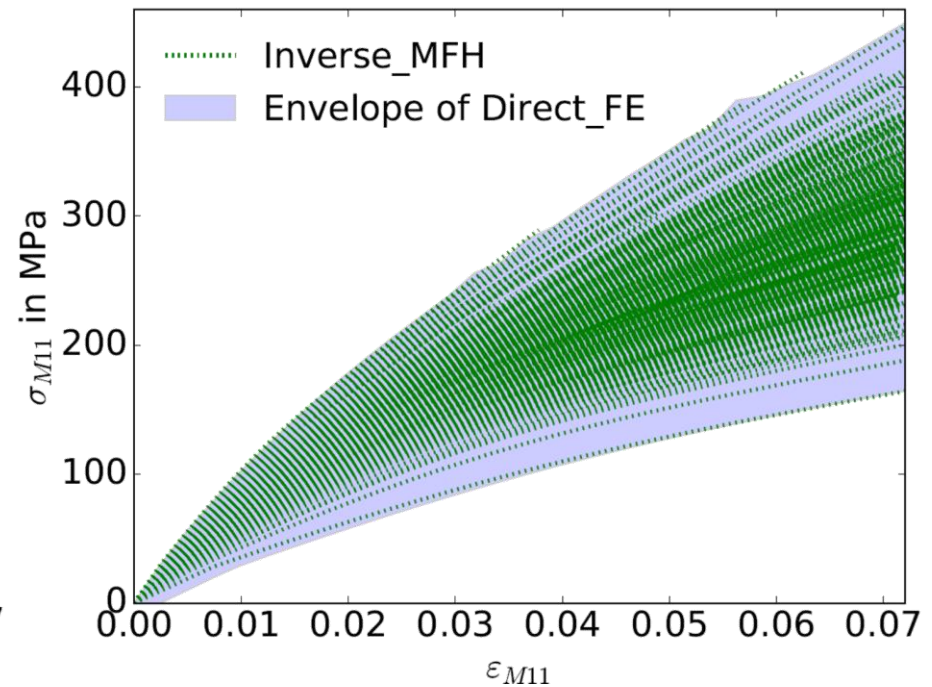
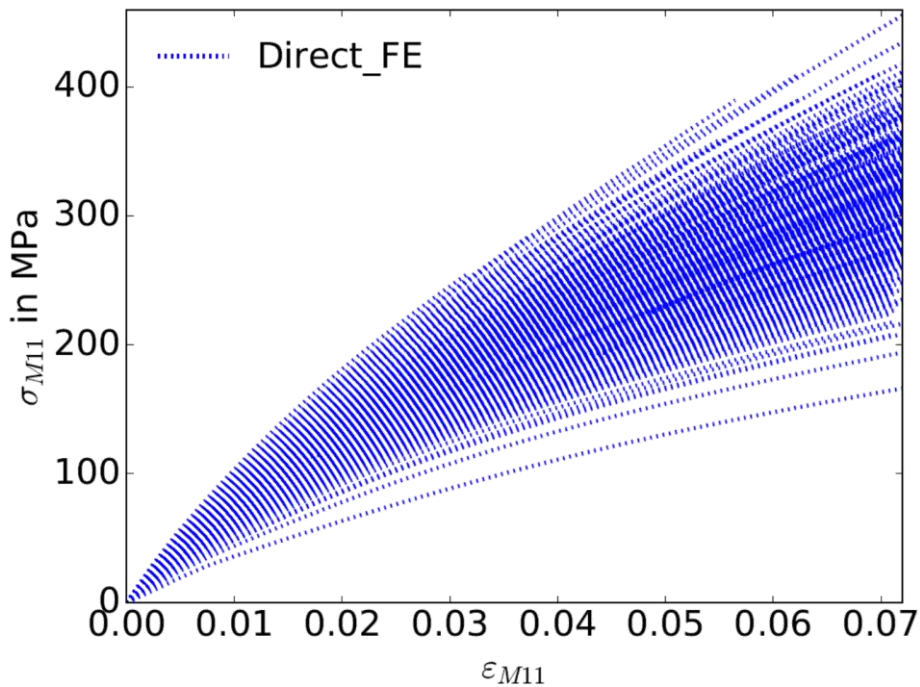
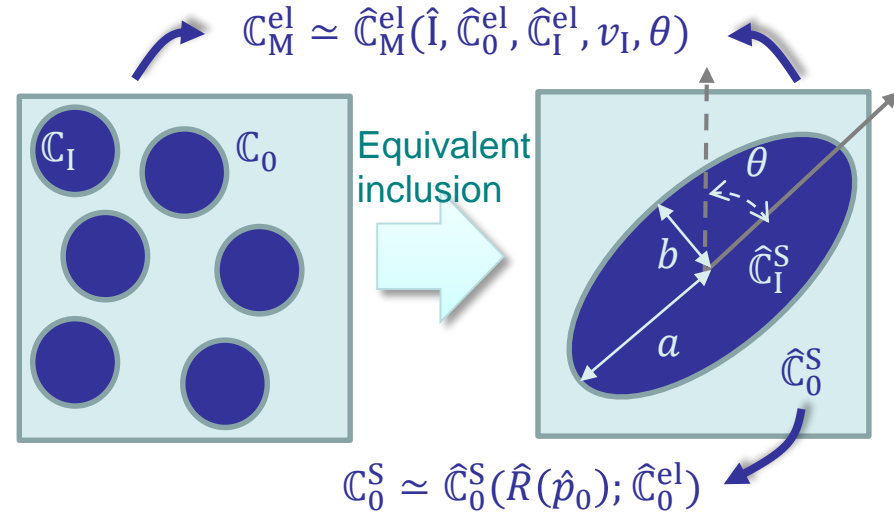
- Extract the equivalent hardening  $\hat{R}(\hat{p}_0)$  from the incremental secant tensor

$$\mathbb{C}_0^S \simeq \hat{\mathbb{C}}_0^S(\hat{R}(\hat{p}_0); \hat{\mathbb{C}}_0^{\text{el}})$$



# Non-linear stochastic Mean-Field Homogenization

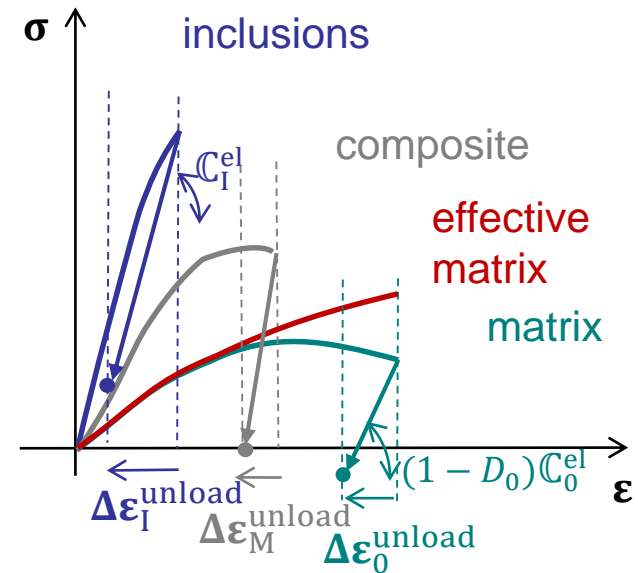
- Non-linear inverse identification
  - Comparison SVE vs. MFH



# Non-linear stochastic Mean-Field Homogenization

- Damage-enhanced Mean-Field-homogenization

- Virtual elastic unloading from previous state
  - Composite material unloaded to reach the stress-free state
  - Residual stress in components



# Non-linear stochastic Mean-Field Homogenization

- Damage-enhanced Mean-Field-homogenization

- Virtual elastic unloading from previous state
  - Composite material unloaded to reach the stress-free state
  - Residual stress in components

- Define Linear Comparison Composite

- From elastic state

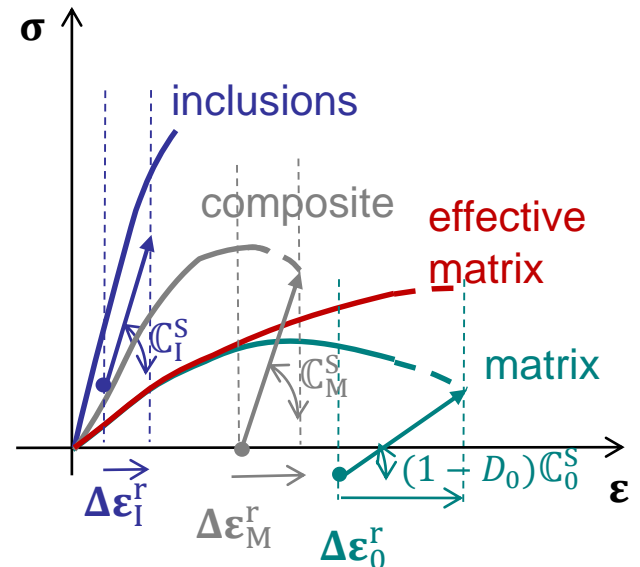
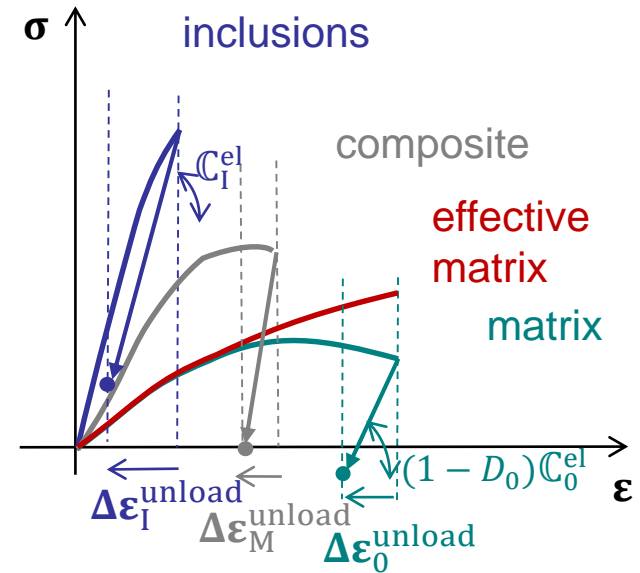
$$\Delta \boldsymbol{\varepsilon}_{I/0}^r = \Delta \boldsymbol{\varepsilon}_{I/0} + \Delta \boldsymbol{\varepsilon}_{I/0}^{\text{unload}}$$

- Incremental-secant loading

$$\left\{ \begin{array}{l} \boldsymbol{\sigma}_M = \bar{\boldsymbol{\sigma}} = v_0 \boldsymbol{\sigma}_0 + v_I \boldsymbol{\sigma}_I \\ \Delta \boldsymbol{\varepsilon}_M^r = \bar{\Delta \boldsymbol{\varepsilon}} = v_0 \Delta \boldsymbol{\varepsilon}_0^r + v_I \Delta \boldsymbol{\varepsilon}_I^r \\ \Delta \boldsymbol{\varepsilon}_I^r = \mathbf{B}^\varepsilon(I, (1 - D_0) \mathbb{C}_0^S, \mathbb{C}_I^S) : \Delta \boldsymbol{\varepsilon}_0^r \end{array} \right.$$

- Incremental secant operator

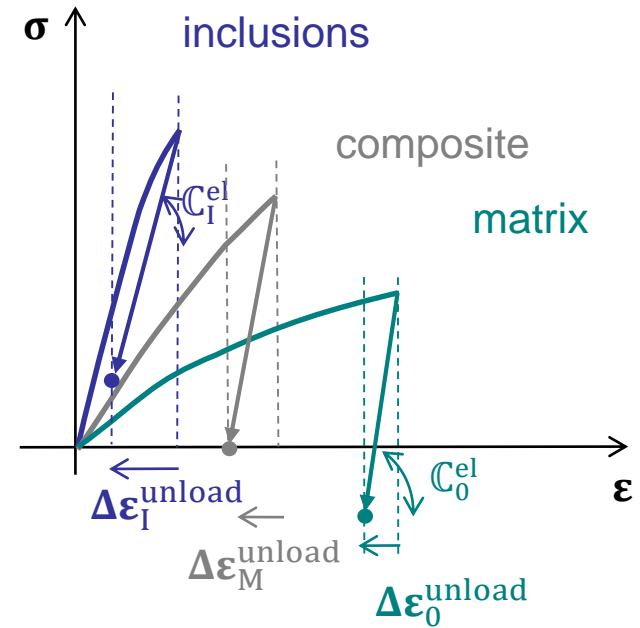
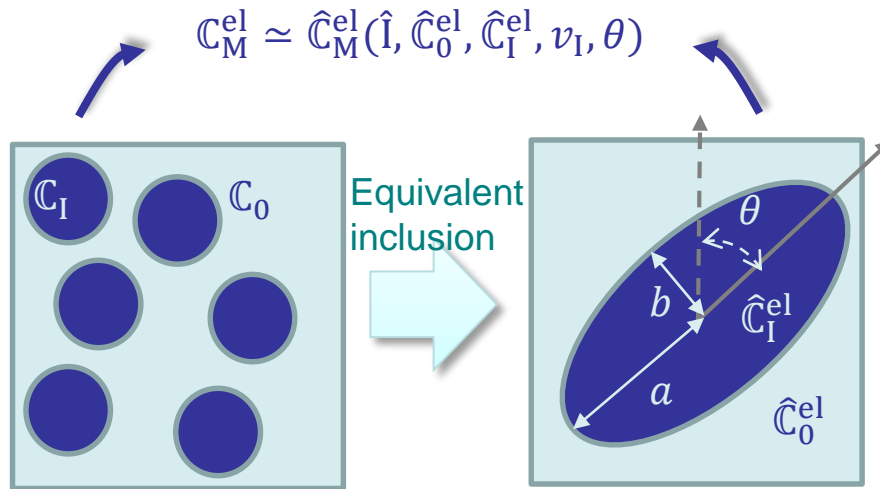
$$\Rightarrow \Delta \boldsymbol{\sigma}_M = \mathbb{C}_M^S(I, (1 - D_0) \mathbb{C}_0^S, \mathbb{C}_I^S, v_I) : \Delta \boldsymbol{\varepsilon}_M^r$$





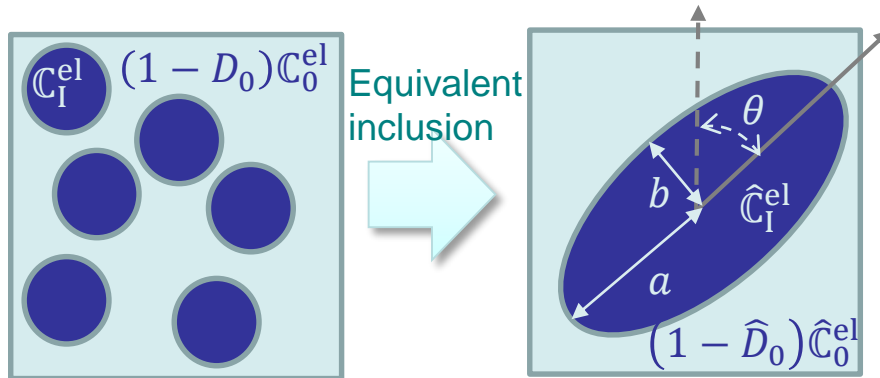
# Non-linear stochastic Mean-Field Homogenization

- Damage-enhanced inverse identification
  - First step from elastic response
    - Before damage occurs



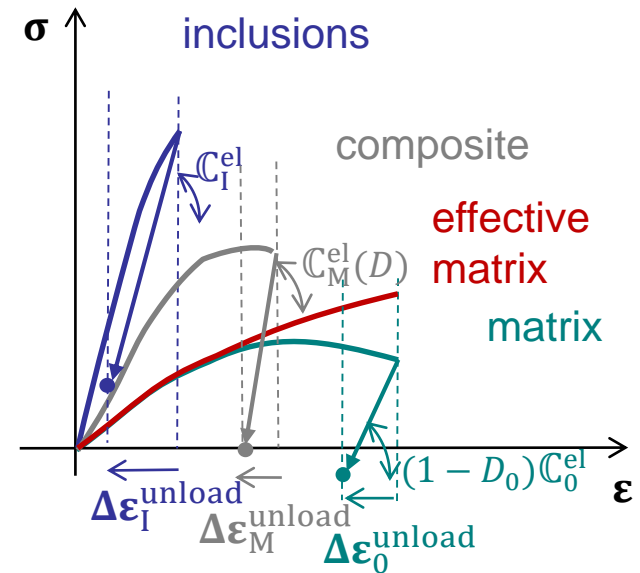
# Non-linear stochastic Mean-Field Homogenization

- Damage-enhanced inverse identification
  - Second step: elastic unloading



- Identify damage evolution  $\hat{D}_0$

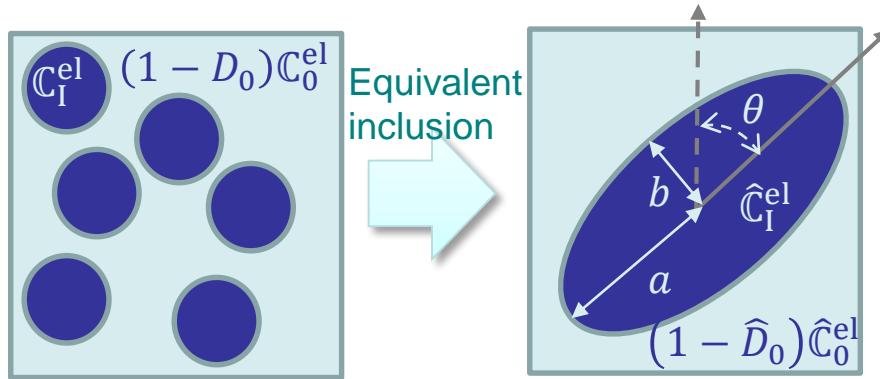
$$\mathbb{C}_M^{el}(D) \simeq \hat{\mathbb{C}}_M^{el}(\hat{I}, (1 - \hat{D}_0)\hat{\mathbb{C}}_0^{el}, \hat{\mathbb{C}}_I^{el}, \nu_I, \theta)$$



# Non-linear stochastic Mean-Field Homogenization

- Damage-enhanced inverse identification

- Second step: elastic unloading



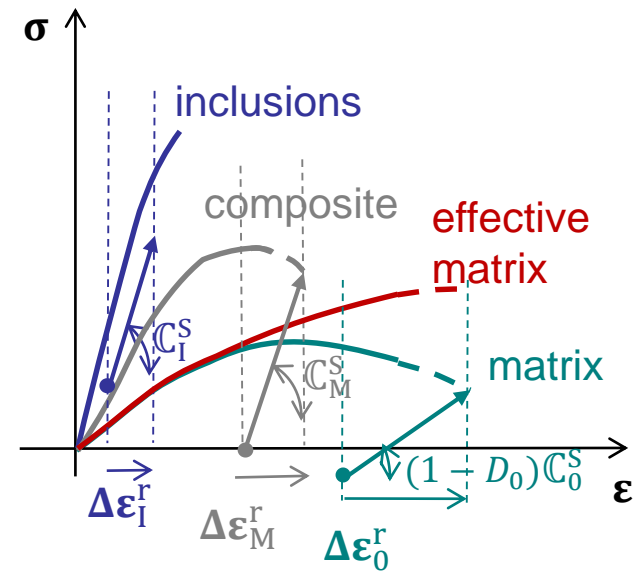
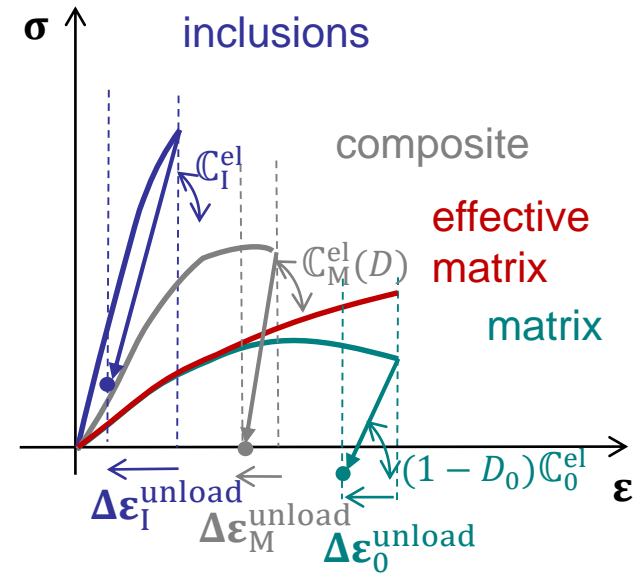
- Identify damage evolution  $\hat{D}_0$

$$\mathbb{C}_M^{el}(D) \simeq \hat{\mathbb{C}}_M^{el}(\hat{I}, (1 - \hat{D}_0)\hat{\mathbb{C}}_0^{el}, \hat{\mathbb{C}}_I^{el}, \nu_I, \theta)$$

- Third step from the LCC

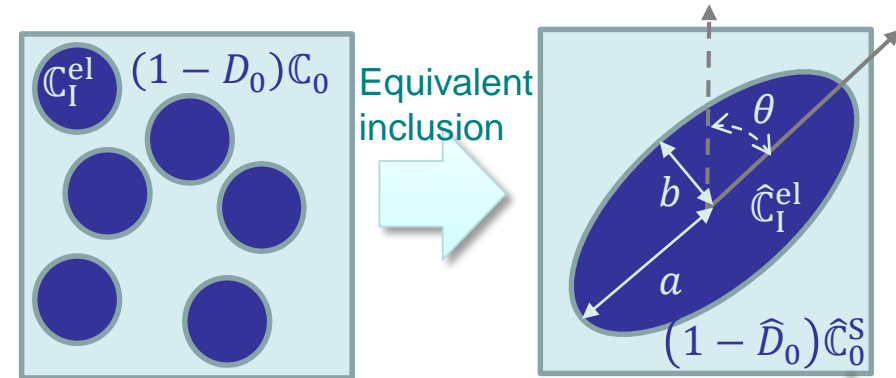
- $\Delta\sigma_M = \mathbb{C}_M^S(I, (1 - D_0)\mathbb{C}_0^S, \mathbb{C}_I^S, \nu_I): \Delta\epsilon_M^r$
- Extract the equivalent hardening  $\hat{R}(\hat{p}_0)$  & damage evolution  $\hat{D}_0(\hat{p}_0)$  from incremental secant tensor:

$$(1 - D_0)\mathbb{C}_0^S \simeq (1 - \hat{D}_0(\hat{p}_0))\hat{\mathbb{C}}_0^S(\hat{R}(\hat{p}_0); \hat{\mathbb{C}}_0^{el})$$

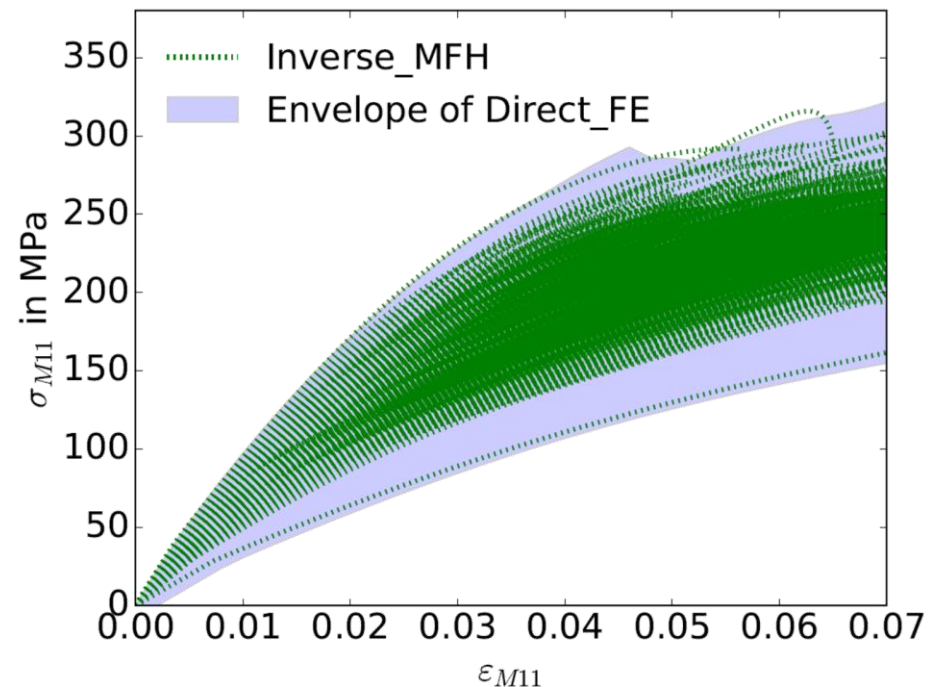
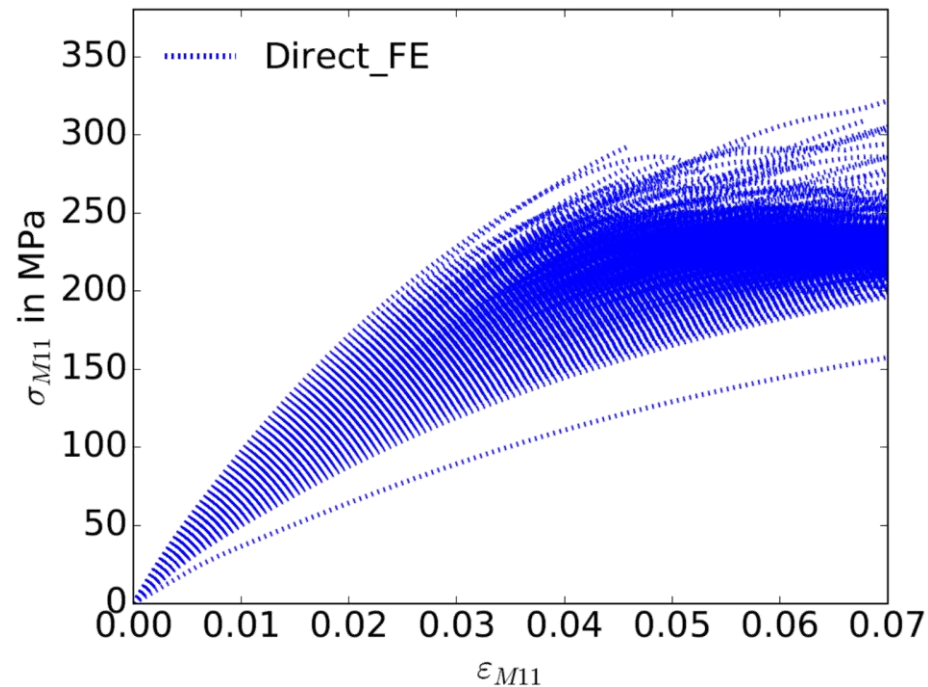


# Non-linear stochastic Mean-Field Homogenization

- Damage-enhanced inverse identification
  - Comparison SVE vs. MFH

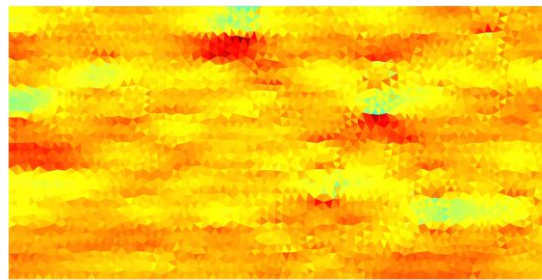
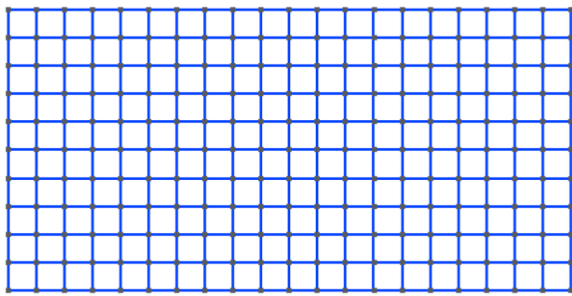


$$(1 - D_0)\mathbb{C}_0^S \simeq (1 - \hat{D}_0(\hat{p}_0))\hat{\mathbb{C}}_0^S(\hat{R}(\hat{p}_0); \hat{\mathbb{C}}_0^{\text{el}})$$

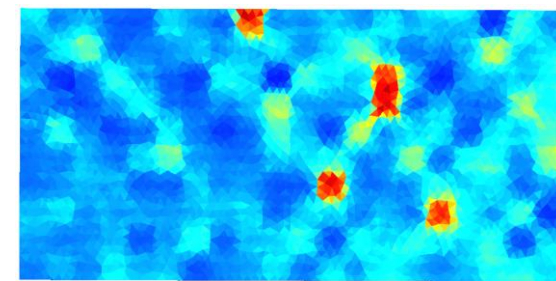


# Non-linear stochastic Mean-Field Homogenization

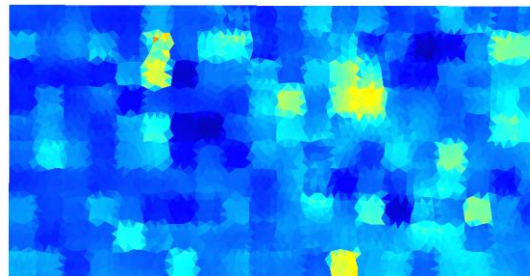
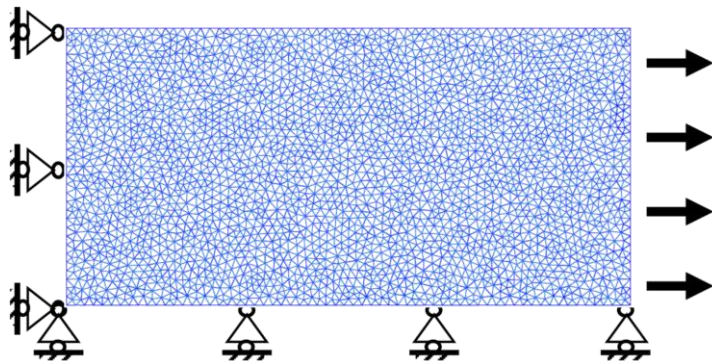
- One single ply loading realization
  - Random field and finite elements discretizations
  - Non-uniform homogenized stress distributions
  - Creates damage localization



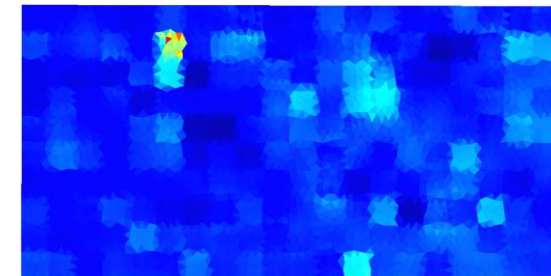
$\sigma_{M_{xx}}$  [Mpa];  $\varepsilon_{M_{xx}} = 2.6\%$   
0 108 215



$\hat{p}_0$  [-];  $\varepsilon_{M_{xx}} = 2.6\%$   
0 108 215



$\hat{D}_0$  [-];  $\varepsilon_{M_{xx}} = 2.4\%$   
0 0.025 0.05

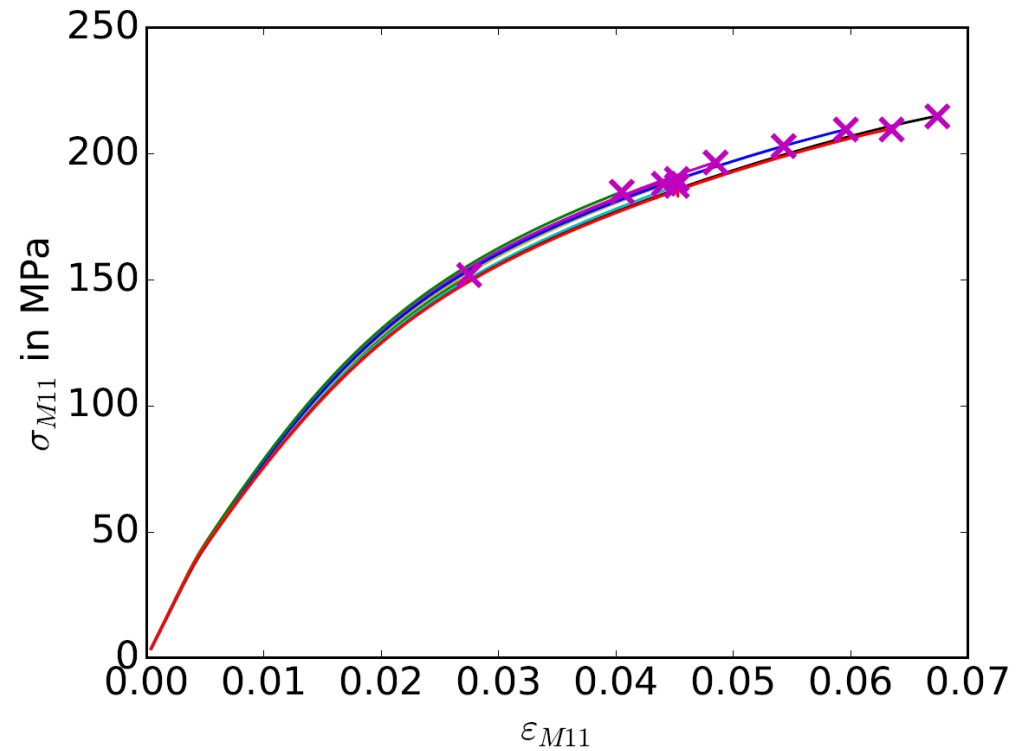
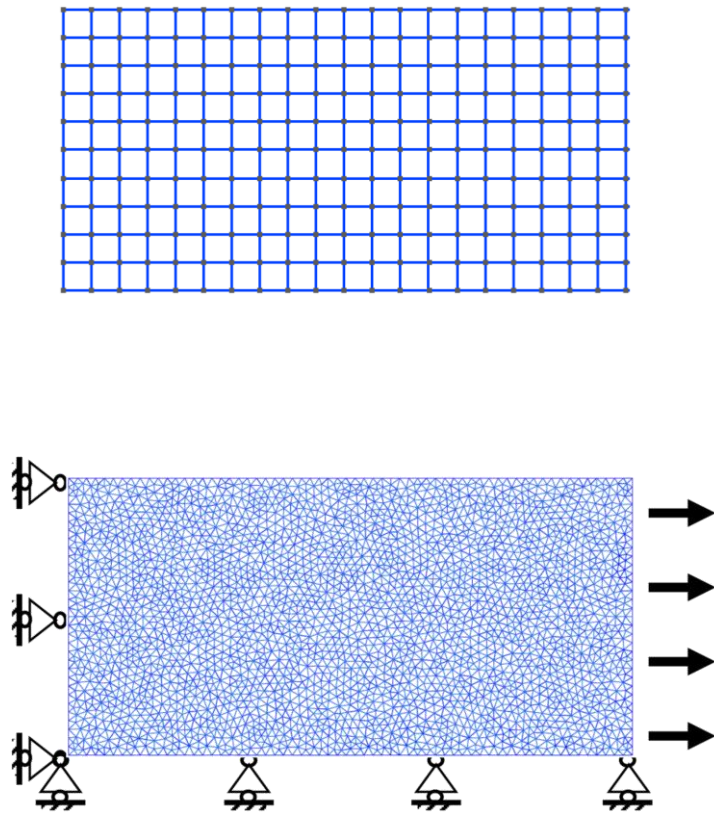


$\hat{D}_0$  [-];  $\varepsilon_{M_{xx}} = 2.6\%$   
0 0.025 0.05



# Non-linear stochastic Mean-Field Homogenization

- Ply loading realizations
  - (Simple) Failure criterion at (homogenized stress) loss of ellipticity
  - Discrepancy in failure point





# Conclusions

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- Stochastic generator based on SEM measurements of unidirectional fibers-reinforced composites
- Computational homogenization on SVEs
- Definition of a Stochastic MFH method
- In progress: nonlinear and failure analyzes



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Thank you for your attention !