Considering polydispersity and new LIÈGE université coalescence models in the description of separators



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Introduction

High viscosity of bio-based materials induces difficulties to design technical settlers due to wide drop-size distribution, e.g. quantitative prediction of the remaining fraction of fine drops found at the settler outlet.

In parallel, trace components influence the coalescence and thus the settling behavior. It varies with the ions type and with their concentration making settling quite unpredictable. Usually, settling experiments are conducted in a so-called settling cell. From the experiment, the system can be characterized [1,2].

A numerical tool, based on the ReDrop concept (Representative Drops) [1], was developed in order to simulate the separation of liquid-liquid dispersion and thus to improve the design of continuous settler. Sedimentation and coalescence are evaluated for a sufficiently large ensemble of representative individual drops at each time step.

The coalescence modeling is a major challenge in these simulations due to trace components influence and is investigated in detail.

Material and Method

- system paraffin oil + deionized water with salt is chosen in order to play easily
- the two-phase system is stirred during 30 sec at 800 min⁻¹



- with the viscosity
- different paraffin oil viscosity and salt concentration are tested
- ReDrop simulation will be compared to the settling experiments in order to validate the coalescence model

Table 1. Density and viscosity of a specific studied system

		25°C
saturated paraffin oil	density (kg/m³) viscosity (mPas)	819.597 8.48
saturated deionized water + 50 mmol/L of NaCl	density (kg/m³) viscosity (mPas)	999.041 1.030

- experiments are conducted 3 times to validate reproducibility
- the settling time is reached when only half of the interface remains covered by a monolayer of droplets
- experiments are recorded on video in order to obtain the experimental data point
- SOPAT inline probe is used to \bullet measure the initial drop-size distribution

second vessel for internals

Figure 1. Henschke settling cell

Coalescence model

- fluid-dynamic dependent variables \bullet have to be characterized once for a dedicated equipment
- the coalescence time depends on \bullet the material properties: solvent, salt concentration, trace components

Collision rate

• the collision rate depends on the diameters of the drops, d_1 and d_2 , their height

Coalescence efficiency

- the coalescence efficiency depends on the contact time, which can be, conceptually divided into time step, Δt .
- for each time step, a probability of non-coalescence can be defined as $p_{non-coalescence,\Delta t}$. For 2 Δt , the following has to hold:

 $p_{non-coalescence,2\Delta t} = p_{non-coalescence,\Delta t}$

• the probability of the entire process is,

$$P_{\text{coalescence}} = 1 - \exp\left(-\frac{t_{\text{contact}}}{t_{\text{coalescence}}}\right)$$

in the settling cell, h_1 and h_2 , on the relative velocity, v_{rel} , and on the area of the cell, A_{cell} and on the correction factor, γ , which takes into account the reduction of the free volume:

collision rate

depends on

fluid dynamics

coalescence probability

contact time

depends on

fluid dynamics

Figure 2. The coalescence model [3]

coalescence efficiency

coalescence time

depends on

material system

$$r_{\text{collision}} = \frac{\gamma \pi \left(d_1 + d_2\right)^2 v_{\text{rel}}}{A_{\text{cell}} \left|h_1 - h_2\right|}$$

Coalescence time

the coalescence time is evaluated by the balance between the fluid-dynamic force induced by the film drainage and the buoyancy force, which is the driving force of the coalescence phenomenon during the settling. The asymmetric dimple model of Henschke was applied [1].

Contact time

- equation of motion of two drops following their own curvature was solved to get a first impression of the contact time, t_{contact}, the results are shown on figure 3
- model found in the literature [6] fits to the simulation



Figure 3. Contact time between a first drop of 1 mm and a second drop with varied diameter

ReDrop concept

definition of the system

- material properties: density, viscosity, etc.
- simulation parameters: initial hold up, drop-size distribution, time step, coalescence parameter, etc.
- horizontal position of drops is assumed to be randomly distributed, special care is taken to evaluate contact probability to quantify correctly the coalescence
- the initial drop-size distribution can be chosen according to various distribution functions
- gas bubbles and solid particles can be accounted for as additional dispersed

First results & Perspectives





drop loop

- individual velocity via sedimentation model
- vertical position of each drop
- coalescence in sedimentation and close-packed zone and with the major interface
- phases
- drop-drop and drop-interface coalescence is accounted for during the simulation
- deformation of the drops in the closepacked zone due to hydrostatic pressure modelled
- ability to record the drop-size and the local holdup at a specific time and height for further validation

holdup (left) and of the Sauter mean diameter (right)

- the ReDrop program can mimic system with curved sedimentation profile, as shown on the left side of Figure 4.
- the evolution of the Sauter-mean diameter shows small dispersed drops in the ${\bullet}$ continuous phase at the end of the simulation. This effect is observed during experiment by a turbid continuous phase.
- as a first conclusion, the ReDrop simulation can mimic effects observed during settling experiment.
- as a next step, settling experiment will be compared to ReDrop simulation in order to validate the coalescence model



References

[1] M. Henschke, L.H. Schlieper, A. Pfennig, Chem Eng. J., 85, 369-378 (2002). [2] J.F. Richardson, W.N. Zaki, Trans. Inst. Chem. Eng., 32, 35-53 (1954). [3] N. Kopriwa, F. Buchbender, M. Kalem, J. Ayesteràn, A. Pfennig, Solvent Extr. Ion Exch., 30, 683-723 (2012). [6] J. Kamp, M. Kraume, *Chem. Eng. Sci.*, **156**, 162-177 (2016).

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