



Magnetic and electrical characterization of superconductors

Philippe VANDERBEMDEN
University of Liège, Belgium

Philippe.Vanderbenden@ulg.ac.be

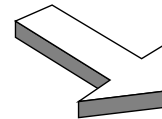
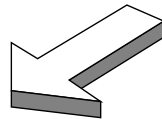
What kind of **measurements** can we make to characterize superconductors ?

What kind of **information** can we extract from measurements ?

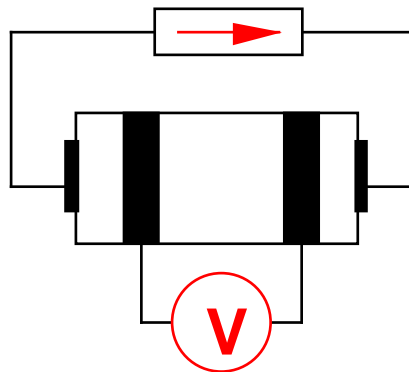
Purpose of this lecture

To better understand how we can characterize the electrical and magnetic properties of materials through

TRANSPORT measurements and **MAGNETIC** measurements

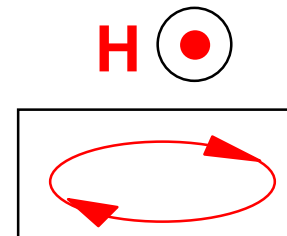


Current source



Transport current
(applied externally)

Magnetic field H



Induced current
(by the applied magnetic field)

Outline

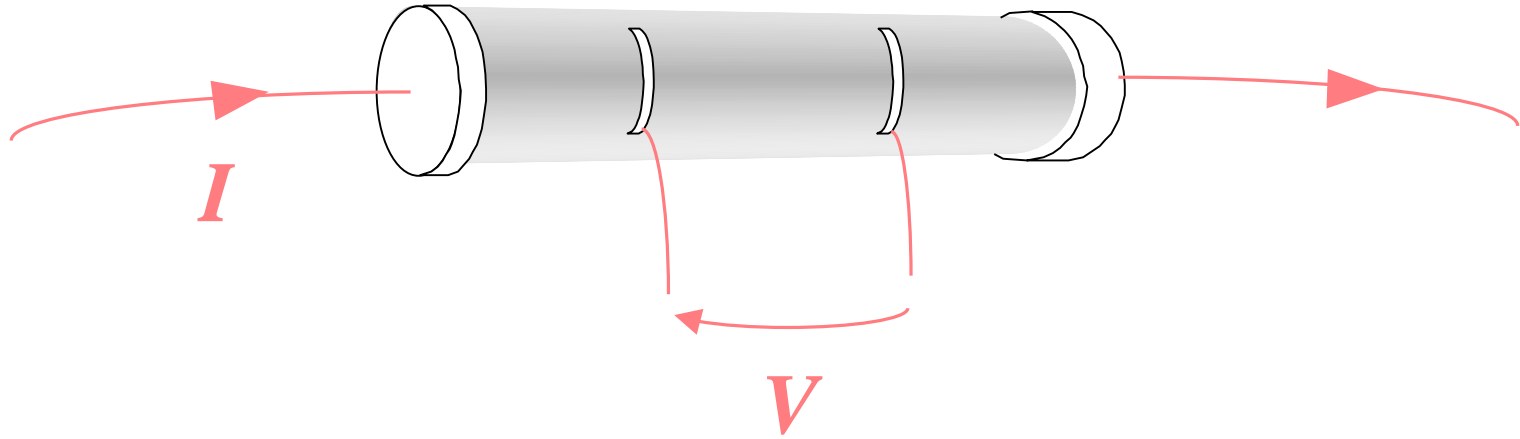
- Transport measurements - $R(T)$
- Transport measurements - $E(J)$

- Magnetic measurements (general)
- Magnetic measurements - $M(H)$

Outline

- Transport measurements - $R(T)$
- Transport measurements - $E(J)$
- Magnetic measurements (general)
- Magnetic measurements - $M(H)$

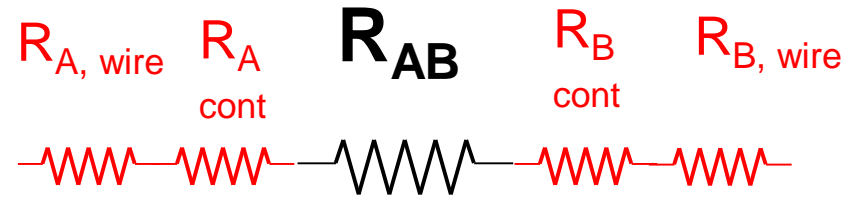
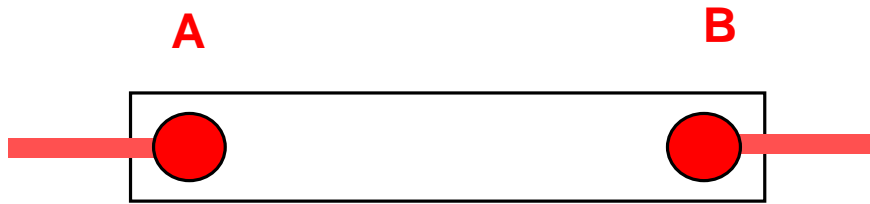
The main difficulty for transport measurements on superconductors = ?



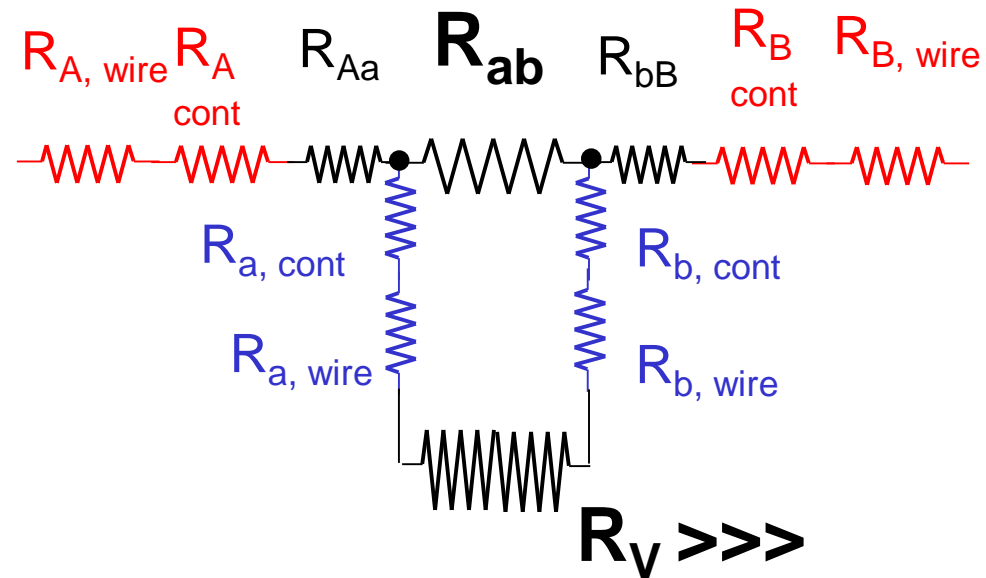
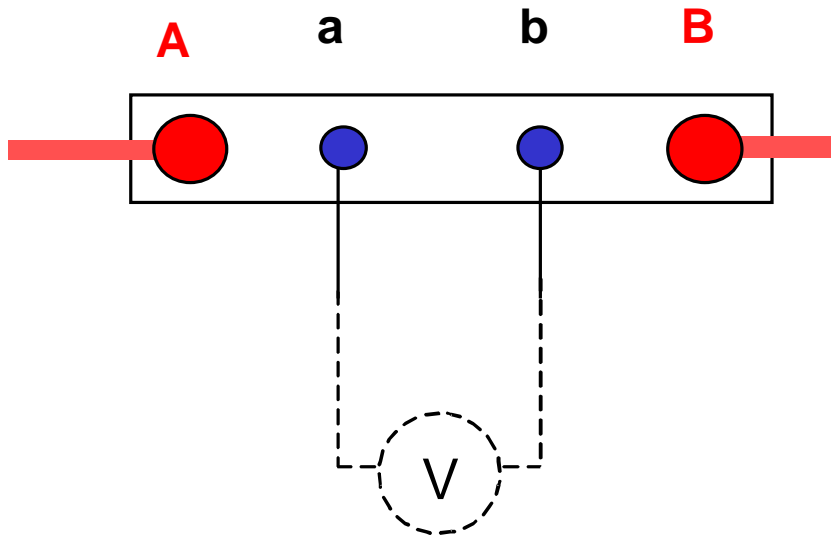
The finite resistance
of electrical contacts

Influence of contact resistance & wire resistance

2-wire connexions



4-wire connexions



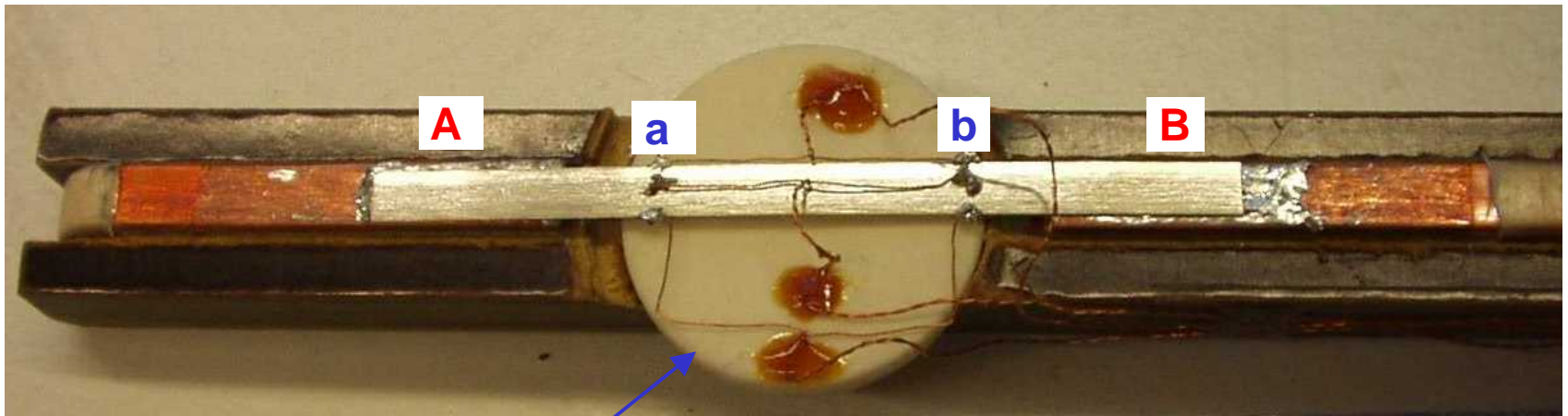
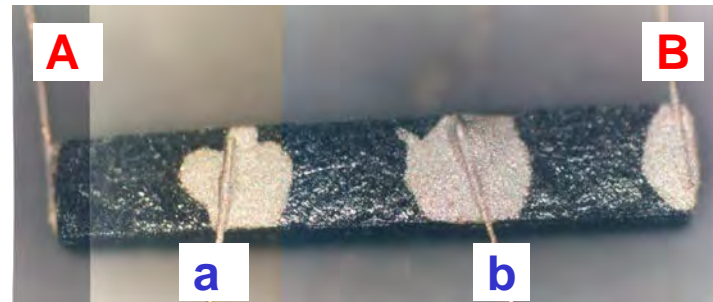
4-contact measurement (Kelvin connections)

4-wire connexions are used to eliminate contact resistances and wire resistances

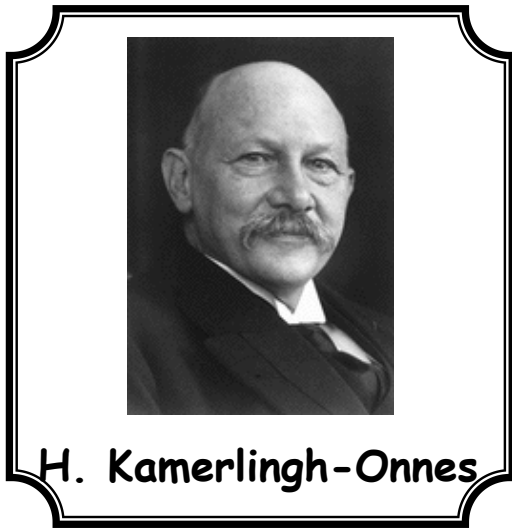
- (i) The **current** contact resistances and wire resistances are outside the measurement circuit
- (ii) The **voltage** contact resistances and wire resistances can be neglected with respect to the resistance of the voltmeter

Examples :

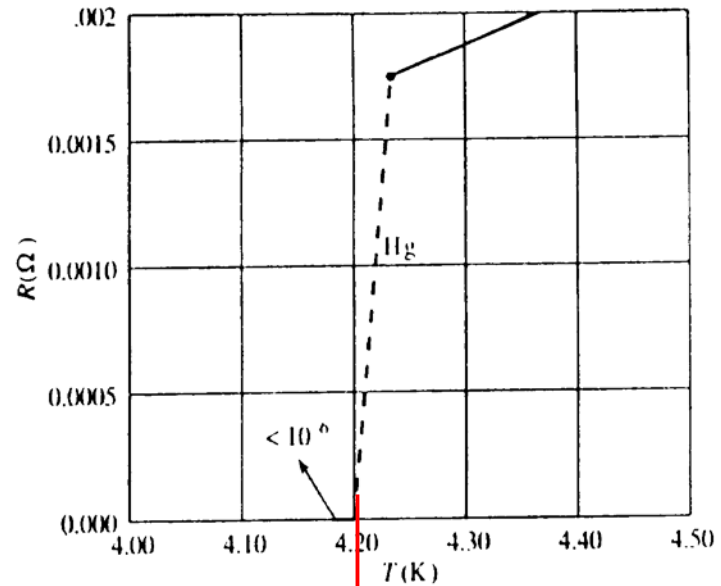
A, B = current contacts
a, b = voltage contacts



NB : for AC measurements : **twisted wires** are required to avoid inductive pick-up loops !!!



Example for type-I superconductor (Hg)



T_c critical temperature

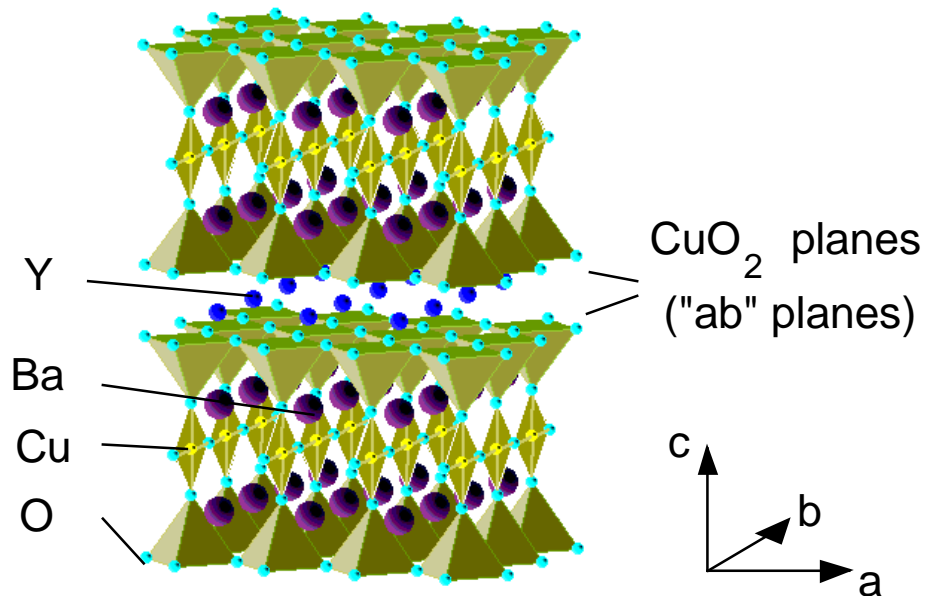
In addition to giving the critical temperature of the superconductor, a $R(T)$ measurement in the presence of a magnetic field can be helpful in characterizing

- (i) anisotropy effects
- (ii) granularity and connectivity between grains
- (iii) the phase diagram (irreversibility line of the material)

These characteristics of HTS materials are briefly recalled hereafter

(i) Anisotropy

Ex : Y - 123 single crystal



The **flow of current density \mathbf{J}** is easier in the ab planes than along the c-axis :

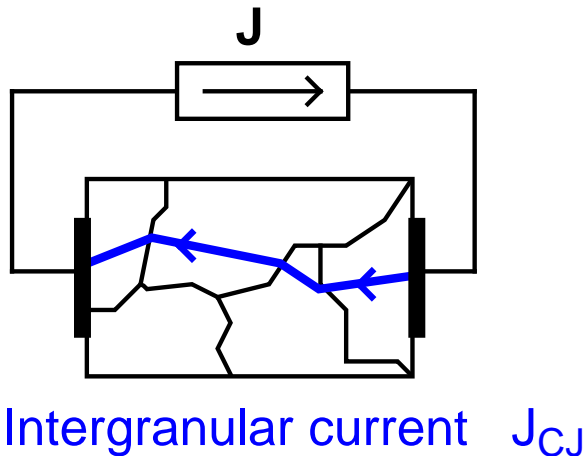
$$\mathbf{J}_c (\parallel \mathbf{ab}) > \mathbf{J}_c (\parallel \mathbf{c})$$

The pinning of **flux lines \mathbf{B}** is larger for $\mathbf{B} \parallel \mathbf{ab}$ than for $\mathbf{B} \parallel \mathbf{c}$

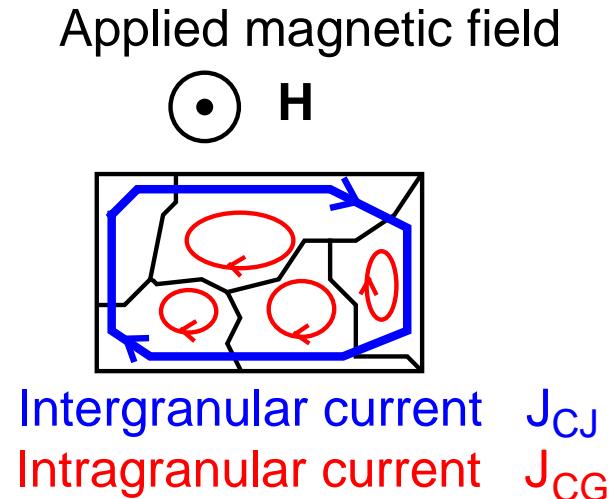
$$\left[(\mathbf{J} \parallel \mathbf{B}) = \text{“force-free” configuration} \right]$$

(ii) Granularity

Transport current



Shielding currents



$$J_{CJ} < J_{CG}$$

Grain alignment - or **texturation** - is a key ingredient to improve the **intergranular** critical current density

Orientation Dependence of Grain-Boundary Critical Currents in $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$ Bicrystals

D. Dimos, P. Chaudhari, J. Mannhart, and F. K. LeGoues

*Thomas J. Watson Research Center, IBM Research Division,
Yorktown Heights, New York, 10598*

(Received 4 May 1988)

The critical current densities across grain boundaries have been measured as a function of misorientation angle in the basal plane of bicrystals of $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$. For small misorientation angles, the ratio of the grain-boundary critical current density to the bulk critical current density is roughly proportional to the inverse of the misorientation angle; for large angles, this ratio saturates to a value of about $\frac{1}{50}$. These results imply that achieving a high degree of texture both normal to and within the basal plane is important for the obtaining of very high critical currents in pure polycrystalline samples.

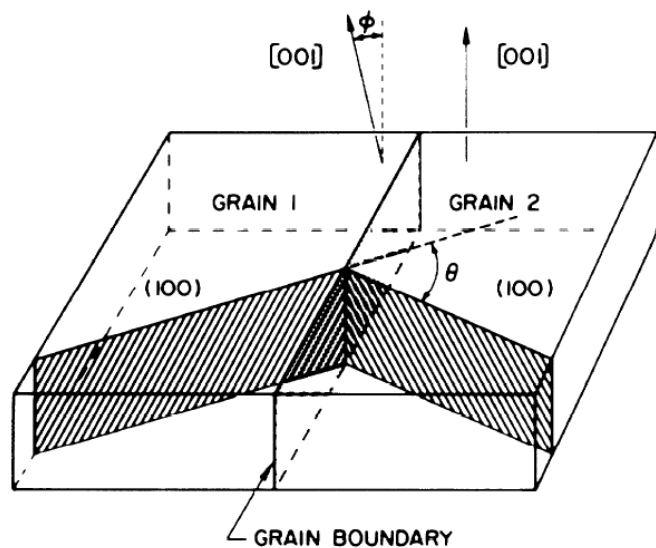
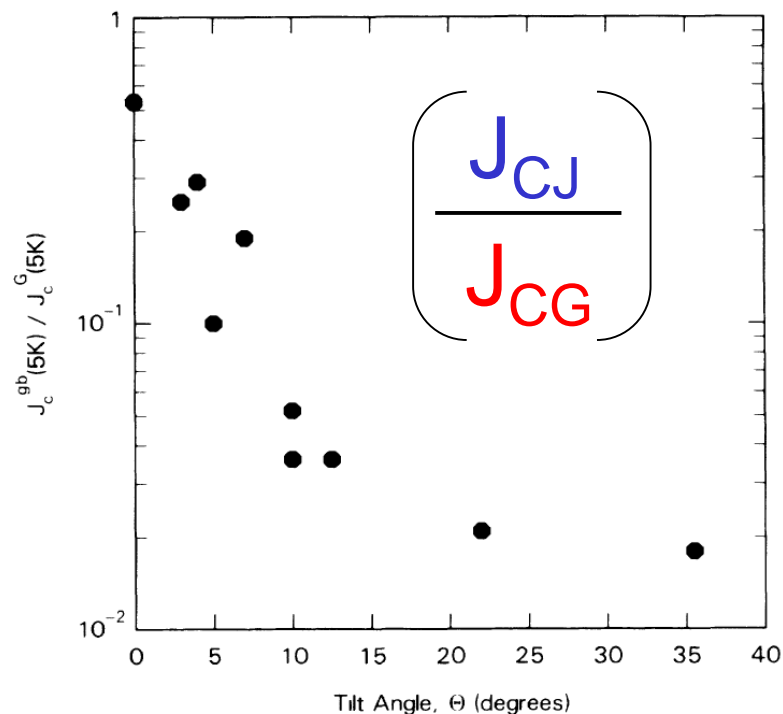
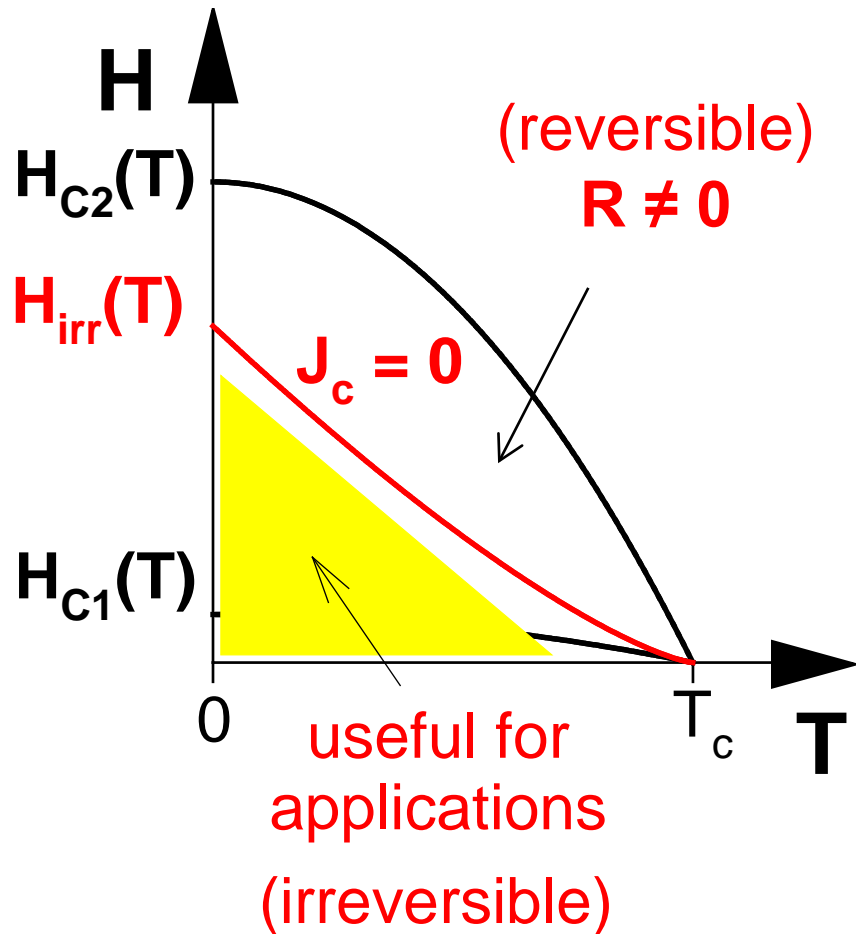


FIG. 1. Schematic diagram showing the important crystallography of the SrTiO_3 bicrystals which were used as substrates for the thin-film deposition.



(iii) Irreversibility line

(relevant for high-temperature superconductors)

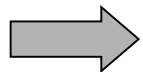
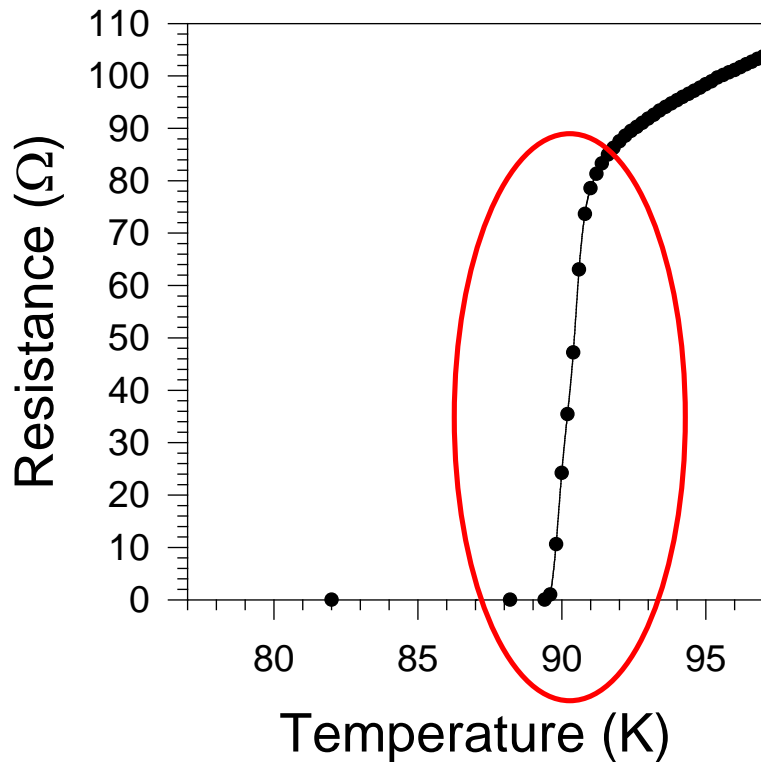


Irreversibility fields of some HTS materials at $T = 77$ K

Bi-2212 :	< 0.1 T
Bi-2223 :	0.3 T
Y-123 :	7-10 T

Typical R(T) curve

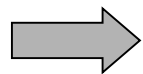
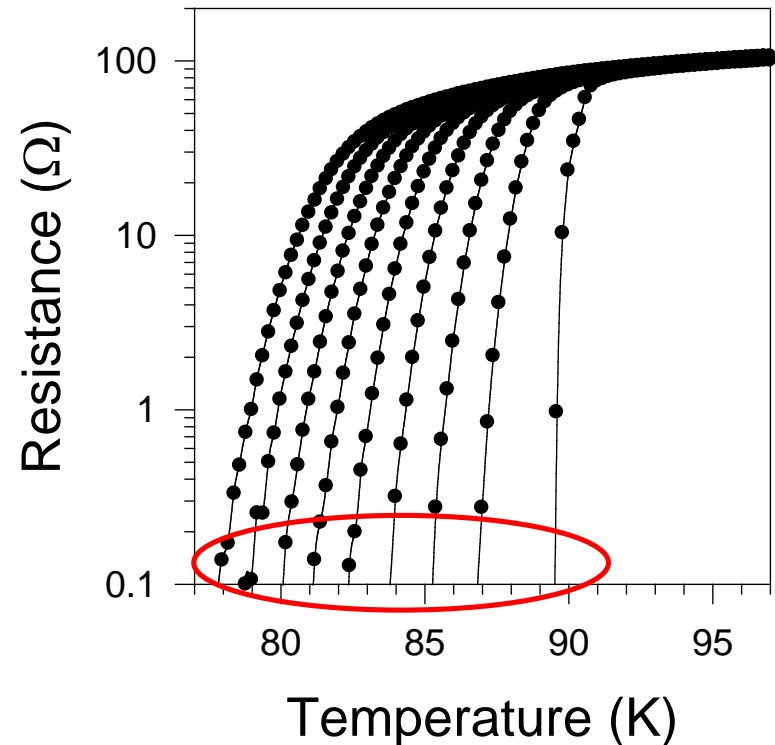
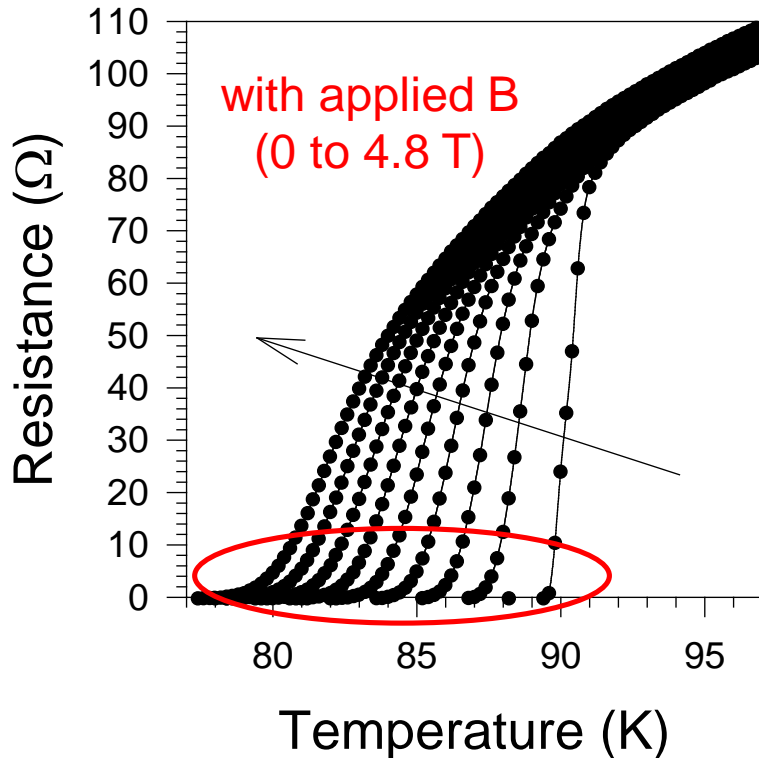
Ex: $\text{YBa}_2\text{Cu}_3\text{O}_7$



The width of the transition requires a **given criterion** to define T_c (usual criterion : inflexion point [change of curvature] but others are possible)

Typical R(T) curve

Ex: $\text{YBa}_2\text{Cu}_3\text{O}_7$



The use of a log scale can be very useful the temperature above which electrical resistance merges from the noise level (= irreversibility line ?)

Vortex Lattice Melting in Untwinned and Twinned Single Crystals of $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$

W. K. Kwok, S. Fleshler, U. Welp, V. M. Vinokur, J. Downey, and G. W. Crabtree
 Science and Technology Center for Superconductivity and Materials Science Division,
 Argonne National Laboratory, Argonne, Illinois 60439

M. M. Miller

Naval Research Laboratory, Washington, D.C. 20375
 (Received 1 October 1992)

The melting transition in twinned and untwinned single crystals is measured resistively in fields up to 8 T as a function of the angle between the c axis and the a - b plane. The angular dependence follows the Lindemann criterion with $c_L = 0.15$. The suppression of melting by strong pinning by twin boundaries is demonstrated.

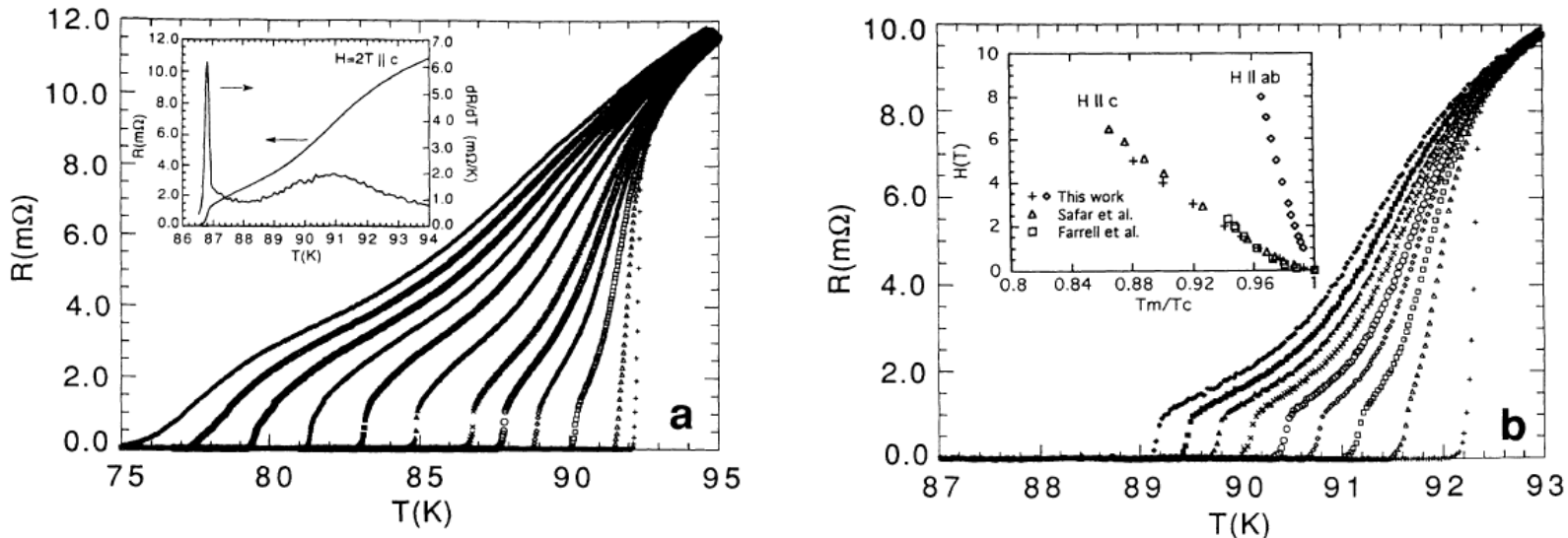
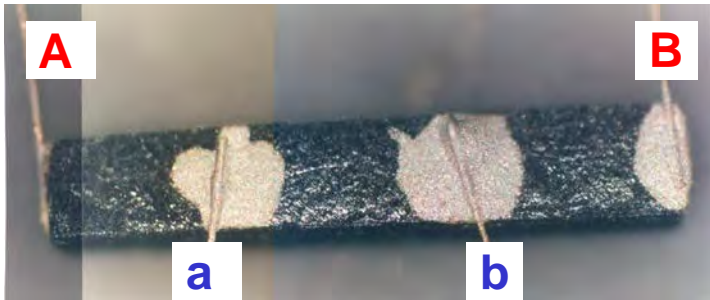
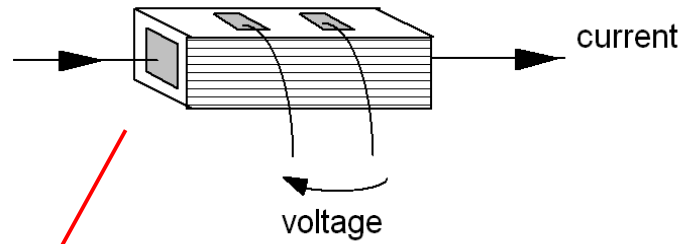


FIG. 1. (a) Resistive transition in magnetic fields of 0, 0.1, 0.5, 1, 1.5, 2, 3, 4, 5, 6, 7, and 8 T for $H \parallel c$ in an untwinned $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$ crystal. Inset: Determination of T_m from the inflection peak of dR/dT for $H = 2$ T. (b) Resistive transition in magnetic fields of 0, 1, 2, 3, 4, 5, 6, 7, and 8 T for $H \parallel (a,b)$. Inset: Phase diagram of the melting transition for $H \parallel c$ and $H \parallel (a,b)$.

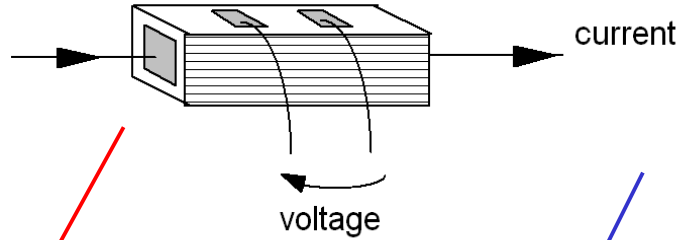
Anisotropy

(a) *ab-plane resistivity*

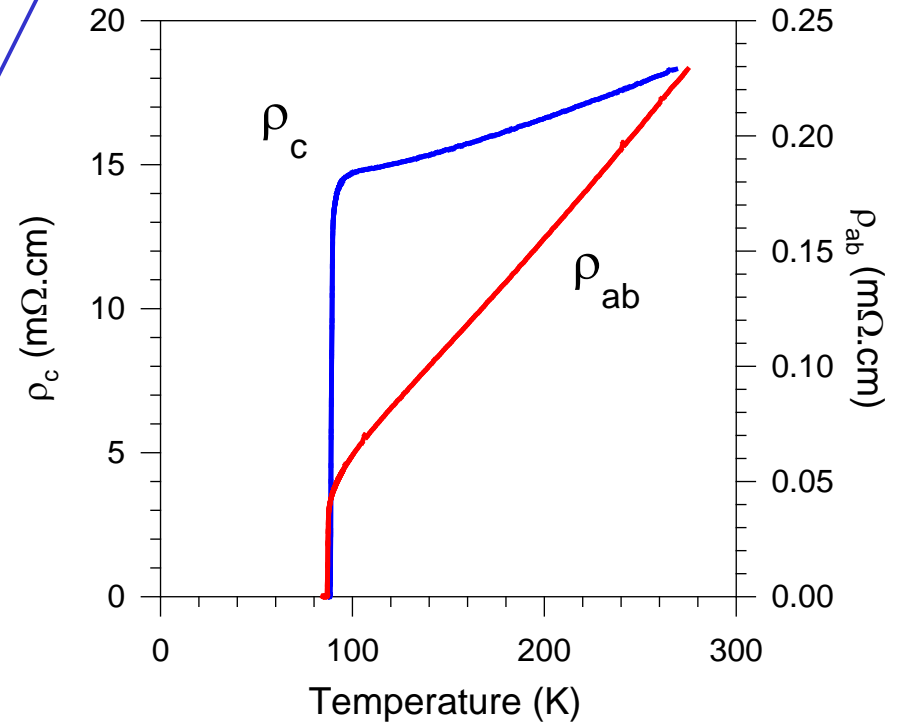
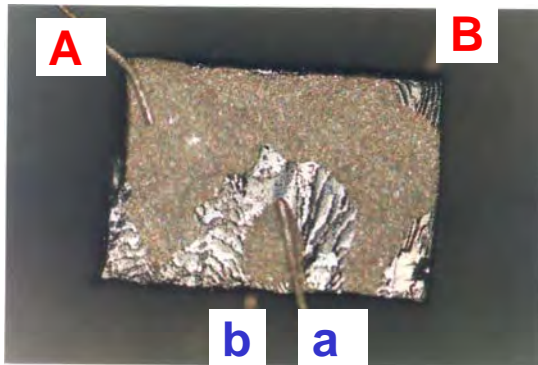
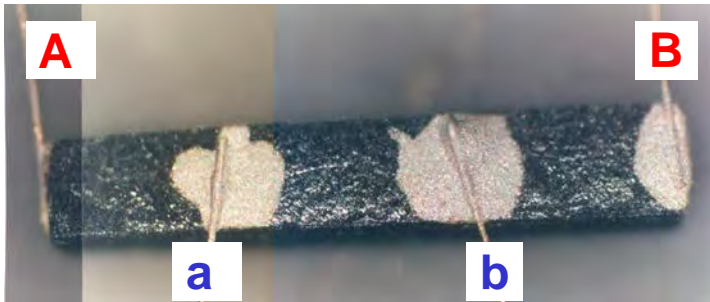
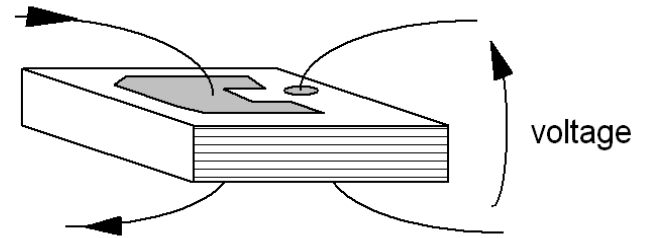


Anisotropy

(a) *ab*-plane resistivity



(b) *c*-axis resistivity



Granularity

PHYSICA C

Superconducting properties of natural and artificial grain boundaries in bulk melt-textured YBCO

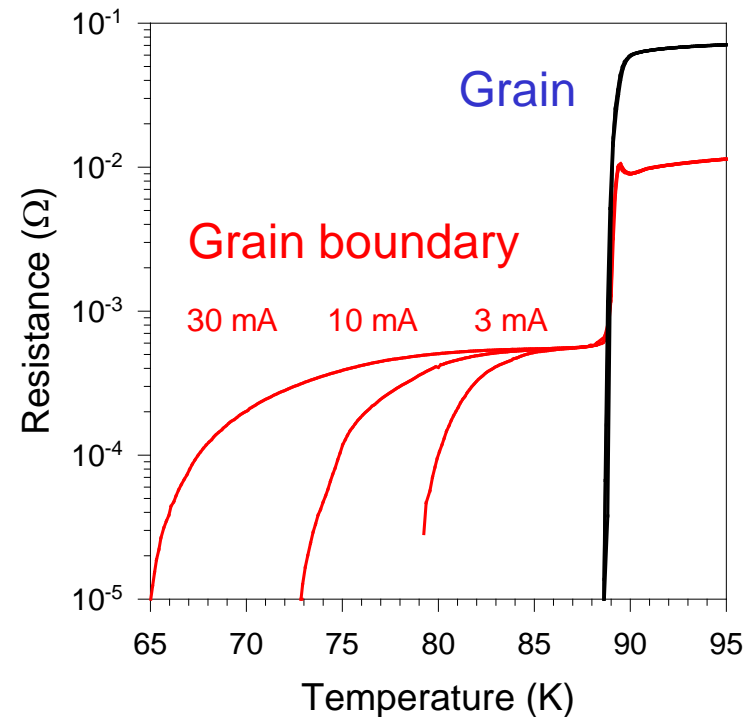
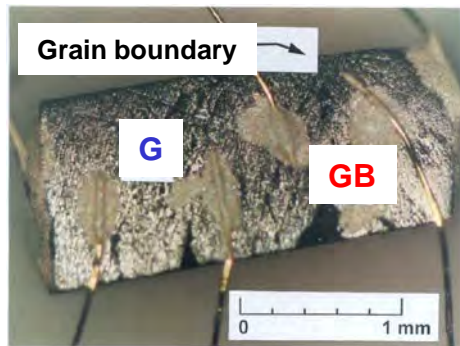
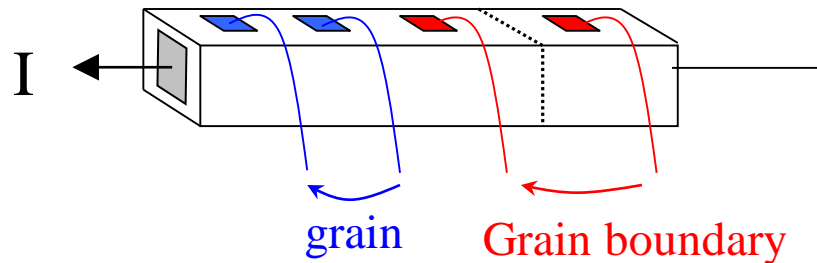
Ph. Vanderbemden^{a,b,*}, A.D. Bradley^b, R.A. Doyle^b, W. Lo^b, D.M. Astill^b,
D.A. Cardwell^b, A.M. Campbell^b

^a SUPRAS, Montefiore Electricity Institute B28, University of Liège, Sart-Tilman, B-4000 Liège, Belgium

^b IRC in Superconductivity, University of Cambridge, Madingley Road, Cambridge CB3 0HE, UK

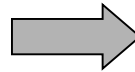
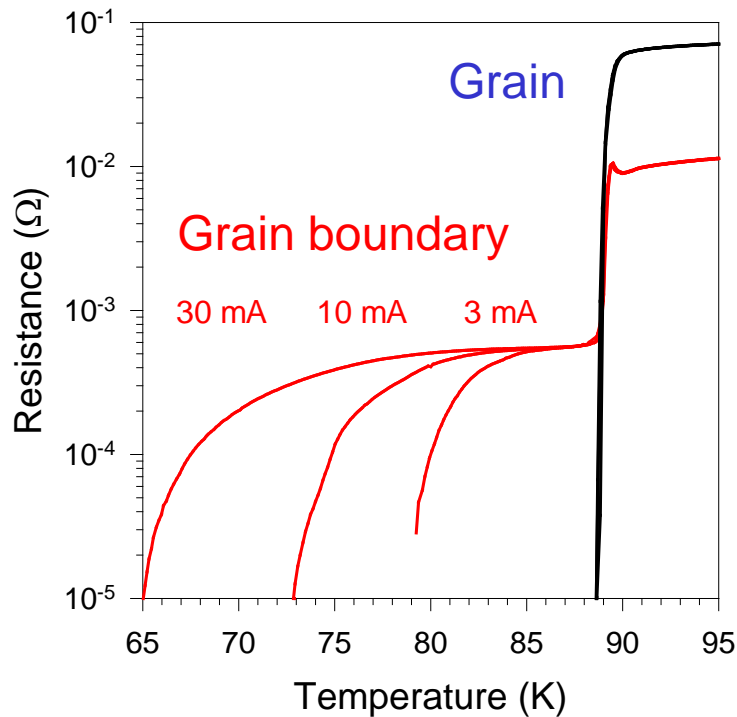
Received 29 December 1997; revised 7 March 1998; accepted 2 May 1998

Physica C 302 (1998) 257–270

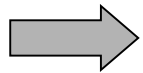
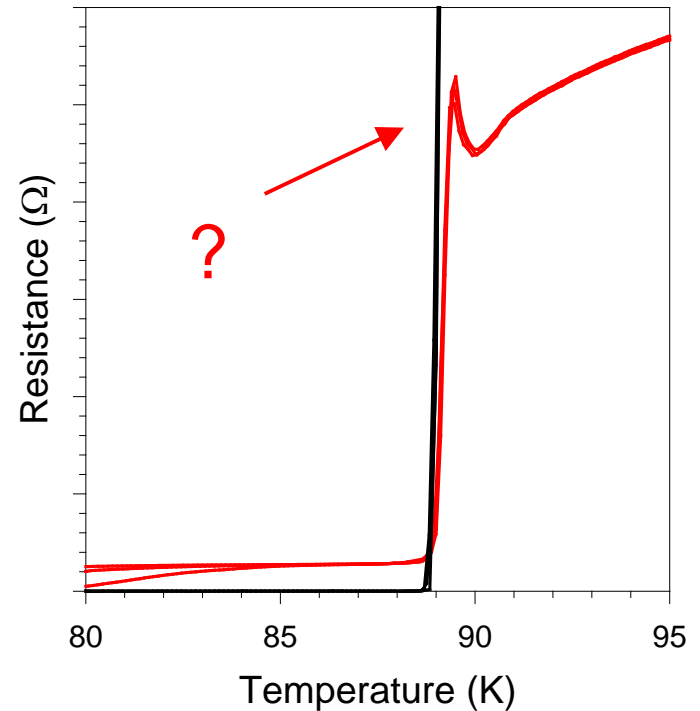


➔ A shoulder in $R(T)$ – possibly using a log scale for R
is a clear signature of the presence of one or more grain boundaries

Some artefacts or difficulties ...



Back to
LINEAR
SCALE



The peak in $R(T)$ just above the superconducting transition is a (relatively) common feature usually attributed to inhomogeneities and current redistribution

Current redistributions in superconductors with non-uniformly distributed T_c -inhomogeneities

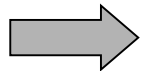
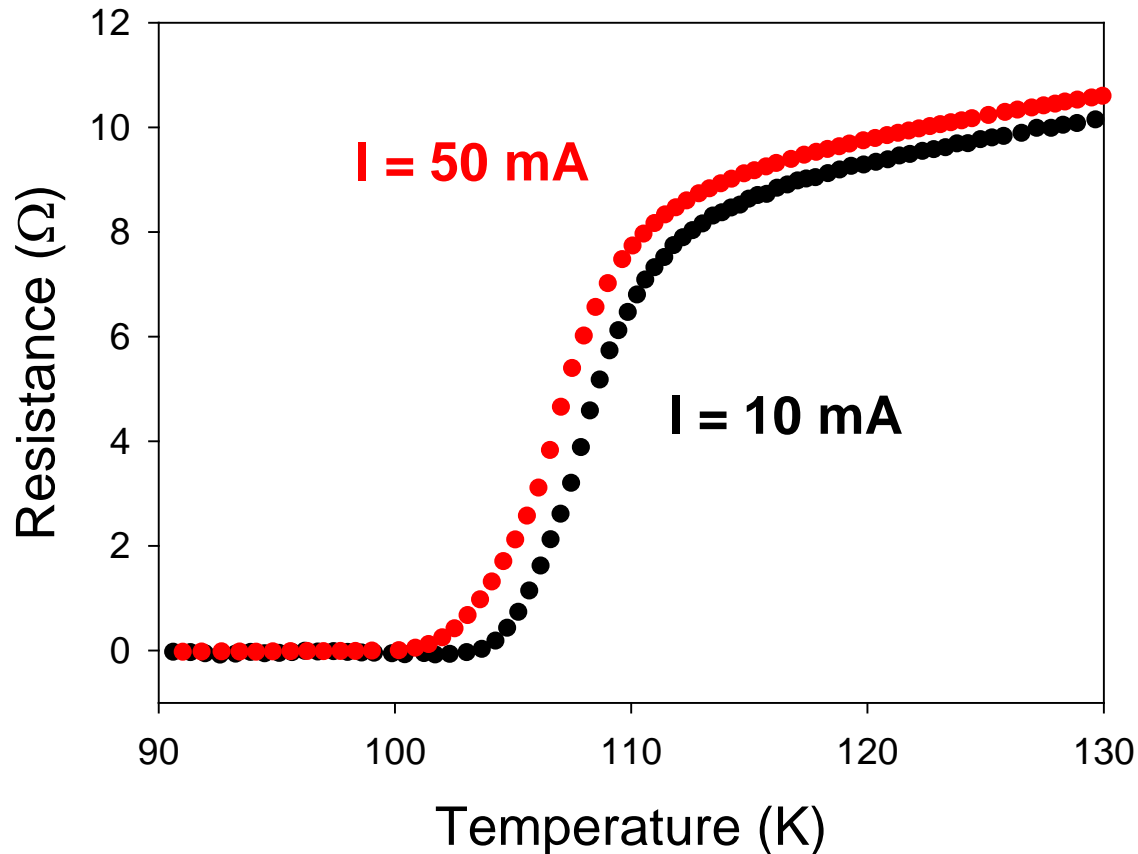
PHYSICA C

Th. Siebold, C. Carballeira, J. Mosqueira, M.V. Ramallo and Félix Vidal

Physica C 282–287 (1997) 1181–1182

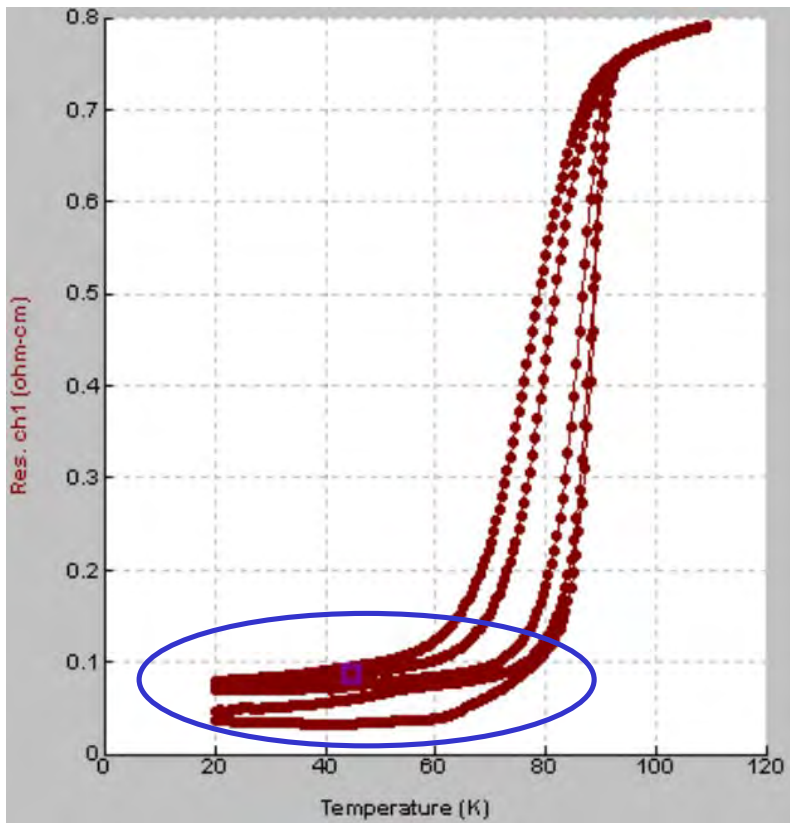
Some artefacts or difficulties ...

Ex: Bi-2223 ceramic

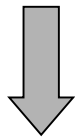


A larger current means also a much larger power dissipated in current contacts ($P = R I^2$!) and, possibly, sample heating and error in the temperature measurement

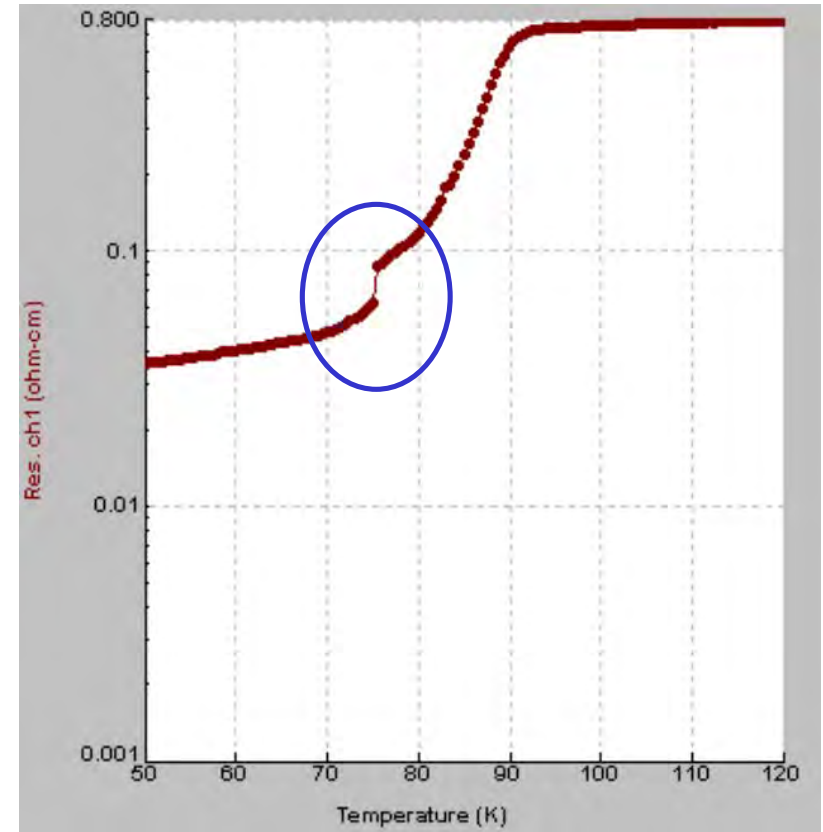
Other errors ...



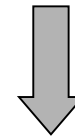
Bad sample or bad contact resistance



Try again with new contacts !

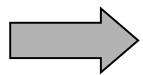
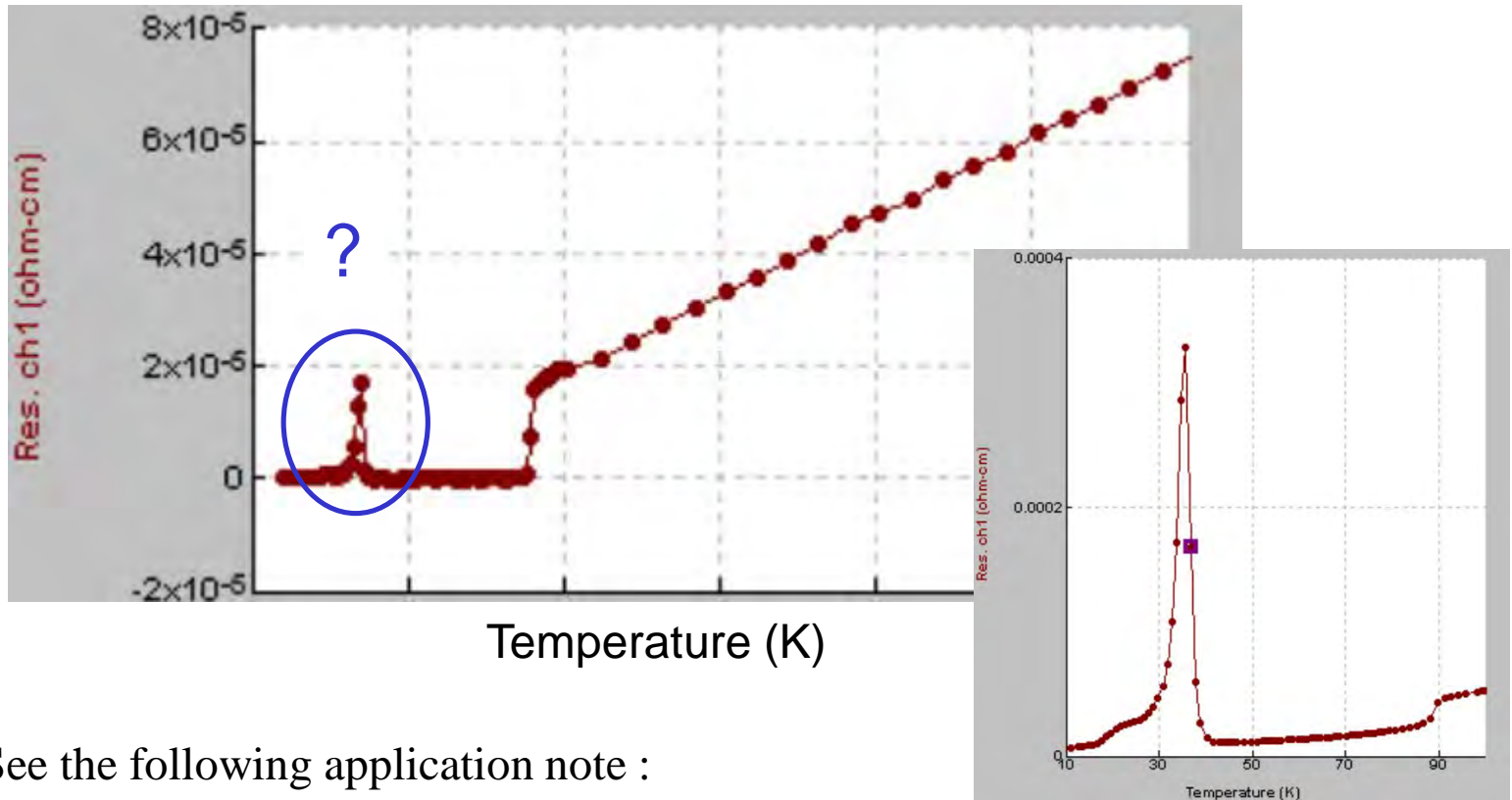


« Jumping » contact



Try again with new contacts !

A well-known error from the QD Physical Property Measurement System (PPMS)



See the following application note :

Quantum Design

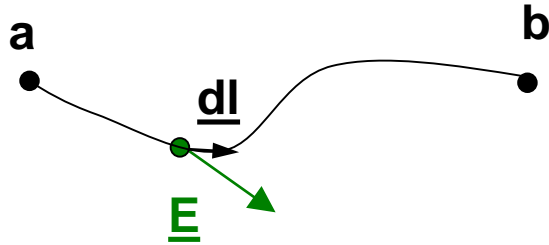


Distorted low-level signal readback of AC signals in the PPMS in the temperature range 25-35 K due to Inconel mitigation of inductive cross talk

Outline

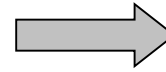
- Transport measurements - $R(T)$
- **Transport measurements - $E(J)$**
- Magnetic measurements (general)
- Magnetic measurements - $M(H)$

Electric field \underline{E} (V/m)



(OK when no time-dependent magnetic flux density)

\underline{E}



$$V_a - V_b = \int_a^b \underline{E} \cdot d\underline{l}$$

Electric field

[V/m]

voltage difference
voltage drop

[volts], [V]

Local quantity

Global quantity

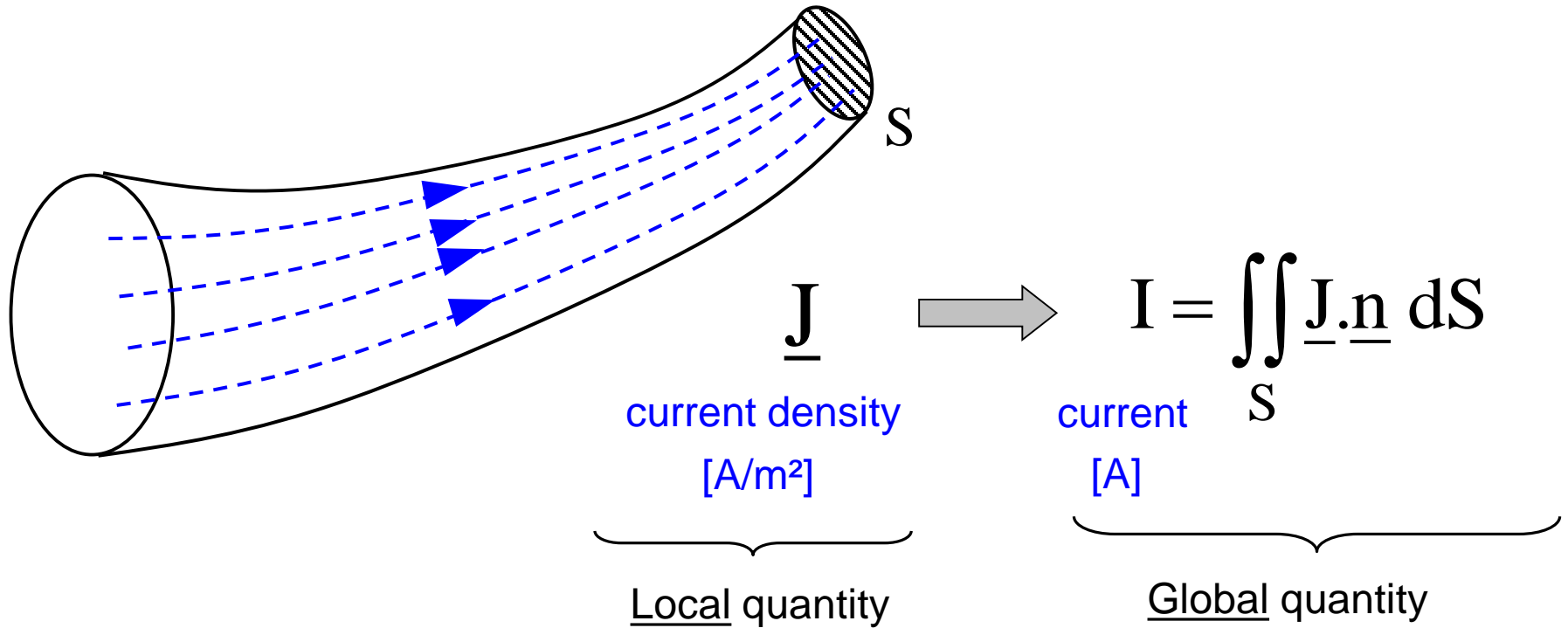
Particular case :



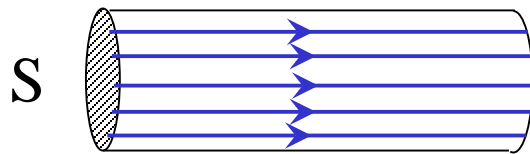
\underline{E} uniform and parallel to the segment between a and b

$$\underline{E} = \frac{V_a - V_b}{l}$$

Current density \underline{J} (A/m^2)



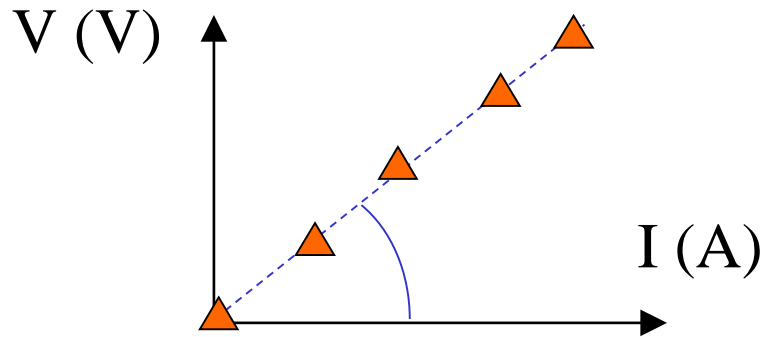
Particular case :



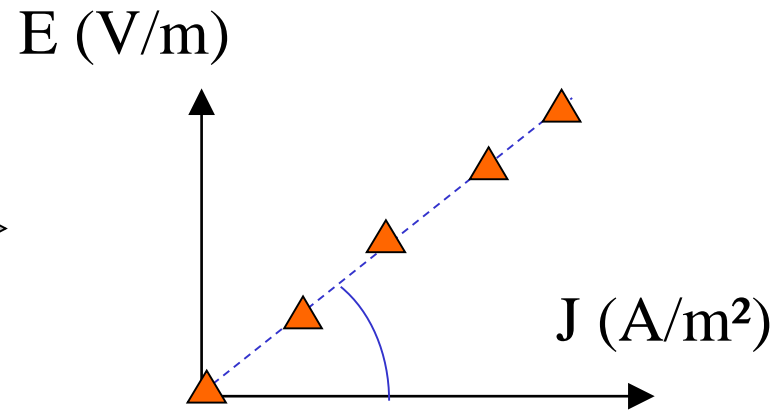
\underline{J} uniform and $\perp S$

$$\underline{J} = \frac{I}{S}$$

Linear conductor

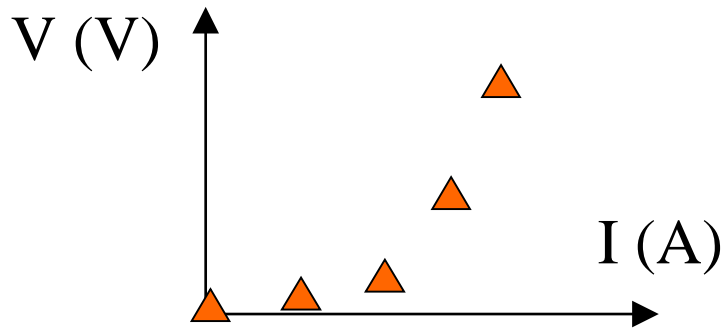


(slope) R = resistance (Ω)

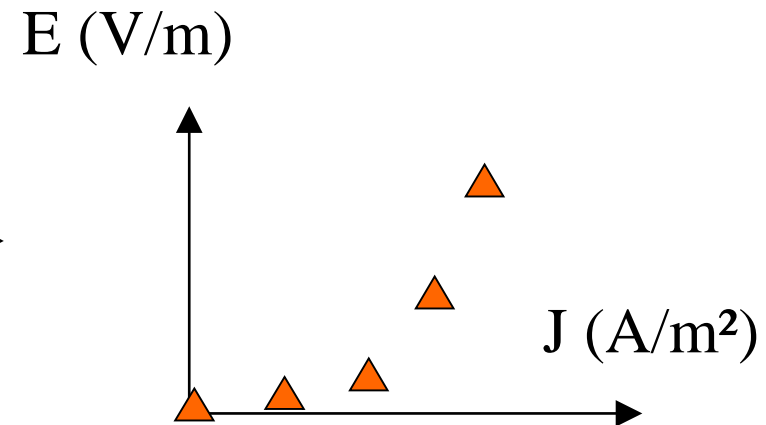


(slope) ρ = resistivity ($\Omega \cdot m$)

Non-linear conductor



(slope) = ???

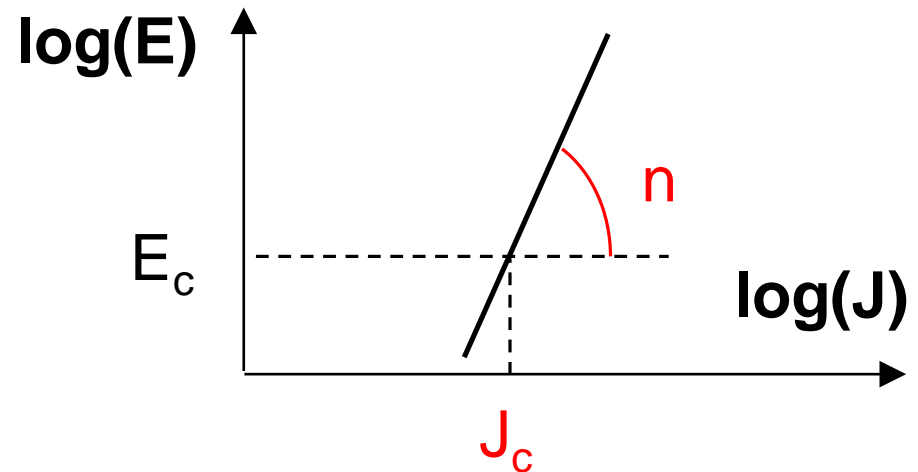
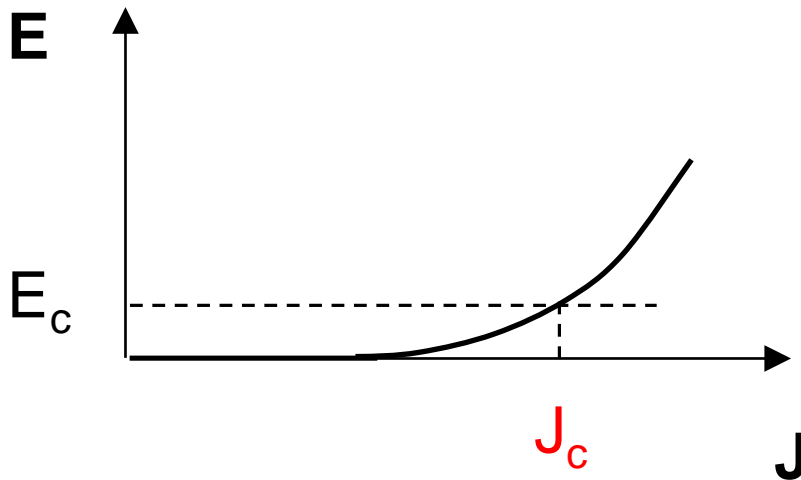


(slope) = ???

In practice ...

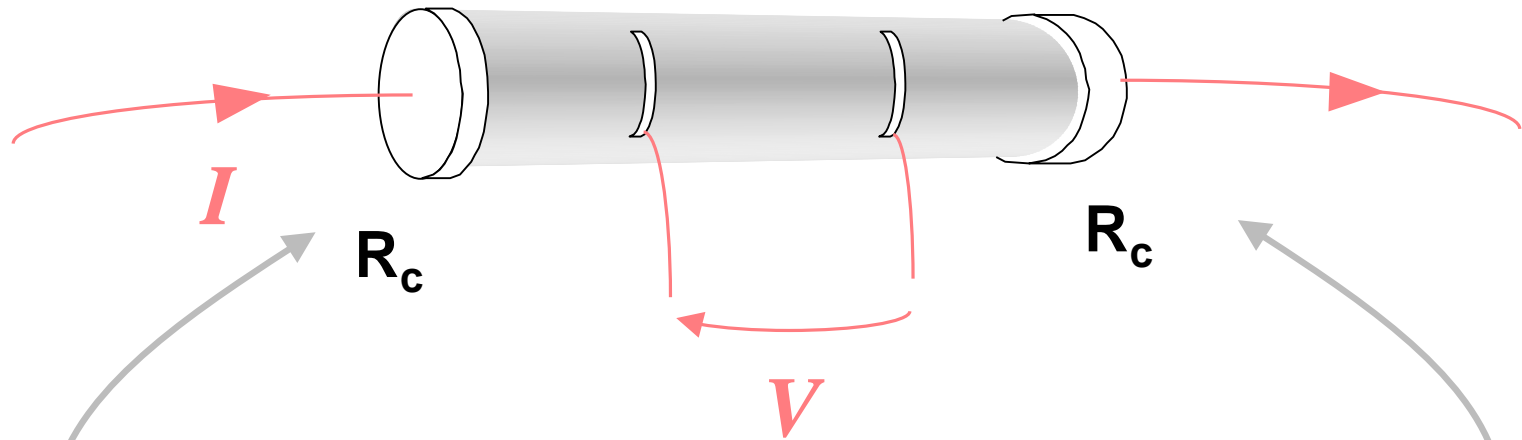
Most high-T_c superconductors have a non-linear characteristic which can be described by a **power law**

$$E(J) = E_c \left(\frac{J}{J_c} \right)^n$$



The definition of J_c requires a electric field threshold often (by convention) referred as $E_c = 1 \mu\text{V/cm}$.

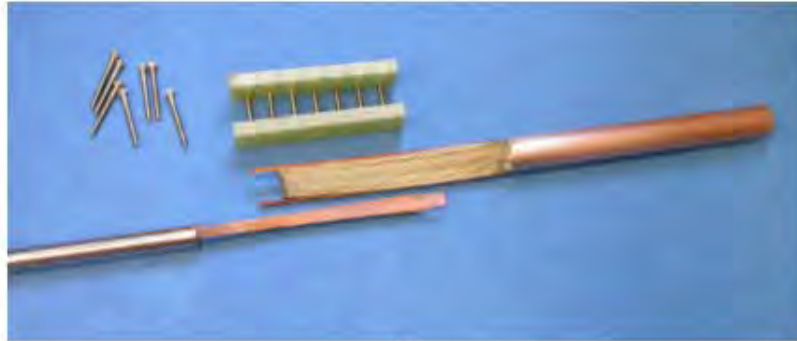
The main difficulty for transport measurements on superconductors = ?



The finite resistance
of electrical contacts

HEATING $P = R_c I^2 (>>)$

Achieving a small contact resistance is essential



(a)



(b)

PSFC/JA-16-41

Termination Methods for REBCO Tape High-Current Cable Conductors

M. Takayasu, L. Chiesa*, and J.V. Minervini

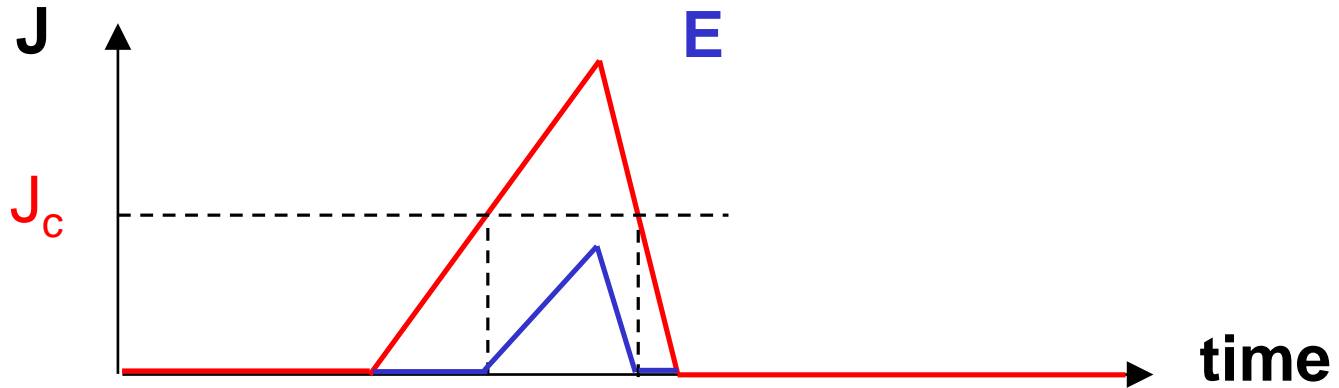
*Tufts University, Mechanical Engineering, Medford, MA 02155, USA

June 19, 2016

Plasma Science and Fusion Center
Massachusetts Institute of Technology
Cambridge, MA 02139

Fig. 10 Termination of a 40 YBCO tape cable tested at KIT, Germany in August 2012. It was operated at 10 kA. (a) Assembling parts of a BSCCO terminator with a stacked tape cable. (b) Assembled termination. The joint section of YBCO and BSCCO tapes was clamped with 70 mm length G10 plate without soldering.

Use of pulsed currents



Study of the superconducting transition at high pulsed current of bulk Bi-2223 sintered and textured by hot forging

J.G. Noudem^{a,b,*}, L. Porcar^{a,b}, O. Belmont^{b,c}, D. Bourgault^a, J.M. Barbut^b,
J. Beille^c, P. Tixador^d, M. Barrault^b, R. Tournier^a

PHYSICA C

Physica C 281 (1997) 339–344

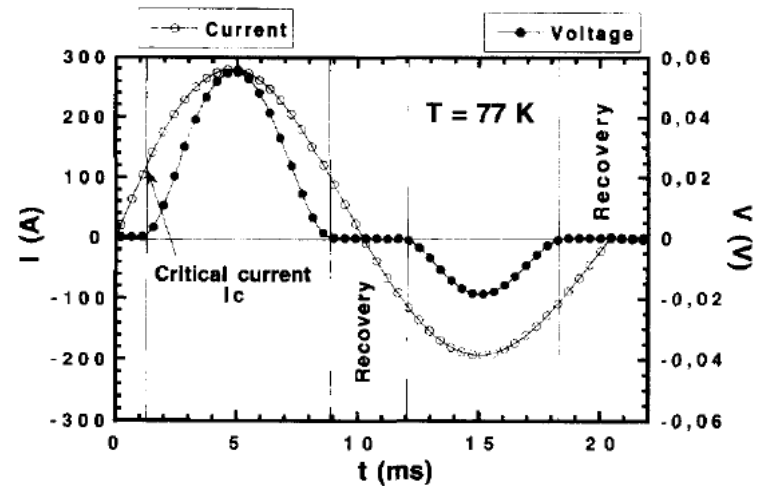
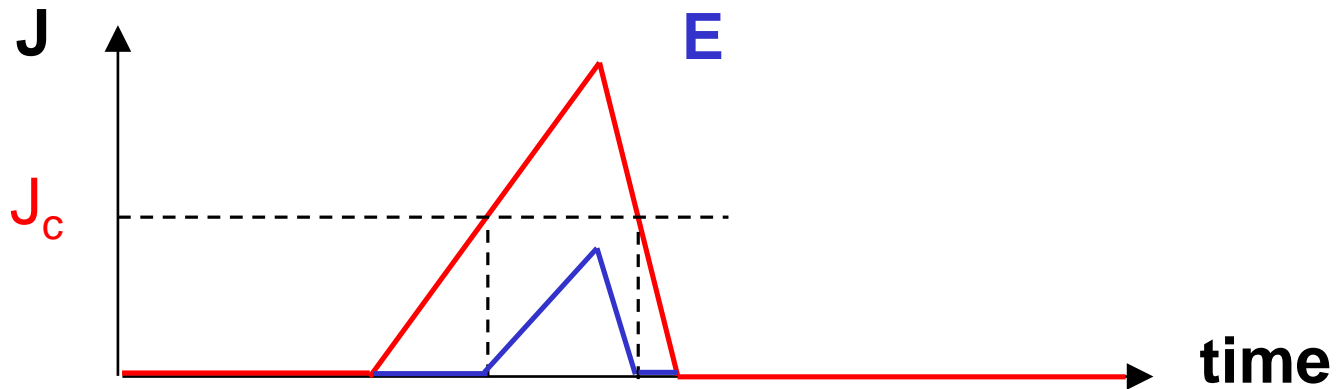
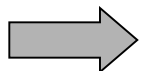
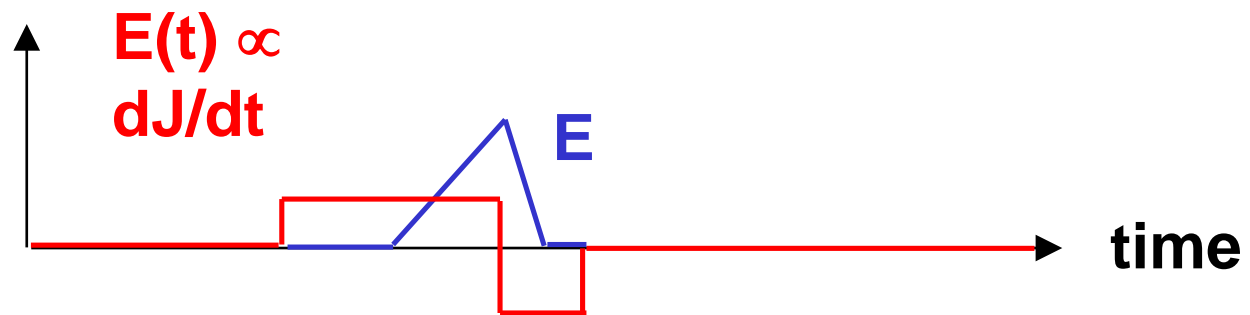


Fig. 4. Current and voltage waveforms given by a textured sample.

Caution : inductive pick-up



$$J(t) \rightarrow B(t) \rightarrow E(t) \propto dJ(t)/dt !$$



In practice, compensation circuits are needed (Rogowski coil, dummy loop...)

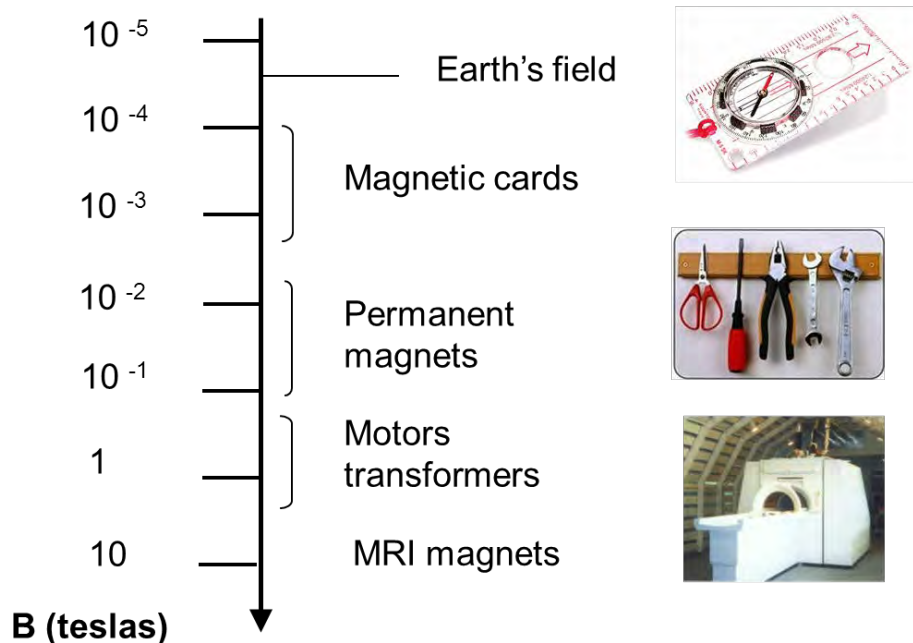
Outline

- Transport measurements - $R(T)$
- Transport measurements - $E(J)$
- **Magnetic measurements (general)**
- Magnetic measurements - $M(H)$

What are we talking about ?

$$\underline{\mathbf{B}} = \mu_0 (\underline{\mathbf{H}} + \underline{\mathbf{M}})$$

H = magnetic field [A / m]
M = magnetization [A / m]
B = magnetic induction [T]



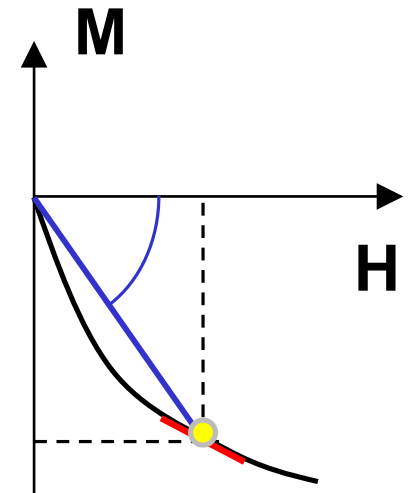
And a little bit more ...

m = magnetic moment [A.m²]

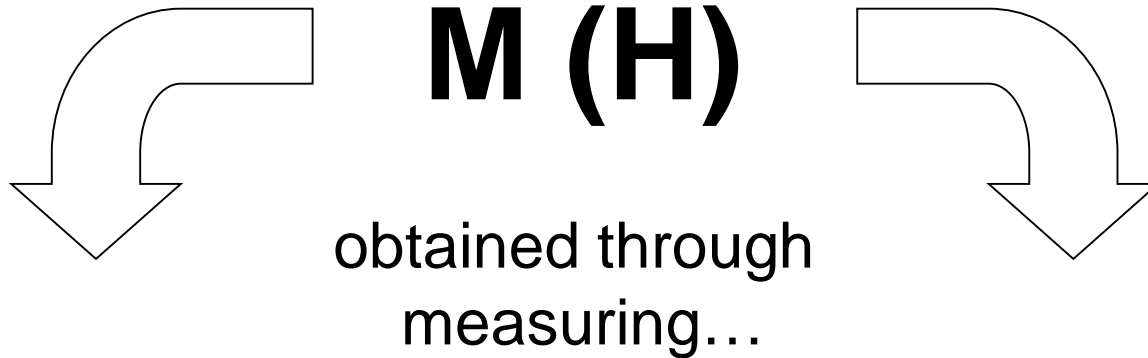
M = magnetization [A / m]
(= m / V)

χ_{DC} = magnetic susceptibility
(= M / H) [DC]

χ_{AC} = magnetic susceptibility
(= dM / dH) [AC]



What do we need to measure ?



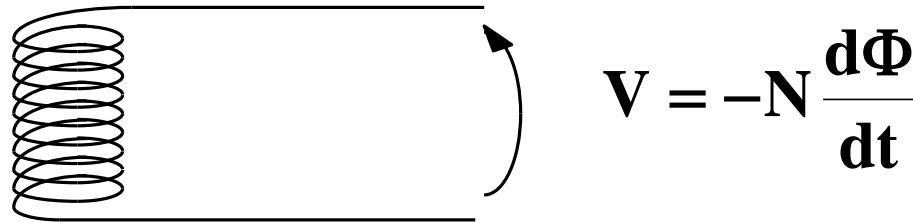
m = magnetic moment
 $M = m / V$

B = magnetic induction
without sample $H = B/\mu_0$

i = magnet current
 $H = k \cdot i$ (k ~ magnet)

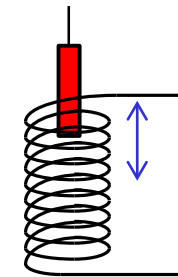
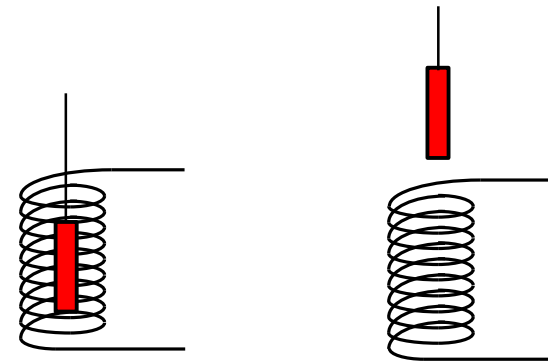
How can we measure ?

A lot of magnetic measurements are carried out using Faraday's law



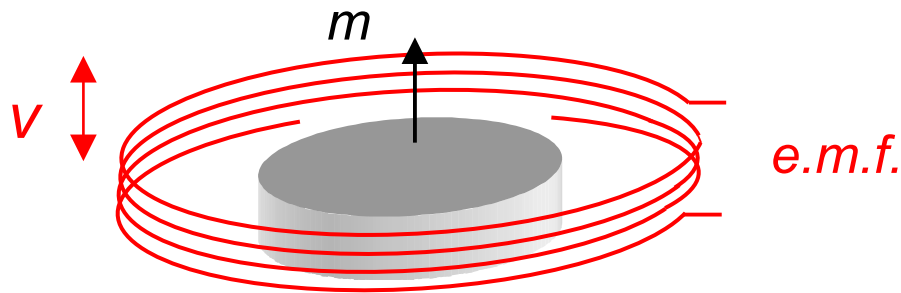
Applications :

- Extraction method (cf. PPMS)
- Vibrating Sample Magnetometer (VSM)
- Measure of a flux variation with analog or digital integration



$$H(t) \rightarrow d\Phi(t)/dt \rightarrow \Delta\Phi$$

**!!! Caution : If one wants probe
the magnetic moment,
the sensing coil must be
much larger than the sample !!!**



REVIEW OF SCIENTIFIC INSTRUMENTS 86, 025107 (2015)



A flux extraction device to measure the magnetic moment of large samples; application to bulk superconductors

R. Egan,¹ M. Philippe,¹ L. Wera,¹ J. F. Fagnard,¹ B. Vanderheyden,¹ A. Dennis,² Y. Shi,²
D. A. Cardwell,² and P. Vanderbemden¹

¹*SUPRATECS and Department of Electrical Engineering and Computer Science B28, Sart-Tilman,
B-4000 Liège, Belgium*

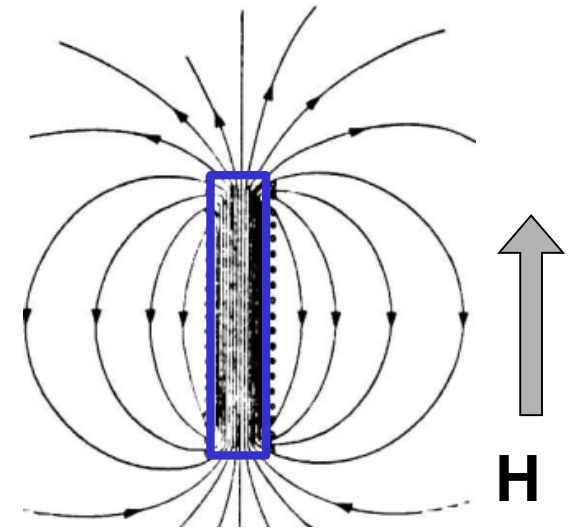
²*Bulk Superconductivity Group, Engineering Department, Cambridge University,
Cambridge CB2 1PZ, United Kingdom*

! “Demagnetizing” effects !

A magnetized sample (e.g. $M > 0$) of *finite size* creates a field in the *surrounding space* and *within the sample* itself.

This field – called *demagnetizing field* H_D – is always *opposite in direction to the sample magnetization*.

Ferromagnetic material



The *total* applied field, H_T , is the sum of the field generated by the magnet H , *and* the demagnetizing field H_D . In the simple case $H \parallel H_D$, one has

$$H_T = H + H_D$$

with

$$H_D = - \mathbf{D} \mathbf{M}$$

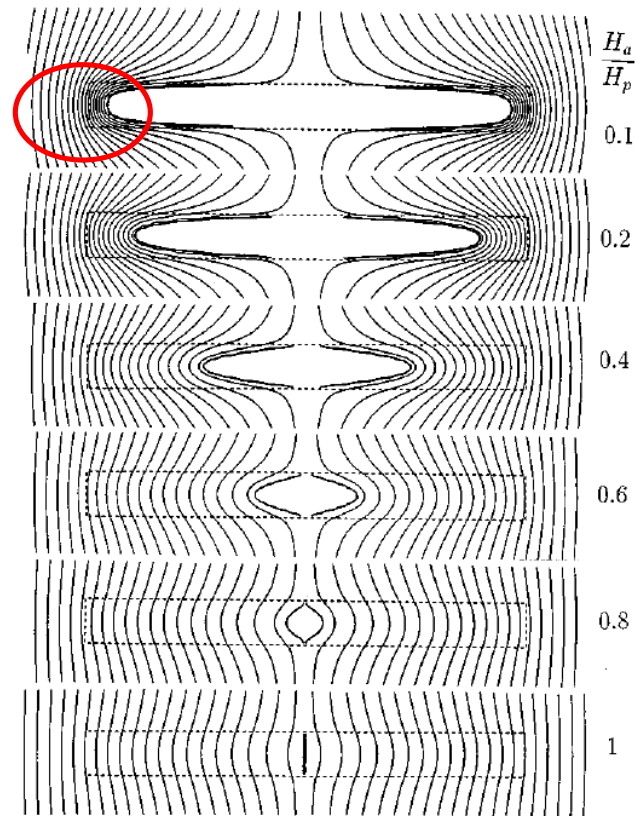
\mathbf{D} represents the dimensionless *demagnetizing factor*

Therefore ...

For ferromagnetic materials ($M > 0$),
 H_T is smaller than H ("de-magnetizing")

while for superconductors in the diamagnetic state ($M < 0$),
 H_T is bigger than H ("re-magnetizing" ?).

Superconductor



NB : To understand magnetic flux penetration in Type-II superconductors of finite size, see...

PHYSICAL REVIEW B

VOLUME 40, NUMBER 13

1 NOVEMBER 1989

Critical state in disk-shaped superconductors

M. Däumling and D. C. Larbalestier*

Applied Superconductivity Center, University of Wisconsin-Madison, Madison, Wisconsin 53706

(Received 24 July 1989)

We have calculated the magnetic fields and currents occurring in a disk-shaped superconductor (radius \gg thickness) in the critical state in a self-consistent way using finite-element analysis. We find that the field shielded (or trapped) in the center of the disk is roughly equal to $J_c d$, where d is the thickness of the disk. The shielding currents also create radial fields which are of order $J_c d/2$ on the disk surface. For low applied fields $H_{\text{appl}} < J_c d$ these self-field effects dominate,

PHYSICAL REVIEW B

VOLUME 58, NUMBER 10

1 SEPTEMBER 1998-II

Superconductor disks and cylinders in an axial magnetic field. I. Flux penetration and magnetization curves

Ernst Helmut Brandt

Max-Planck-Institut für Metallforschung, D-70506 Stuttgart, Germany

(Received 14 November 1997)

.... as well as all Helmut Brandt's papers ☺

Note however the important distinction :

Demagnetizing effects should always be taken into account when the sample cannot be considered infinitely long

BUT...

the conventional « demagnetizing factor » approach, strictly speaking, is valid for linear materials.

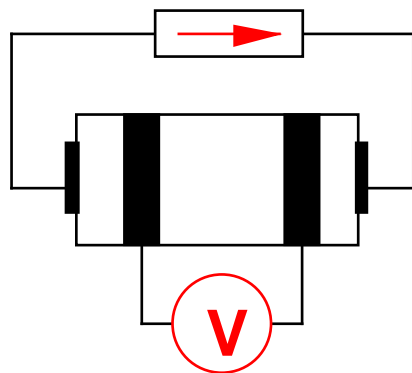
For type-II superconductors, only (semi-) analytical calculations and numerical modelling are appropriate !

Outline

- Transport measurements - $R(T)$
- Transport measurements - $E(J)$
- Magnetic measurements (general)
- **Magnetic measurements - $M(H)$**

Transport measurement

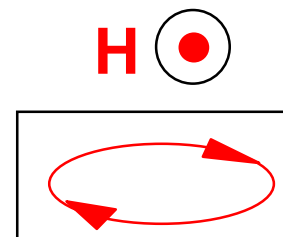
Current source



Transport current
(applied externally)

Magnetic measurement

Magnetic field H



Induced current
(by the applied magnetic field)

ADVANTAGE of
magnetic measurements :

**No need
of electrical contacts !**

DRAWBACK of
magnetic measurements :

**Requires a suitable model
(geometry-dependent!)**

Bean model : relation $B \leftrightarrow J_c$

Hypotheses :

$$H_{C1} \rightarrow 0 \quad H_{C2} \rightarrow \infty \quad \text{Very strong pinning}$$

Model :

$$\text{curl } B = \mu_0 J$$

$$J = +J_c, -J_c \text{ or } 0$$

Critical state

VOLUME 8, NUMBER 6

PHYSICAL REVIEW LETTERS

MARCH 15, 1962

MAGNETIZATION OF HARD SUPERCONDUCTORS

C. P. Bean

General Electric Research Laboratory, Schenectady, New York

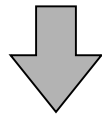
(Received October 26, 1961; revised manuscript received February 21, 1962)

Bean model : relation $B \leftrightarrow J_c$

2 additional hypotheses

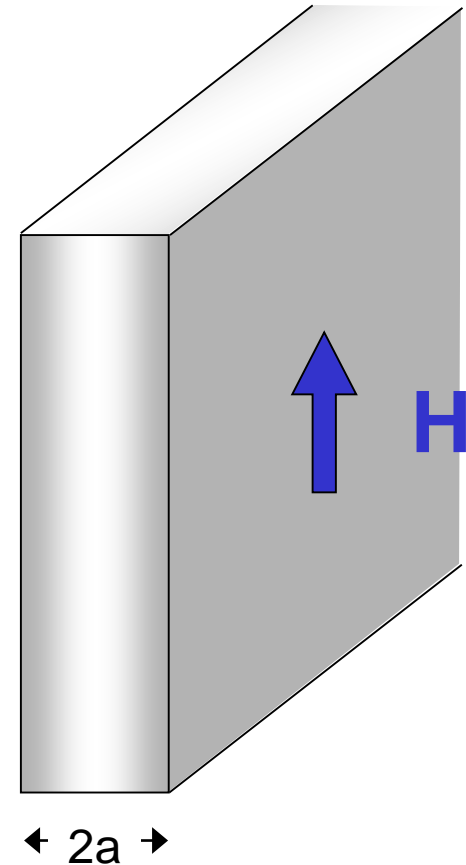
- (1) supercond. ∞ || applied field
(ex. infinite slab)

$$\text{curl } \mathbf{B} = \pm \mu_0 \mathbf{J}_c \text{ ou } 0$$

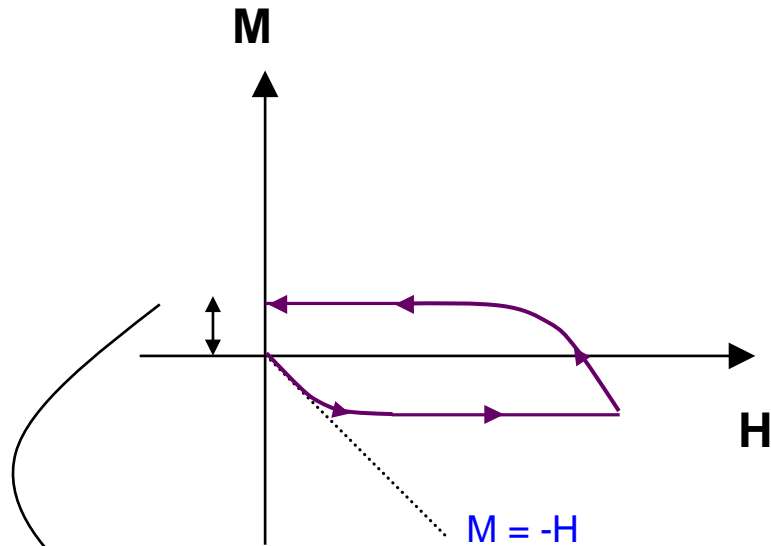


$$\left| \frac{\partial \mathbf{B}}{\partial y} \right| = \mu_0 \mathbf{J}_c \text{ ou } 0$$

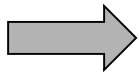
- (2) $J_c = \text{constant}$ (indep. of B)



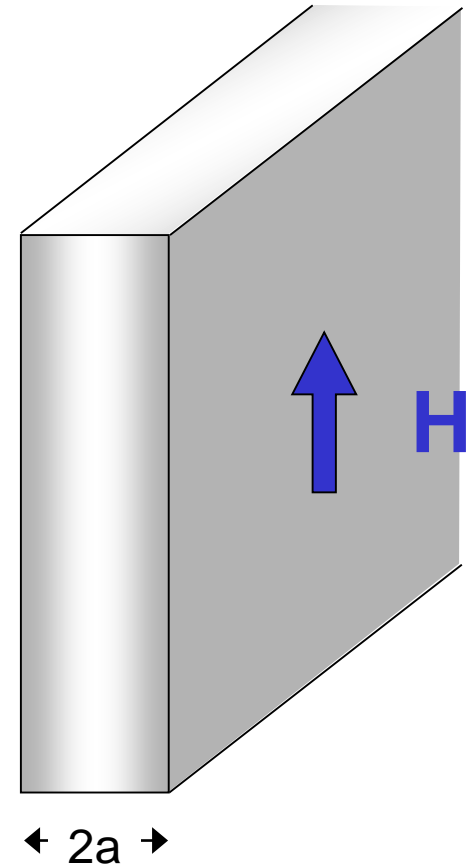
Bean model : relation $B \leftrightarrow J_c$



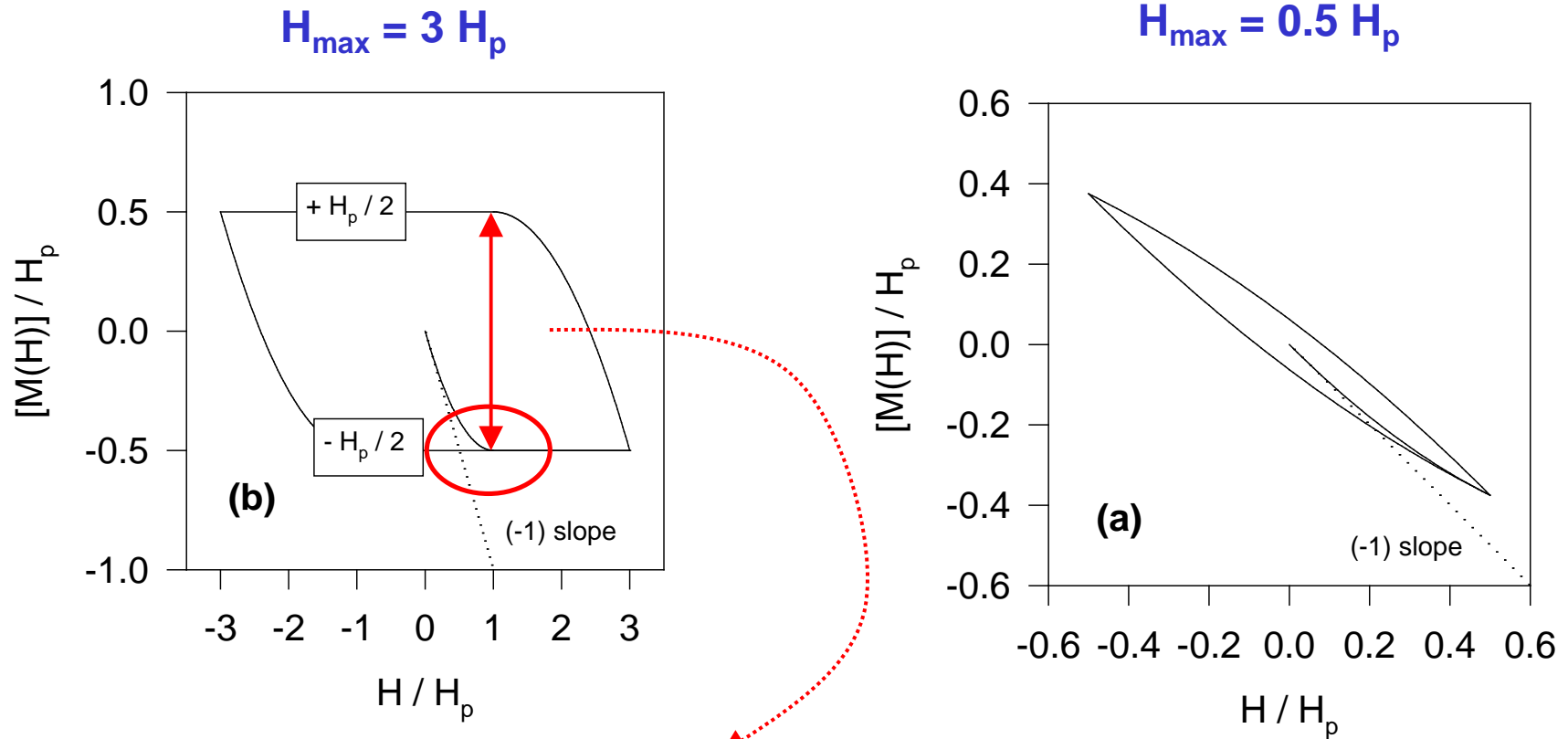
Remnant magnetization
 $= (J_c a) / 2$



Indirect
determination of J_c



Different “M(H)” curves for type II (hard) superconductor as a function of H_{\max}

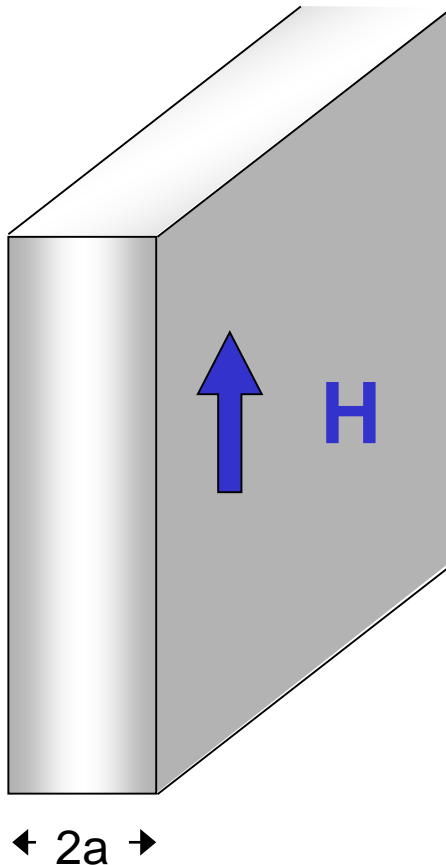


The difference betw. M_{\downarrow} and M_{\uparrow} is H_p ($= J_c \cdot a$) in the case of an infinite slab

BUT... this is only true when the maximum field H_{\max} is large enough !

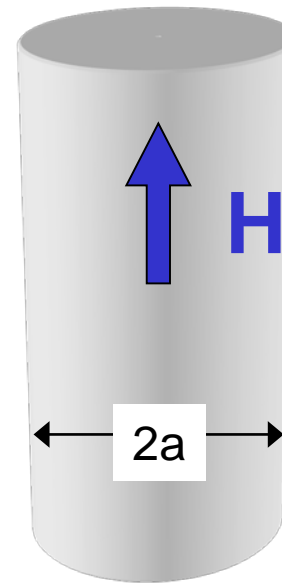
The relation between ΔM and J_c depends on the geometry of the sample

Infinite slab



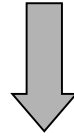
$$J_c = \frac{\Delta M}{a}$$

Infinite cylinder



$$J_c = \frac{3\Delta M}{2a}$$

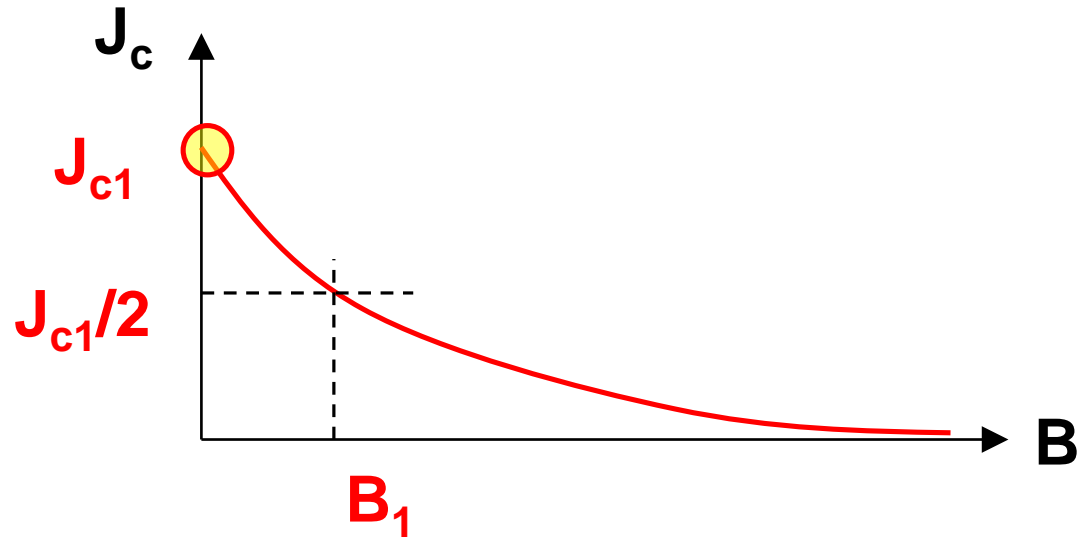
And what happens in the case of $J_c(B)$?



A model of $J_c(B)$ is required !

Ex : Kim model

$$J_c = J_{c1} \left(\frac{B_1}{B + B_1} \right)$$



Kim model for magnetization of type-II superconductors

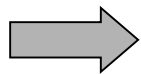
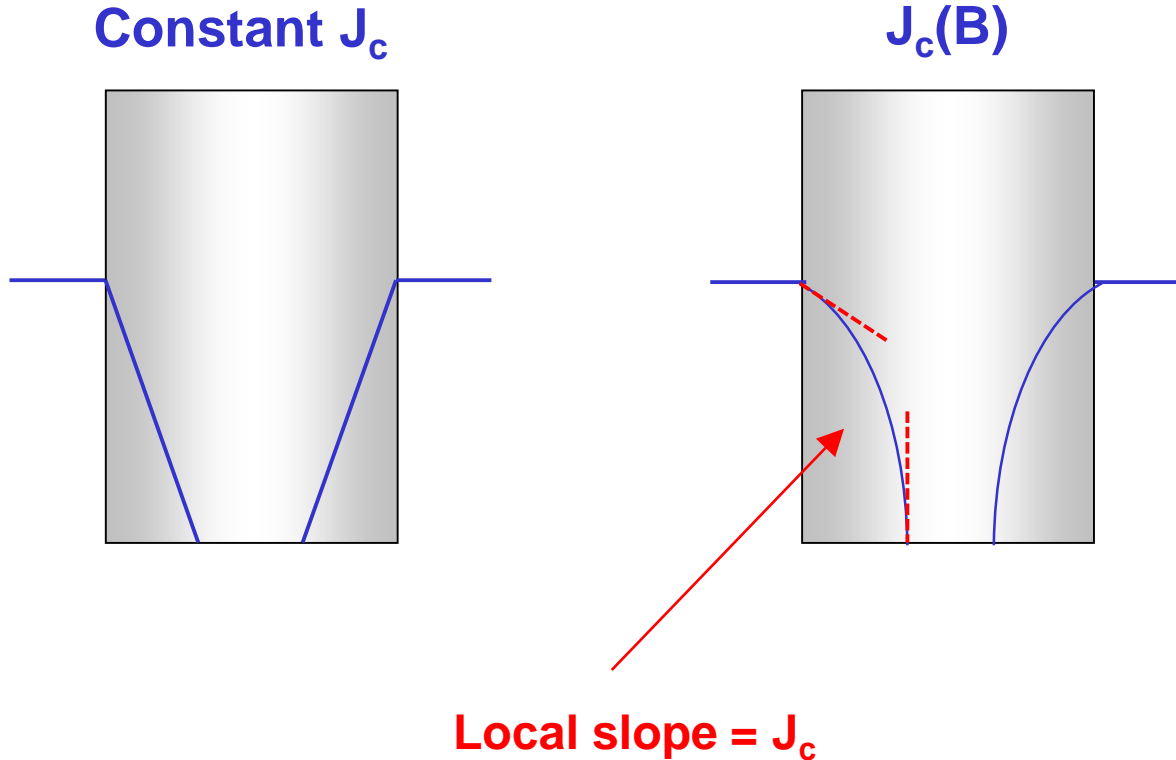
D.-X. Chen^{a)} and R. B. Goldfarb

*Electromagnetic Technology Division, National Institute of Standards and Technology,^{b)}
Boulder, Colorado 80303*

(Received 31 January 1989; accepted for publication 18 May 1989)

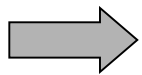
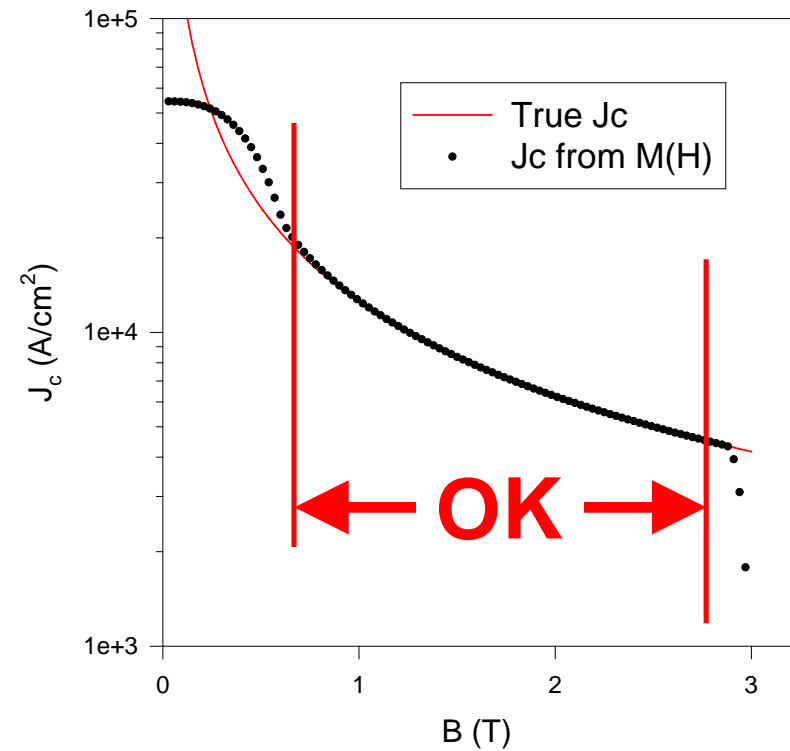
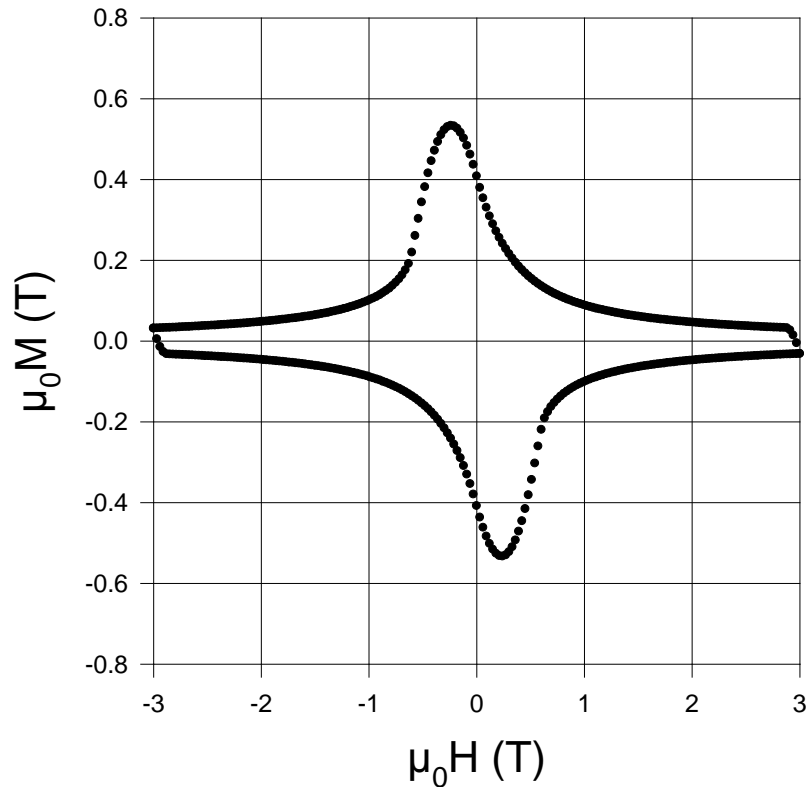
J. Appl. Phys. **66** (6) 15 September 1989

Consequences on the magnetic field penetration



Completely different magnetization curves are expected !

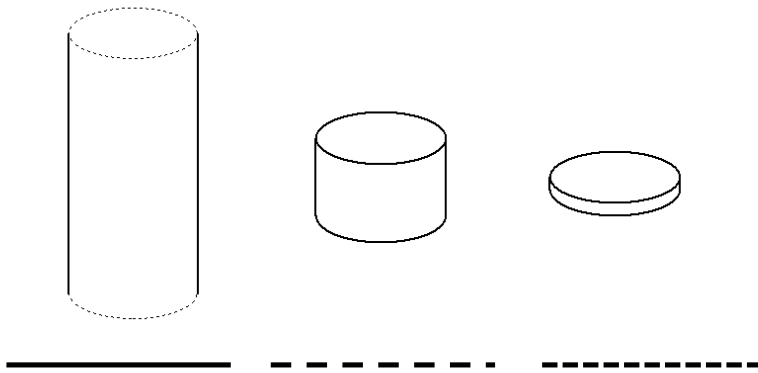
Infinite slab with $J_c \propto (1/B)$



Remarkably, the $J_c(B)$ can often (not always...) be determined from ΔM , provided that the magnetic field range does not extend too close to 0 and to H_{max} !

And what happens if the superconductor cannot be assumed to be infinite ?

Modelling needed !



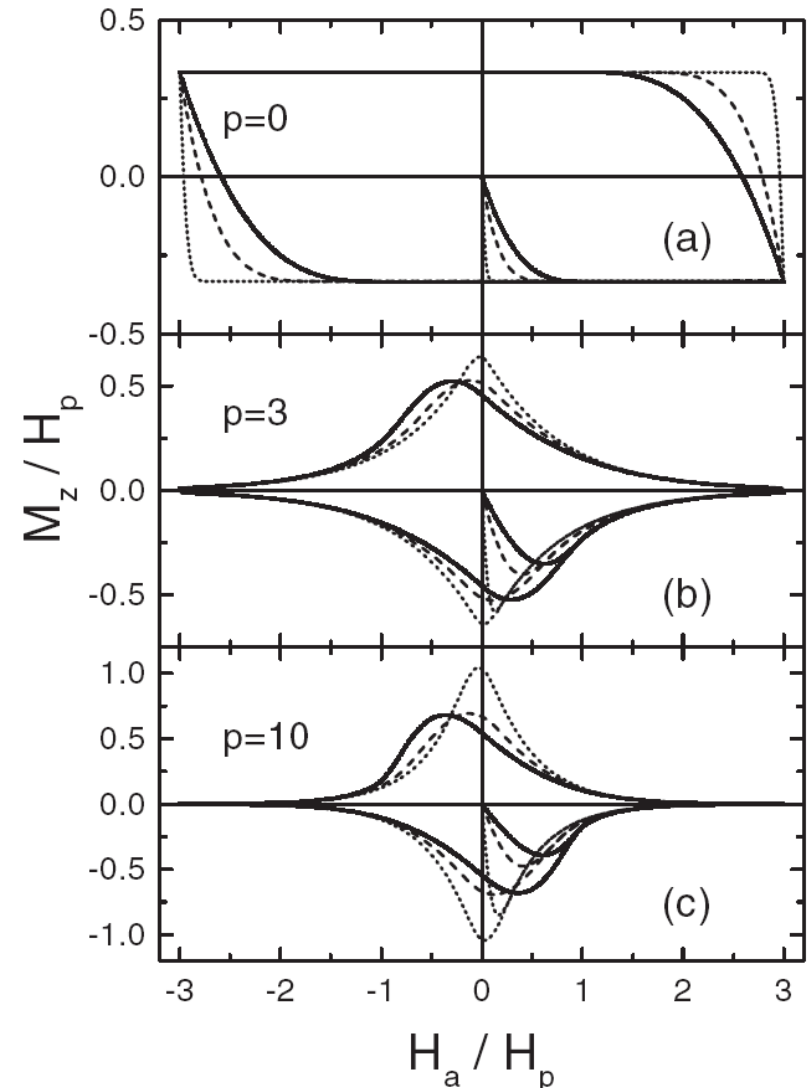
Critical-current density from magnetization loops of finite high- T_c superconductors

Alvaro Sanchez¹ and Carles Navau^{1,2}

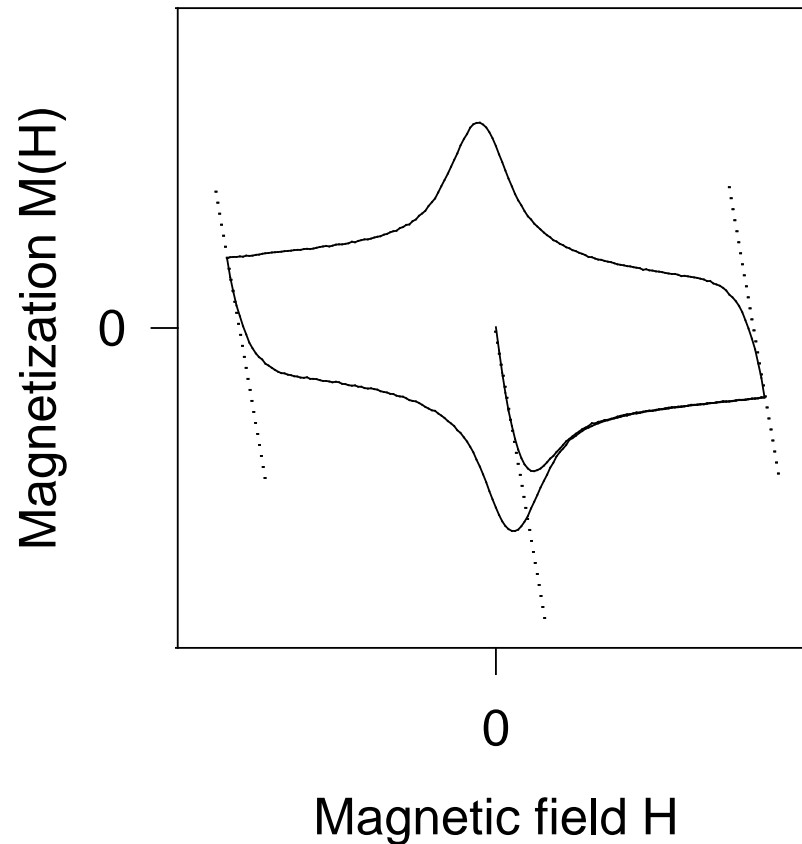
¹ Grup d'Electromagnetisme, Departament de Física, Universitat Autònoma Barcelona, 08193 Bellaterra (Barcelona), Catalonia, Spain

² Escola Universitària Salesiana de Sarrià, Rafael Batlle 7, 08017 Barcelona, Catalonia, Spain

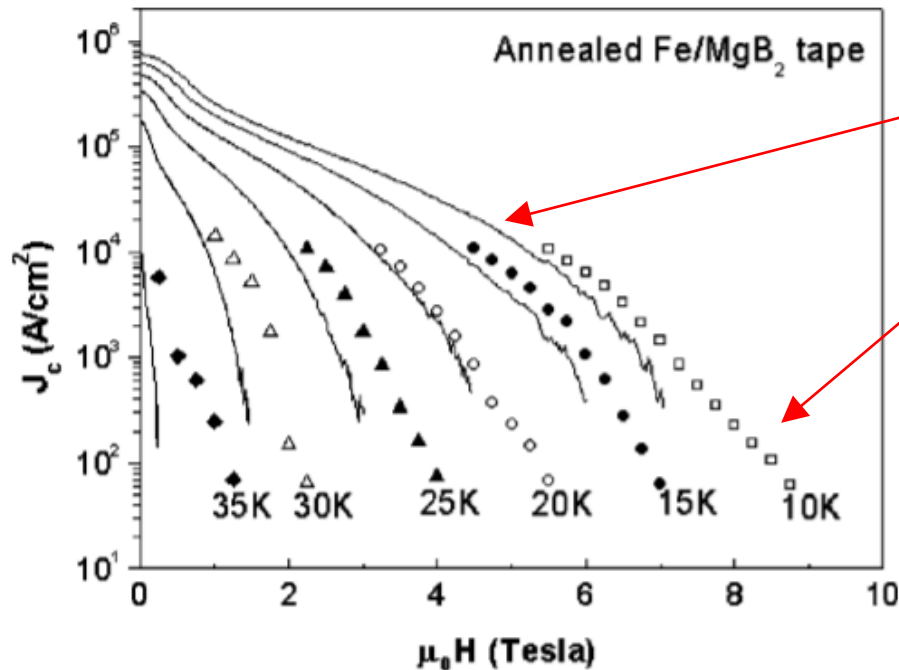
Supercond. Sci. Technol. **14** (2001) 444–447



A typical $M(H)$ curve at “medium” applied fields...



If weak links (granularity) are not a problem, nice agreement between magnetic J_c & transport J_c



MAGNETIC

TRANSPORT



ELSEVIER

Available online at www.sciencedirect.com

SCIENCE @ DIRECT®

Physica C 385 (2003) 286–305

PHYSICA C

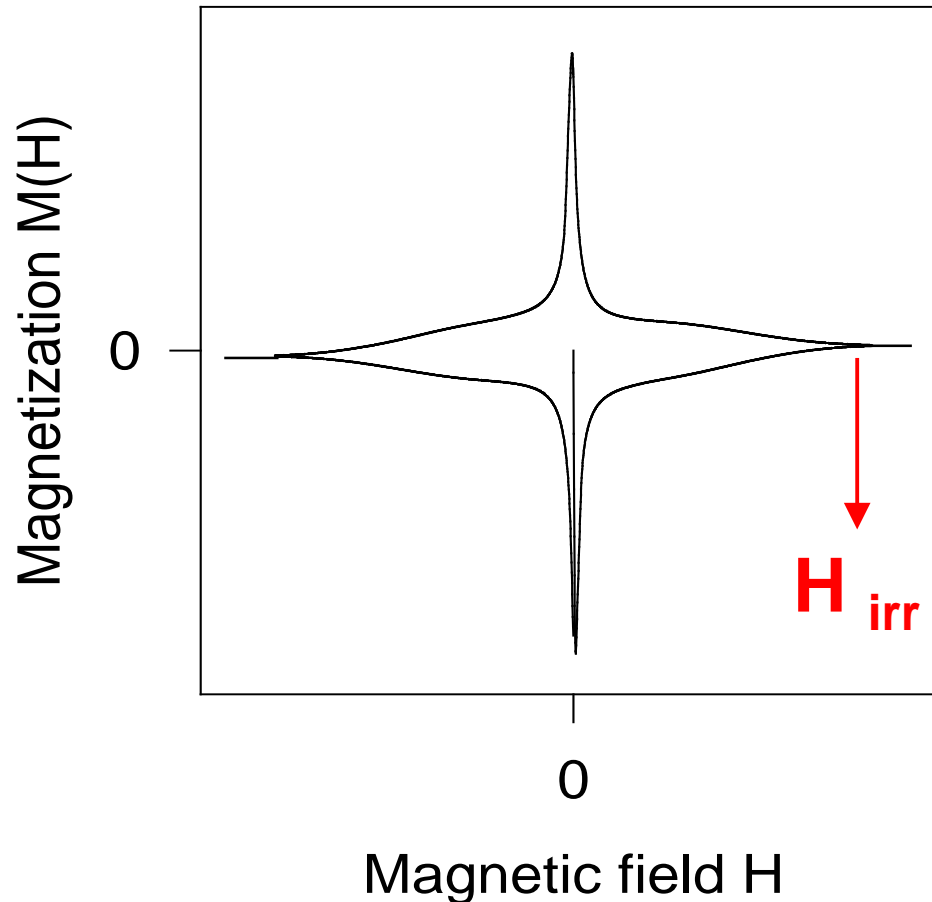
www.elsevier.com/locate/physc

Superconducting properties of MgB₂ tapes and wires

R. Flükiger *, H.L. Suo, N. Musolino, C. Beneduce, P. Toulemonde, P. Lezza

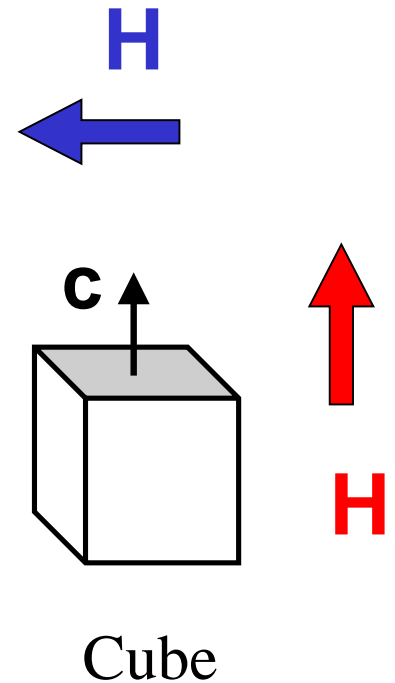
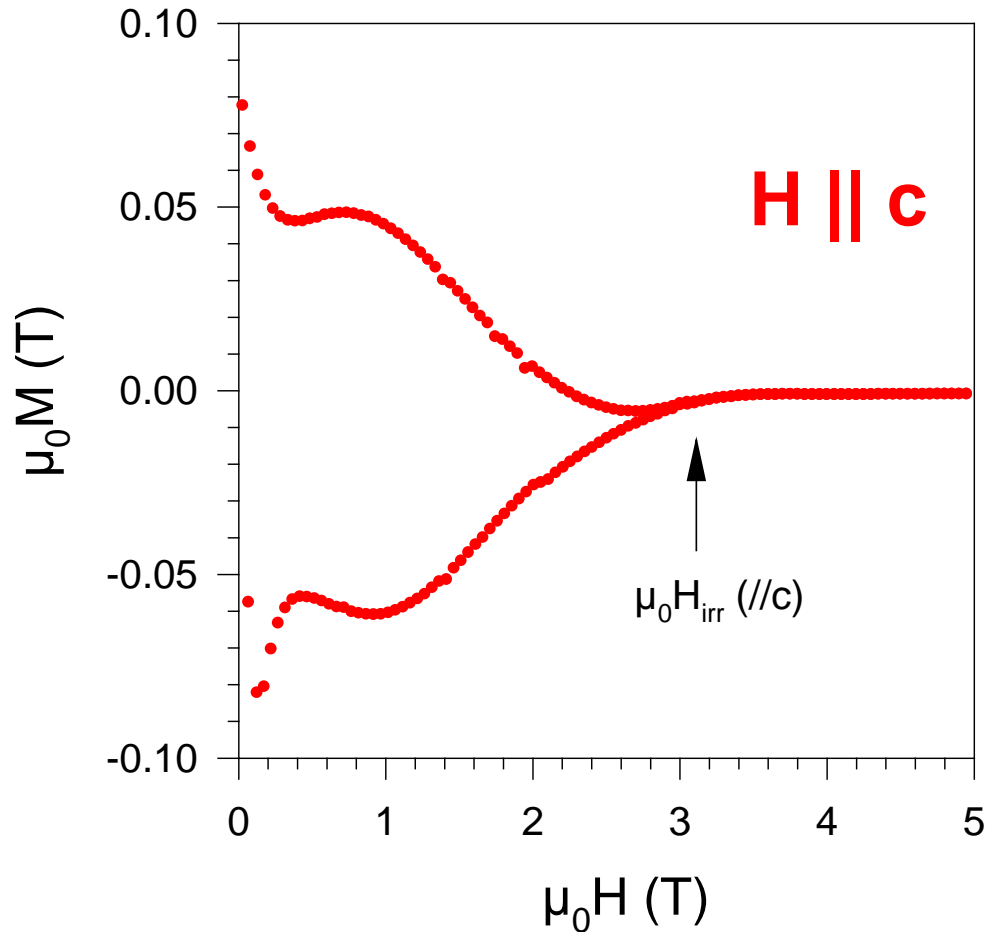
Département de Physique de la Matière Condensée, Université de Genève, 24 Quai Ernest-Ansermet, CH-1211 Genève 4, Switzerland

And when the applied field is very large ...

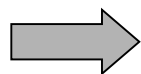
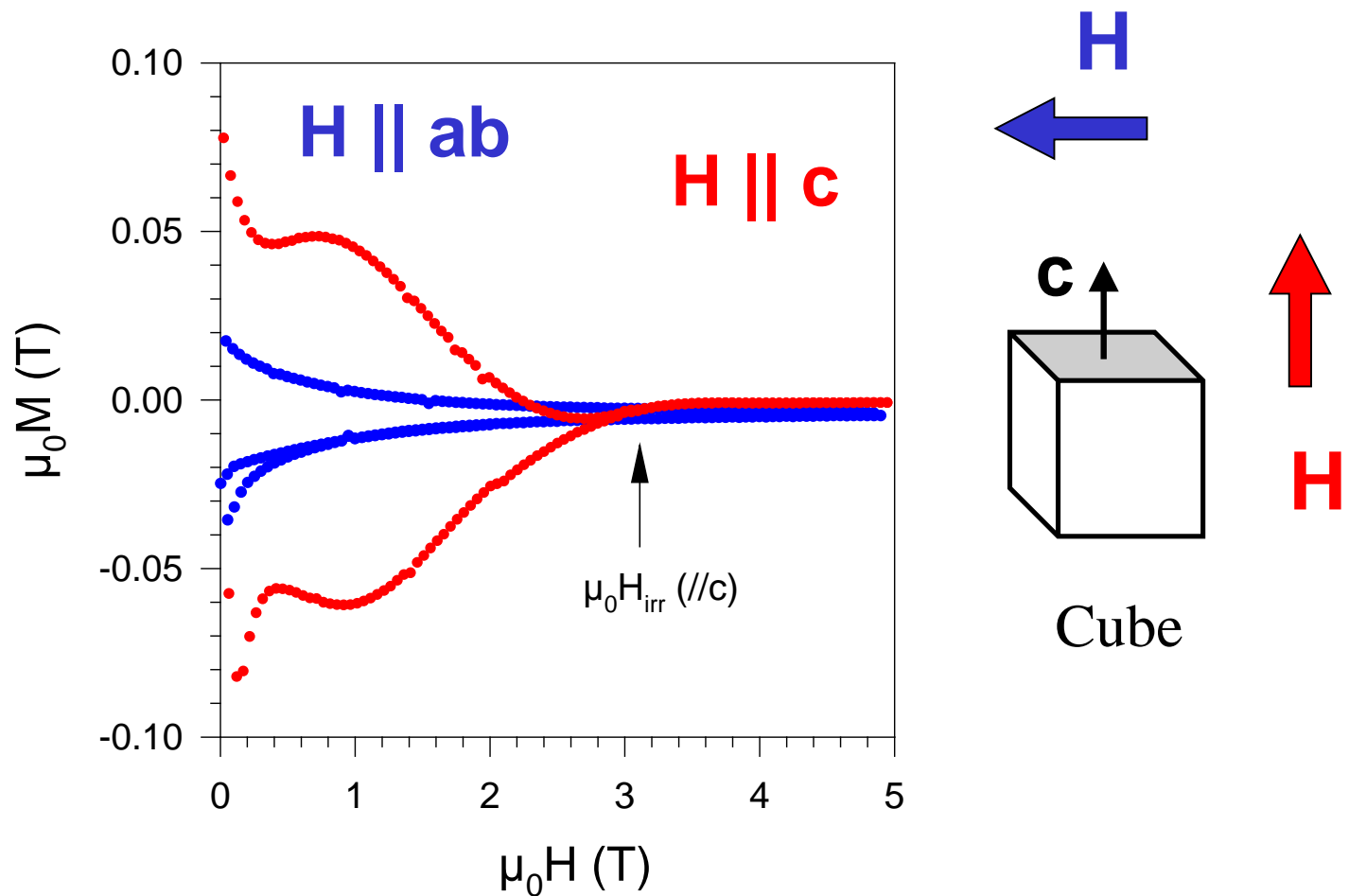


The irreversibility field can be determined from the point where the upper and lower branches of the magnetization loop merge into one

A typical curve for $\text{YBa}_2\text{Cu}_3\text{O}_7$



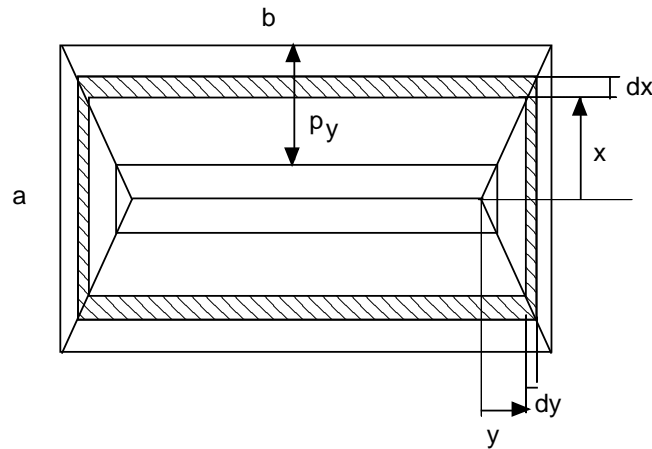
A typical curve for $\text{YBa}_2\text{Cu}_3\text{O}_7$



Anisotropy of the current loops should be taken into account to determine the critical current density J_c

Anisotropic Bean model

Analytical calculations can be made in simple geometries (ex. rectangle)



But some results have been published for quite a long time now !

Anisotropic critical currents in $\text{Ba}_2\text{YCu}_3\text{O}_7$ analyzed using an extended Bean model

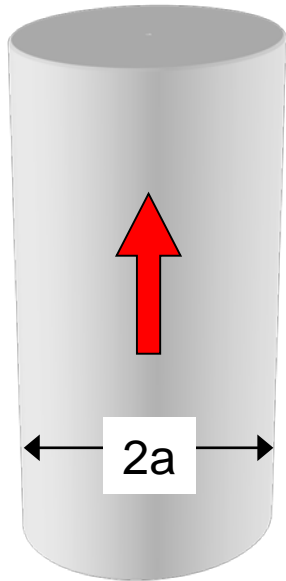
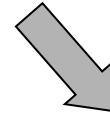
E. M. Gyorgy, R. B. van Dover, K. A. Jackson, L. F. Schneemeyer, and J. V. Waszczak
AT&T Bell Laboratories, Murray Hill, New Jersey 07974

(Received 20 March 1989; accepted for publication 12 May 1989)

We have extended Bean's critical state model to explicitly include anisotropic critical currents.

Appl. Phys. Lett. 55 (3), 17 July, 1989

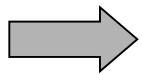
And what happens if we consider an E-J curve instead of the Bean model ?



$$H(t) \rightarrow B(t)$$

**Do NOT forget
Faraday's law**

$$E = \left(\frac{a}{2} \right) \frac{dB}{dt}$$



There is always an **electric field** in magnetic experiments !

The amplitude of this field is **much smaller than in transport experiments**

Do not forget to consider these 3 quantities...

Current density : **J (A/m²)**

Magnetic flux density : **B (T)**

Electric field : **E (V/m)**

Supercond. Sci. Technol. 7 (1994) 412–422. Printed in the UK

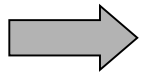
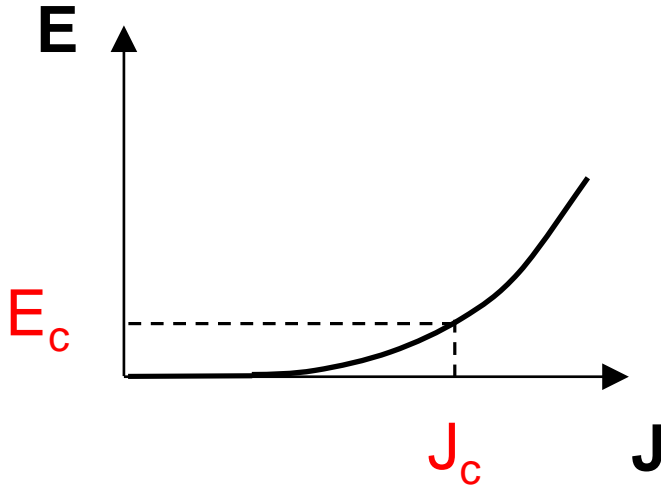
**The electric field within high-
temperature superconductors:
mapping the E – J – B surface**

A D Caplin, L F Cohen, G K Perkins and A A Zhukov†

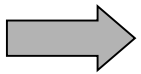
Centre for High Temperature Superconductivity, Blackett Laboratory, Imperial
College, London SW7 2BZ, UK

Received 13 January 1994

Consequence ...



The amplitude of induced currents increases for large dB/dt !



Always specify dB/dt !

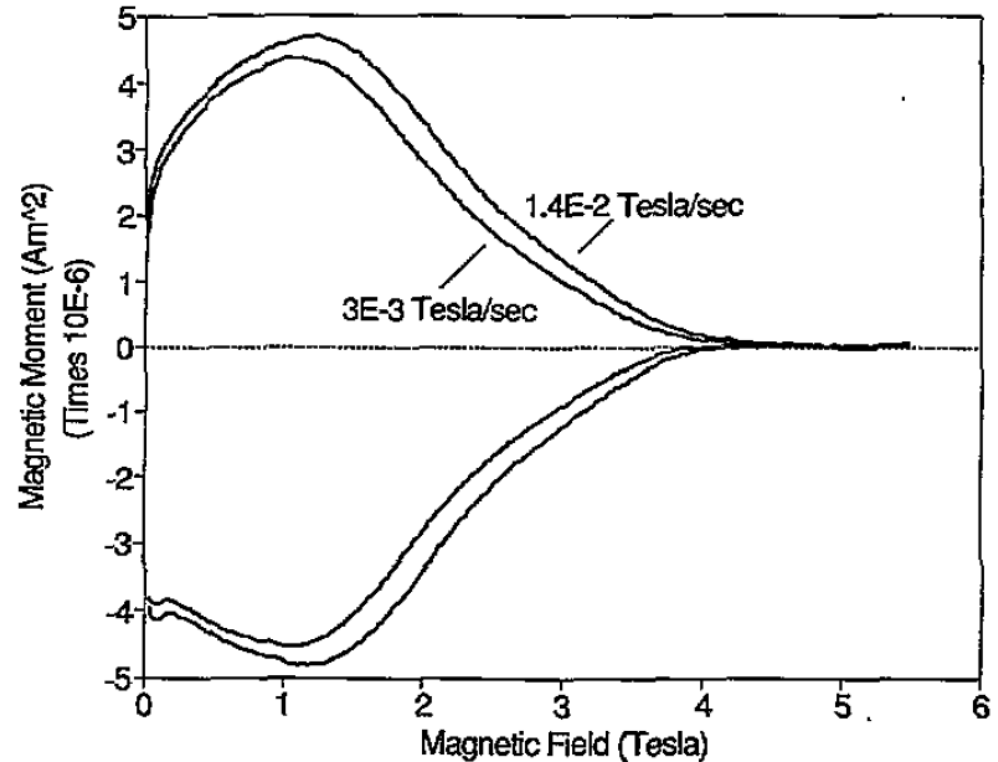
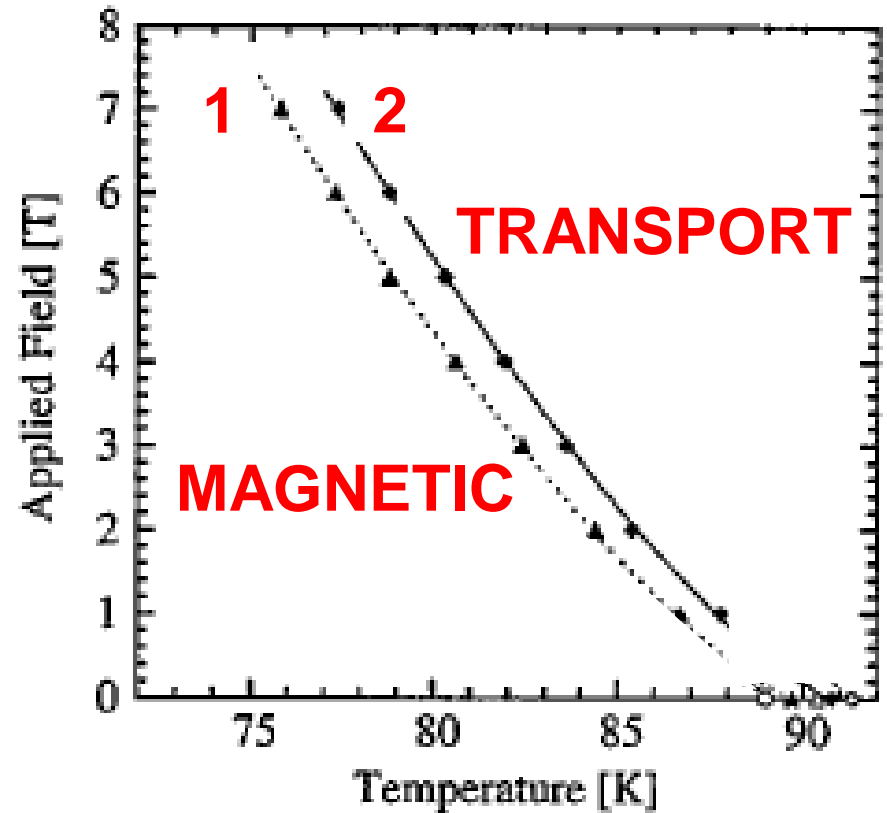
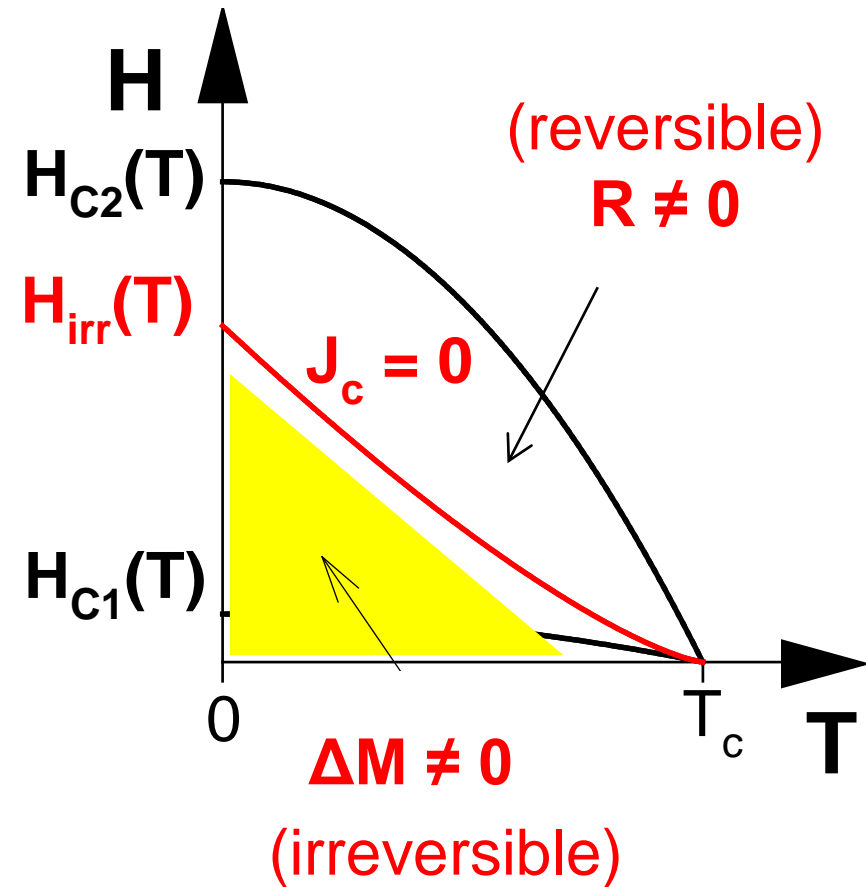


Figure 1. Typical magnetization loops of a high-quality YBa₂Cu₃O₇ single crystal at 84 K. Two loops are shown, the outer one having a field sweep rate \dot{H}_{app} of about five times the inner one. H_{app} is parallel to the c -axis. Note the maximum (the 'fishtail' feature) in the magnetic moment at about 1.2 T.

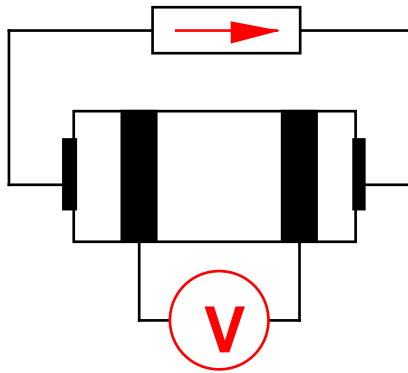
Irreversibility field from TRANSPORT and MAGNETIC



Doyle et al., APL 73, 117 (1998)

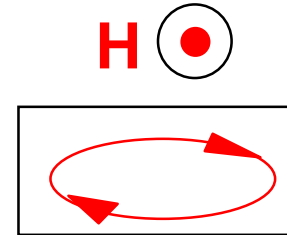
Conclusion

Current source



Transport current
(applied externally)

Magnetic field H



Induced current
(by the applied magnetic field)

**Both kind of measurements are very useful
and can provide invaluable information on the material properties**

BUT ... Be always careful when interpreting the results !

References

- [1] D. Dimos, P. Chaudhari, J. Mannhart, and F. K. LeGoues, “*Orientation Dependence of Grain-Boundary Critical Currents in $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$ Bicrystals*”, Phys. Rev. Lett. 61, 219 (1988)
- [2] W. K. Kwok, S. Fleshier, U. Welp, V. M. Vinokur, J. Downey, G. W. Crabtree and M. M. Miller, “*Vortex Lattice Melting in Untwinned and Twinned Single Crystals of $\text{YBa}_2\text{Cu}_3\text{O}_7$* ” Phys. Rev. Lett. 69, 3370 (1992)
- [3] Ph. Vanderbemden, A.D. Bradley, R.A. Doyle, W. Lo, D.M. Astill, D.A. Cardwell, and A.M. Campbell, “*Superconducting properties of natural and artificial grain boundaries in bulk melt-textured YBCO*”, Physica C 302, 257 (1998)
- [4] Th. Siebold, C. Carballeira, J. Mosqueira, M.V. Ramallo and Félix Vidal “*Current redistributions in superconductors with non-uniformly distributed T_c -inhomogeneities*”, Physica C 282-287, 1181 (1997)
- [5] “*Distorted low-level signal readback of AC signals in the PPMS in the temperature range 25-35 K due to Inconel mitigation of inductive cross talk*”, Quantum Design Application Note
- [6] J.G. Noudem, L. Porcar, O. Belmont, D. Bourgault, J.M. Barbut, J. Beille, P. Tixador, M. Barrault and R. Tournier “*Study of the superconducting transition at high pulsed current of bulk Bi-2223 sintered and textured by hot forging*”, Physica C 281, 339 (1997)
- [7] R. Egan, M. Philippe, L. Wera, J. F. Fagnard, B. Vanderheyden, A. Dennis, Y. Shi, D. A. Cardwell, and P. Vanderbemden “*A flux extraction device to measure the magnetic moment of large samples; application to bulk superconductors*” Review of Scientific Instruments 86, 025107 (2015)
- [8] M. Takayasu, L. Chiesa, and J.V. Minervini “*Termination Methods for REBCO Tape High-Current Cable Conductors*” PSFC/JA-16-41 (2016)
- [9] E. H. Brandt “*Superconductor disks and cylinders in an axial magnetic field. I. Flux penetration and magnetization curves*”, Phys. Rev. B 58, 6506 (1998)
- [10] M. Däumling and D. C. Larbalestier “*Critical state in disk-shaped superconductors*” Phys. Rev. B 40 9350 (1989)
- [11] C. P. Bean “*Magnetization of hard superconductors*”, Phys. Rev. Lett. 8, 250 (1962)
- [12] D.-X. Chen and R. B. Goldfarb “*Kim model for magnetization of type-II superconductors*”, J. Appl. Phys. 66, 2489 (1989)
- [13] A. Sanchez and C. Navau “*Critical-current density from magnetization loops of finite high- T_c superconductors*”, Supercond. Sci. Technol. 14, 444 (2001)
- [14] R. Flükiger, H.L. Suo, N. Musolino, C. Beneduce, P. Toulemonde, P. Lezza “*Superconducting properties of MgB_2 tapes and wires*” Physica C 385, 286-305 (2003)
- [15] E. M. Gyorgy, R. B. van Dover, K. A. Jackson, L. F. Schneemeyer, and J. V. Waszczak, “*Anisotropic critical currents in $\text{Ba}_2\text{YCu}_3\text{O}_7$ analyzed using an extended Bean model*”, Appl. Phys. Lett. 55, 283 (1989)
- [16] A. D. Caplin, L. F. Cohen, G. K. Perkins and A. A. Zhukov, “*The electric field within high-temperature superconductors: mapping the E - J - B surface*”, Supercond. Sci. Technol. 7, 412 (1994)
- [17] R. A. Doyle, A. D. Bradley, W. Lo, D. A. Cardwell, A. M. Campbell, Ph. Vanderbemden, and R. Cloots “*High field behavior of artificially engineered boundaries in melt-processed $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$* ”, Appl. Phys. Lett. 73, 117 (1998).