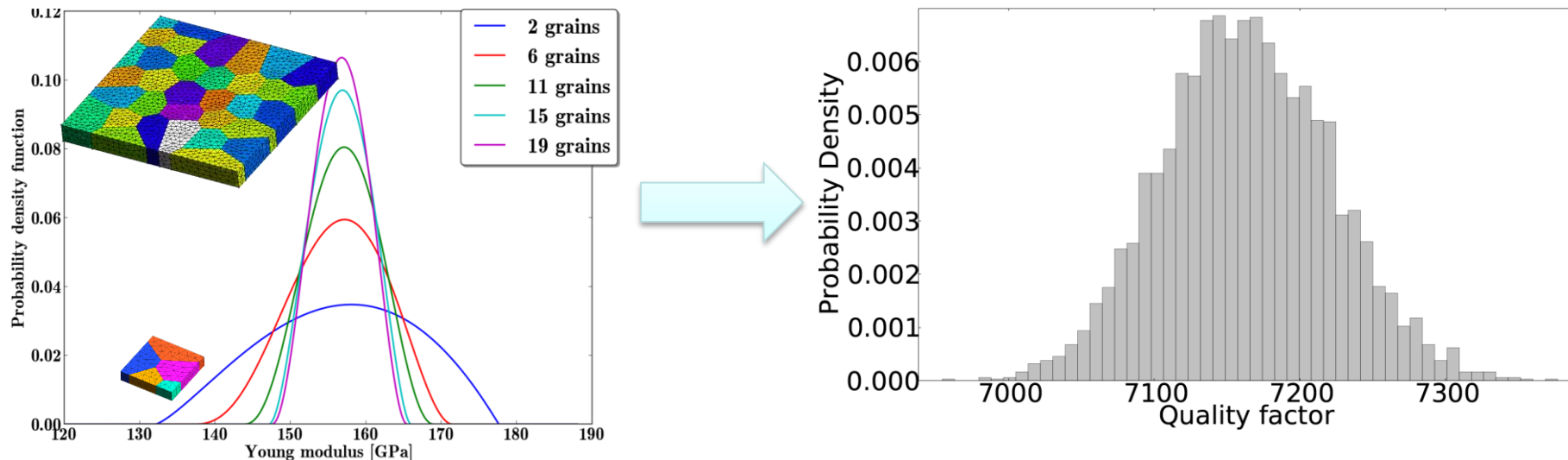


# Probabilistic prediction of the quality factor of micro-resonator using a stochastic thermo-mechanical multi-scale approach

*Wu Ling, Lucas Vincent, Nguyen Van-Dung, Paquay Stéphane,  
Golinval Jean-Claude, Noels Ludovic*



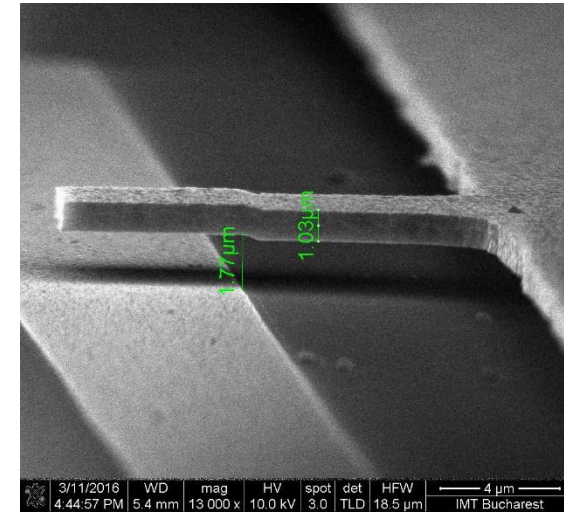
3SMVIB: The research has been funded by the Walloon Region under the agreement no 1117477 (CT-INT 2011-11-14) in the context of the ERA-NET MNT framework. Experimental measurements provided by IMT Bucharest (Voicu Rodica, Baracu Angela, Muller Raluca)

# The problem

- MEMS structures

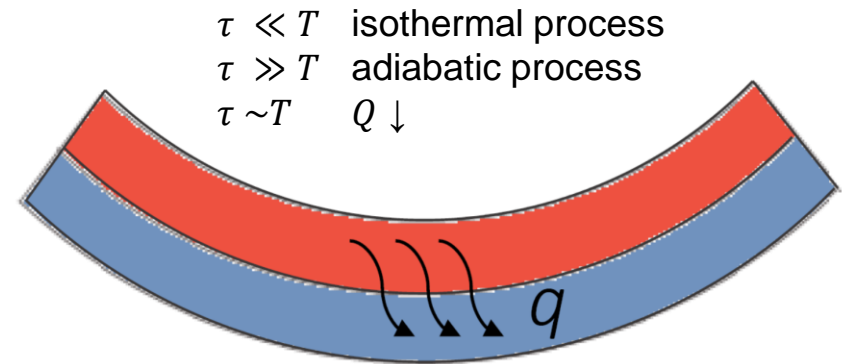
- Are not several orders larger than their micro-structure size
- Parameters-dependent manufacturing process
  - Low Pressure Chemical Vapor Deposition (LPCVD)
  - Properties depend on the temperature, time process, and flow gas conditions
- As a result, their macroscopic properties can exhibit a **scatter**
  - Due to the fabrication process (photolithography, wet and dry etching)
  - Due to uncertainties of the material
  - ...

➔ The objective of this work is to estimate this scatter



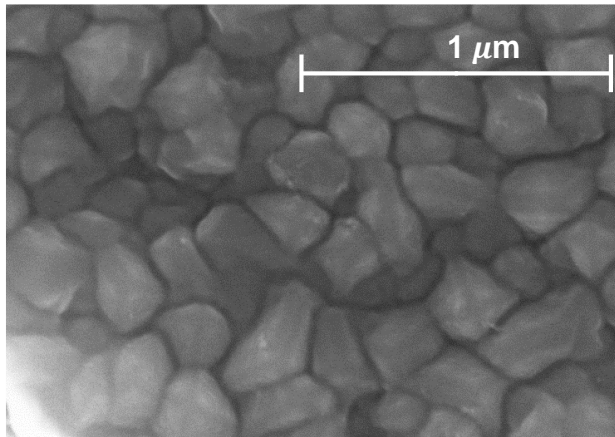
# The problem

- Application example
  - Poly-silicon resonators
  - Quantities of interest
    - Eigen frequency
    - Quality factor due to thermoelastic damping  $Q \sim W/\Delta W$
    - Thermoelastic damping is a source of intrinsic material damping present in almost all materials

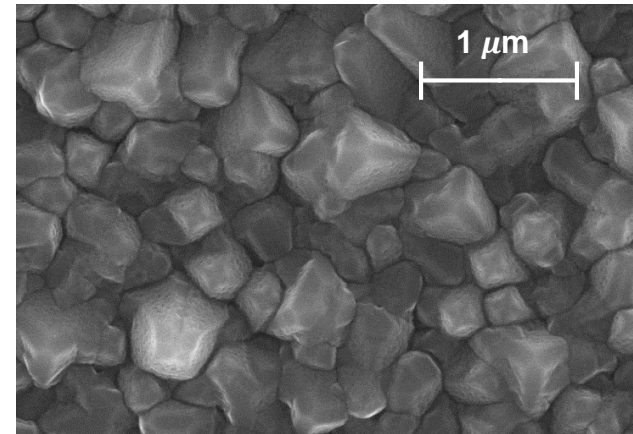


# The problem

- Material structure: grain size distribution
  - SEM Measurements (Scanning Electron Microscope)
    - Grain size dependent on the LPCVD temperature process
    - 2  $\mu\text{m}$ -thick poly-silicon films



Deposition temperature: 580 °C



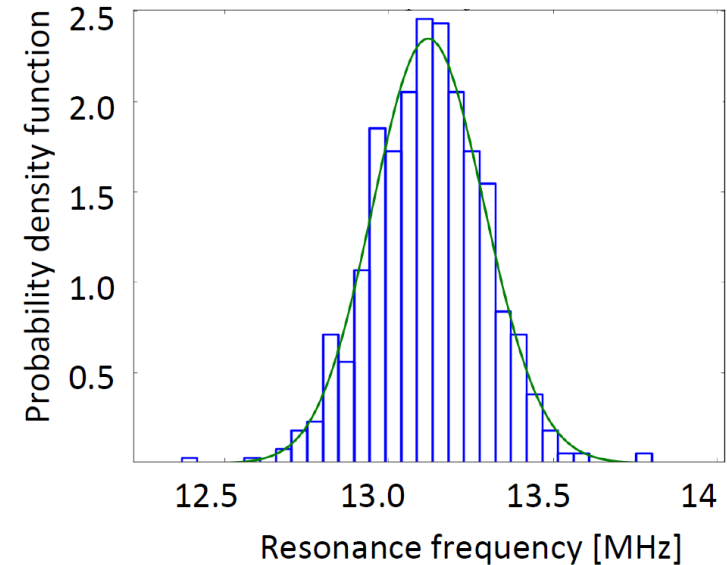
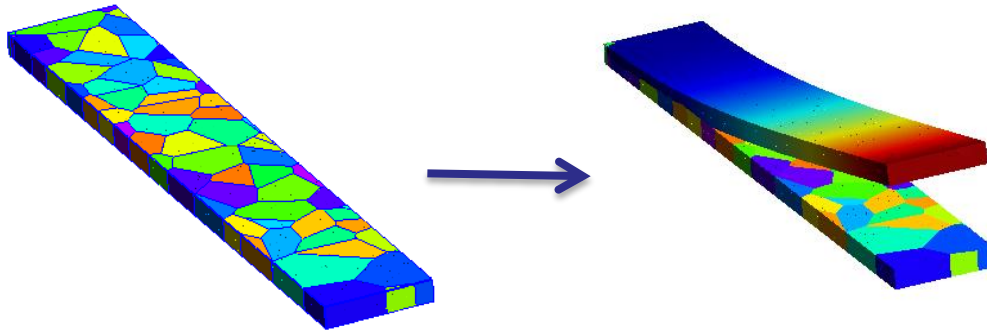
Deposition temperature: 650 °C

Deposition temperature [°C]	580	610	630	650
Average grain diameter [ $\mu\text{m}$ ]	0.21	0.45	0.72	0.83

SEM images provided by IMT Bucharest, Rodica Voicu, Angela Baracu, Raluca Muller

# Monte-Carlo for a fully modelled beam

- The first mode frequency distribution can be obtained with
  - A 3D beam with each grain modelled
  - Grains distribution according to experimental measurements
  - Monte-Carlo simulations

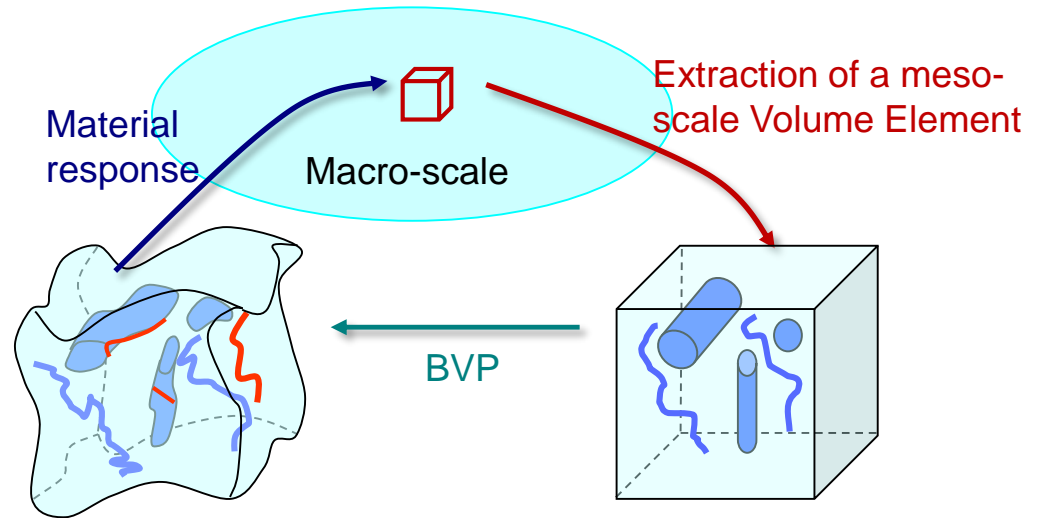


- Considering each grain is expensive and time consuming
  - ↳ Motivation for stochastic multi-scale methods

# Motivations

- Multi-scale modelling

- 2 problems are solved concurrently
  - The macro-scale problem
  - The meso-scale problem (on a meso-scale Volume Element)



- Length-scales separation

$$L_{\text{macro}} \gg L_{\text{VE}} \gg L_{\text{micro}}$$

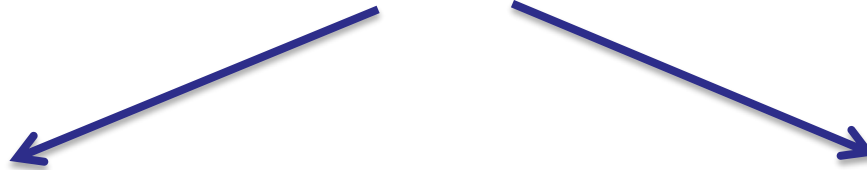
For accuracy: Size of the meso-scale volume element smaller than the characteristic length of the macro-scale loading

To be statistically representative: Size of the meso-scale volume element larger than the characteristic length of the micro-structure

# Motivations

- For structures not several orders larger than the micro-structure size

$$L_{\text{macro}} \gg L_{\text{VE}} \sim L_{\text{micro}}$$



For accuracy: Size of the meso-scale volume element smaller than the characteristic length of the macro-scale loading

Meso-scale volume element no longer statistically representative: Stochastic Volume Elements\*

- Possibility to propagate the uncertainties from the micro-scale to the macro-scale

\*M Ostoja-Starzewski, X Wang, 1999

P Trovalusci, M Ostoja-Starzewski, M L De Bellis, A Murralli, 2015

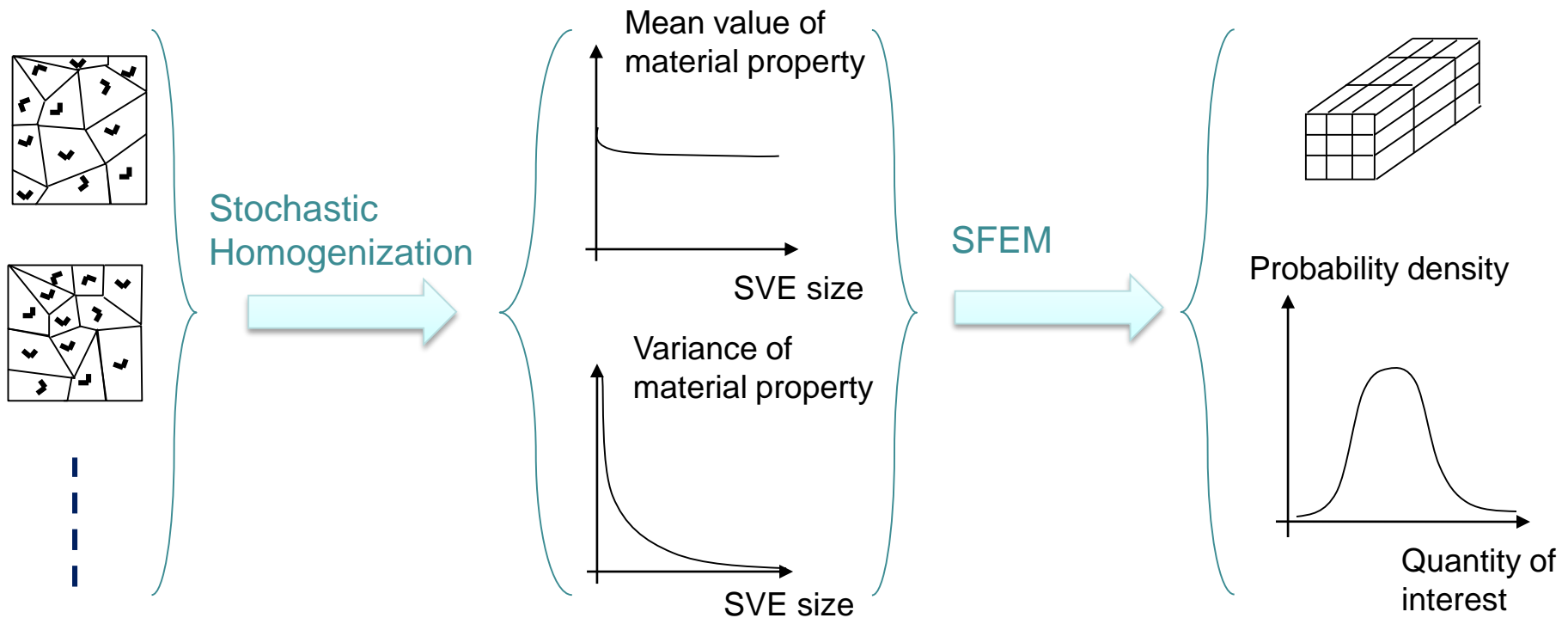
X. Yin, W. Chen, A. To, C. McVeigh, 2008

J. Guillemot, A. Noshadravan, C. Soize, R. Ghanem, 2011

....

# A 3-scale process

Grain-scale or micro-scale	Meso-scale	Macro-scale
<ul style="list-style-type: none"> <li>➤ Samples of the microstructure (volume elements) are generated</li> <li>➤ Each grain has a random orientation</li> </ul>	<ul style="list-style-type: none"> <li>➤ Intermediate scale</li> <li>➤ The distribution of the material property <math>\mathbb{P}(C)</math> is defined</li> </ul>	<ul style="list-style-type: none"> <li>➤ Uncertainty quantification of the macro-scale quantity</li> <li>➤ E.g. the first mode frequency <math>\mathbb{P}(f_1)</math> /Quality factor <math>\mathbb{P}(Q)</math></li> </ul>





- Thermo-mechanical problems
  - Governing equations
  - Macro-scale stochastic finite element
  - Meso-scale volume elements
- From the micro-scale to the meso-scale
  - Thermo-mechanical homogenization
  - Definition of Stochastic Volume Elements (SVEs) & Stochastic homogenization
  - Need for a meso-scale random field
- The meso-scale random field
  - Definition of the thermo-mechanical meso-scale random field
  - Stochastic model of the random field: Spectral generator & non-Gaussian mapping
- From the meso-scale to the macro-scale
  - 3-Scale approach verification
  - Application to extract the quality factor

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- Macro-scale stochastic finite element method
    - Meso-scale material properties subjected to uncertainties
      - Elasticity tensor  $\mathbb{C}_M(\boldsymbol{\theta})$ ,
      - Heat conductivity tensor  $\boldsymbol{\kappa}_M(\boldsymbol{\theta})$ , and
      - Thermal expansion tensors  $\boldsymbol{\alpha}_M(\boldsymbol{\theta})$
- in the sample space  $\boldsymbol{\theta} \in \Omega$

$$\begin{bmatrix} \mathbf{M}(\rho_M) & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{u}} \\ \dot{\boldsymbol{\vartheta}} \end{bmatrix} + \begin{bmatrix} \mathbf{0} & \mathbf{0} \\ \mathbf{D}_{\vartheta u}(\boldsymbol{\alpha}_M, \mathbb{C}_M) & \mathbf{D}_{\vartheta\vartheta}(\rho_M c_{vM}) \end{bmatrix} \begin{bmatrix} \dot{\mathbf{u}} \\ \dot{\boldsymbol{\vartheta}} \end{bmatrix} + \begin{bmatrix} \mathbf{K}_{uu}(\mathbb{C}_M) & \mathbf{K}_{u\vartheta}(\boldsymbol{\alpha}_M, \mathbb{C}_M) \\ \mathbf{0} & \mathbf{K}_{\vartheta\vartheta}(\boldsymbol{\kappa}_M) \end{bmatrix} \begin{bmatrix} \mathbf{u} \\ \boldsymbol{\vartheta} \end{bmatrix} = \begin{bmatrix} \mathbf{F}_u \\ \mathbf{F}_\vartheta \end{bmatrix}$$

$$\hookrightarrow \begin{bmatrix} \mathbf{M} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{u}} \\ \dot{\boldsymbol{\vartheta}} \end{bmatrix} + \begin{bmatrix} \mathbf{0} & \mathbf{0} \\ \mathbf{D}_{\vartheta u}(\boldsymbol{\theta}) & \mathbf{D}_{\vartheta\vartheta} \end{bmatrix} \begin{bmatrix} \dot{\mathbf{u}} \\ \dot{\boldsymbol{\vartheta}} \end{bmatrix} + \begin{bmatrix} \mathbf{K}_{uu}(\boldsymbol{\theta}) & \mathbf{K}_{u\vartheta}(\boldsymbol{\theta}) \\ \mathbf{0} & \mathbf{K}_{\vartheta\vartheta}(\boldsymbol{\theta}) \end{bmatrix} \begin{bmatrix} \mathbf{u} \\ \boldsymbol{\vartheta} \end{bmatrix} = \begin{bmatrix} \mathbf{F}_u \\ \mathbf{F}_\vartheta \end{bmatrix}$$

- Defining the random properties at the meso-scale by
  - Using micro-scale information (SEM, XRD, images)
  - Homogenization method

# Thermo-mechanical problem

- Meso-scale Volume Elements (VE)

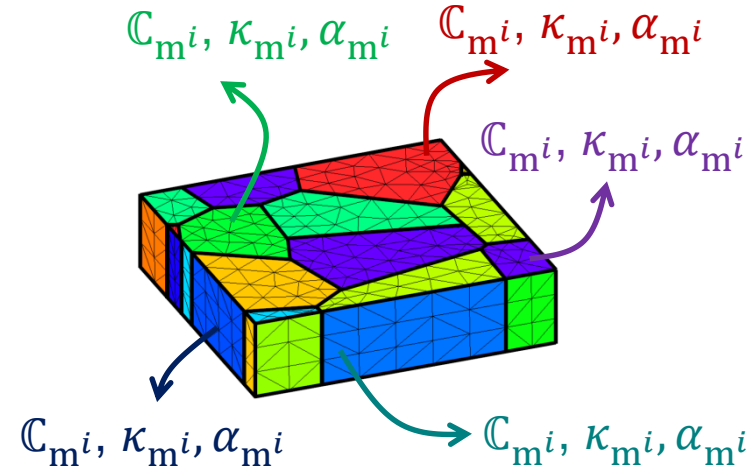
- Micro-scale material properties

- Elasticity tensor  $\mathbb{C}_m$ ,
- Heat conductivity tensor  $\kappa_m$ , and
- Thermal expansion tensors  $\alpha_m$

defined on each phase/heterogeneity

- Length scales separation assumptions

- VE small enough for the time for strain wave to propagate in the SVE to remain negligible
- VE small enough for the time variation of heat storage to remain negligible



$$\begin{bmatrix} \mathbf{M}(\rho_m) & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{u}} \\ \dot{\boldsymbol{\vartheta}} \end{bmatrix} + \begin{bmatrix} \mathbf{0} & \mathbf{0} \\ \mathbf{D}_{\vartheta u}(\alpha_m, \mathbb{C}_m) & \mathbf{D}_{\vartheta\vartheta}(\rho_m C_{vm}) \end{bmatrix} \begin{bmatrix} \dot{\mathbf{u}} \\ \dot{\boldsymbol{\vartheta}} \end{bmatrix} + \begin{bmatrix} \mathbf{K}_{uu}(\mathbb{C}_m) & \mathbf{K}_{u\vartheta}(\alpha_m, \mathbb{C}_m) \\ \mathbf{0} & \mathbf{K}_{\vartheta\vartheta}(\kappa_m) \end{bmatrix} \begin{bmatrix} \mathbf{u} \\ \boldsymbol{\vartheta} \end{bmatrix} = \begin{bmatrix} \mathbf{F}_u \\ \mathbf{F}_\vartheta \end{bmatrix}$$

$$\hookrightarrow \begin{bmatrix} \mathbf{K}_{uu} & \mathbf{K}_{u\vartheta} \\ \mathbf{0} & \mathbf{K}_{\vartheta\vartheta} \end{bmatrix} \begin{bmatrix} \mathbf{u} \\ \boldsymbol{\vartheta} \end{bmatrix} = \begin{bmatrix} \mathbf{F}_u \\ \mathbf{F}_\vartheta \end{bmatrix}$$

- Transition from meso-scale BVP realizations to the meso-scale random properties



Stochastic thermo-mechanical homogenization

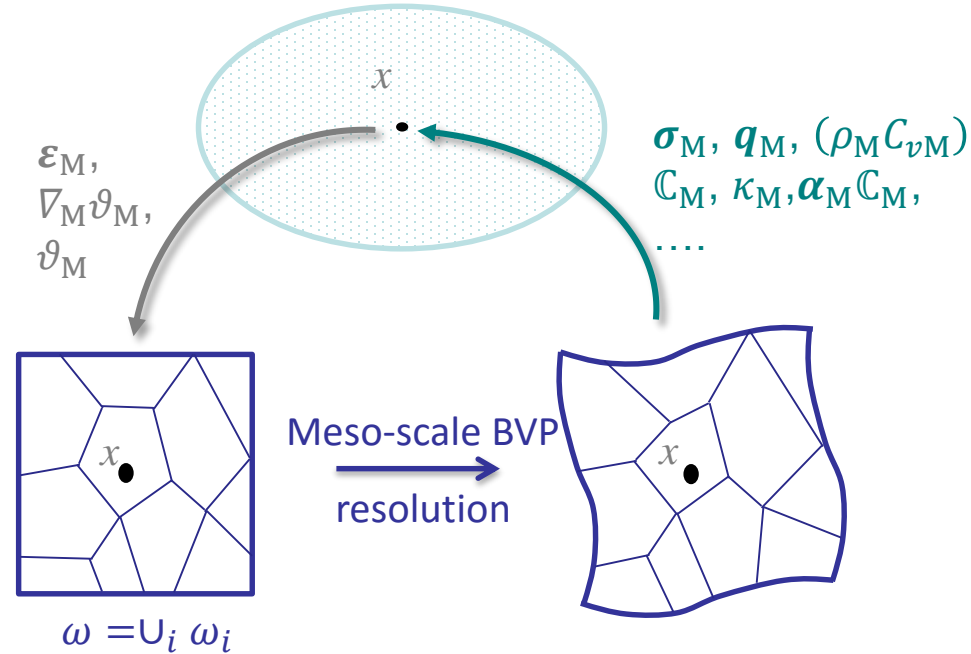
- Thermo-mechanical problems
  - Governing equations
  - Macro-scale stochastic finite element
  - Meso-scale volume elements
- **From the micro-scale to the meso-scale**
  - Thermo-mechanical homogenization
  - Definition of Stochastic Volume Elements (SVEs) & Stochastic homogenization
  - Need for a meso-scale random field
- The meso-scale random field
  - Definition of the thermo-mechanical meso-scale random field
  - Stochastic model of the random field: Spectral generator & non-Gaussian mapping
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  - 3-Scale approach verification
  - Application to extract the quality factor

# From the micro-scale to the meso-scale

- Thermo-mechanical homogenization

- Down-scaling

$$\left\{ \begin{array}{l} \varepsilon_M = \frac{1}{V(\omega)} \int_{\omega} \varepsilon_m d\omega \\ \nabla_M \vartheta_M = \frac{1}{V(\omega)} \int_{\omega} \nabla_m \vartheta_m d\omega \\ \vartheta_M = \frac{1}{V(\omega)} \int_{\omega} \frac{\rho_m C_{vm}}{\rho_M C_{vM}} \vartheta_m d\omega \end{array} \right.$$



- Up-scaling

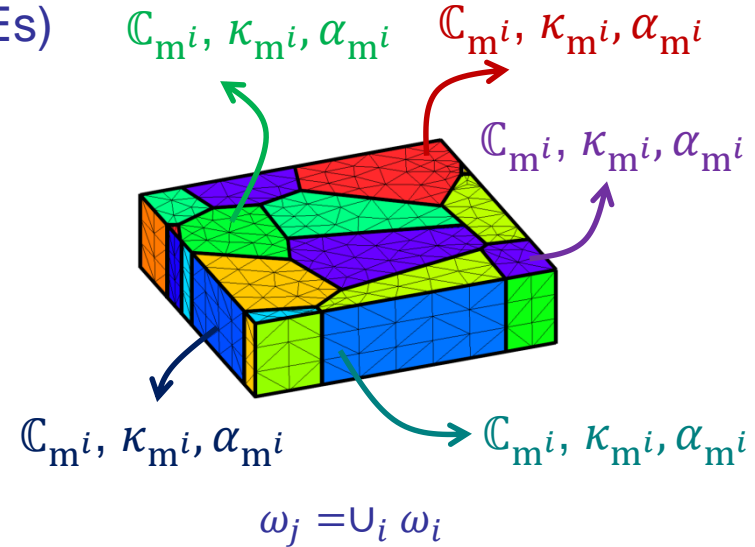
$$\left\{ \begin{array}{l} \sigma_M = \frac{1}{V(\omega)} \int_{\omega} \sigma_m d\omega \\ \mathbf{q}_M = \frac{1}{V(\omega)} \int_{\omega} \mathbf{q}_m d\omega \\ \rho_M C_{vM} = \frac{1}{V(\omega)} \int_{\omega} \rho_m C_{vm} dV \end{array} \right. \longrightarrow \left\{ \begin{array}{l} \mathbb{C}_M = \frac{\partial \sigma_M}{\partial \mathbf{u}_M \otimes \nabla_M} \quad \& \quad \alpha_M: \mathbb{C}_M = - \frac{\partial \sigma_M}{\partial \vartheta_M} \\ \kappa_M = - \frac{\partial \mathbf{q}_M}{\partial \nabla_M \vartheta_M} \end{array} \right.$$

- Consistency  $\longrightarrow$  Satisfied by periodic boundary conditions

# From the micro-scale to the meso-scale

- Definition of Stochastic Volume Elements (SVEs)

- Poisson Voronoï tessellation realizations
  - SVE realization  $\omega_j$
- Each grain  $\omega_i$  is assigned material properties
  - $\mathbb{C}_{m^i}, \kappa_{m^i}, \alpha_{m^i}$ ,
  - Defined from silicon crystal properties
- Each set  $\mathbb{C}_{m^i}, \kappa_{m^i}, \alpha_{m^i}$  is assigned a random orientation
  - Following XRD distributions



- Stochastic homogenization

- Several SVE realizations
- For each SVE  $\omega_j = \cup_i \omega_i$

$$\mathbb{C}_{m^i}, \kappa_{m^i}, \alpha_{m^i} \quad \forall i$$



Computational  
homogenization

$$\mathbb{C}_{M^j}, \kappa_{M^j}, \alpha_{M^j}$$

Samples of the meso-scale  
homogenized  
elasticity tensors

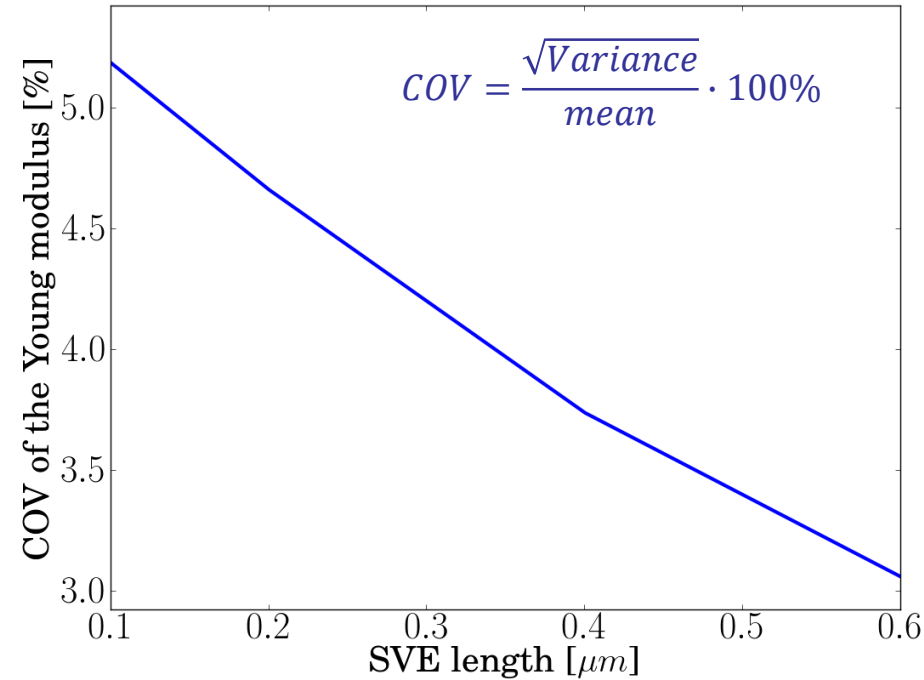
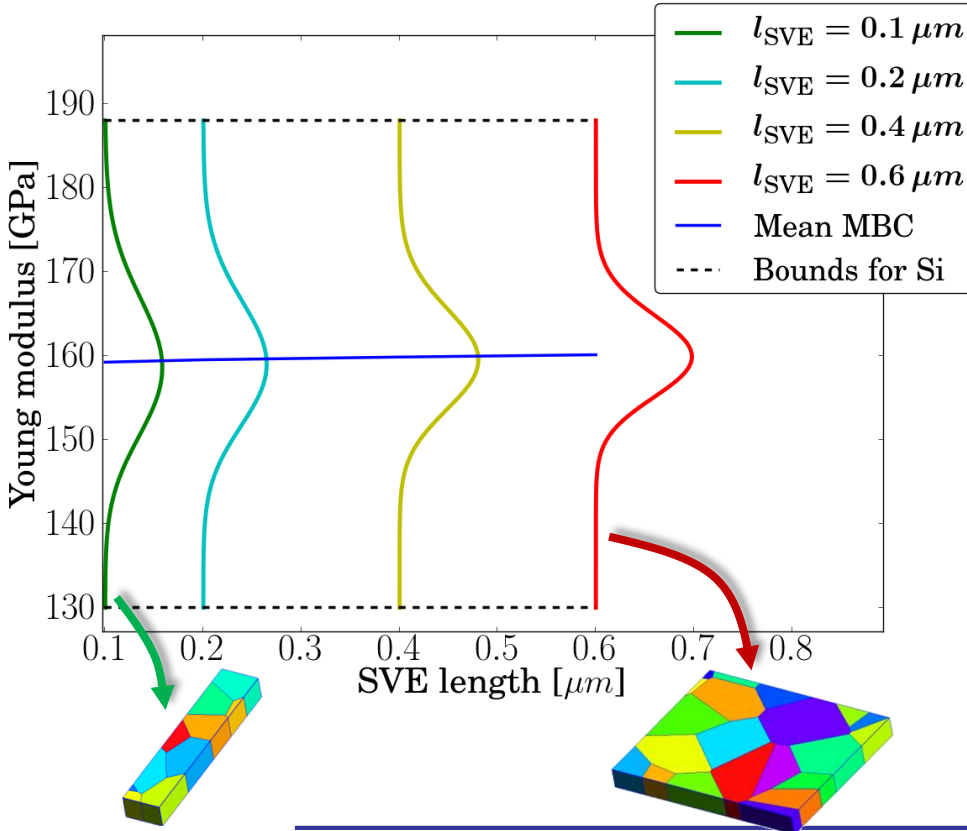
- Homogenized material tensors not unique as statistical representativeness is lost\*

\*C. Huet, 1990

# From the micro-scale to the meso-scale

- Distribution of the apparent meso-scale elasticity tensor  $\mathbb{C}_M$

➤ For large SVEs, the apparent tensor tends to the effective (and unique) one

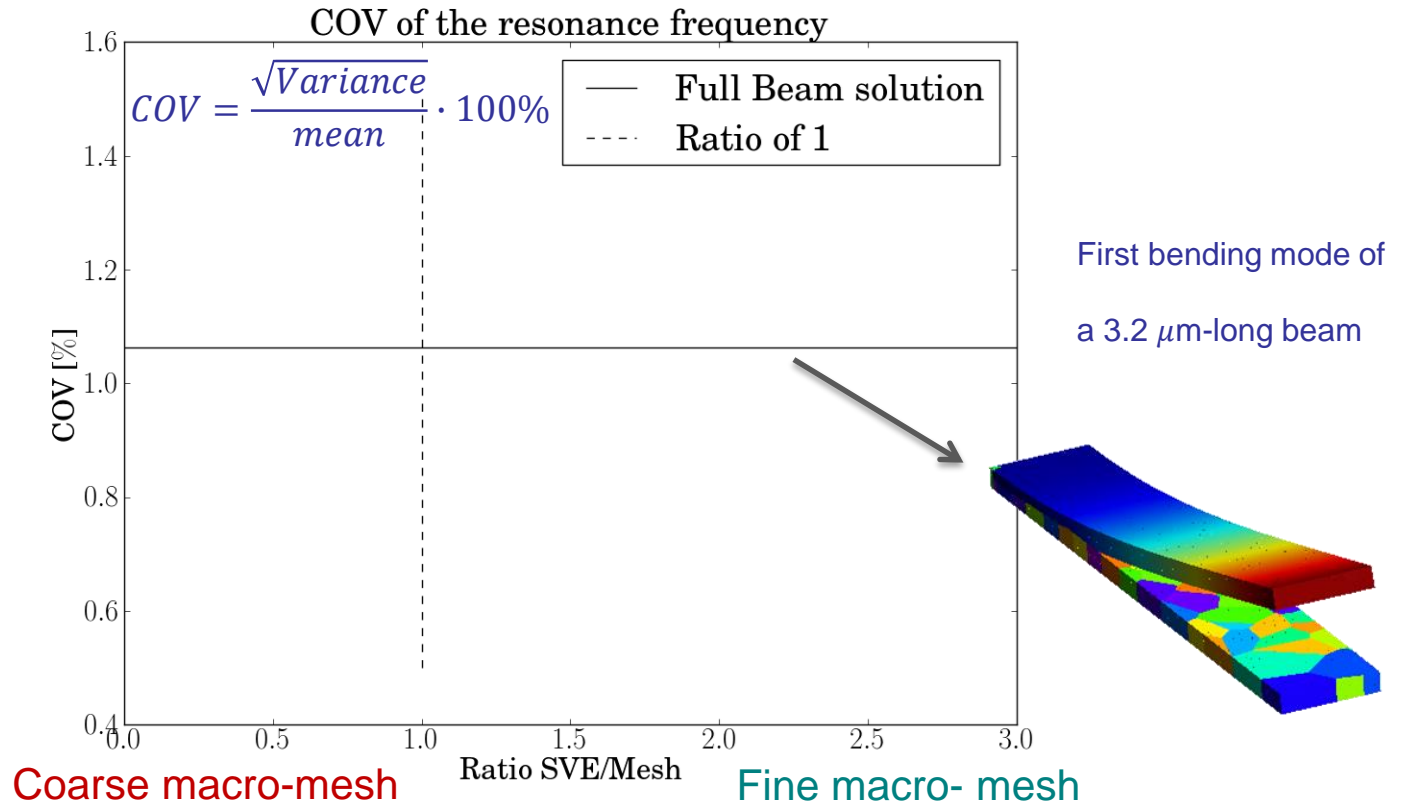


- The bounds do not depend on the SVE size but on the silicon elasticity tensor
- However, the larger the SVE, the lower the probability to be close to the bounds



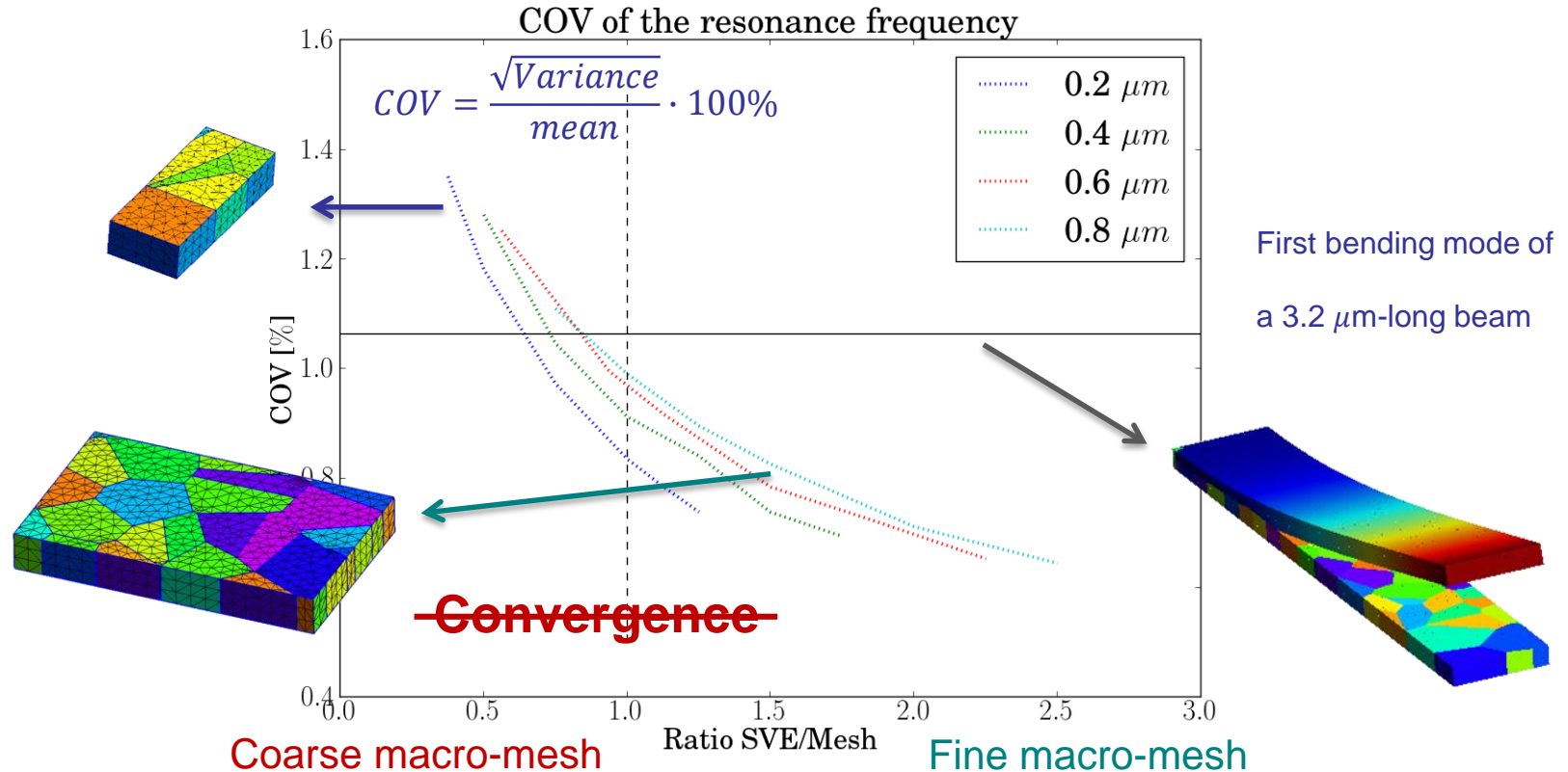
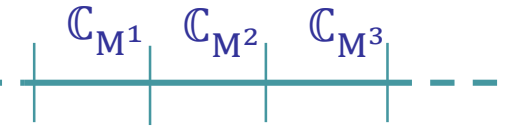
# From the micro-scale to the meso-scale

- Use of the meso-scale distribution with macro-scale finite elements
  - Beam macro-scale finite elements
  - Use of the meso-scale distribution as a random variable
  - Monte-Carlo simulations



# From the micro-scale to the meso-scale

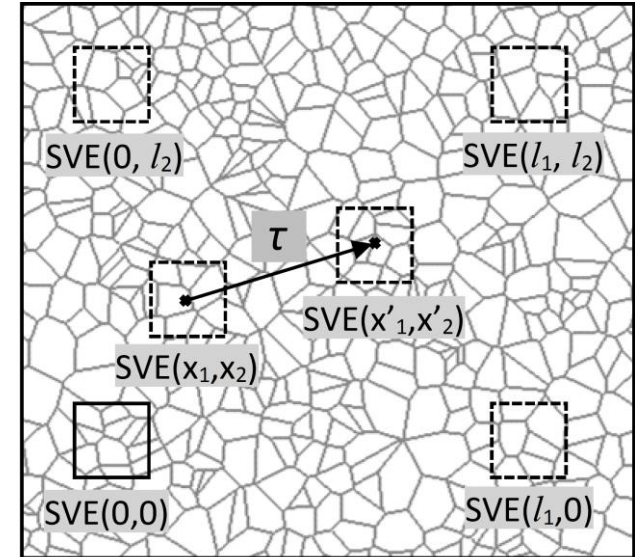
- Use of the meso-scale distribution with macro-scale finite elements
  - Beam macro-scale finite elements
  - Use of the meso-scale distribution as a random variable
  - Monte-Carlo simulations



- No convergence: the macro-scale distribution (first resonance frequency) depends on SVE and mesh sizes

# From the micro-scale to the meso-scale

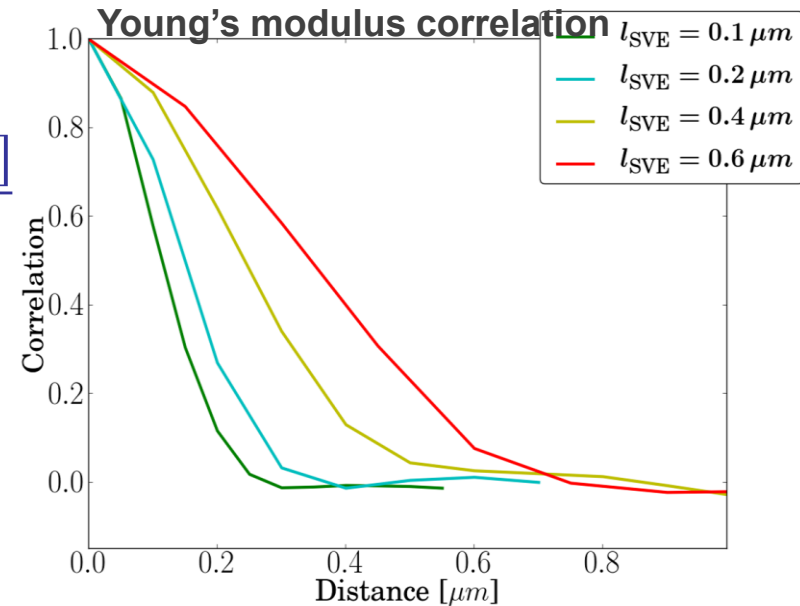
- Need for a meso-scale random field
  - Introduction of the (meso-scale) spatial correlation
    - Define large tessellations
    - SVEs extracted at different distances in each tessellation
  - Evaluate the spatial correlation between the components of the meso-scale material operators
  - For example, in 1D-elasticity
    - Young's modulus correlation



$$R_{E_x}(\tau) = \frac{\mathbb{E}[(E_x(x) - \mathbb{E}(E_x))(E_x(x + \tau) - \mathbb{E}(E_x))]}{\mathbb{E}[(E_x - \mathbb{E}(E_x))^2]}$$

- Correlation length

$$L_{E_x} = \frac{\int_{-\infty}^{\infty} R_{E_x}(\tau) d\tau}{R_{E_x}(0)}$$



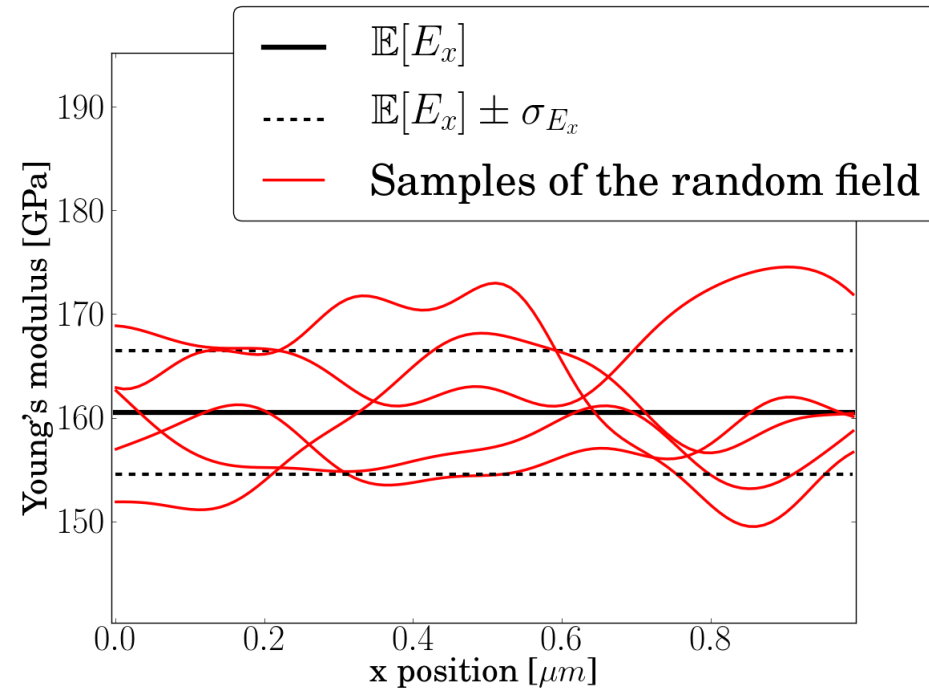
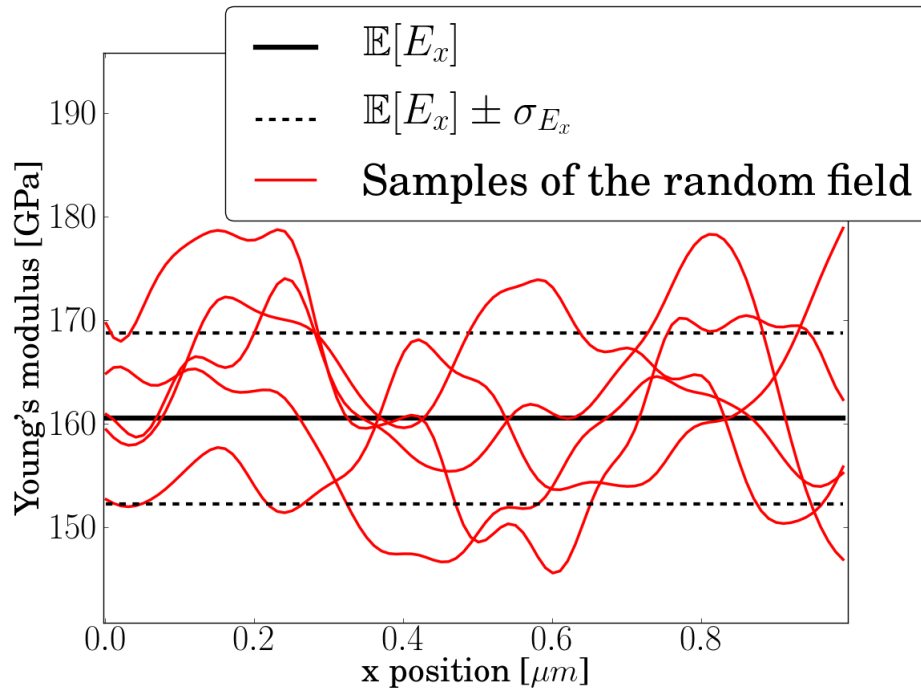
# From the micro-scale to the meso-scale

- Need for a meso-scale random field (2)
  - The meso-scale random field is characterized by the correlation length  $L_{E_x}$
  - The correlation length  $L_{E_x}$  depends on the SVE size

Random field with different SVEs sizes

$l_{\text{SVE}} = 0.1 \mu\text{m}$

$l_{\text{SVE}} = 0.4 \mu\text{m}$

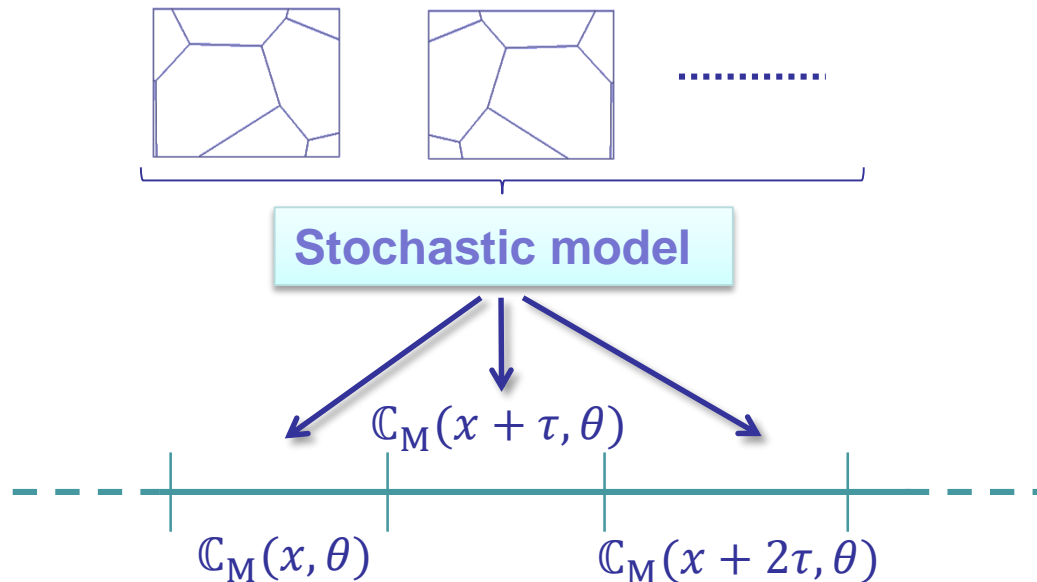


- Thermo-mechanical problems
  - Governing equations
  - Macro-scale stochastic finite element
  - Meso-scale volume elements
- From the micro-scale to the meso-scale
  - Thermo-mechanical homogenization
  - Definition of Stochastic Volume Elements (SVEs) & Stochastic homogenization
  - Need for a meso-scale random field
- **The meso-scale random field**
  - Definition of the thermo-mechanical meso-scale random field
  - Stochastic model of the random field: Spectral generator & non-Gaussian mapping
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  - 3-Scale approach verification
  - Application to extract the quality factor

# The meso-scale random field

- Use of the meso-scale distribution with stochastic (macro-scale) finite elements
  - Use of the meso-scale random field
    - Monte-Carlo simulations at the macro-scale
  - BUT we do not want to evaluate the random field from the stochastic homogenization for each simulation → Meso-scale random field from a generator

Stochastic model of meso-scale  
elasticity tensors



# The meso-scale random field

- Definition of the thermo-mechanical meso-scale random field

- Elasticity tensor  $\mathbb{C}_M(x, \theta)$  (matrix form  $\mathbf{C}_M$ ) & thermal conductivity  $\kappa_M$  are bounded
  - Ensure existence of their inverse
  - Define lower bounds  $\mathbb{C}_L$  and  $\kappa_L$  such that

$$\left\{ \begin{array}{ll} \boldsymbol{\varepsilon} : (\mathbb{C}_M - \mathbb{C}_L) : \boldsymbol{\varepsilon} > 0 & \forall \boldsymbol{\varepsilon} \\ \nabla \vartheta \cdot (\kappa_M - \kappa_L) \cdot \nabla \vartheta > 0 & \forall \nabla \vartheta \end{array} \right.$$

- Use a Cholesky decomposition when semi-positive definite matrices are required

$$\left\{ \begin{array}{l} \mathbf{C}_M(x, \theta) = \mathbf{C}_L + (\bar{\mathbf{A}} + \mathbf{A}'(x, \theta))^T (\bar{\mathbf{A}} + \mathbf{A}'(x, \theta)) \\ \kappa_M(x, \theta) = \kappa_L + (\bar{\mathbf{B}} + \mathbf{B}'(x, \theta))^T (\bar{\mathbf{B}} + \mathbf{B}'(x, \theta)) \\ \alpha_{M,ij}(x, \theta) = \bar{\nu}^{(t)} + \nu'^{(t)}(x, \theta) \end{array} \right.$$

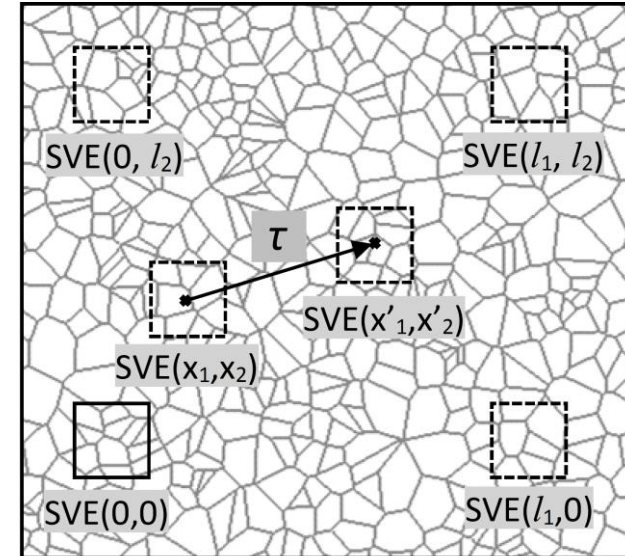
- We define the homogenous zero-mean random field  $\nu'(x, \theta)$ , with as entries

- Elasticity tensor  $\mathbf{A}'(x, \theta) \Rightarrow \nu'^{(1)} \dots \nu'^{(21)}$ ,
- Heat conductivity tensor  $\mathbf{B}'(x, \theta) \Rightarrow \nu'^{(22)} \dots \nu'^{(27)}$
- Thermal expansion tensors  $\nu'^{(t)} \Rightarrow \nu'^{(28)} \dots \nu'^{(33)}$

# The meso-scale random field

- Characterization of the meso-scale random field

- Generate large tessellation realizations
- For each tessellation realization
  - Extract SVEs centred on  $\mathbf{x} + \boldsymbol{\tau}$
  - For each SVE evaluate  $\mathbb{C}_M(\mathbf{x} + \boldsymbol{\tau}), \kappa_M(\mathbf{x} + \boldsymbol{\tau}), \alpha_M(\mathbf{x} + \boldsymbol{\tau})$
- From the set of realizations  $\mathbb{C}_M(\mathbf{x}, \boldsymbol{\theta}), \kappa_M(\mathbf{x}, \boldsymbol{\theta}), \alpha_M(\mathbf{x}, \boldsymbol{\theta})$ 
  - Evaluate the bounds  $\mathbb{C}_L$  and  $\kappa_L$
  - Apply the Cholesky decomposition  $\Rightarrow \mathcal{A}'(\mathbf{x}, \boldsymbol{\theta}), \mathcal{B}'(\mathbf{x}, \boldsymbol{\theta})$
  - Fill the 33 entries of the zero-mean homogenous field  $\boldsymbol{\nu}'(\mathbf{x}, \boldsymbol{\theta})$
- Compute the auto-/cross-correlation matrix



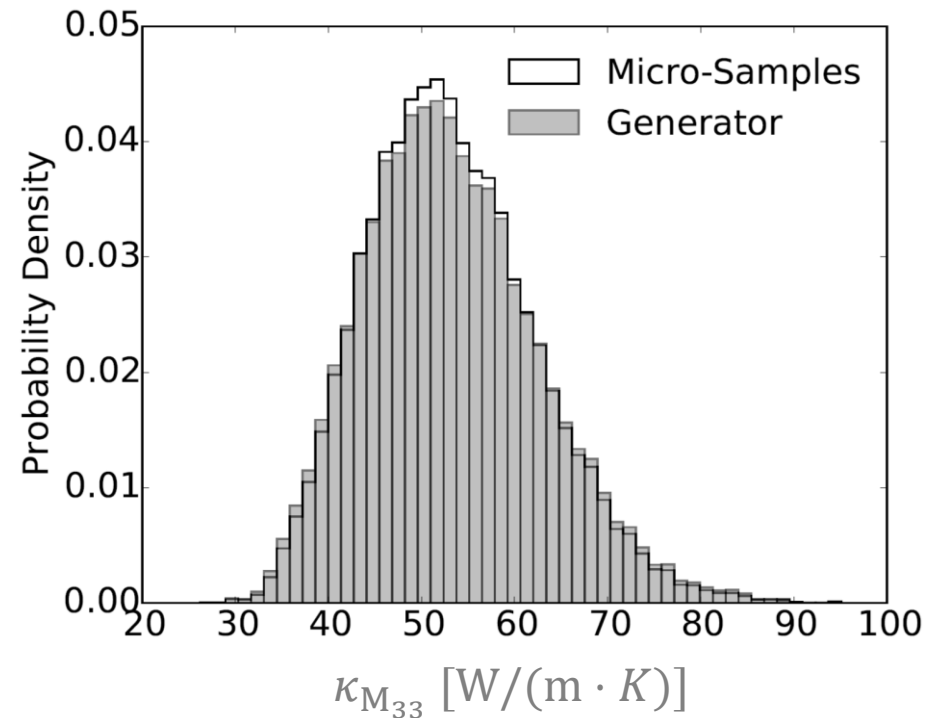
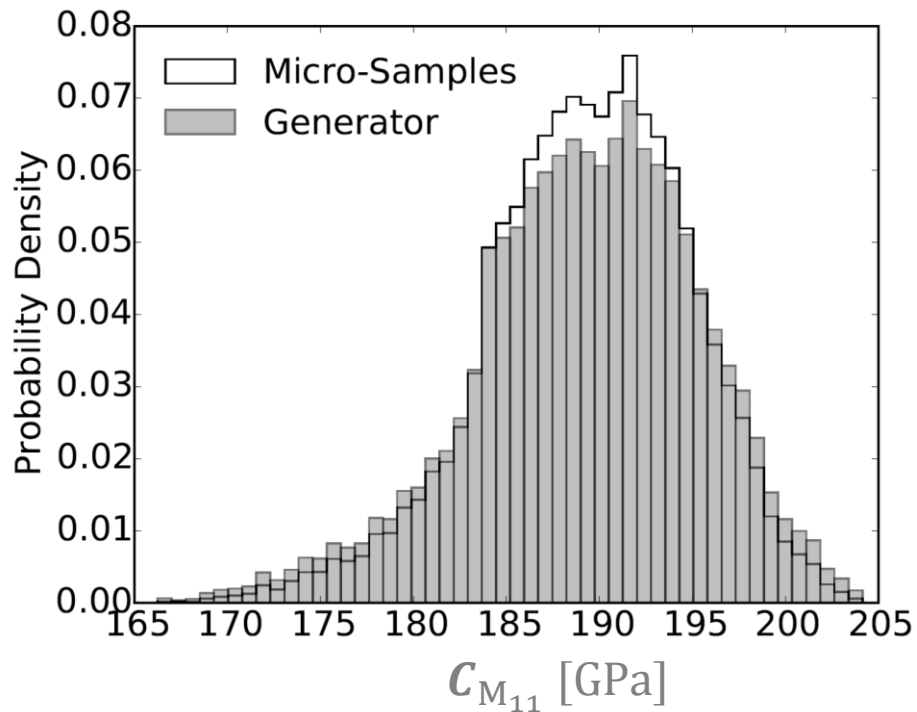
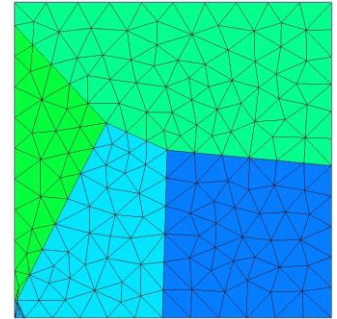
$$R_{\boldsymbol{\nu}'}^{(rs)}(\boldsymbol{\tau}) = \frac{\mathbb{E} \left[ \left( \boldsymbol{\nu}'^{(r)}(\mathbf{x}) - \mathbb{E}(\boldsymbol{\nu}'^{(r)}) \right) \left( \boldsymbol{\nu}'^{(s)}(\mathbf{x} + \boldsymbol{\tau}) - \mathbb{E}(\boldsymbol{\nu}'^{(s)}) \right) \right]}{\sqrt{\mathbb{E} \left[ \left( \boldsymbol{\nu}'^{(r)} - \mathbb{E}(\boldsymbol{\nu}'^{(r)}) \right)^2 \right] \mathbb{E} \left[ \left( \boldsymbol{\nu}'^{(s)} - \mathbb{E}(\boldsymbol{\nu}'^{(s)}) \right)^2 \right]}}$$

- Generate zero-mean random field  $\boldsymbol{\nu}'(\mathbf{x}, \boldsymbol{\theta})$ 
  - Spectral generator & non-Gaussian mapping



# The meso-scale random field

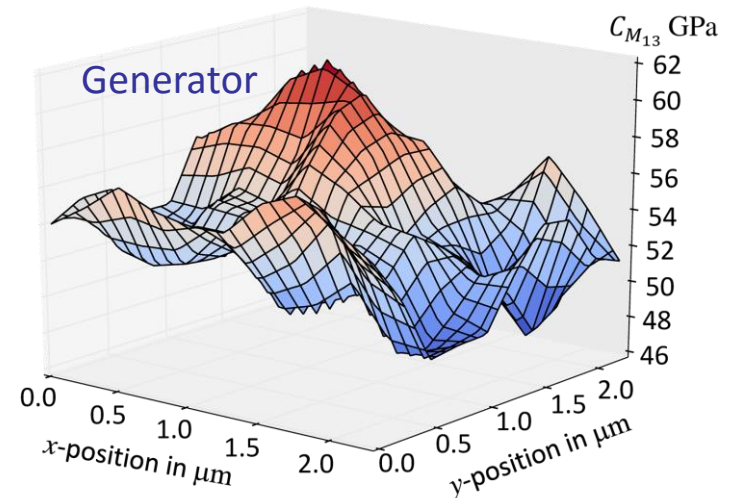
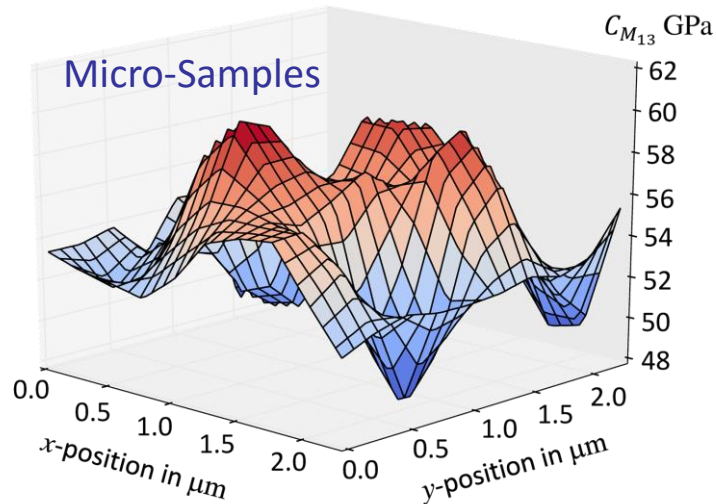
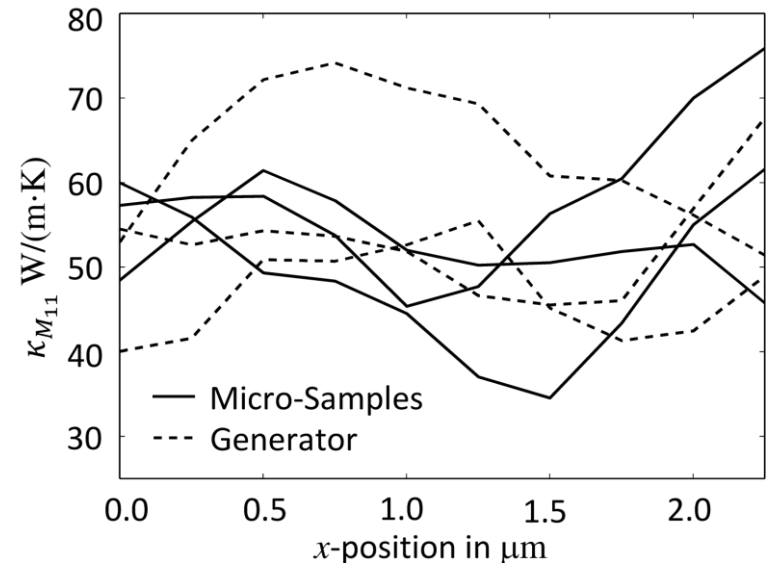
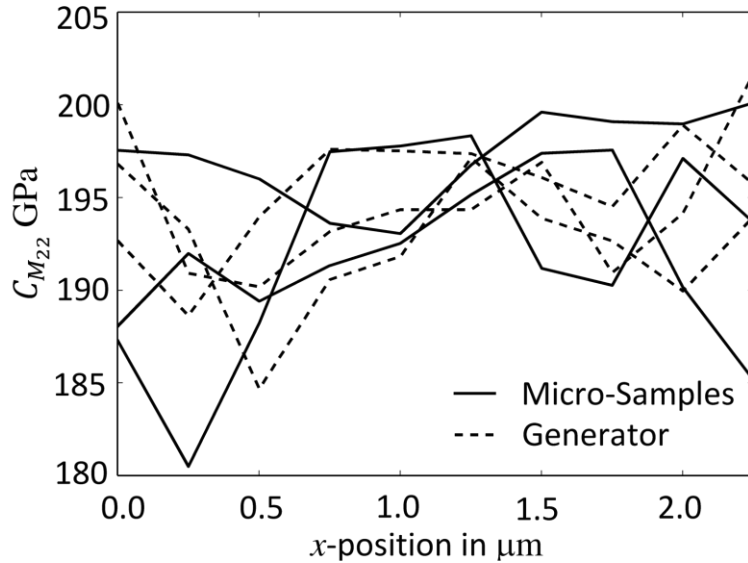
- Polysilicon film deposited at 610 °C
  - SVE size of  $0.5 \times 0.5 \mu\text{m}^2$
  - Comparison between micro-samples and generated field PDFs



# The meso-scale random field

- Polysilicon film deposited at 610 °C (3)

- Comparison between micro-samples and generated random field realizations



- Thermo-mechanical problems
  - Governing equations
  - Macro-scale stochastic finite element
  - Meso-scale volume elements
- From the micro-scale to the meso-scale
  - Thermo-mechanical homogenization
  - Definition of Stochastic Volume Elements (SVEs) & Stochastic homogenization
  - Need for a meso-scale random field
- The meso-scale random field
  - Definition of the thermo-mechanical meso-scale random field
  - Stochastic model of the random field: Spectral generator & non-Gaussian mapping
- **From the meso-scale to the macro-scale**
  - 3-Scale approach verification
  - Application to extract the quality factor

# From the meso-scale to the macro-scale

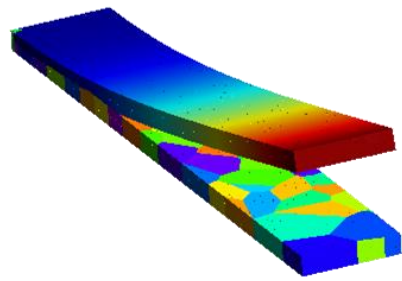
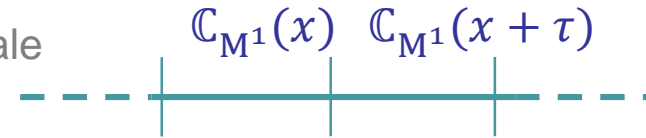
- 3-Scale approach verification with direct Monte-Carlo simulations

- Use of the meso-scale random field

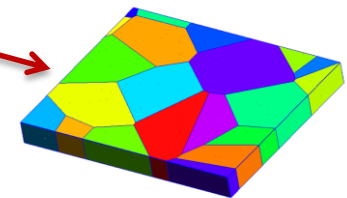
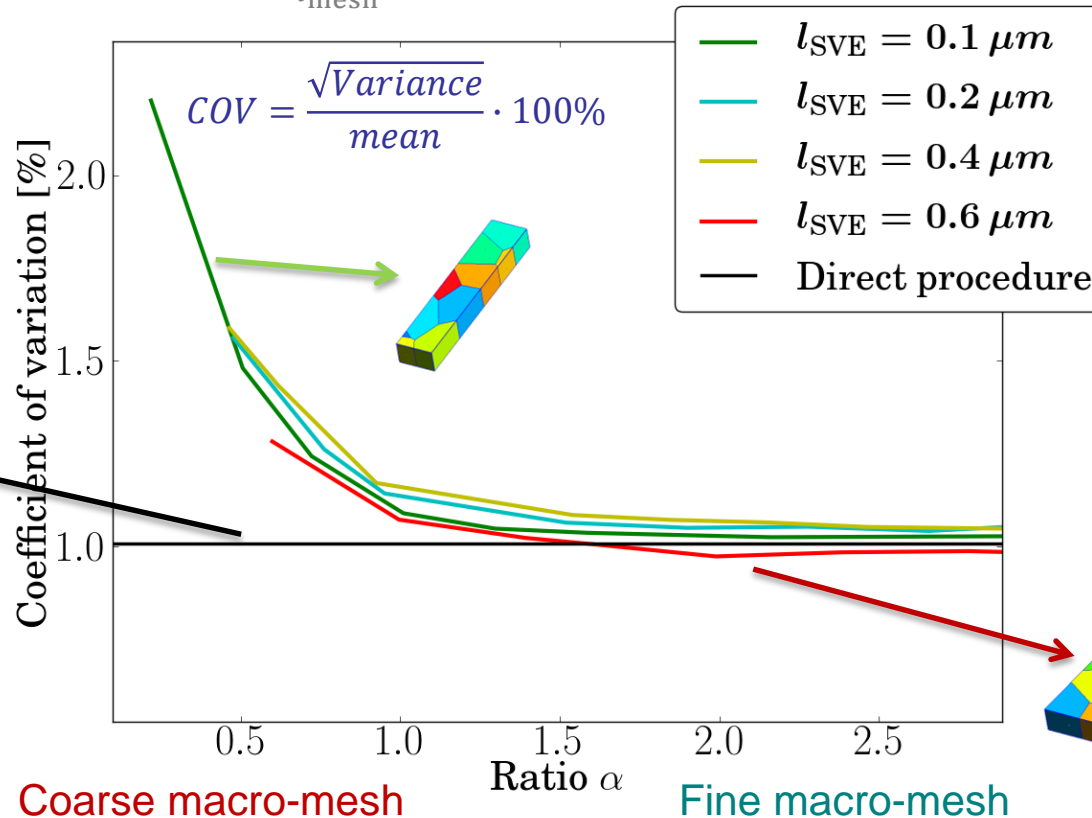
→ Monte-Carlo simulations at the macro-scale

- Macro-scale beam elements of size  $l_{\text{mesh}}$

- Convergence in terms of  $\alpha = \frac{l_{Ex}}{l_{\text{mesh}}}$

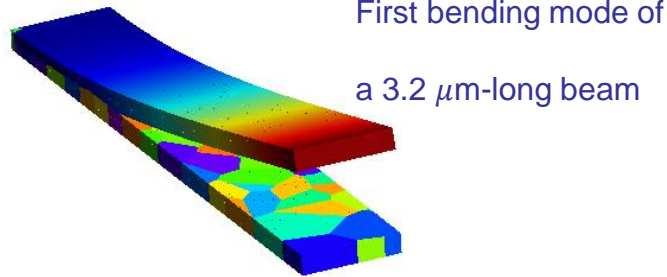


First bending mode of a  $3.2 \mu\text{m}$ -long beam

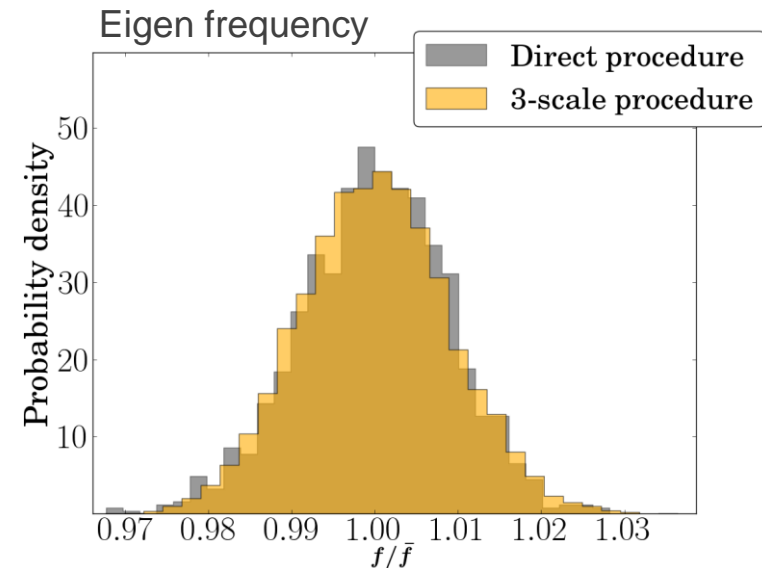
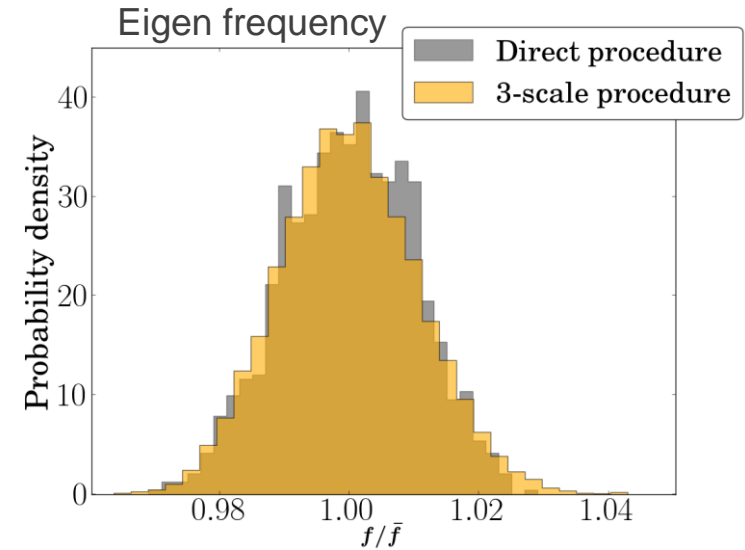
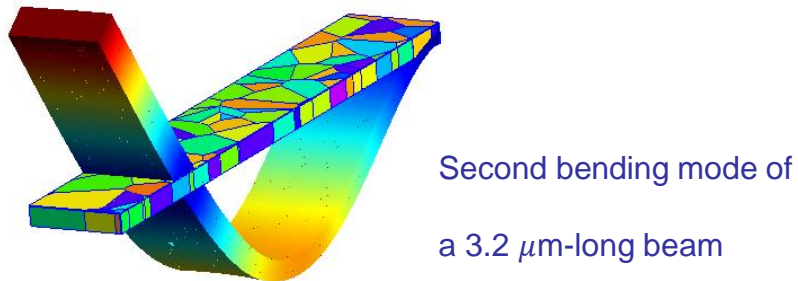


# From the meso-scale to the macro-scale

- 3-Scale approach verification ( $\alpha \sim 2$ ) with direct Monte-Carlo simulations
  - First bending mode



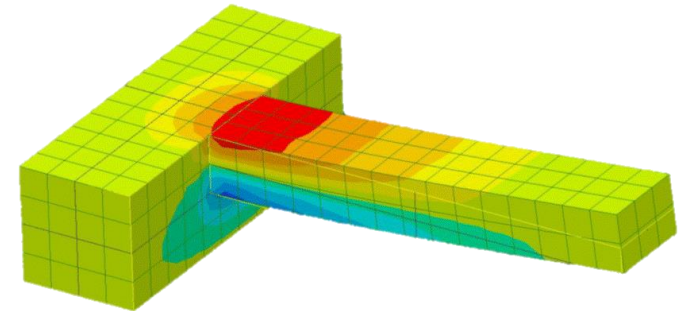
- Second bending mode



- Quality factor

- Micro-resonators

- Temperature changes with compression/traction
    - Energy dissipation



- Eigen values problem

- Governing equations

$$\begin{bmatrix} \mathbf{M} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{u}} \\ \ddot{\boldsymbol{\vartheta}} \end{bmatrix} + \begin{bmatrix} \mathbf{0} & \mathbf{0} \\ \mathbf{D}_{u\vartheta}(\boldsymbol{\theta}) & \mathbf{D}_{\vartheta\vartheta} \end{bmatrix} \begin{bmatrix} \dot{\mathbf{u}} \\ \dot{\boldsymbol{\vartheta}} \end{bmatrix} + \begin{bmatrix} \mathbf{K}_{uu}(\boldsymbol{\theta}) & \mathbf{K}_{u\vartheta}(\boldsymbol{\theta}) \\ \mathbf{0} & \mathbf{K}_{\vartheta\vartheta}(\boldsymbol{\theta}) \end{bmatrix} \begin{bmatrix} \mathbf{u} \\ \boldsymbol{\vartheta} \end{bmatrix} = \begin{bmatrix} \mathbf{F}_u \\ \mathbf{F}_\vartheta \end{bmatrix}$$

- Free vibrating problem

$$\begin{bmatrix} \mathbf{u}(t) \\ \boldsymbol{\vartheta}(t) \end{bmatrix} = \begin{bmatrix} \mathbf{u}_0 \\ \boldsymbol{\vartheta}_0 \end{bmatrix} e^{i\omega t}$$

$$\hookrightarrow \begin{bmatrix} -\mathbf{K}_{uu}(\boldsymbol{\theta}) & -\mathbf{K}_{u\vartheta}(\boldsymbol{\theta}) & \mathbf{0} \\ \mathbf{0} & -\mathbf{K}_{\vartheta\vartheta}(\boldsymbol{\theta}) & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{I} \end{bmatrix} \begin{bmatrix} \mathbf{u} \\ \boldsymbol{\vartheta} \\ \dot{\mathbf{u}} \end{bmatrix} = i\omega \begin{bmatrix} \mathbf{0} & \mathbf{0} & \mathbf{M} \\ \mathbf{D}_{\vartheta u}(\boldsymbol{\theta}) & \mathbf{D}_{\vartheta\vartheta} & \mathbf{0} \\ \mathbf{I} & \mathbf{0} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{u} \\ \boldsymbol{\vartheta} \\ \dot{\mathbf{u}} \end{bmatrix}$$

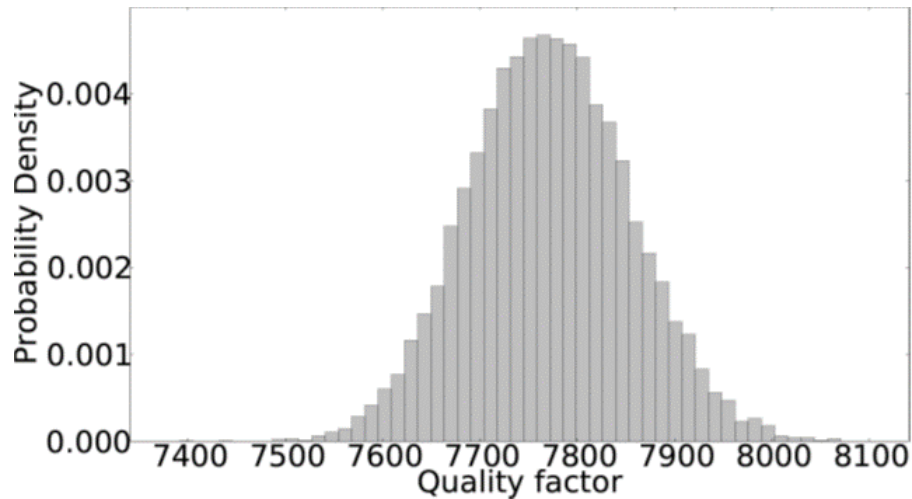
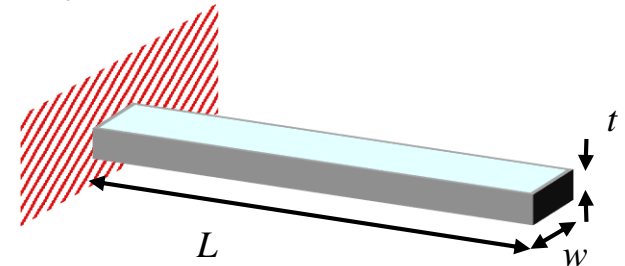
- Quality factor

- From the dissipated energy per cycle

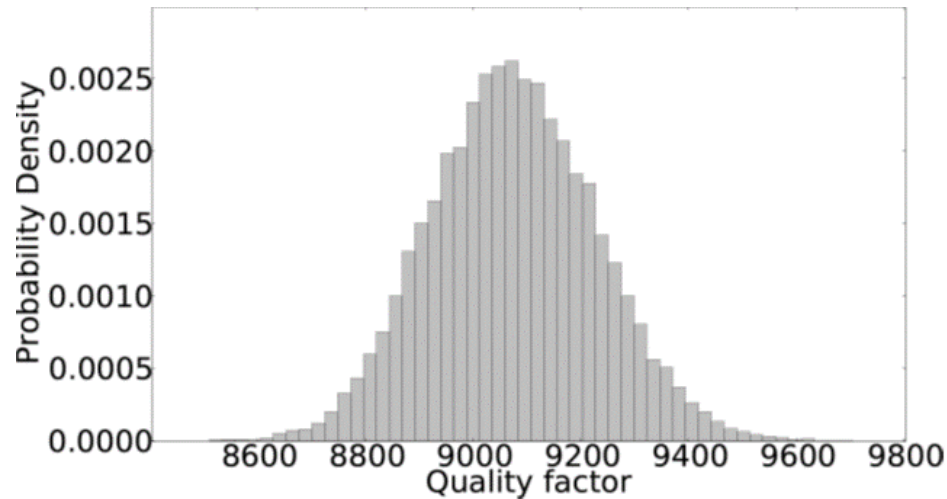
- $$Q^{-1} = \frac{2|\Im\omega|}{\sqrt{(\Re\omega)^2 + (\Im\omega)^2}}$$

# From the meso-scale to the macro-scale

- Application of the 3-Scale method to extract the quality factor distribution
  - Perfectly clamped micro-resonator
    - Different sizes easily considered
  - Meso-scale random fields
    - From stochastic homogenization
    - Generated for different deposition temperatures
  - Effect of the deposition temperature



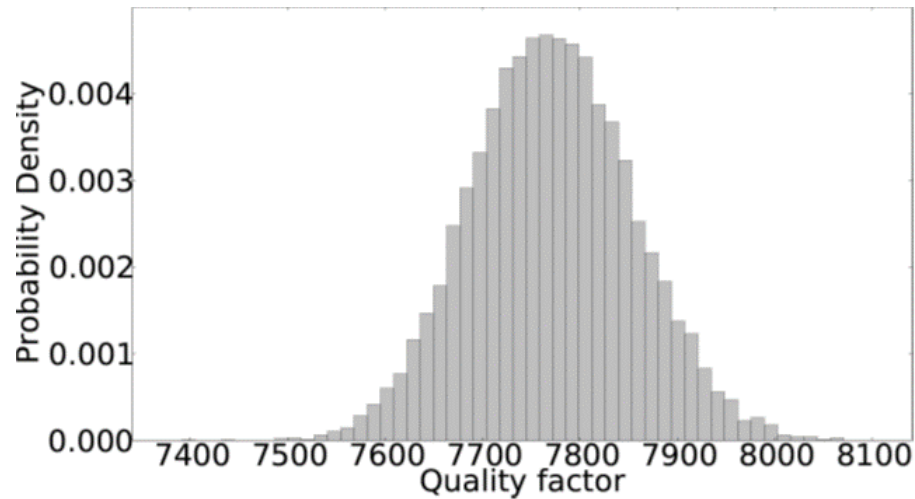
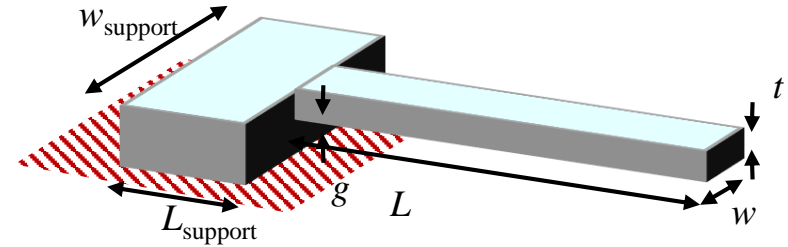
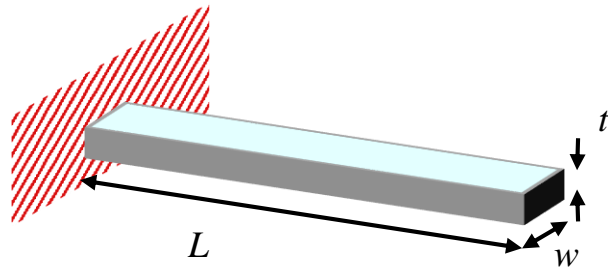
15 x 3 x 2  $\mu\text{m}^3$ -beam,  
deposited at 610 °C



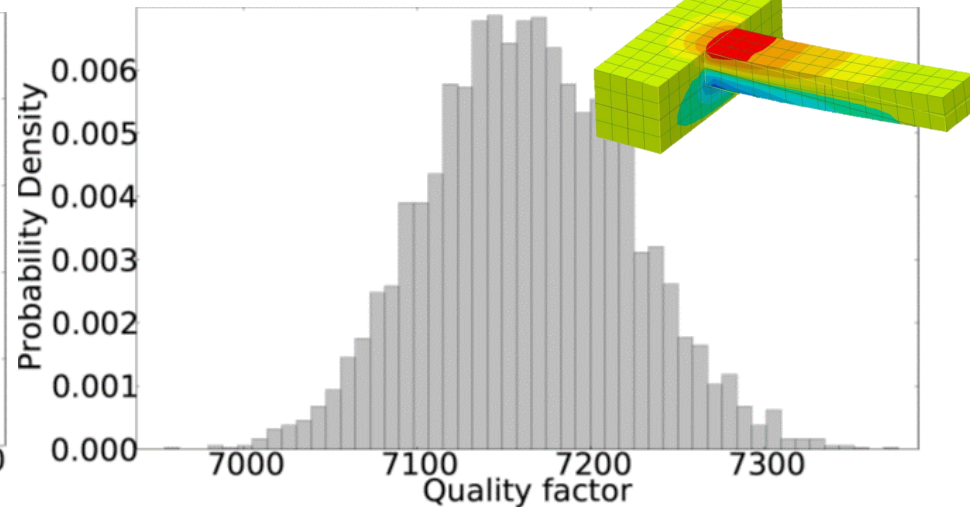
15 x 3 x 2  $\mu\text{m}^3$ -beam,  
deposited at 630 °C

# From the meso-scale to the macro-scale

- Application of the 3-Scale method to extract the quality factor distribution (3)
  - 3D models readily available
  - The effect of the anchor can be studied



$15 \times 3 \times 2 \mu\text{m}^3$ -beam,  
deposited at  $610 \text{ }^\circ\text{C}$



$15 \times 3 \times 2 \mu\text{m}^3$ -beam & anchor,  
deposited at  $610 \text{ }^\circ\text{C}$



# Conclusions & Perspectives

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- **Efficient stochastic multi-scale method**
  - Micro-structure based on experimental measurements
  - Computational efficiency relies on the meso-scale random field generator
  - Used to study probabilistic behaviors
  
- **Perspectives**
  - Other material systems
  - Non-linear behaviors
  - Non-homogenous random fields

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Thank you for your attention !