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Modeling of flexible link robots for end-effector trajectory tracking tasks

<u>Arthur Lismonde¹</u>, Valentin Sonneville² and Olivier Brüls¹

¹University of Liège, Belgium Department of Aerospace and Mechanical engineering

²University of Maryland, USA Aerospace engineering

Context

Current trend in robotics:

- Optimize energy consumption.
- Improve mass to pay-load ratio.
- Improve safety of robots.

Design of lightweight and compliant robots that could have elastic deformation issues.

⇒ Elastic deformation and vibrations can be taken care of using the control system: feedback and feed-forward commands.



Context

- Computation of a **feed-forward action** that takes into account elastic deformations.
- For trajectory tracking tasks, the **inverse dynamics** of such flexible multibody systems (MBS) has **to be solved**.
- Motion 8000 duration But flexible systems might have ۲ Command unstable internal dynamics (non-minimum phase). Time integration methods lead ۲ to unbounded solutions. -800023 1 Time 0

Context

• **Particular methods** to solve the inverse dynamics of flexible MBS:

 Stable inversion method: Boundary value problem, [Seifried 2013], [Devasia et al 1996].

2. Optimal control method:Minimization of objective function,[Bastos et al 2013] for **2D systems**.

 Both lead to similar solution that are non-causal but bounded.



Objective and originality

- Solve the inverse dynamics of 3D flexible MBS for trajectory tracking tasks:
 - 1. Model using finite elements with SE(3) formalism to avoid direct parameterization of 3D equation of motion.
 - **2. Optimal control formulation** to avoid the definition of suitable boundary conditions (as for the stable inversion).
- The **method** is developed to deal with **general flexible MBS**: serial or parallel systems, localized or distributed flexibility, 1-6 controls,...

Formulation

- To illustrate, we first consider the following **3D serial manipulator**:
 - 1. Robot with 3 dof.
 - 2. Made up of a rigid and a flexible link.
 - 3. Point mass end-effector that follows a prescribed trajectory over time.



Formulation

Finite element formalism on SE(3): [Sonneville et al 2014, 2015]

- Rigid, flexible elements and kinematic joints.
- Spatial discretization of flexible bodies (e.g., beam finite elements).
- Kinematics described using position & orientation of the N nodes.



Configuration variable: $\mathbf{H} = \operatorname{diag}(\mathbf{H}_1, ..., \mathbf{H}_N)$

Formulation

Optimal control problem as a NLP problem:

• **Objective** function *J*: **strain energy** and **controls** of the system.

$$\min_{\mathbf{H}} J = \min_{\mathbf{H}} \frac{1}{2T} \int_{t_i}^{t_f} [\boldsymbol{\epsilon}^T(\mathbf{H}) \mathbf{K} \boldsymbol{\epsilon}(\mathbf{H}) + \mathbf{u}^T \mathbf{G} \mathbf{u}] dt$$

• Constraints of the NLP: equation of inverse dynamics of the MBS. $\dot{\mathbf{H}}_I = \mathbf{H}_I \tilde{\mathbf{v}}_I$ Compatibility equation $\mathbf{M}\dot{\mathbf{v}} + \mathbf{g}(\mathbf{H}, \mathbf{v}) + \mathbf{B}^T \boldsymbol{\lambda} = \mathbf{A}\mathbf{u}$ Equation of motion $\Phi(\mathbf{H}) = \mathbf{0}$ Kinematic constraints $\mathbf{y}_{eff}(\mathbf{H}) - \mathbf{y}_{presc}(t) = \mathbf{0}$ "Servo" constraints

Use of the direct transcription method:

- **Discretization** of all states into "s" time steps (of size "h").
- Optimization variables at each time steps "k" (k = 1, ..., s).
- Optimum after "*n*" iterations.



Resulting **discrete form** of the NLP problem:

• Objective function *J*:

$$\min_{\mathbf{H}^1,\dots,\mathbf{H}^s} J = \min_{\mathbf{H}^1,\dots,\mathbf{H}^s} \frac{1}{2T} \sum_{k=1}^s [\boldsymbol{\epsilon}^{k,T}(\mathbf{H}^k)\mathbf{K}\boldsymbol{\epsilon}^k(\mathbf{H}^k) + \mathbf{u}^{k,T}\mathbf{G}\mathbf{u}^k]h$$

• Constraints of the NLP:

$$egin{aligned} \dot{\mathbf{H}}_{I}^{k} - \mathbf{H}_{I}^{k} \tilde{\mathbf{v}}_{I}^{k} &= \mathbf{0} \ \mathbf{M}^{k} \dot{\mathbf{v}}^{k} + \mathbf{g}(\mathbf{H}^{k}, \mathbf{v}^{k}) + \mathbf{B}^{k,T} oldsymbol{\lambda}^{k} - \mathbf{A} \mathbf{u}^{k} &= \mathbf{0} \ \mathbf{\Phi}(\mathbf{H}^{k}) &= \mathbf{0} \ \mathbf{y}_{eff}(\mathbf{H}^{k}) - \mathbf{y}_{presc}(t^{k}) &= \mathbf{0} \end{aligned}$$

Need for additional time constraints between time steps:

- Standard methods (e.g., Euler-implicit type) are not acceptable: $\mathbf{H}_{I}^{k+1} = \mathbf{H}_{I}^{k} + h\dot{\mathbf{H}}_{I}^{k+1} \notin SE(3)$
- On SE(3), exponential mapping can be used:

$$\mathbf{H}_{I}^{k+1} = \mathbf{H}_{I}^{k} \exp_{SE(3)}(\widetilde{\Delta \mathbf{Q}_{I}^{k}}) \in SE(3)$$

where $\Delta Q^k = (\Delta Q_1^k, ..., \Delta Q_N^k)$ is the change in configuration between two consecutive times k and k + 1.

• Possible set of optimization variables would be $(\mathbf{H}^1, \mathbf{v}^1, \dot{\mathbf{v}}^1, \mathbf{\lambda}^1, \mathbf{u}^1, ..., \mathbf{H}^s, \mathbf{v}^s, \dot{\mathbf{v}}^s, \mathbf{\lambda}^s, \mathbf{u}^s)$

with $H \in SE(3)$, which can not be dealt with by classical NLP solvers.

Alternative: use of a new vector Δq = (Δq₁, ..., Δq_N) which is the change in configuration between the initial guess states and the optimized states, through the exponential mapping

$$\mathbf{H}_{I,n}^{k} = \mathbf{H}_{I,0}^{k} \exp_{SE(3)}(\Delta \mathbf{q}_{I,n}^{k})$$

• At the end, the optimization variables are

$$\mathbf{x} = (\Delta \mathbf{q}^1, \mathbf{v}^1, \dot{\mathbf{v}}^1, \boldsymbol{\lambda}^1, \mathbf{u}^1, ..., \Delta \mathbf{q}^s, \mathbf{v}^s, \dot{\mathbf{v}}^s, \boldsymbol{\lambda}^s, \mathbf{u}^s)$$



Time steps Axis

• Important remark:

 $\begin{array}{l} \text{Difference between "time" related} \\ \text{mapping} \\ \Delta \mathbf{q}_n^{k+1} & \mathbf{H}_I^{k+1} = \mathbf{H}_I^k \exp_{SE(3)}(\widetilde{\Delta \mathbf{Q}_I^k}) \\ \text{and "iteration" related mapping} \\ \mathbf{H}_{I,n}^k = \mathbf{H}_{I,0}^k \exp_{SE(3)}(\widetilde{\Delta \mathbf{q}_{I,n}^k}) \end{array}$

Computation

- NLP problem is very large but sparse.
- Tests using NLP solvers such as KNITRO, IPOPT and FMINCON.
- Use of the "interior point" algorithm with large scale and sparse options and analytical gradients are provided.

Results – Serial robot

- Serial robot with **3 dof**.
- Made up of 2 links:
 - Rigid link: Alu, 1 x 0,02 x 0,02 m.
 - **2.** Flexible link (4 beams): Alu, 1 x 0,005 x 0,005 m.
- **Point mass** at the end-effector (0,1 kg).
- Trajectory: half-circle with 0,5 m radius in the *yz* plan, to be completed in 1 s.
- Analysis: 1st unstable pole at 8 Hz.



Results – Serial robot

s = 300 (h = 0,005s, 70k var.), 20 min. and RMS error from 5,2% to 0,1%



Results – Parallel robot



- Parallel robot with **3 dof**.
- Made up of 2 links:
 - **1. Rigid links** (3):
 - Alu, 0,25 x 0,02 x 0,02 m.
 - **2.** Flexible links (3 x 4 beams): Alu, 0,51 x 0,005 x 0,005 m.
 - Point mass at the end-effector (0,1 kg).
- Trajectory: half-circle with 0,1 m radius in the *xy* plan, to be completed in 1 s.
- Analysis: 1st unstable pole at 14 Hz.

Results – Parallel robot

s = 150 (h = 0,01s, 110k var.), 40 min. and RMS error from 2% to 0,7%



Summary

- In this work:
 - Use of a *SE*(3) formalism to reduce non-linearity in the equations of 3D flexible MBS problem.
 - Formulation of the inverse dynamics problem as an optimal control problem.
 - New vectorial variable is introduced to solve the optimization with classical NLP tools.
 - Method successful for **3D flexible serial** and **parallel** systems.
- On going work and perspectives:
 - Feed-forward solution on **robotic testbed** (adding feedback).
 - Consider compliant joints.
 - Consider contact problems with end-effector.

Thank you for your attention.



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