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FP7- INFRASTRUCTURES-2008-1
SP4-Capacities



SERIES

SEISMIC ENGINEERING RESEARCH INFRASTRUCTURES
FOR EUROPEAN SYNERGIES

General Committee Final workshop

Ispra (IT), May 30th, 2013



MAID project :



*Seismic behavior of L- and T-shaped unreinforced
Masonry shear walls including Acoustic Isolation Devices*

H. Degée & C. Mordant, ULg (BE), M. Dietz, Bristol (UK), L. Vasseur, WB

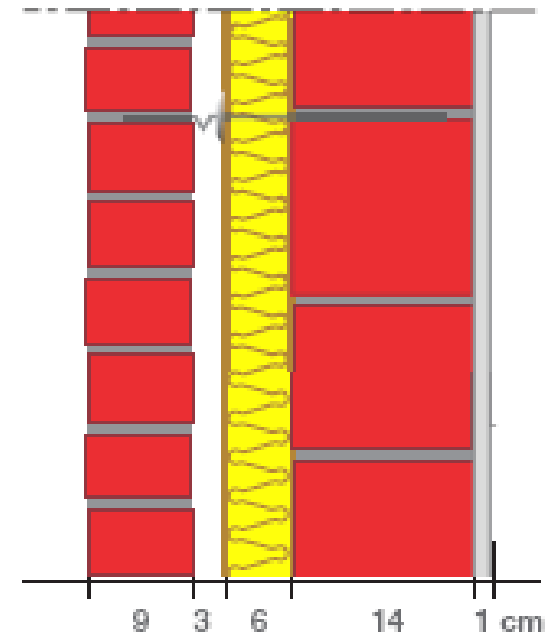
With the contribution of: ULg (ARGENCO), EQUALS, Wienerberger, CDM,
RWTH

MAID - Context and objectives of the Project

- Fast evolution of contemporary masonry architecture (North-Western European area):

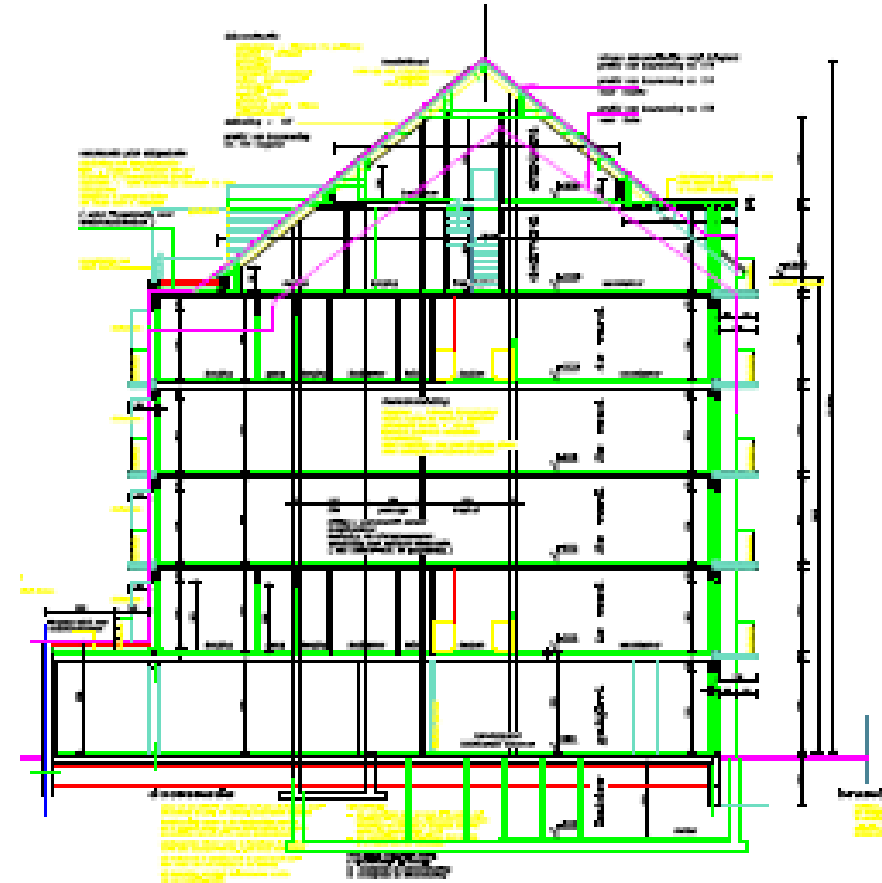
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- Fast evolution of contemporary masonry architecture (North-Western European area):
 - Requirement for energy performances



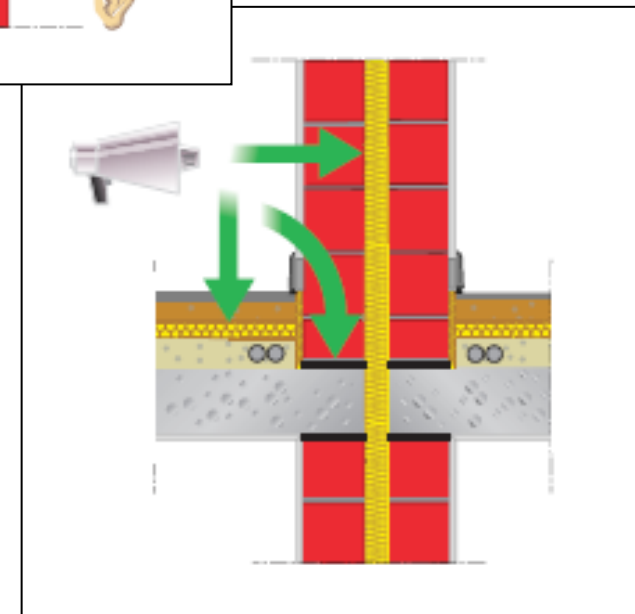
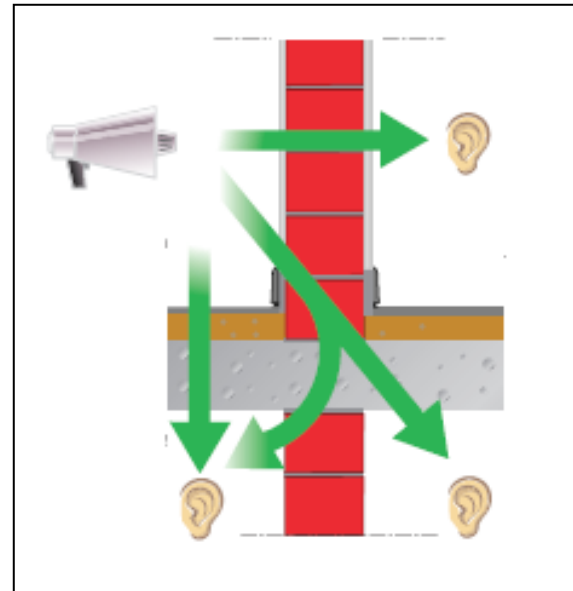
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- Fast evolution of contemporary masonry architecture (North-Western European area):
 - Requirement for energy performances
 - Use of unreinforced bearing masonry for mid-rise buildings



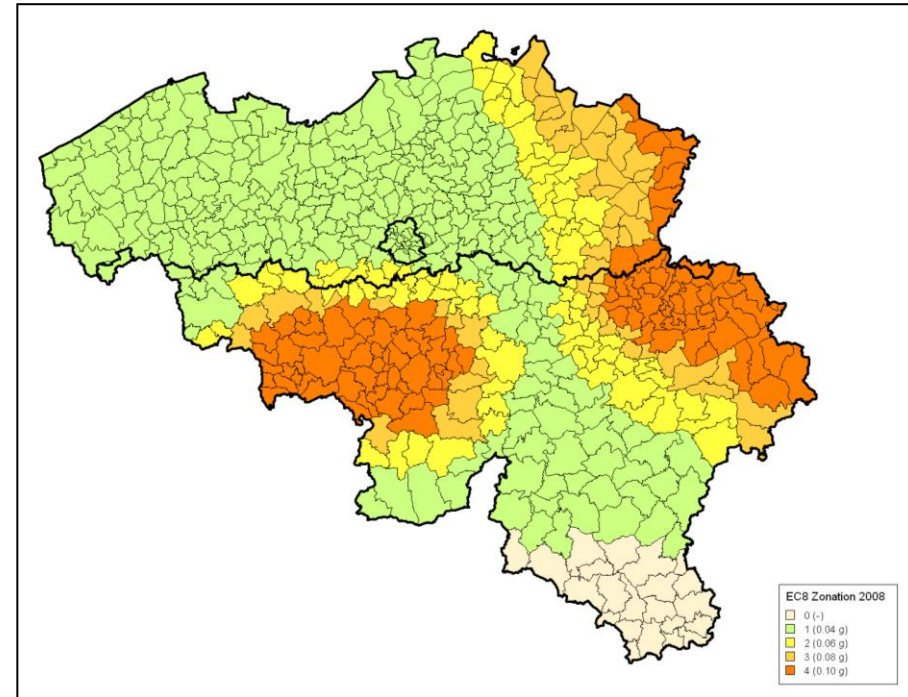
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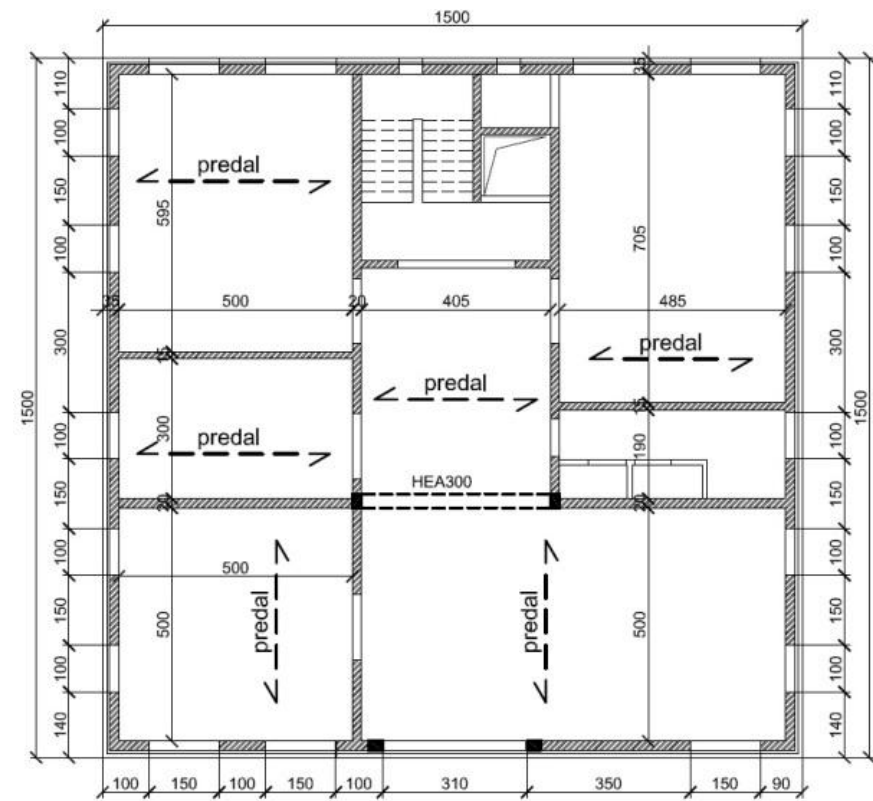
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 - Seismic resistance (low to moderate seismicity)



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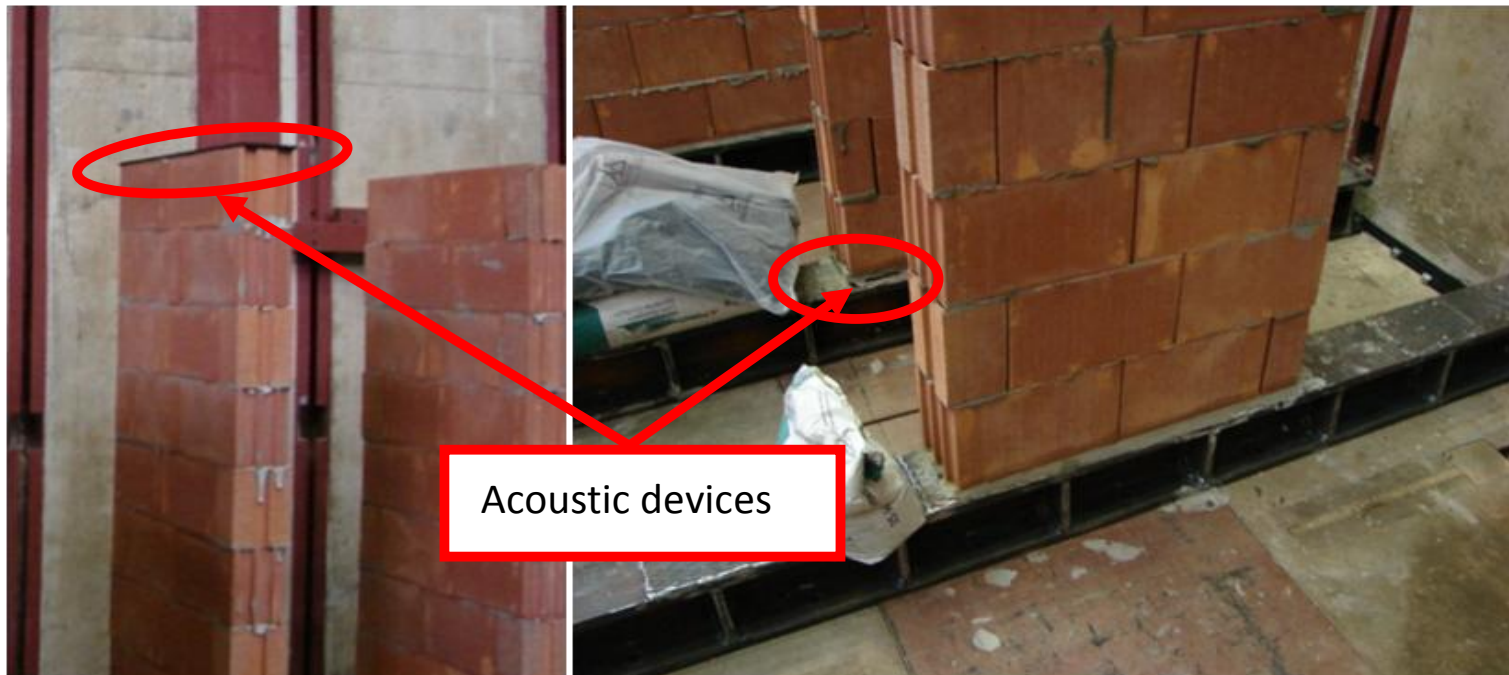
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 - Use of unreinforced bearing masonry for mid-rise buildings
 - Requirements for acoustic performances
 - Seismic resistance (low to moderate seismicity)
 - Preferential spanning of prefabricated floors



MAID - Context and objectives of the Project

➤ Objectives of the experimental work within SERIES:

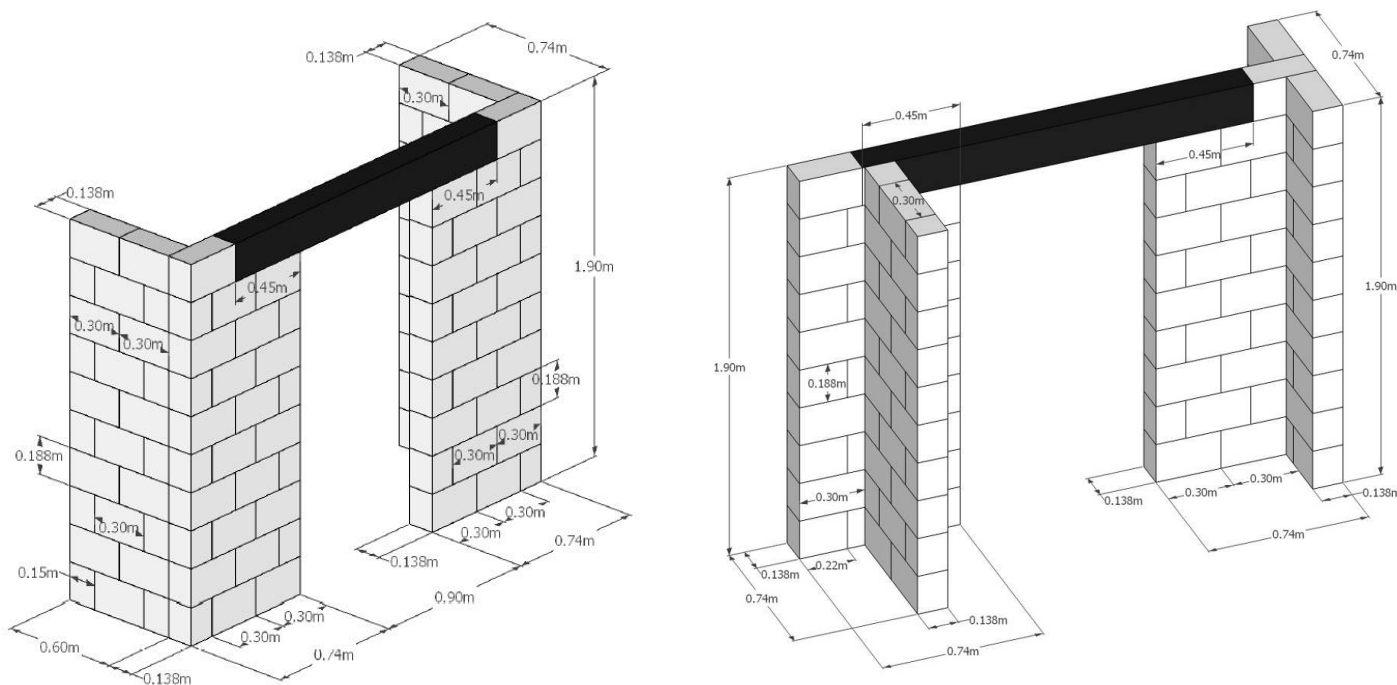
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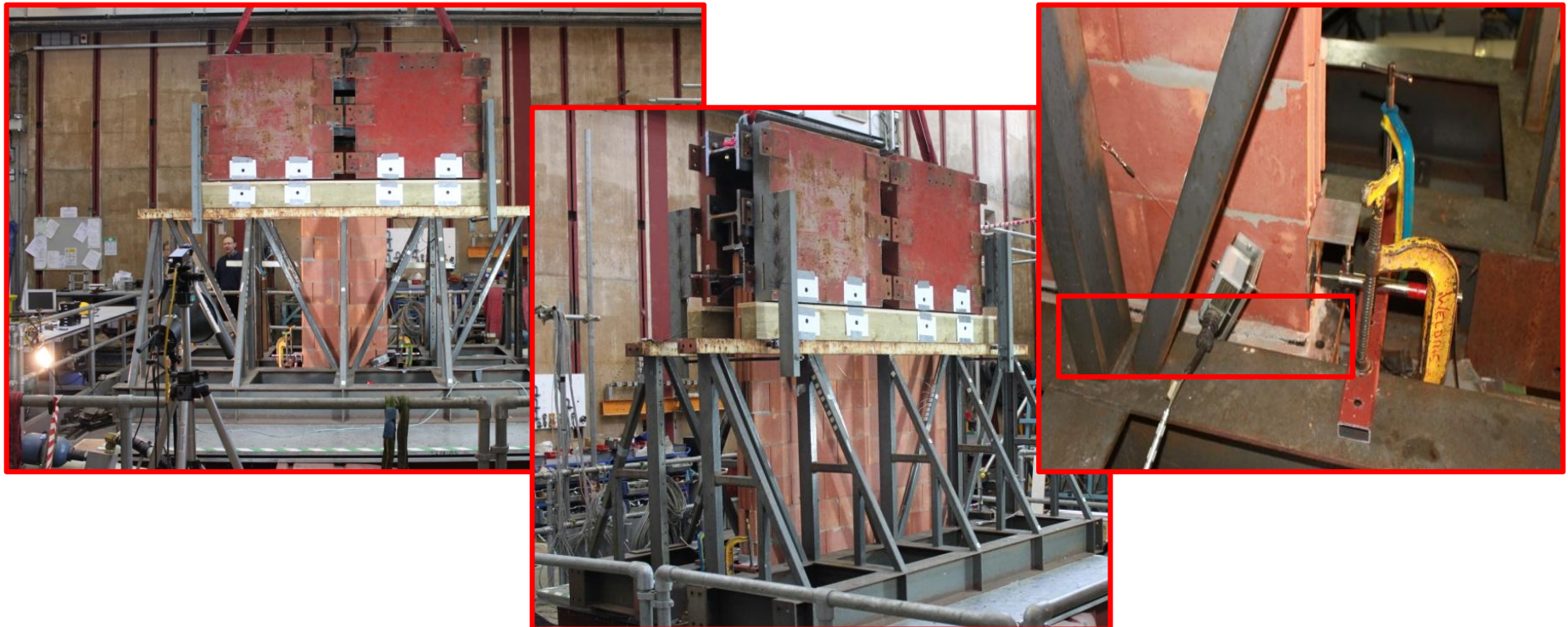
1. Characterization of the dynamic behavior of walls with acoustic rubber devices (comparative study)
2. Characterization of the dynamic behavior of flanged walls with differential loading



MAID - Testing phase 1 - Single walls

Mock ups:

- Four single walls
- **With** and **without** rubber soundproofing devices
- Two different aspect ratios (0.4 and 1.0: bending \leftrightarrow shear behavior)



MAID - Testing phase 1 - Single walls

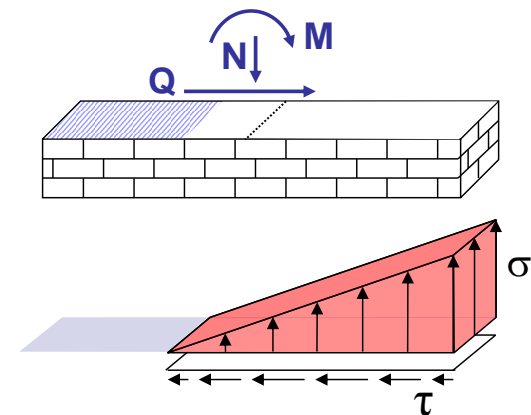
Preliminary design:

- Based on the classical EC6 model with nominal material properties (static equivalent seismic forces)

Maximum acceleration for 5 tons: **0.07 g / 0.2 g**

Testing procedure:

- EC8 spectrum-compatible time-history
 - Increasing acceleration level (with some levels duplicated)
 - Tests stopped at \sim **0.2 g / 0.7 g** (“excessive” displacements)
- + Identification stages



MAID - Testing phase 1 - Single walls



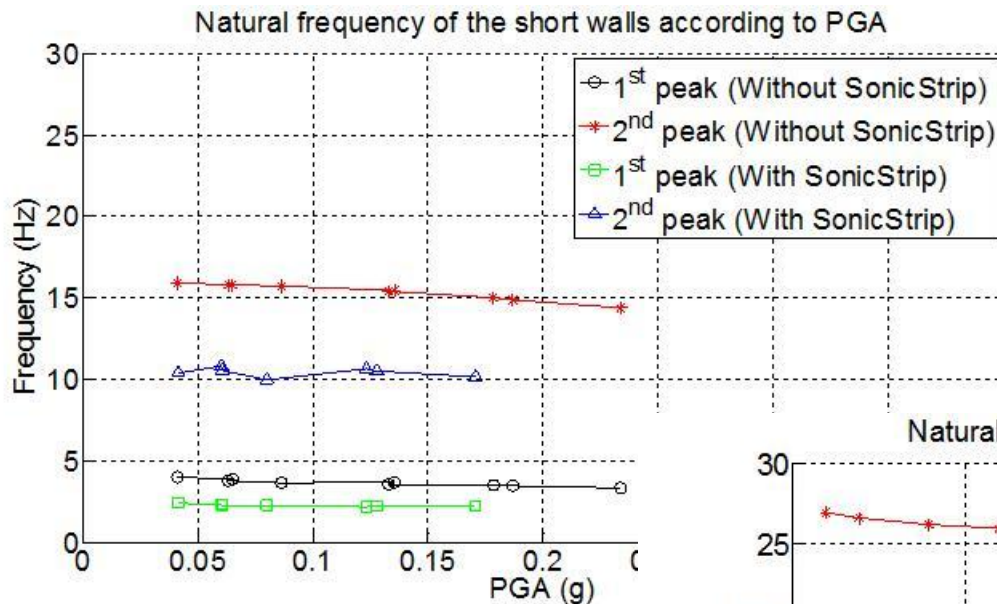
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Camera shake-table-yaxis

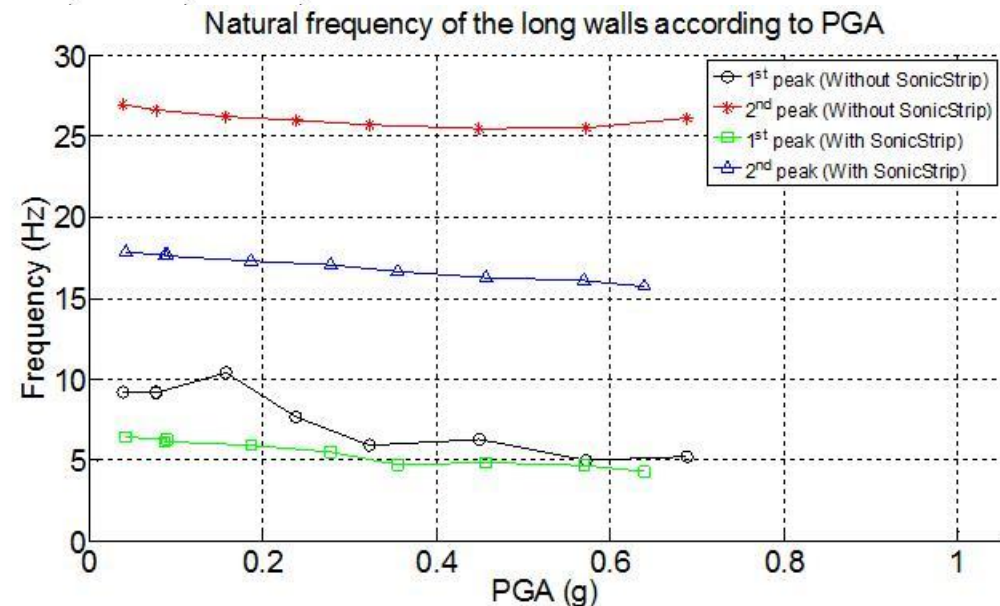
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MAID - Testing phase 1 - Single walls

Main experimental results and first numerical/theoretical exploitations:

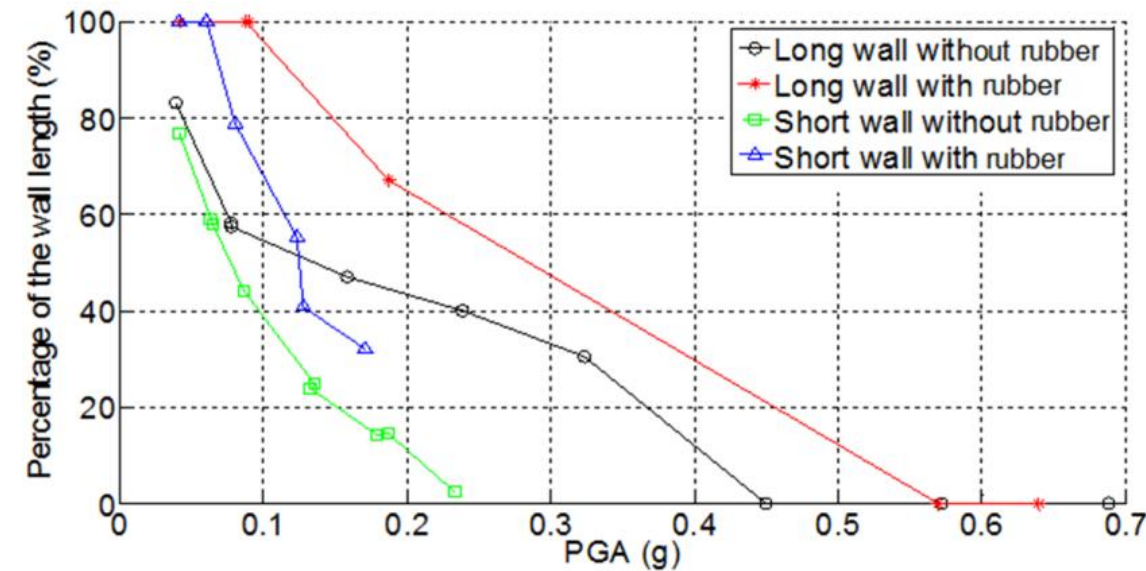


Frequency drop



MAID - Testing phase 1 - Single walls

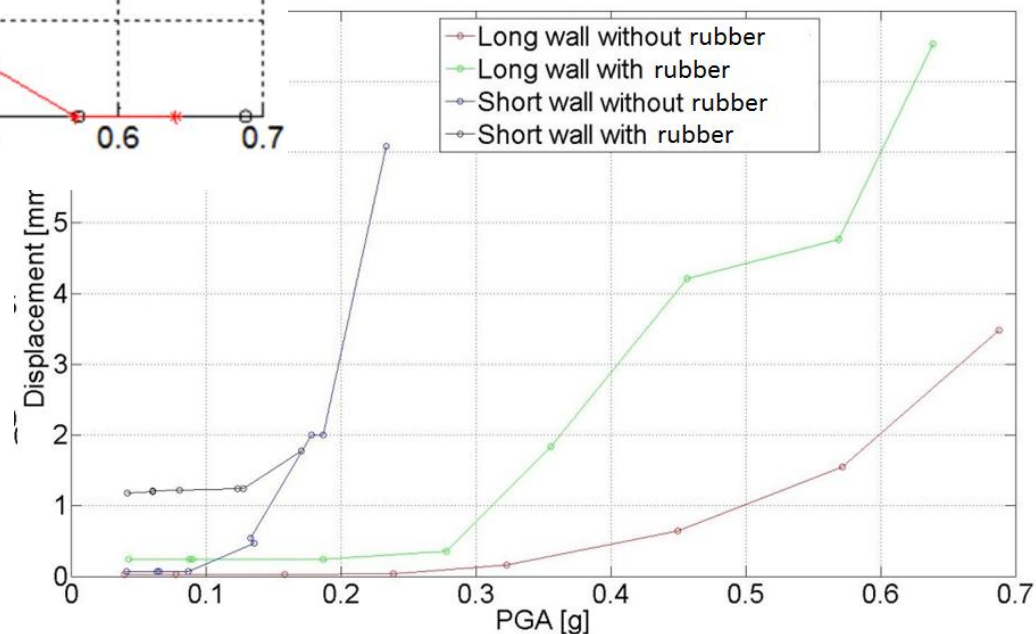
Main experimental results and first numerical/theoretical exploitations:



Compression length

Maximum displacement

Seismic behavior

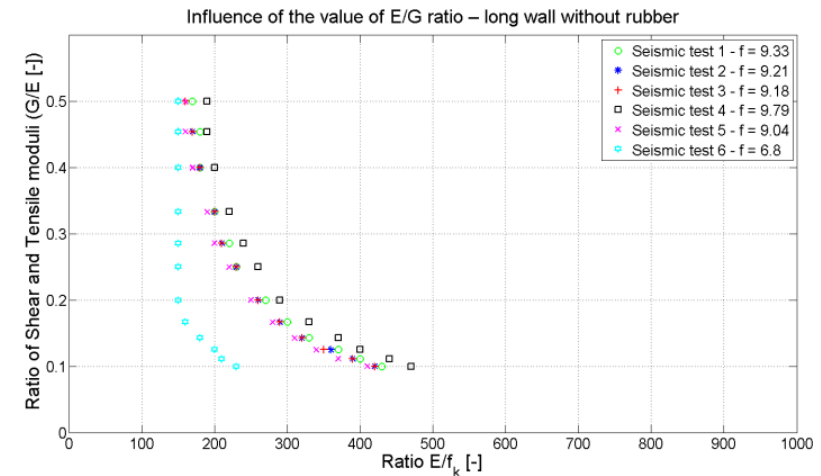
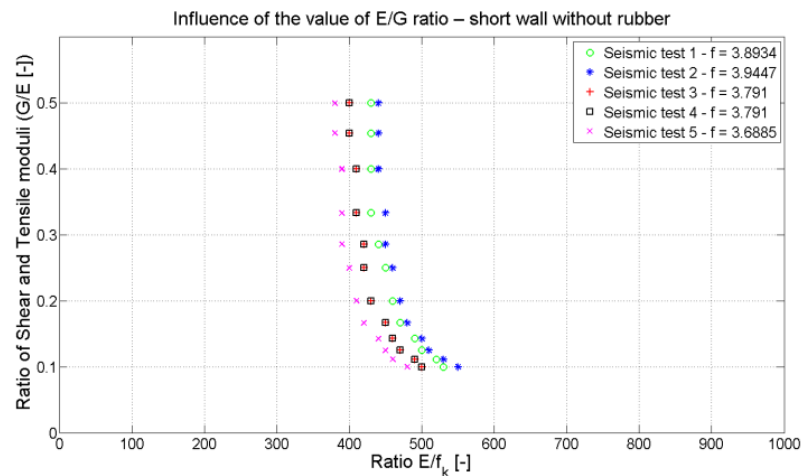


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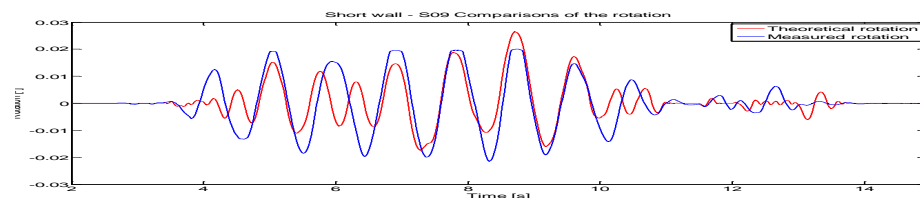
Main experimental results and first numerical/theoretical exploitations:

Calibration of numerical models

- Cantilever model (relevant for identification tests or limited accelerations): calibration of E and G modulus (see paper VEESD)



- Rigid body rocking model (suitable for large acceleration) – see paper COMPDYN



MAID - Testing phase 2 - Sub-structures

Mock ups:

- Two masonry portal frames coupled by a lintel and loaded by a concrete slab (+ additional masses)
- Case 1: piers with T cross section / Case 2: piers with L cross section
 - Case 1: Uniform gravity loading (significant overall and local **torsion effects**)
 - Case 2: Uniform gravity loading + Gravity only on flange walls



MAID - Testing phase 2 - Sub-structures

Preliminary design:

- Based on a conventional EC6/EC8 model with nominal material properties for characterizing each pier + pushover/N2 method to evaluate the redistribution capacity

→ Maximum acceleration (longitudinal earthquake):

▫ **Case 1 (T)**

- **Uniform loading:** 0.76 g
- **Loads on shear wall:** 0.78 g (shear wall alone: 0.71 g)
- **Loads on flanges:** 0.64 g

▫ **Case 2 (L)**

- **Uniform loading:** 0.83 g
- **Loads in shear wall:** 0.85 g (shear wall alone: 0.71 g)
- **Loads on flanges:** 0.65 g (shear wall alone: 0.22 g)

MAID - Testing phase 2 - Sub-structures

Testing procedure:

- EC8 spectrum-compatible time-history
- Increasing acceleration level - Tests stopped at
 - Case 1 (T): **0.45 g** – Important rocking effect + damaging of piers due to local torsion effects

MAID - Testing phase 2 - Sub-structures

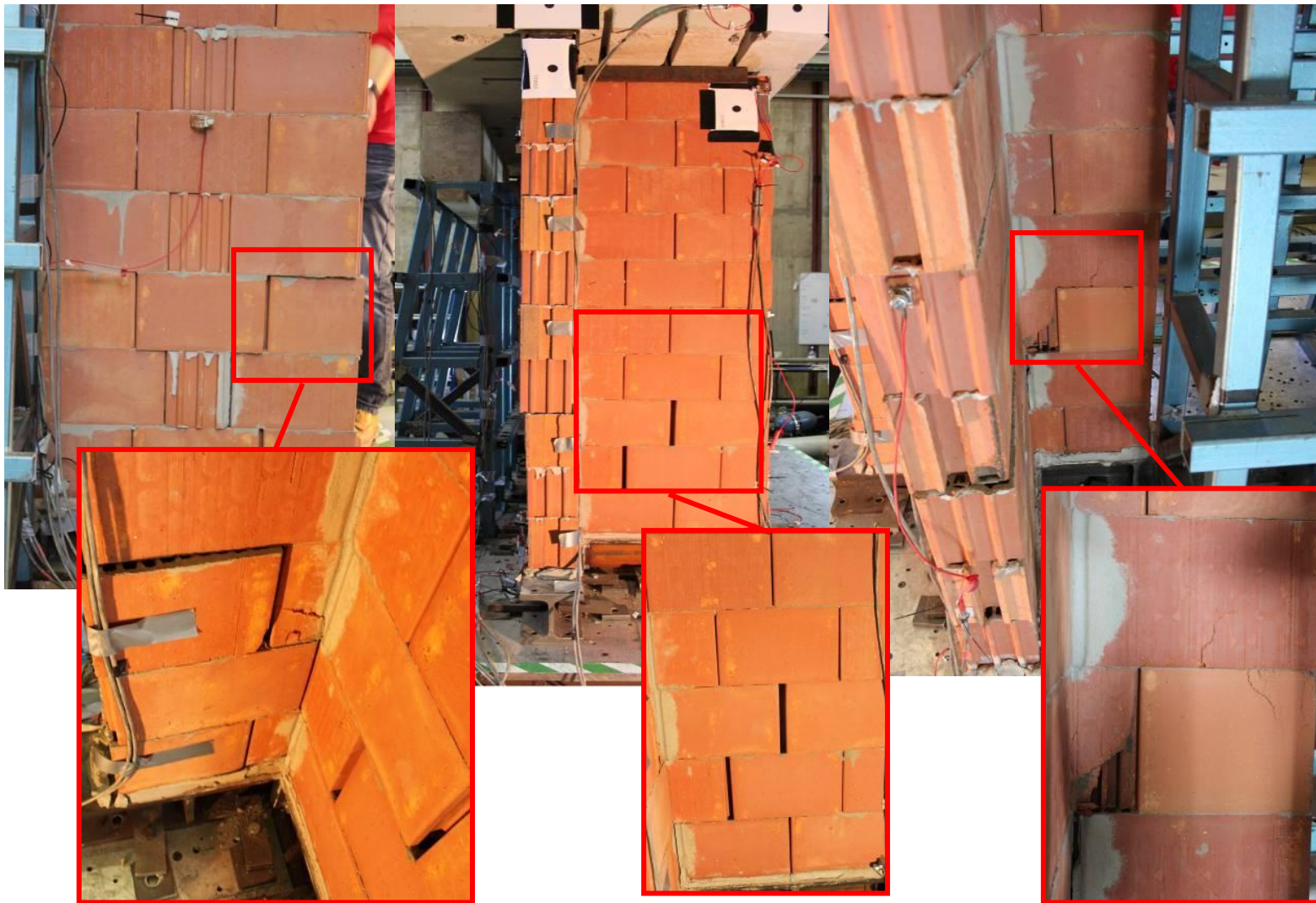


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MAID - Testing phase 2 - Sub-structures

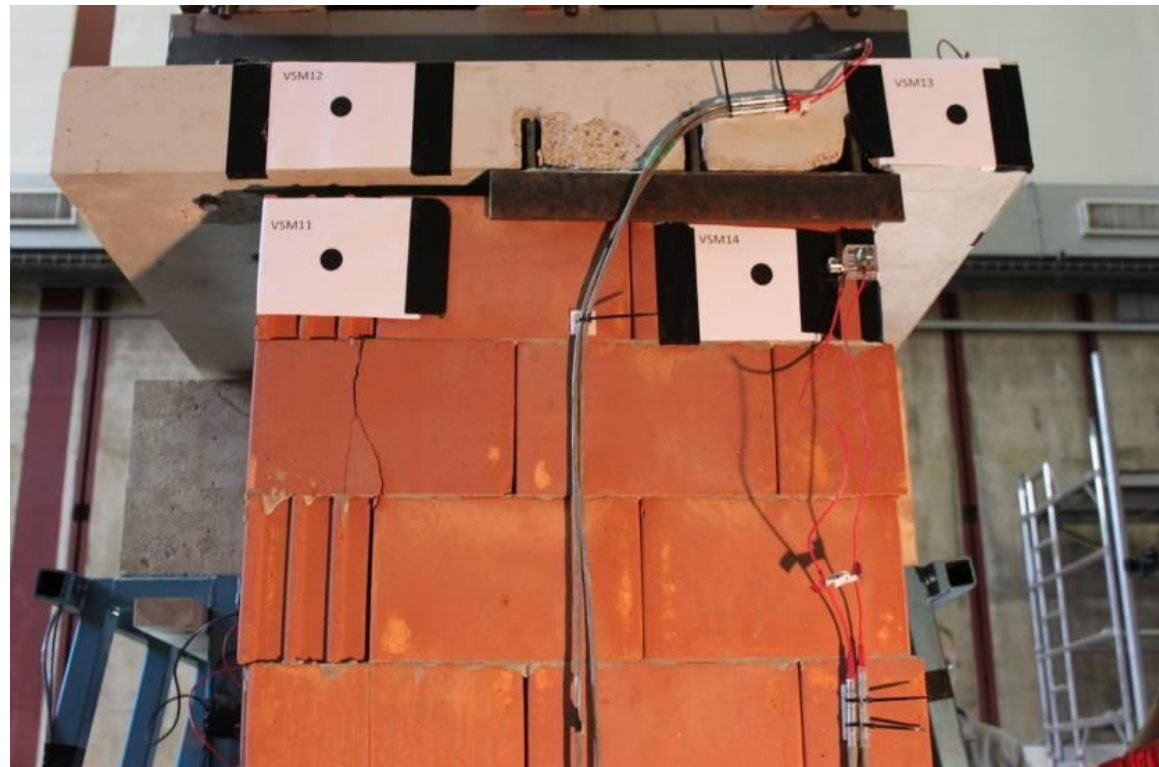


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 - Case 2.a (L – uniform): **0.32 g** – Stopped before damaging to allow testing case 2.b in good conditions (slight rocking however observed)
 - Case 2.b (L – load on flanges): **0.25 g !!** – Failure of the connection of the shear wall with the flange (not considered in the preliminary design)

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- Quantitative post-processing of the results and model calibration still in progress...

MAID – Conclusions

- Effect of the soundproofing rubber elements:
 - Increase the deformability of the system (longer period)
 - Limits the damage associated with rocking motion
 - Simple predictive models of the compression length are reliable
 - Cantilever and rocking models accurate in their range of applicability
- Frame behavior of flanged shear walls:
 - Basic models strongly overestimate the seismic capacity
 - Flanges trigger less usual effects
 - Importance of further investigating local effects of torsion and force transfer mechanisms at the interface flange/shear wall
- Further analyses still to come ...