THE NORDIC TEST SYSTEM FOR VOLTAGE STABILITY ASSESSMENT

Thierry Van Cutsem

Department of Electrical and Computer Engineering University of Liège, Belgium



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Context

- One of the two systems prepared by the Task Force on « Test Systems for Voltage Stability and Security Assessment »
 - under the auspices of Power System Stability Sub-committee
- modified version of a so-called "Nordic32" system
 - proposed in 1995 by a CIGRE WG
- focus is on long-term voltage stability
 - system evolution over several minutes after a disturbance
 - system also exposed to short-term (angle) instability

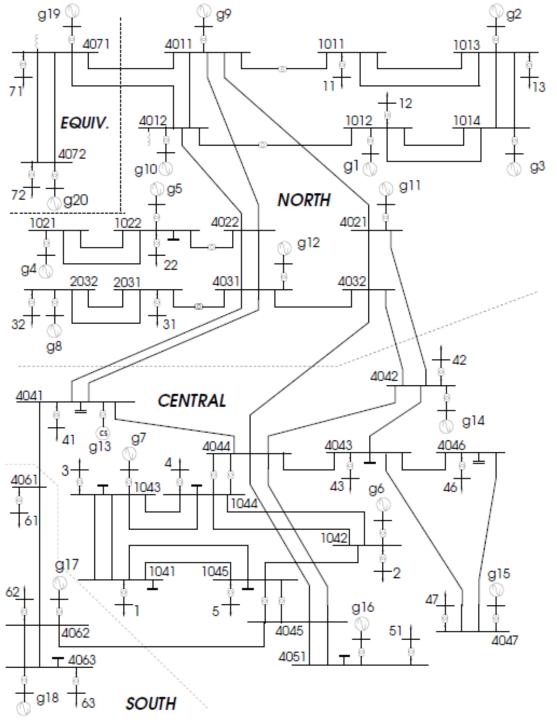




- System overview
- Modelling
- Dynamic responses to disturbances
- Preventive voltage security assessment
- Corrective (post-disturbance) control

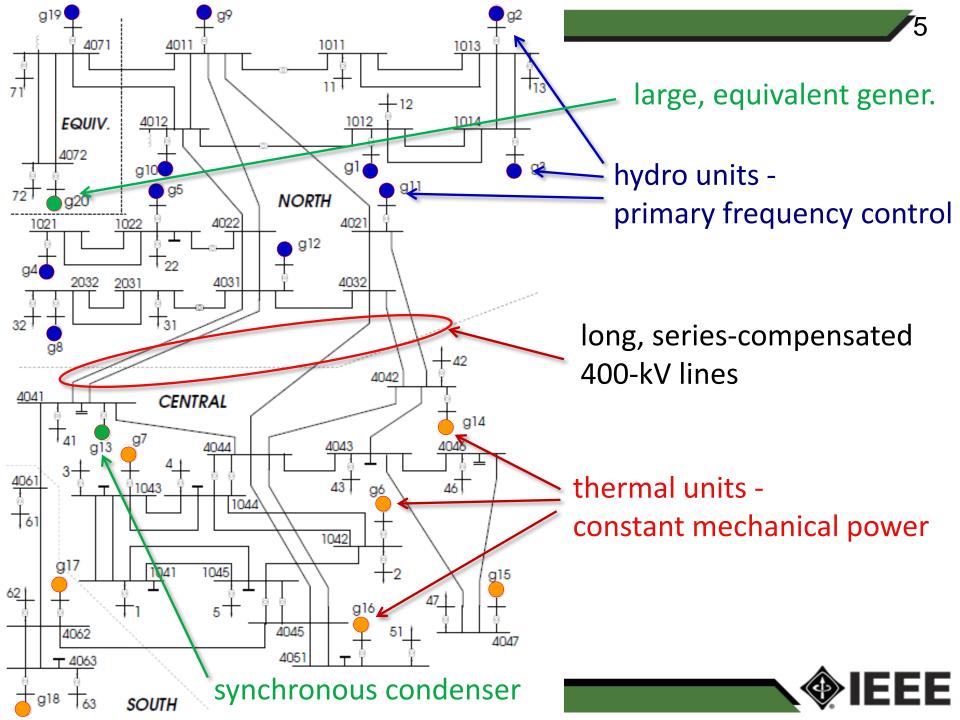


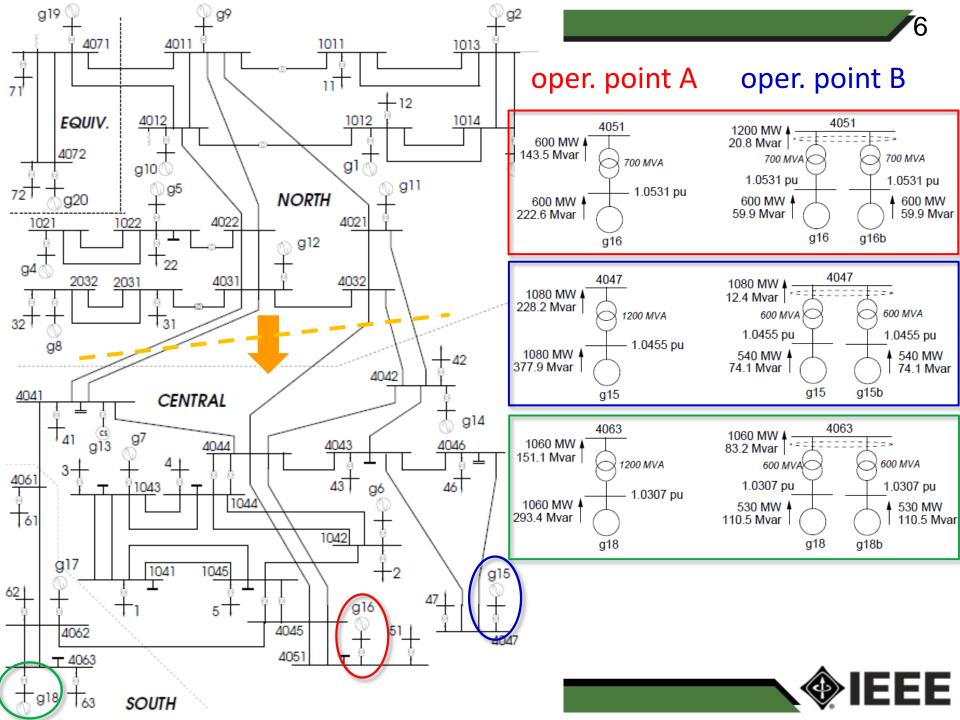




- transmission: 400 & 220 kV
- sub-transmission: 130 kV
- 50 Hz system
- 74 buses
- 20 generators
- 102 branches, including
 - 20 step-up transformers
 - 22 distribution transformers







Dynamic security assessment

- Operating point A: very insecure
 - several single contingencies cause instability
 - even some transient angle instability cases
- Operating point B : secure
 - the system can stand a 5-cyle (0.1 s) fault on any line, cleared by tripping the line
 - the system can stand the outage of any single generator
- Criteria used in long-term dynamic simulation
 - all distribution voltages restored into their deadband by Load Tap Changers (⇒ all load powers restored)
 - no loss of synchronism
 - no generator has its terminal voltage settling below 0.85 pu



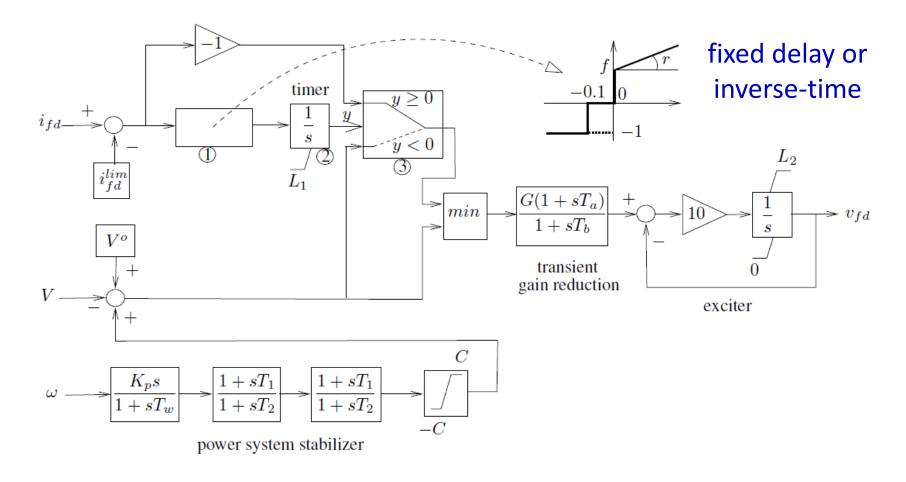


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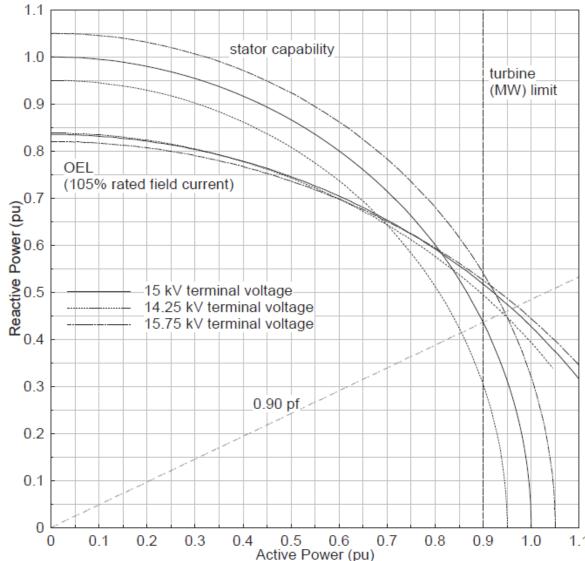
Exciter, AVR, PSS and OverExcitation Limiter (OEL)







Capability curves of round-rotor generators for various terminal voltages

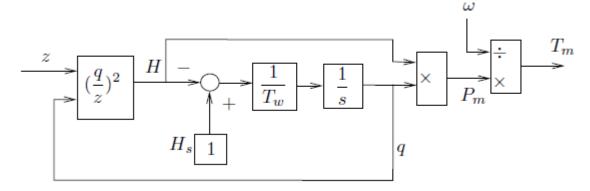




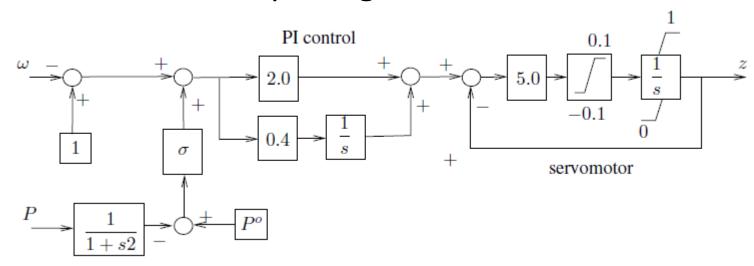




Hydro Turbine model



Speed-governor model

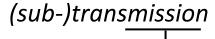




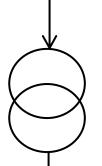


Load model

Load Tap Changers (LTC):



distribution



- voltage deadband :
 - [0.99 1.01] pu
- range of transformer ratio:
 [0.88 1.20] pu/pu
 - ...
- 33 tap positions
- various tapping delays

$$P = P_o(\frac{V}{V_o})^{\alpha} \qquad Q = Q_o(\frac{V}{V_o})^{\beta}$$

transformer	delays	
	τ_1 (s)	τ_2 (s)
11-1011	30	8
12-1012	30	9
13-1013	30	10
22-1022	30	11
1-1041	29	12
2-1042	29	8
3-1043	29	9
4-1044	29	10
5-1045	29	11
31-2031	29	12
32-2032	31	8
41-4041	31	9
42-4042	31	10
43-4043	31	11
46-4046	31	12
47-4047	30	8
51-4051	30	9
61-4061	30	10
62-4062	30	11
63-4063	30	12
71-4071	31	9
72-4072	31	11





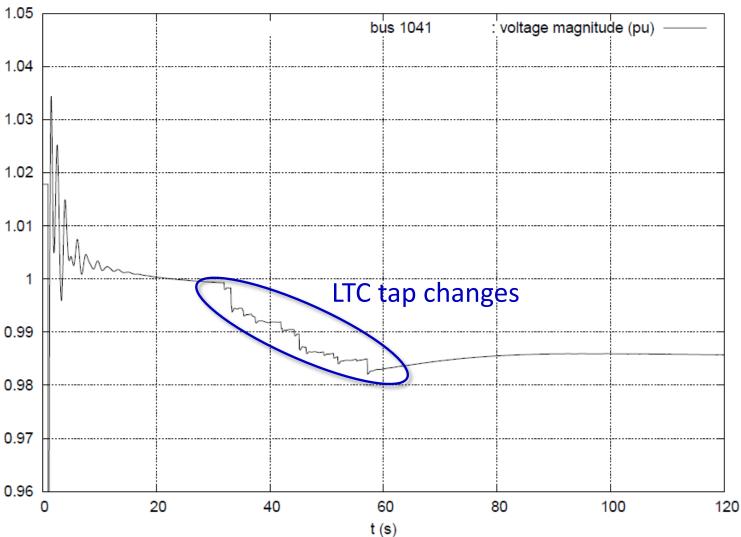
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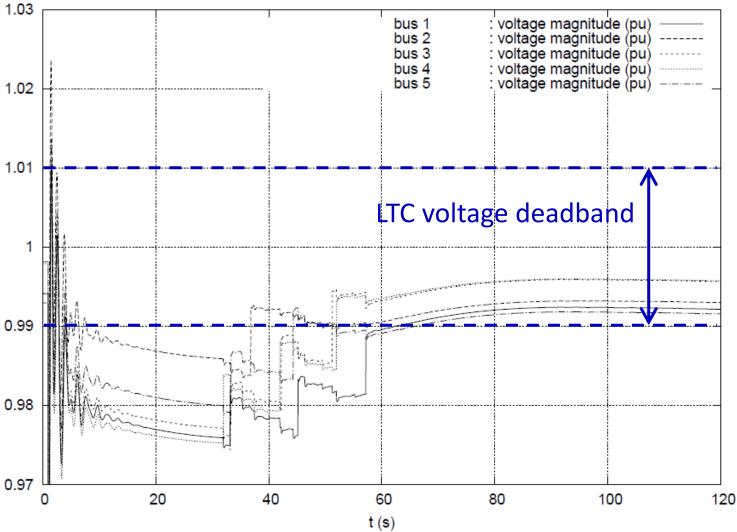
Secure oper. point B - Transmission voltage







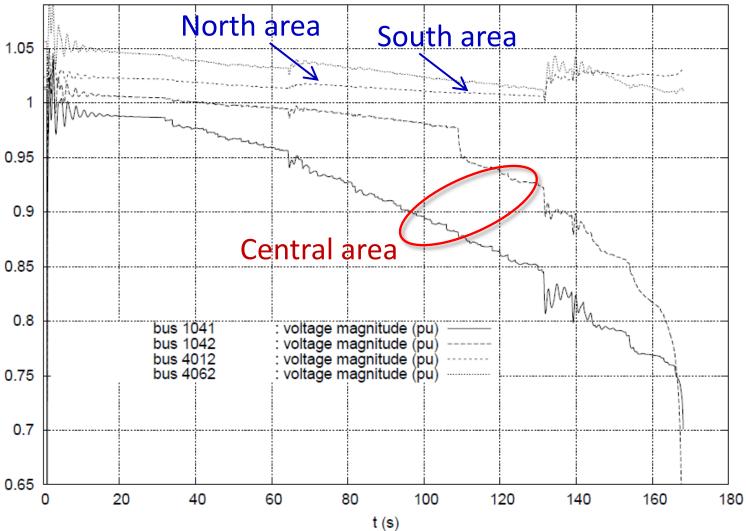
Secure oper. point B - Voltage at LTC-controlled distrib. buses







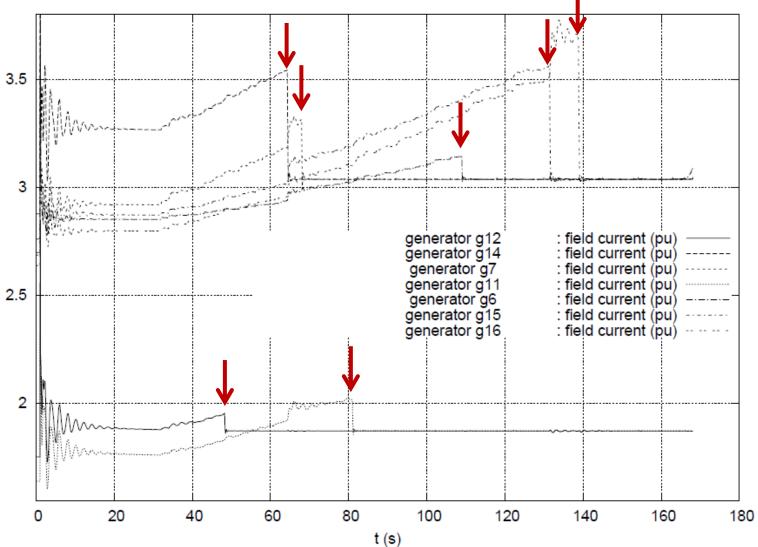
Insecure oper. point A - Transmission voltages







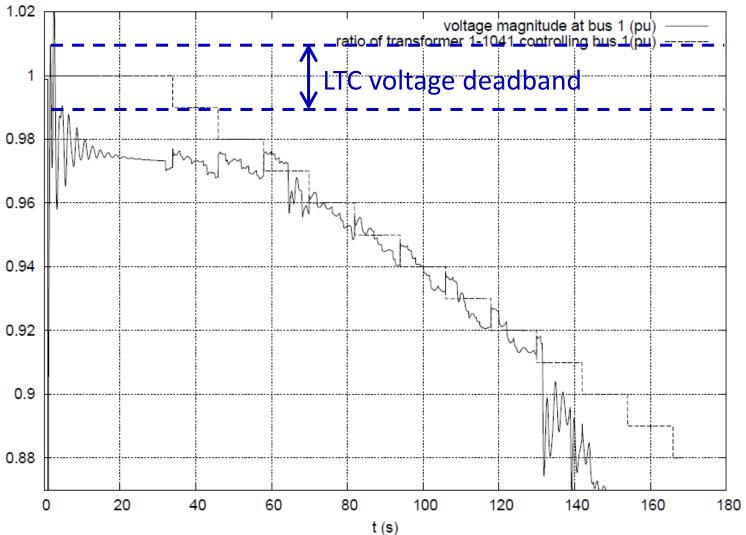
Insecure oper. point A - Generator field currents







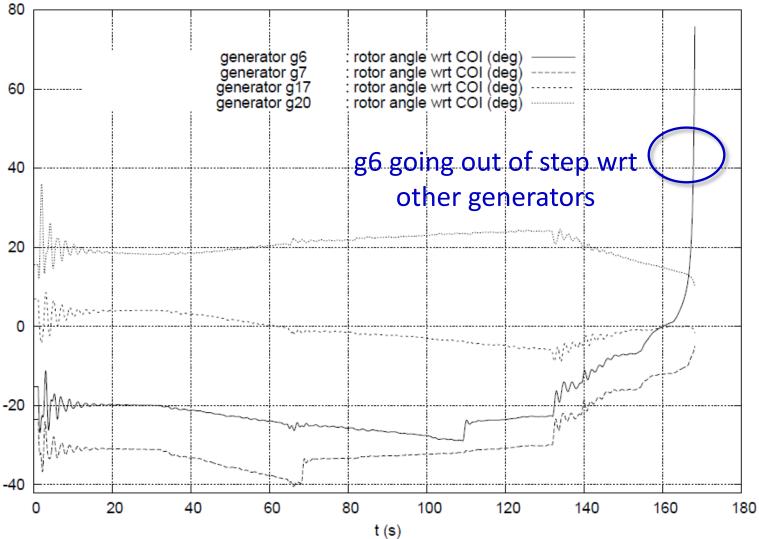
Insecure op. point A - Voltage at LTC-controlled distrib. bus







Insecure op. point A - rotor angles (wrt center of inertia)







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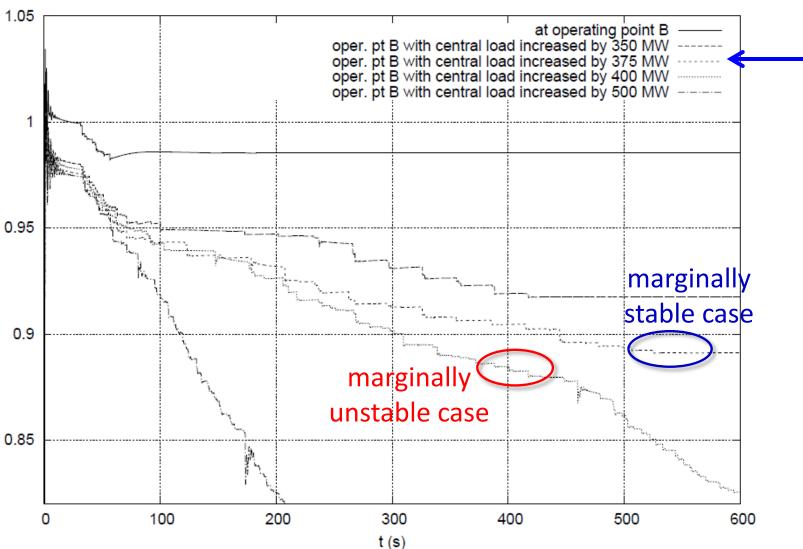
Secure Operation Limit (SOL)

- An SOL corresponds to the maximum « stress » that can be accepted in the pre-contingency configuration such that the system responds in a stable way to each of the specified contingencies
- stress = increase of load power in Central area
- tools:
 - power flow computations for various values of Central area load
 - long-term dynamic simulations to assess the system response to each contingency





Example of SOL determination - secure oper. pt B





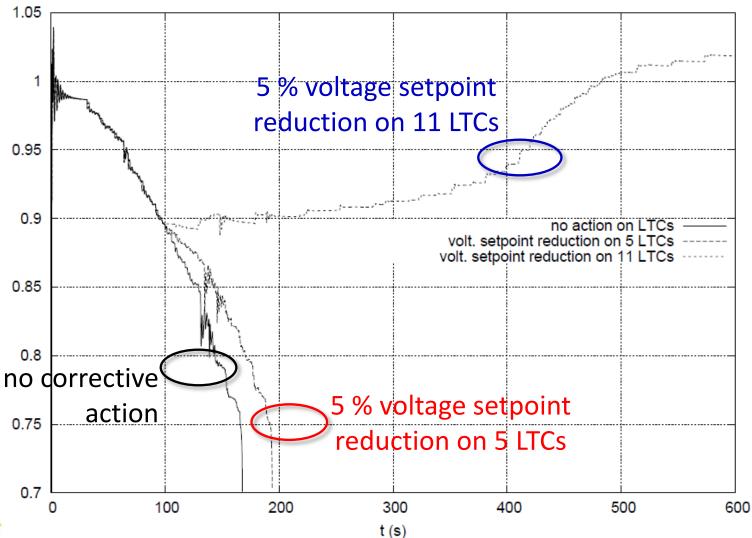


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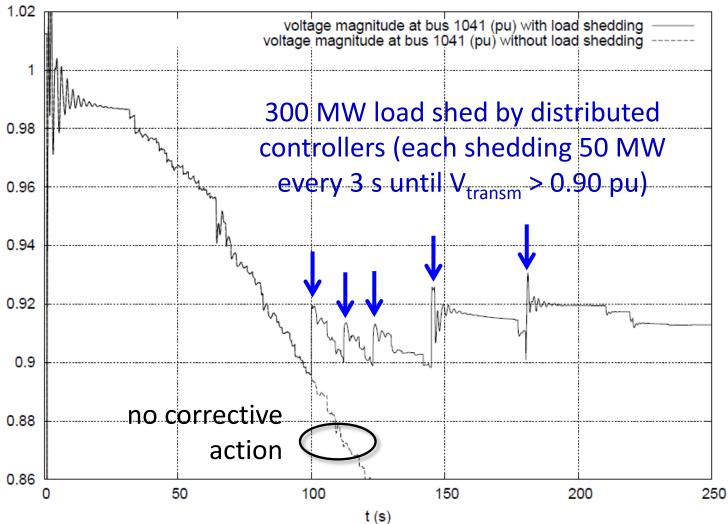
Corrective control: LTC voltage set-point reduction







Corrective control: undervoltage load shedding







Concluding remarks

- A truly voltage stability limited system
 - post-disturbance critical voltage ~ 0.92 pu at some transmission buses in the example shown
- Can be easily extended to other models and components:
 - new IEEE OEL models
 - induction motor loads (→ short-term voltage stability)
 - HVDC links
 - effect of generation connected at distribution level
 - etc.
- Its use should be encouraged in research and in publications





Thank you for your attention!

t.vancutsem@ulg.ac.be

www.montefiore.ulg.ac.be/~vct



