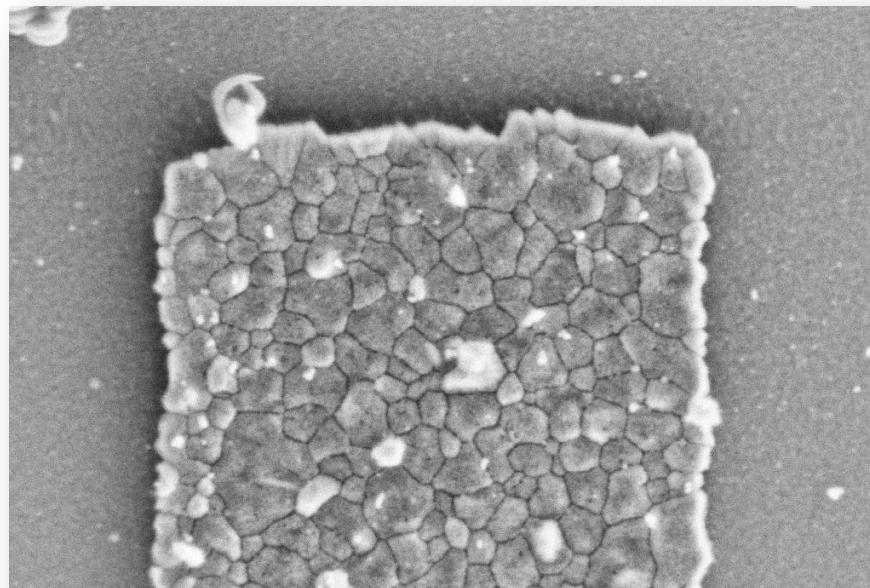


# Probabilistic model for MEMS micro-beam resonance frequency



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- Introduction
- Definition of the problem
  - A 3-scale procedure
  - First results
- From the microstructure towards the elasticity tensor
  - RVE & SVE
  - Samples of the microstructure
  - First results
- Conclusions & Perspectives

- **MEMS**

- MicroElectroMechanical systems
- Application in a wide variety of fields

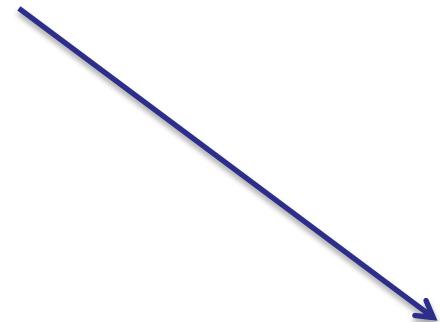
- Automobile industry



- Aeronautics



- Medecine



- Telecom

- ...

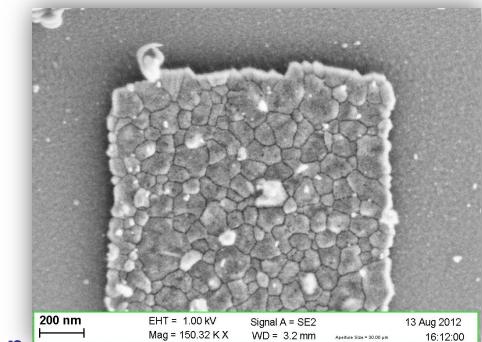


Common denominator: microscopic scale.

- How does it affect the material properties ?

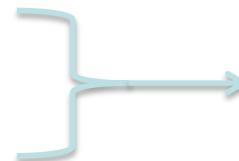
# The problem

- A macroscopic property of a MEMS can exhibit a scatter
  - Due to the fabrication process
  - Due to uncertainties of the material
  - ...



→ The objective of this work is to estimate this scatter

- Characteristic of the model:
  - Clamped microbeam
  - Macroscopic property of interest: first mode eigenfrequency
    - For a MEMS gyroscope for example
- In our model, the uncertainties come from the material:
  - Polysilicon is anisotropic
  - Polysilicon is polycrystalline
- Considering each grain to compute the macro quantity is too heavy



Each grain has a random orientation



3-scale procedure

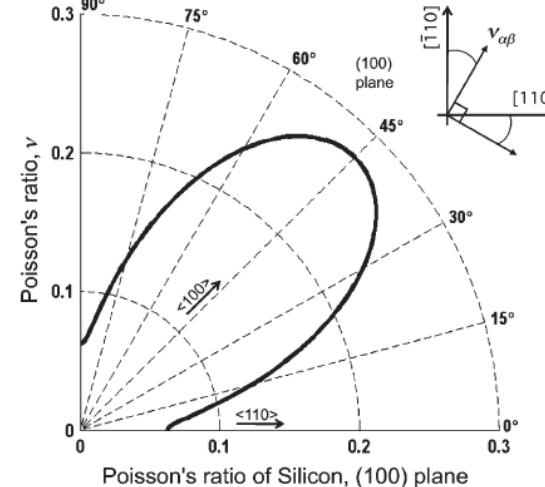
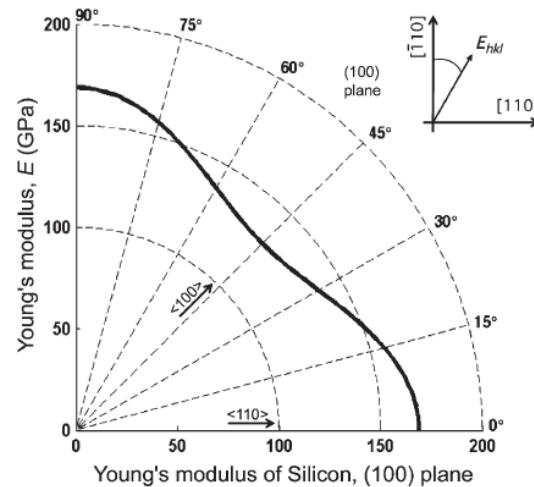
# A Silicon crystal

- What is the Young's Modulus of Silicon ? <sup>[1]</sup>

Based on Hall, with  $x, y, z$  aligned with [100], [010] and [001], we have:

$E_x$ [GPa]	$\nu_{yz}$	$G_{yz}$ [GPa]	$c_{11}$ [GPa]	$c_{12}$ [GPa]	$c_{44}$ [GPa]
130	0,28	79,6	165,6	63,9	79,5

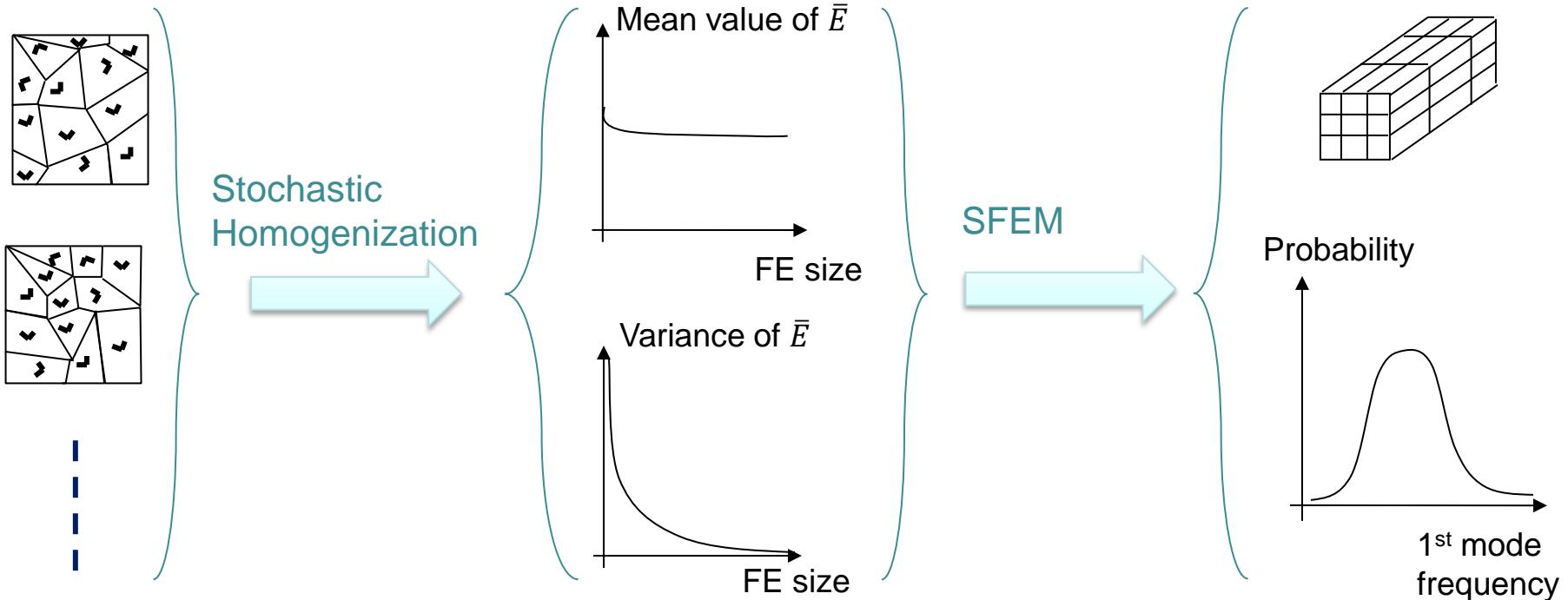
- Maximum value of  $E$  in  $\langle 111 \rangle$  direction: 188 GPa



[1] "What is the Young's Modulus of Silicon", M.A. Hopcroft, W.D. Nix, T.W. Kenny, Journal of microelectromechanical systems, april 2010, p.229-238

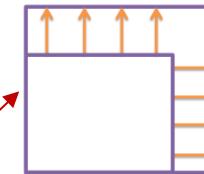
# A 3-scale procedure

Grain-scale or micro-scale	Meso-scale	Macro-scale
<ul style="list-style-type: none"> <li>➢ Samples of the microstructure (volume elements) are generated</li> <li>➢ Each grain has a random orientation</li> </ul>	<ul style="list-style-type: none"> <li>➢ Intermediate scale</li> <li>➢ The distribution of the material property <math>\mathbb{P}(C)</math> is defined</li> </ul>	<ul style="list-style-type: none"> <li>➢ Uncertainty quantification of the macro-scale quantity</li> <li>➢ E.g. the first mode frequency <math>\mathbb{P}(f_1)</math></li> </ul>



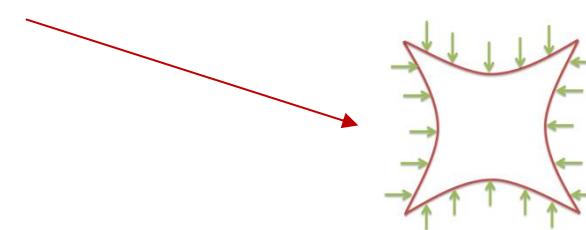
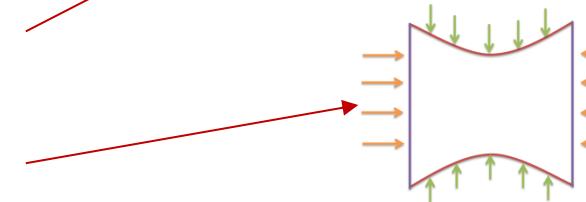
- **Representative Volume Element (RVE)**

- 1 elasticity tensor :  $C^{eff}$



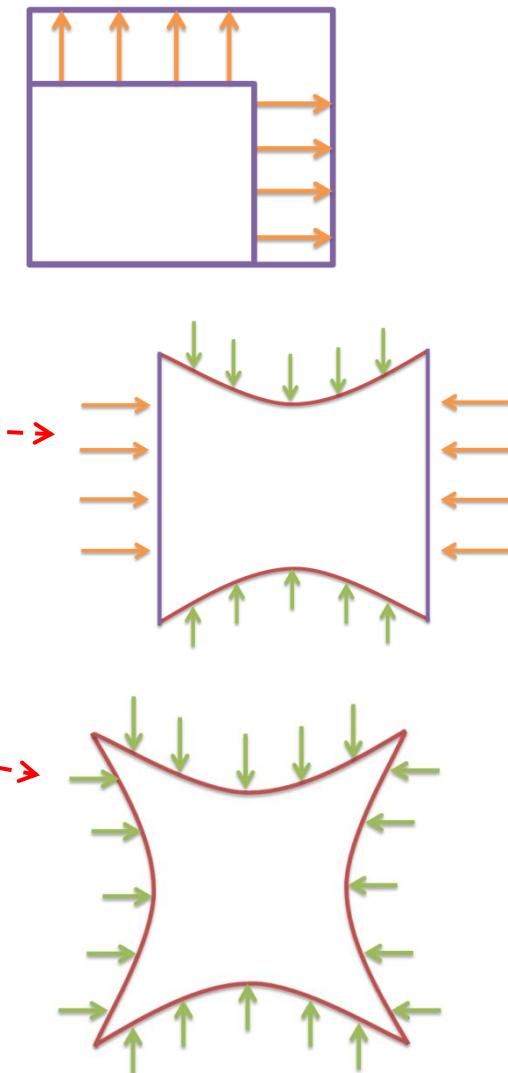
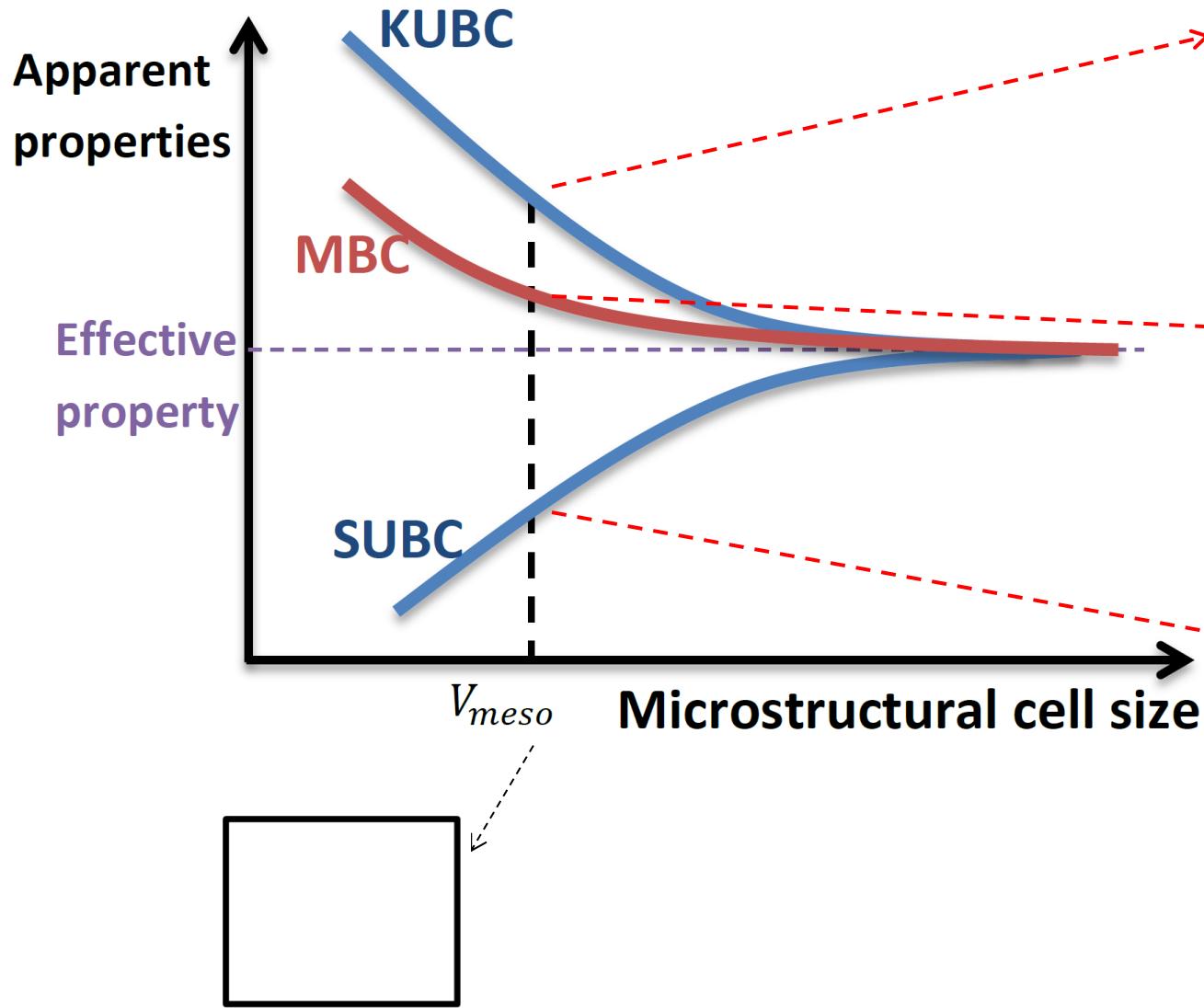
- **Statistical Volume Element (SVE)**

- A range of elasticity tensor
  - Depends on boundary conditions
    - Kinematic Uniform BC (KUBC)
    - Periodic BC (PBC)
    - Mixed BC (MBC)
    - Static Uniform BC (SUBC)

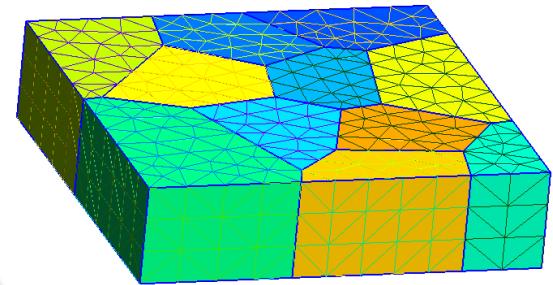
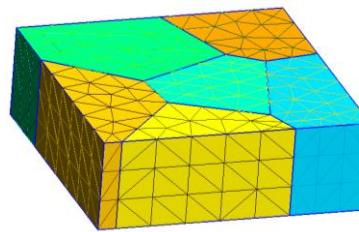
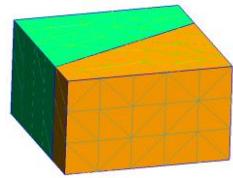


Note :  $A > B$  iff  $A - B$  is positive – definite (Loewner ordering)

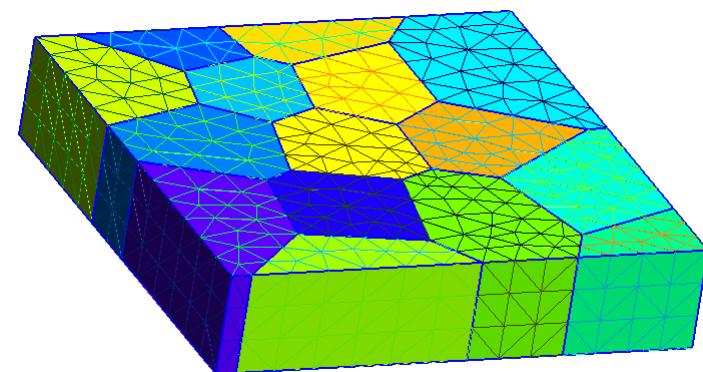
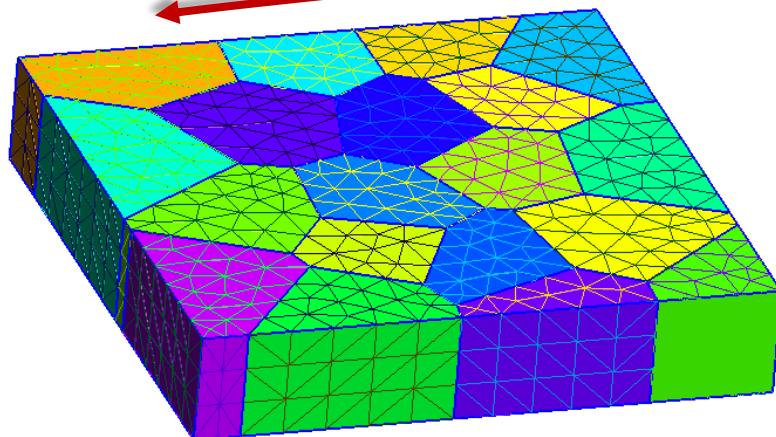
## Different boundary conditions



# SVE of different sizes



Different SVE sizes are considered



# Elasticity tensor computation

- When no access to the finite element stiffness matrix  $K$ :

$$\mathcal{C}_{BC} = \arg \min_{\mathcal{C}^{Lower} < \mathcal{C} < \mathcal{C}^{Upper}} \|\langle \sigma \rangle_{BC} - \mathcal{C} \langle \epsilon \rangle_{BC} \|$$

- The bounds can be :

- » Voight & Reuss bounds
- » KUBC & SUBC
- » In Between (Huet partition theorem [1])



Each are used in [3] and [4]

- E.g., this can happen with concrete experimental samples (see [2])

- When access to the finite element stiffness matrix  $K$ :

- The elasticity tensor can be directly computed from the stiffness matrix
- This is computational homogenization [5]
- $K^*$  being a rewritten version of  $K$  depending on the boundary condition:

$$\mathbb{C}_{BC} = \frac{1}{V_0} \sum_i \sum_j \mathbf{X}_{(i)} \mathbf{K}_{(ij)}^* \mathbf{X}_{(j)}$$

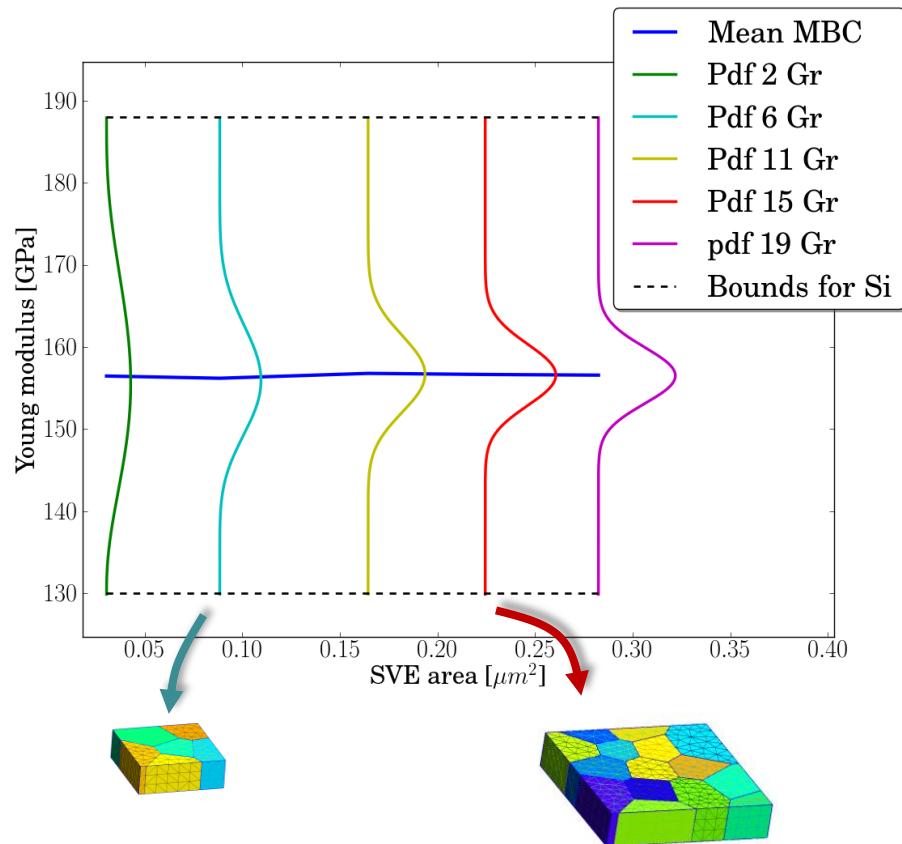
[2] "Application of variational concepts to size effects in elastic heterogenous bodies", Huet C., J.Mech.Phys.Solids, 1990

[3] "A probabilistic model for bounded elasticity tensor random fields with application to polycrystalline microstructures", Guilleminot J., Noshadravan A., Soize C., Ghanem R.G., Elsevier, 2011

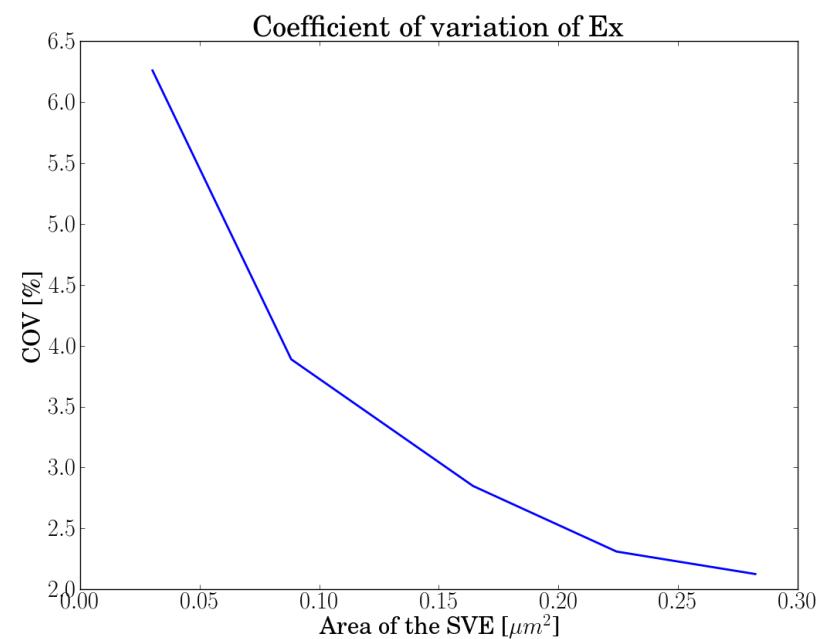
[4] "Validation of a probabilistic model for mesoscale elasticity tensor of random polycrystals", Noshadravan A., Ghanem R., Guilleminot J., Atodaria I., International journal for uncertainty quantification, 2011

[5] "Computational homogenization: implementation and extension", Kouznetsova V., Eindhoven University of Technology, 2010

# From micro to meso: results



- The bounds do not depend on the SVE size
- However → The bigger the SVE, the less likely  $\mathbb{C}$  is close to them



- The coefficient of variation is defined as :

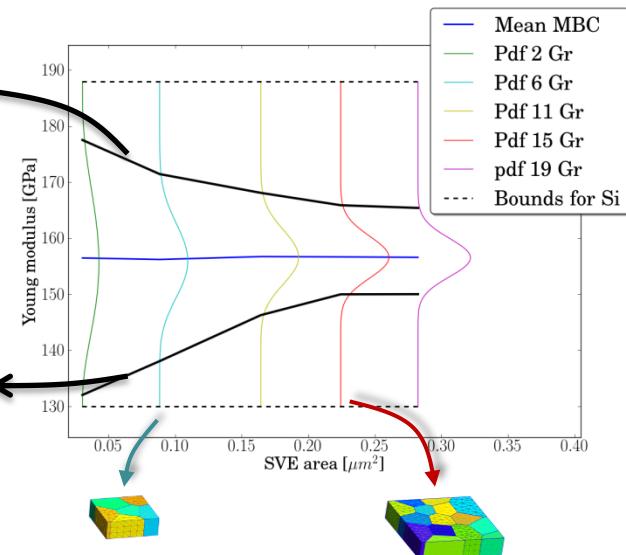
$$COV = \frac{\sqrt{Variance}}{mean} \cdot 100$$

- The bigger the SVE, the lower the COV

# From micro to meso: results

1D case

$$E_x^u = \text{Max}(E_x^{KUBC})$$



$$E_x^l = \text{Min}(E_x^{SUBC})$$

Matrix case [3,4]

$$\mathcal{C}_l = \arg \min_{\mathcal{C} \in \mathcal{C}_{ad}^l} \sum_{k=1}^{N_s} \|\mathcal{C}^{SUBC}(\theta_k) - \mathcal{C}\|_F$$

$$\mathcal{C}_{ad}^l = \{\mathcal{C} \in \mathbb{M}_n^+(\mathbb{R}) | \mathcal{C} < \mathcal{C}^{SUBC}(\theta_k), k = 1, \dots, N_s\}$$

$$\mathcal{C}_u = \arg \min_{\mathcal{C} \in \mathcal{C}_{ad}^u} \sum_{k=1}^{N_s} \|\mathcal{C} - \mathcal{C}^{KUBC}(\theta_k)\|_F$$

$$\mathcal{C}_{ad}^u = \{\mathcal{C} \in \mathbb{M}_n^+(\mathbb{R}) | \mathcal{C}^{SUBC}(\theta_k) < \mathcal{C}, k = 1, \dots, N_s\}$$

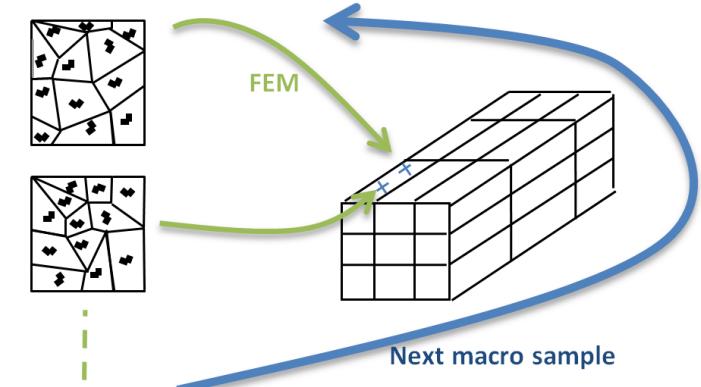
- [3] "A probabilistic model for bounded elasticity tensor random fields with application to polycrystalline microstructures", Guilleminot J., Noshadravan A., Soize C., Ghanem R.G., Elsevier, 2011
- [4] "Validation of a probabilistic model for mesoscale elasticity tensor of random polycrystals", Noshadravan A., Ghanem R., Guilleminot J., Atodaria I, International journal for uncertainty quantification, 2011

# The problem

- If a Monte-Carlo procedure is applied with FEM over a microbeam:

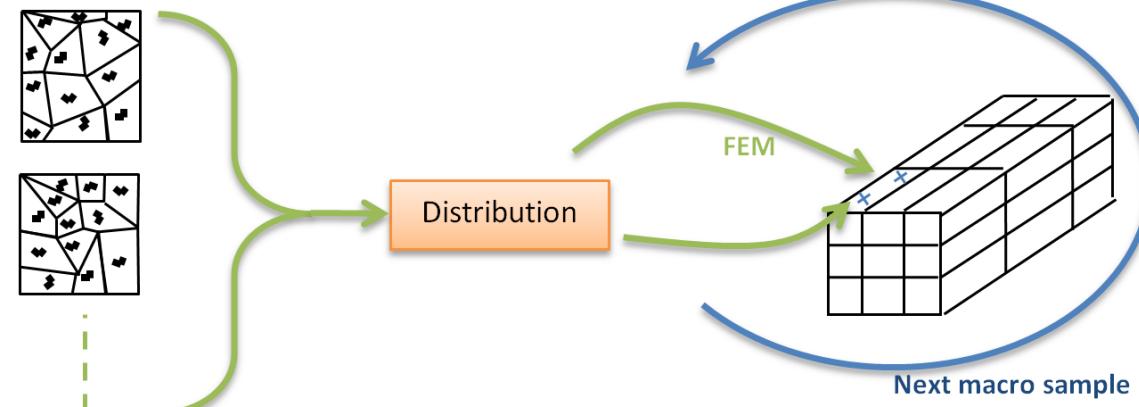
- No distribution and no generator:

- For each macro realization
    - At each Gauss points:
    - » a SVE should be computed



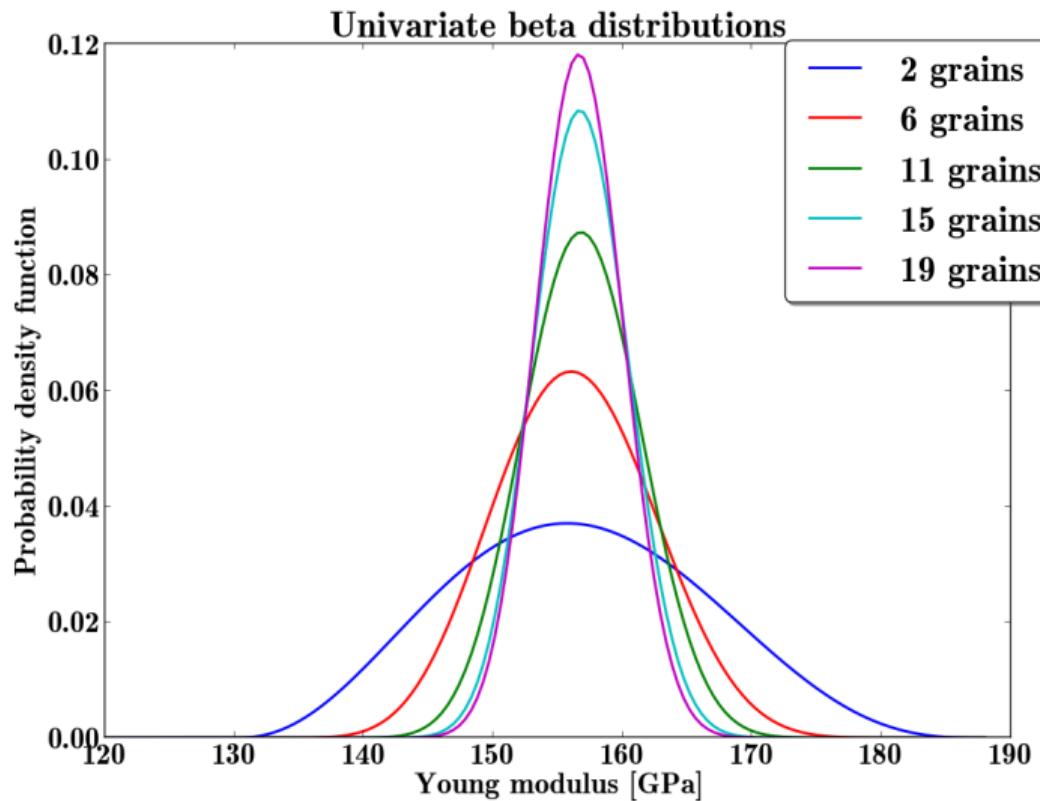
- With distribution and generator:

- Define a distribution encompassing the microstructure statistical behaviour
    - At each Gauss point:
    - Use the generator



➤ 1D case of  $E_x$ : Beta-based distribution of 4 parameters

$$P(E_x) = \frac{1}{\beta(\alpha, \beta)} \left[ \frac{E_x - E_x^l}{E_x^u - E_x^l} \right]^{\alpha-1} \left[ \frac{E_x^u - E_x}{E_x^u - E_x^l} \right]^{\beta-1}$$



## Extension to matrix case

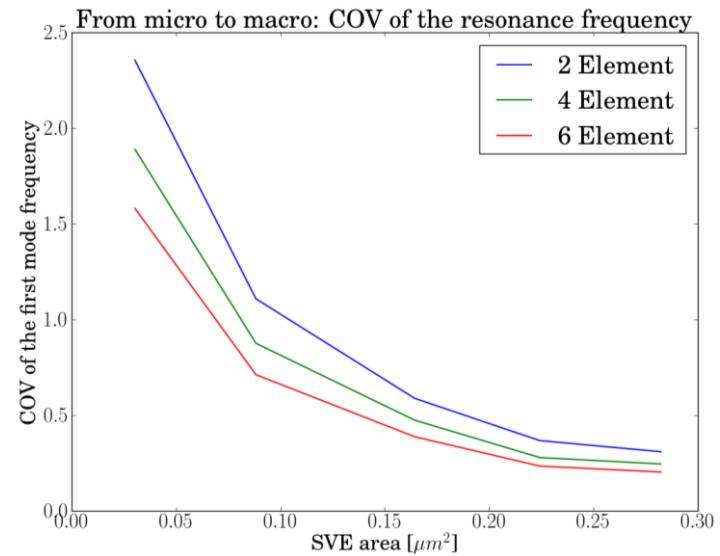
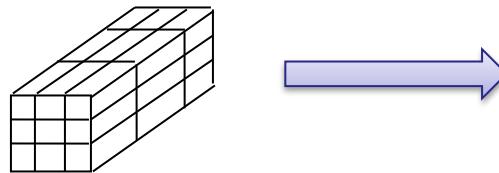
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- Maximize the information entropy  $\rightarrow \max_{\mathbb{C}} - \int_{M_n^+(\mathbb{R})} p([\mathbb{C}]) \ln(p([\mathbb{C}])) d\mathbb{C}$ 
  - Under constraints encompassing the available information
    - Samples of  $\mathbb{C}$
    - Bounds  $\mathbb{C}_u$  and  $\mathbb{C}_l$
  - No change of variable
    - Matrix-variate Kummer-beta distribution [6]
  - Using the  $N$  space [3,4]  $\rightarrow N = \frac{1}{c - c_l} - \frac{1}{c_u - c_l}$ 
    - Non-linear change of variable
    - Matrix-variate Gamma distribution [7]
  - Using the  $N'$  space  $\rightarrow N' = C - C_l$ 
    - Linear change of variable
    - Matrix-variate Gamma distribution
    - Loose the bound information

[6] "A bounded random matrix approach for stochastic upscaling", S. Das and R. Ghanem, Society for industrial and appl. Math., 2009,

[7] "Random matrix theory for modeling uncertainties in computational mechanics", Soize C., Comp. meth. In Appl. Mech. And Engrg., 2004

- From samples of grain orientations, elasticity tensors can be generated at meso-scale.
- How can we propagate the uncertainties up to the macroscopic scale?
  - Relevant SVE size
  - Correlation
  - ...



- Upgrades can take various forms:
  - 3D meso to macro part
  - Perturbation or Spectral Finite Element
  - Periodic boundary condition for the microstructure
  - ...

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Thank you for your attention !