

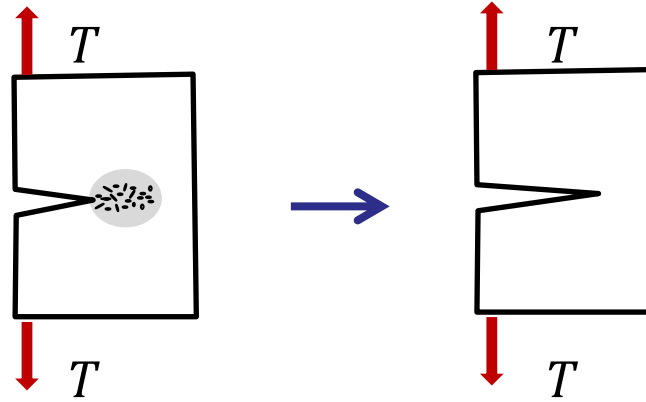
Modeling of Damage to Crack Transition using a Coupled Discontinuous Galerkin / Cohesive Extrinsic Law Framework

L. Wu , G. Becker and L. Noels

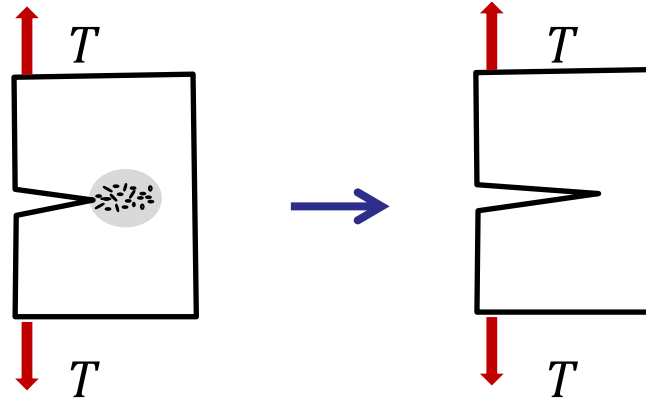
CFRAC 2013

- Introduction
- Non-local damage model to cohesive zone model
 - Implicit gradient enhanced damage model
 - Energy equivalence of damage model and cohesive zone model
 - 1D bar case
- Damage to crack
 - Discontinuous Galerkin / Cohesive Extrinsic Law Framework
 - Damage to crack transition
- Application
 - Compact tension specimen
- Conclusions

- Material fracture process
 - Damage accumulation
 - crack

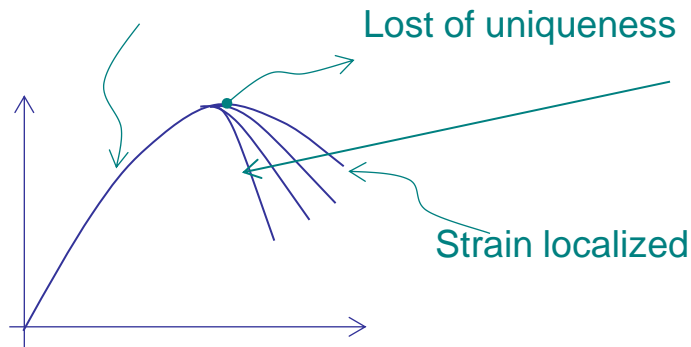


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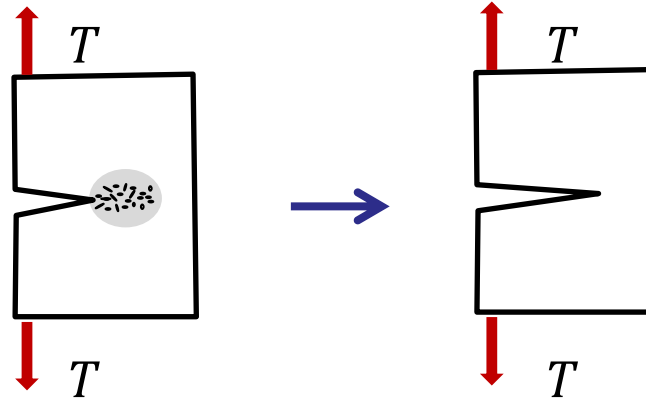
- Finite element solutions for strain softening problems suffer from:
 - The loss the uniqueness and strain localization
 - Mesh dependence

Homogenous unique solution



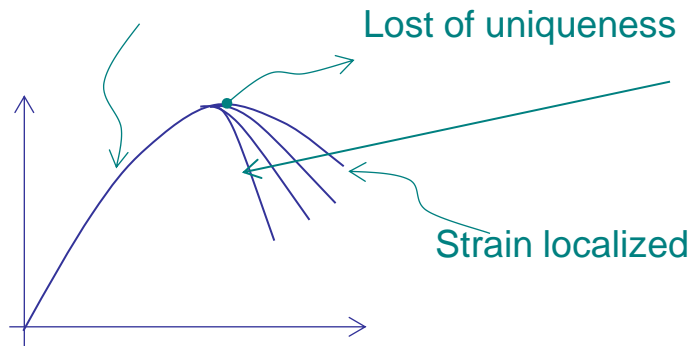
The numerical results change with the size and the direction of the mesh

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- Finite element solutions for strain softening problems suffer from:
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The numerical results change with the size and the direction of the mesh

- Discontinuous Galerkin / Cohesive Extrinsic Law Framework

- **Implicit gradient enhanced damage model** [Peerlings et al. 96, Geers et al. 97, ...]
 - A state variable is replaced by a non-local value reflecting the interaction between neighboring material points

$$\tilde{a}(\mathbf{x}) = \frac{1}{V_c} \int_{V_c} a(\mathbf{y}) w(\mathbf{y}; \mathbf{x}) dV$$

- Use Green functions as weight $w(\mathbf{y}; \mathbf{x})$  Implicit gradient enhanced model

$$\tilde{a} - c \nabla^2 \tilde{a} = a \quad \text{with} \quad \frac{\partial \tilde{a}}{\partial n} = n_i \frac{\partial \tilde{a}}{\partial x_i} = 0$$

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- General form for anisotropic cases

$$\tilde{a} - \nabla \cdot (\mathbf{c}_g \cdot \nabla \tilde{a}) = a \quad \mathbf{n} \cdot (\mathbf{c}_g \cdot \nabla \tilde{a}) = 0$$

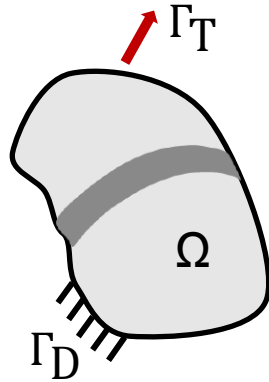
- Damage evolution $D(\tilde{e}; t)$

$$\tilde{e} - \nabla \cdot (\mathbf{c}_g \cdot \nabla \tilde{e}) = e \quad e = \sqrt{\sum_{i=1,2,3} (\varepsilon_i^+)^2}$$

Non-local damage model to cohesive zone model

- Energy equivalence of damage model and cohesive zone model
 - Cohesive law can be constructed from damage model [Planas et al. 1993, Cazes et al. 2009...]

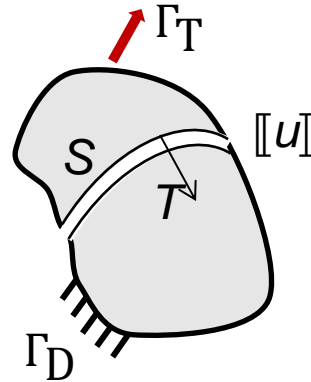
Non-local damage



Free energy

$$\frac{1}{2} \int_{\Omega} (1 - D) \boldsymbol{\varepsilon} : \mathbf{C}^e : \boldsymbol{\varepsilon} dV$$

Cohesive zone



$$\frac{1}{2} \int_{\Omega} (1 - D') \boldsymbol{\varepsilon}' : \mathbf{C}^e : \boldsymbol{\varepsilon}' dV$$

$$\boldsymbol{\sigma} = (1 - D) \mathbf{C}^e : \boldsymbol{\varepsilon}$$

$$Y = -\frac{1}{2} \boldsymbol{\varepsilon} : \mathbf{C}^e : \boldsymbol{\varepsilon}$$

Before damage
localization

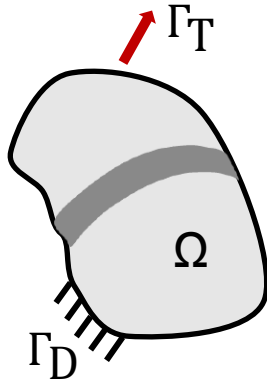
$$D = D' \text{ (diffuse damage)}$$

$$\boldsymbol{\varepsilon} = \boldsymbol{\varepsilon}'$$

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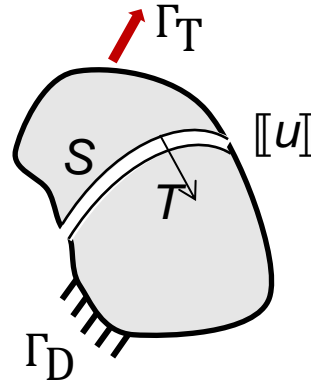
Non-local damage



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Cohesive zone



$$\frac{1}{2} \int_{\Omega} (1 - D') \boldsymbol{\varepsilon}' : \mathbf{C}^e : \boldsymbol{\varepsilon}' dV + \frac{1}{2} \int_S T [[u]] dA$$

$$\boldsymbol{\sigma} = (1 - D) \mathbf{C}^e : \boldsymbol{\varepsilon}$$

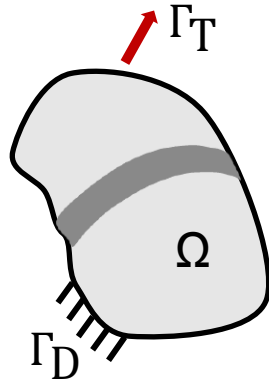
$$Y = -\frac{1}{2} \boldsymbol{\varepsilon} : \mathbf{C}^e : \boldsymbol{\varepsilon}$$

Out of damage
localization zone
 $D = D'$ (diffuse damage)
 $\boldsymbol{\varepsilon} = \boldsymbol{\varepsilon}'$

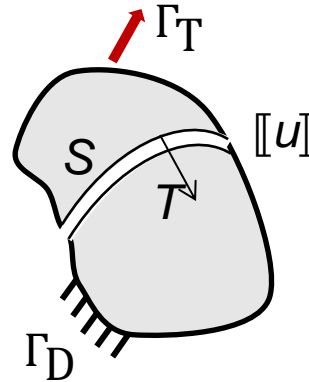
Non-local damage model to cohesive zone model

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Non-local damage



Cohesive zone



$$\sigma = (1 - D)\mathbf{C}^e : \boldsymbol{\varepsilon}$$

$$Y = -\frac{1}{2}\boldsymbol{\varepsilon} : \mathbf{C}^e : \boldsymbol{\varepsilon}$$

Free energy

$$\frac{1}{2} \int_{\Omega} (1 - D)\boldsymbol{\varepsilon} : \mathbf{C}^e : \boldsymbol{\varepsilon} dV$$

Increment of dissipated energy

$$d\Phi_{loc} = \int_{\Omega} (-Y dD) dV$$

Dissipated energy

$$\int_{\Omega} \left(\int_{D'}^1 -Y dD \right) dV$$

$$\frac{1}{2} \int_{\Omega} (1 - D')\boldsymbol{\varepsilon}' : \mathbf{C}^e : \boldsymbol{\varepsilon}' dV + \frac{1}{2} \int_S T [[u]] dA$$

$$d\Phi_s = \frac{1}{2} \int_S (T d[[u]] - [[u]] dT) dA$$

$$\int_S \int_0^{\infty} T [[u]] dA$$

Out of damage
localization zone

$$D = D' \text{ (diffuse damage)}$$

$$\boldsymbol{\varepsilon} = \boldsymbol{\varepsilon}'$$

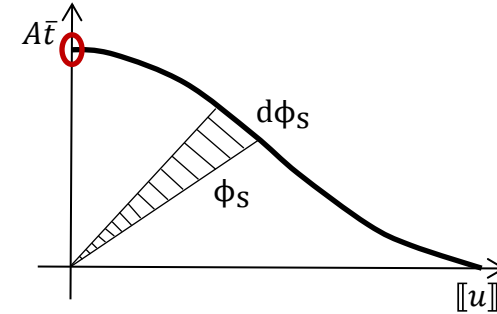
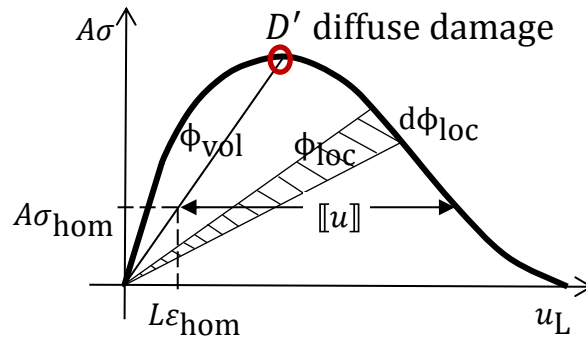
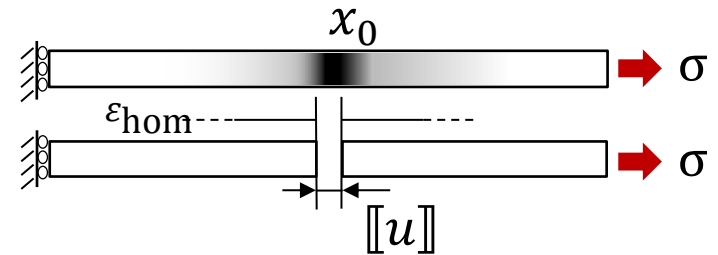
Non-local damage model to cohesive zone model

- 1D case analysis

A – cross section of the bar

σ – tensile stress

u_L – the displacement at right end of the bar



Transition at D'

$$[[u]] = \int_0^L (\varepsilon - \varepsilon_{\text{hom}}) dL$$

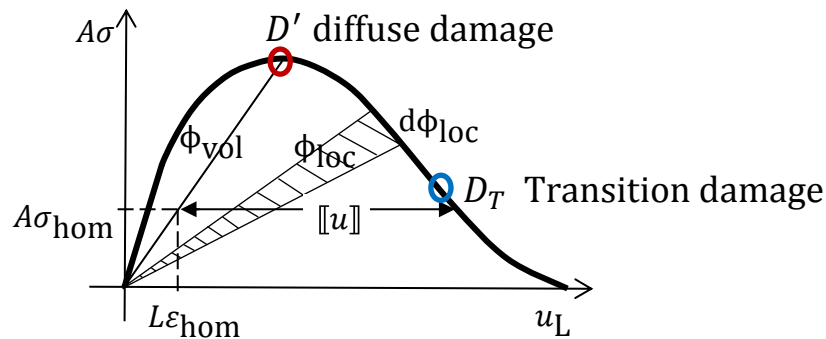
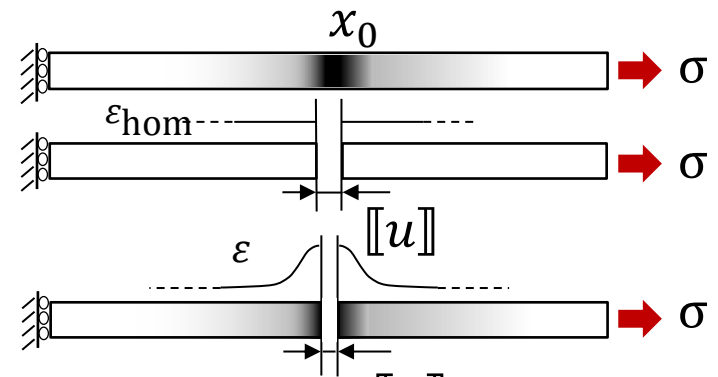
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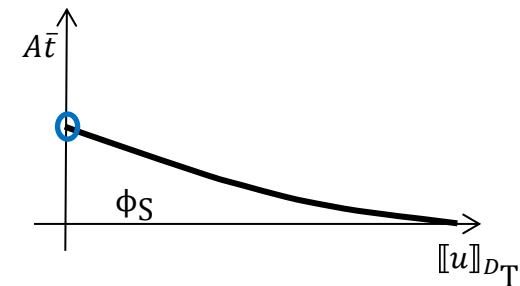
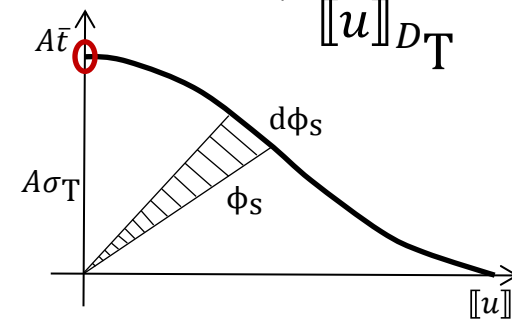


Transition at D'

$$[[u]] = \int_0^L (\varepsilon - \varepsilon_{\text{hom}}) dL$$

Transition at D_T

$$[[u]]_{D_T} \neq [[u]]$$



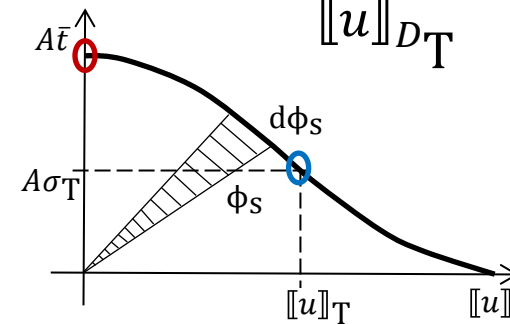
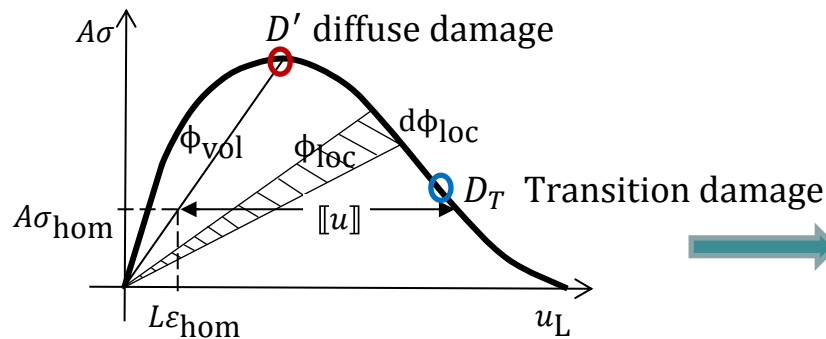
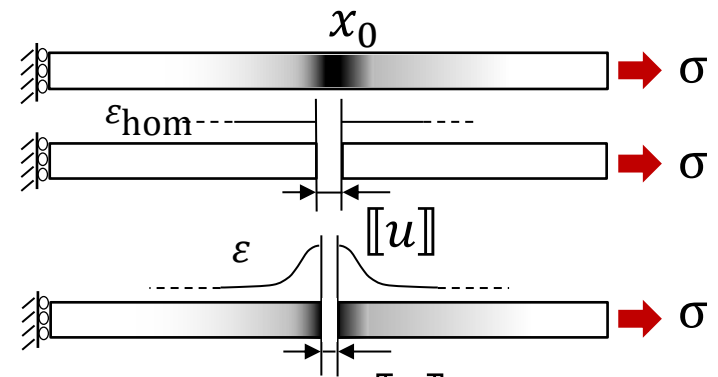
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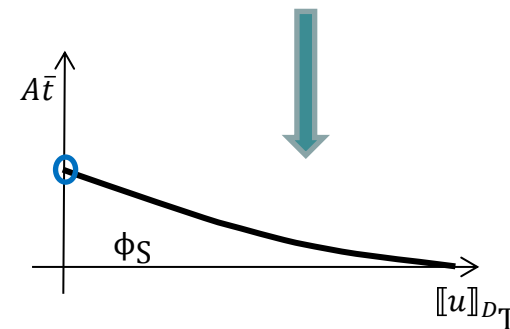


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Transition at D_T

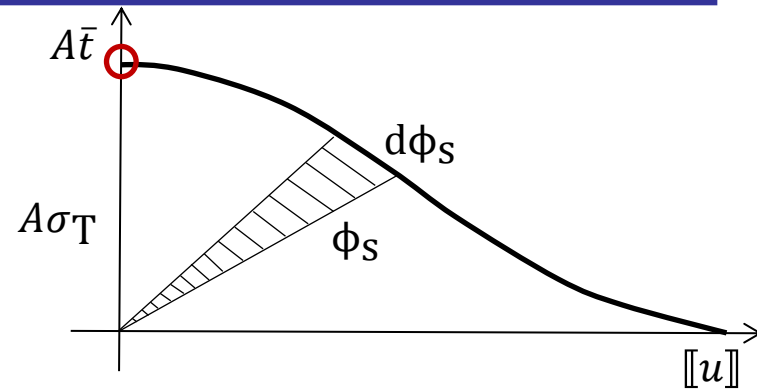
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Key issue: ϕ_S !!!

Non-local damage model to cohesive zone model

- 1D case analysis
 - Numerical solution



Non-local damage model to cohesive zone model

- 1D case analysis
 - Numerical solution
 - Approximation at high damage

When damage is rather high:

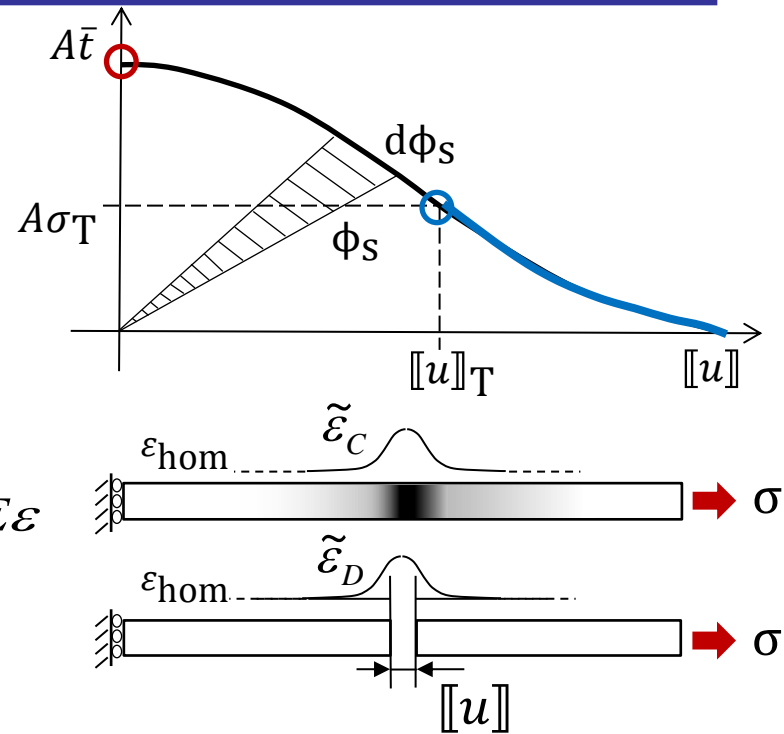
[Dufour et al. 2008, ...]

$$\tilde{\varepsilon}_C \approx \tilde{\varepsilon}_D(\varepsilon_{\text{hom}}, \llbracket u \rrbracket)$$

Stress equivalence:

$$(1 - D')E\varepsilon_{\text{hom}} = (1 - D(\tilde{\varepsilon}_C))E\varepsilon$$

$$\llbracket u \rrbracket = \int_0^L (\varepsilon - \varepsilon_{\text{hom}}) dL$$



Non-local damage model to cohesive zone model

- 1D case analysis
 - Numerical solution
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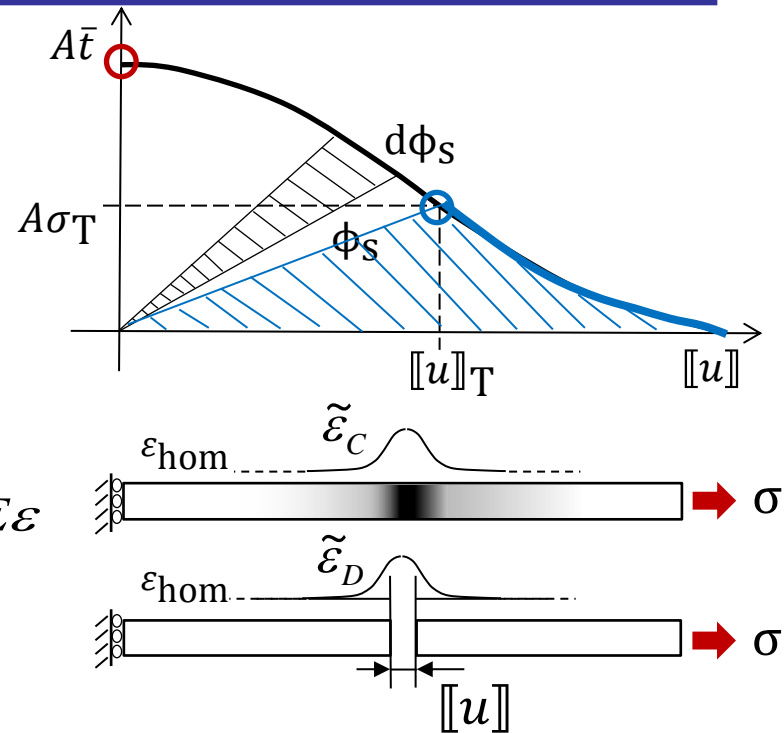
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Example: [Geers et al. 1999, ...]

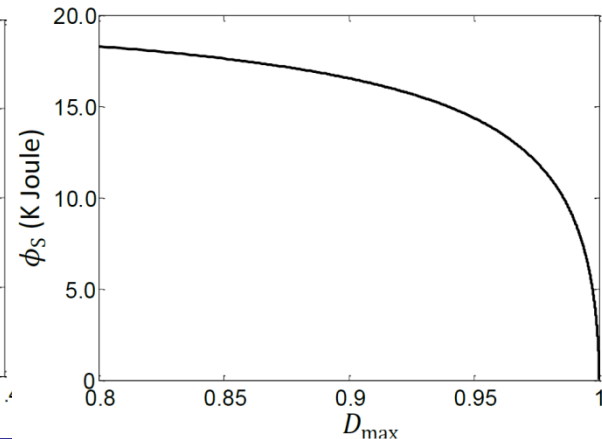
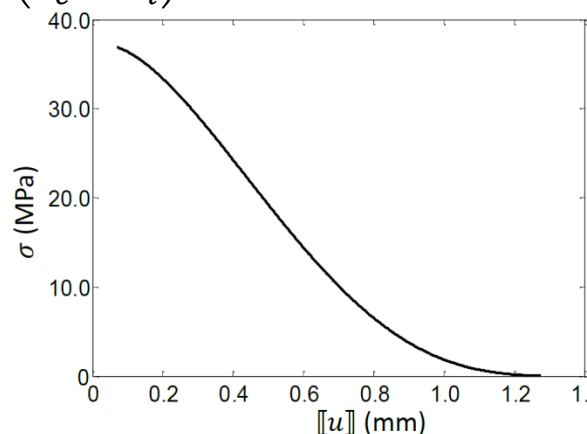
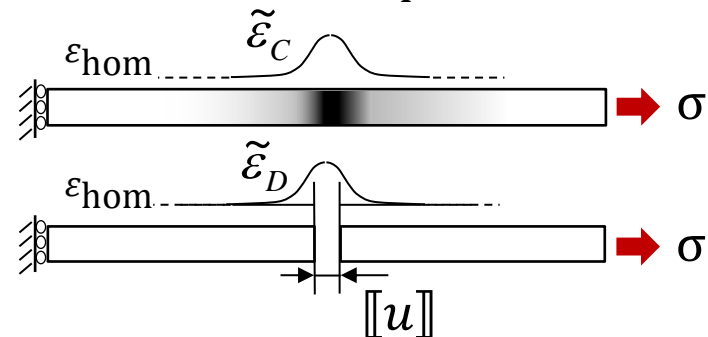
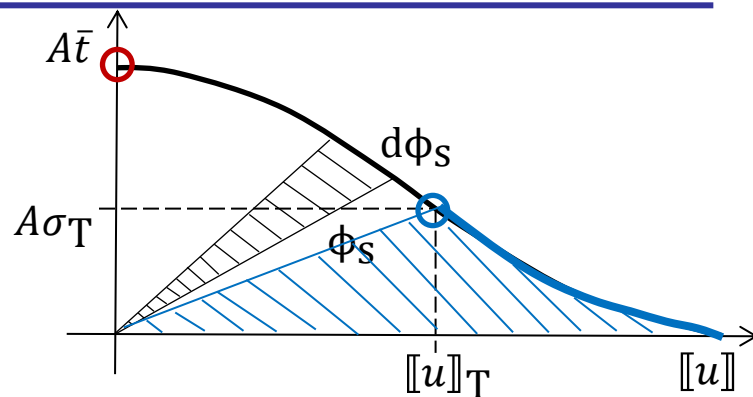
$$D = 1 - \left(\frac{\kappa_i}{\kappa}\right)^\beta \left(\frac{\kappa_c - \kappa}{\kappa_c - \kappa_i}\right)^\alpha$$

$$\kappa\{x\} = \max[\tilde{\varepsilon}(x, \tau) | \tau \leq t]$$

E	3.2[GPa]
ν	0.28

κ_i	0.011
κ_c	0.5
α	5.0
β	0.75

$$c_g = \text{diag}\{2.0\} \text{ mm}^2$$



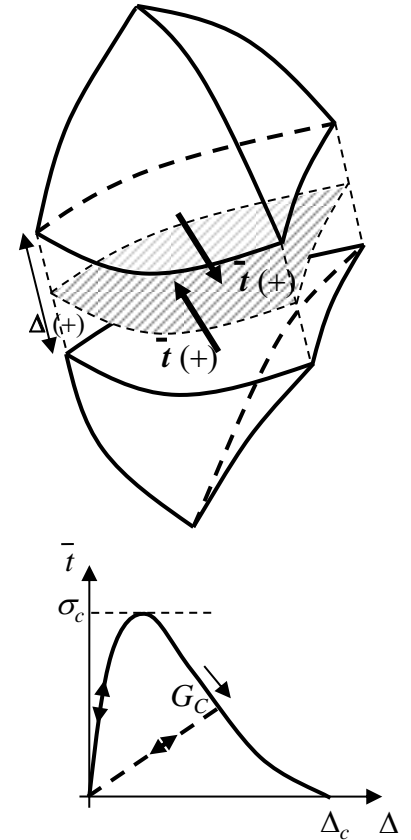
- Problems with cohesive elements

- Intrinsic Cohesive Law (ICL)

- Cohesive elements inserted from the beginning

- Drawbacks:

- Efficient if a priori knowledge of the crack path
- Mesh dependency [Xu & Needleman, 1994]
- Initial slope modifies the effective elastic modulus
- This slope should tend to infinity [Klein et al. 2001]:
 - » Alteration of a wave propagation
 - » Critical time step is reduced



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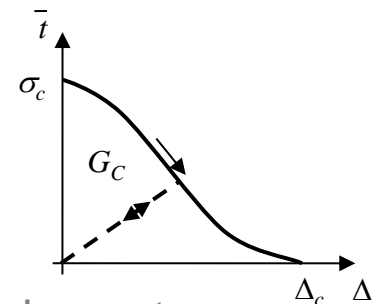
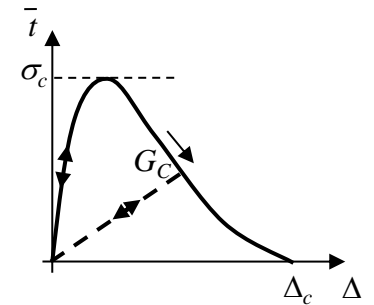
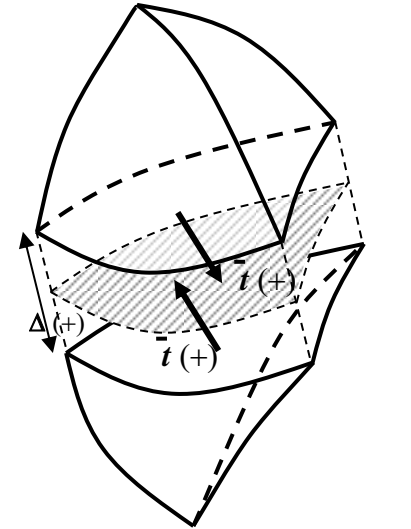
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- Extrinsic Cohesive Law (ECL)

- Cohesive elements inserted on the fly when failure criterion is verified [Ortiz & Pandolfi 1999]
 - Drawback
 - Complex implementation in 3D (parallelization)

- Solution

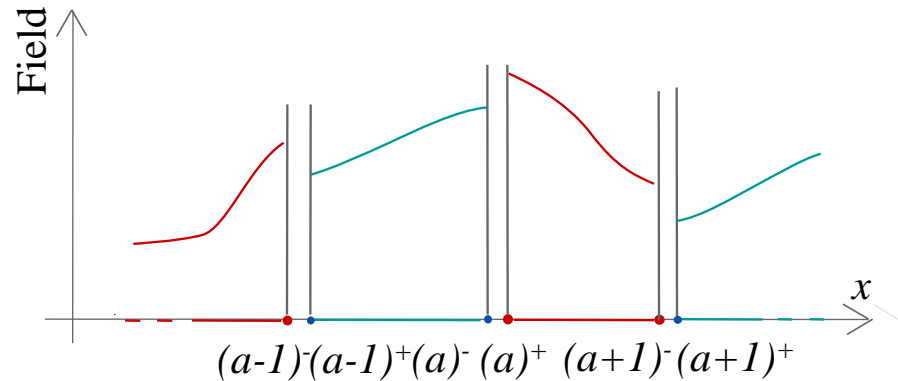
- Use discontinuous Galerkin methods embedding interface elements



- Discontinuous Galerkin (DG) methods

- Finite-element discretization
- Same **discontinuous** polynomial approximations for the

- **Test** functions u_h and
- **Trial** functions δu



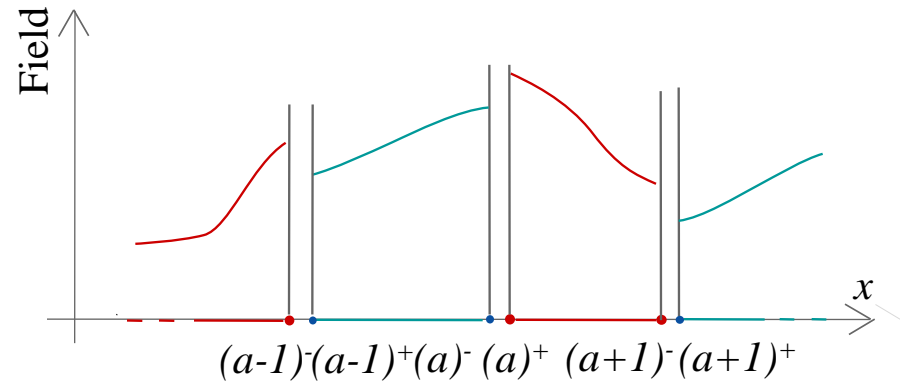
- Definition of operators on the interface trace:

- **Jump operator:** $[[\bullet]] = \bullet^+ - \bullet^-$
- **Mean operator:** $\langle \bullet \rangle = \frac{\bullet^+ + \bullet^-}{2}$

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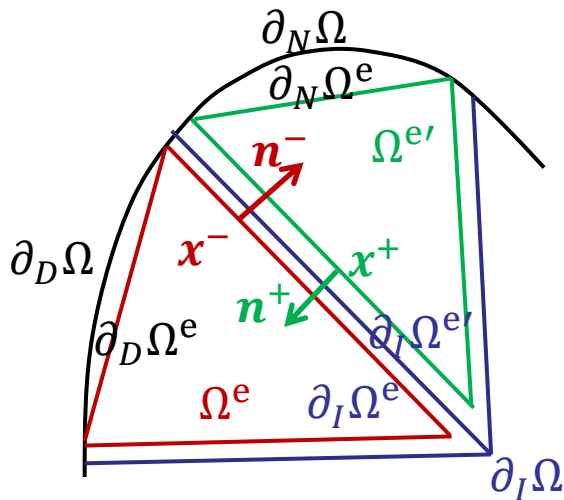
- Continuity is weakly enforced, such that the method

- Is consistent
- Is stable
- Has the optimal convergence rate

- Governing equations

$$\left\{ \begin{array}{l} \nabla \cdot \boldsymbol{\sigma}^T = \mathbf{0} \\ \tilde{e} - \nabla \cdot (\mathbf{c}_g \cdot \nabla \tilde{e}) = e \end{array} \right. \text{ Boundary conditions} \quad \left\{ \begin{array}{l} \boldsymbol{\sigma} \cdot \mathbf{n} = \bar{\mathbf{t}} \\ \mathbf{n} \cdot (\mathbf{c}_g \cdot \nabla \tilde{e}) = 0 \end{array} \right.$$

- Weak formulation obtained by integration by parts **on each element** Ω^e



$$\sum_e \int_{\Omega^e} -\boldsymbol{\sigma}(\mathbf{u}_h) : \nabla \delta \mathbf{u} \, d\Omega + \sum_e \int_{\partial \Omega^e} \delta \mathbf{u} \cdot \boldsymbol{\sigma} \cdot \mathbf{n} \, d\partial \Omega = 0$$

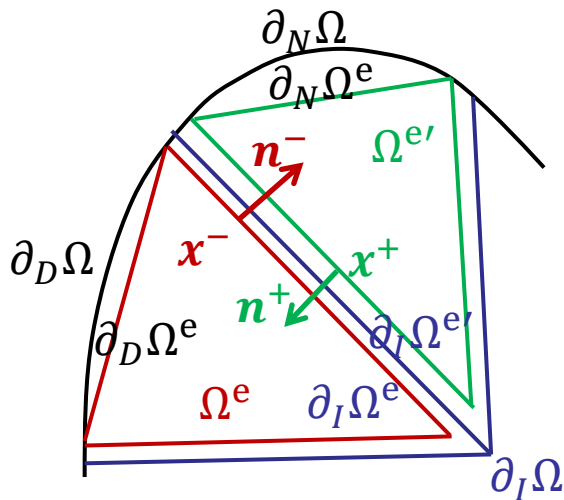
$$\sum_e \int_{\Omega^e} \nabla \cdot \boldsymbol{\sigma}^T(\mathbf{u}_h) \cdot \delta \mathbf{u} \, d\Omega = 0$$

Discontinuous Galerkin / Cohesive Extrinsic Law Framework

- Governing equations

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$$\sum_e \int_{\Omega^e} -\boldsymbol{\sigma}(\mathbf{u}_h) : \nabla \delta \mathbf{u} \, d\Omega + \sum_e \int_{\partial \Omega^e} \delta \mathbf{u} \cdot \boldsymbol{\sigma} \cdot \mathbf{n} \, d\partial \Omega = 0$$

$$\int_{\Omega} \boldsymbol{\sigma}(\mathbf{u}_h) : \nabla \delta \mathbf{u} \, d\Omega + \int_{\partial_I \Omega} [[\delta \mathbf{u} \cdot \boldsymbol{\sigma}]] \cdot \mathbf{n}^- \, d\partial \Omega = \int_{\partial_N \Omega} \bar{\mathbf{t}} \cdot \delta \mathbf{u} \, d\partial \Omega$$

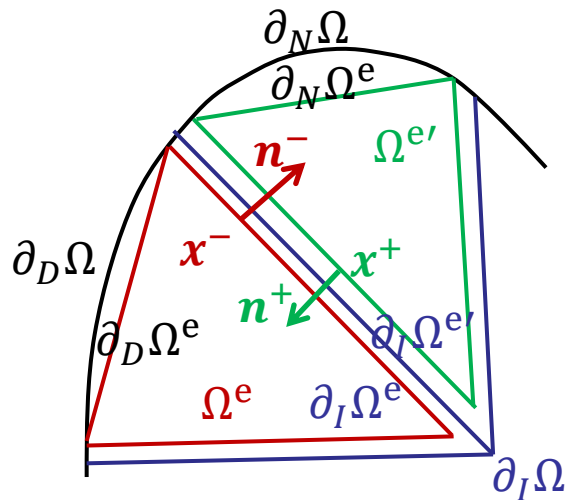
New interface termes

Discontinuous Galerkin / Cohesive Extrinsic Law Framework

- Governing equations

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- Weak formulation obtained by integration by parts **on each element** Ω^e



$$\sum_e \int_{\Omega^e} \nabla \cdot \boldsymbol{\sigma}^T(\mathbf{u}_h) \cdot \delta \mathbf{u} \, d\Omega = 0$$

$$\sum_e \int_{\Omega^e} -\boldsymbol{\sigma}(\mathbf{u}_h) : \nabla \delta \mathbf{u} \, d\Omega + \sum_e \int_{\partial \Omega^e} \delta \mathbf{u} \cdot \boldsymbol{\sigma} \cdot \mathbf{n} \, d\partial \Omega = 0$$

$$\int_{\Omega} \boldsymbol{\sigma}(\mathbf{u}_h) : \nabla \delta \mathbf{u} \, d\Omega + \int_{\partial_I \Omega} [[\delta \mathbf{u} \cdot \boldsymbol{\sigma}]] \cdot \mathbf{n}^- \, d\partial \Omega = \int_{\partial_N \Omega} \bar{\mathbf{t}} \cdot \delta \mathbf{u} \, d\partial \Omega$$

New interface terms

$$\int_{\Omega} \boldsymbol{\sigma}(\mathbf{u}_h) : \nabla \delta \mathbf{u} \, d\Omega + \int_{\partial_I \Omega} [[\delta \mathbf{u}]] \cdot \langle \boldsymbol{\sigma} \rangle \cdot \mathbf{n}^- \, d\partial \Omega +$$

$$+ \int_{\partial_I \Omega} [[\delta \mathbf{u}]] \otimes \mathbf{n}^- : \langle \frac{\beta_s}{h_s} \mathbf{C}^e \rangle : [[\mathbf{u}]] \otimes \mathbf{n}^- \, d\partial \Omega + \int_{\partial_I \Omega} [[\mathbf{u}]] \cdot \langle \mathbf{C}^e : \nabla \delta \mathbf{u} \rangle \cdot \mathbf{n}^- \, d\partial \Omega = \int_{\partial_N \Omega} \bar{\mathbf{t}} \cdot \mathbf{n} \, d\partial \Omega$$

Stabilization

Enforcement of the compatibility

- Combining with cohesive law

$$\begin{aligned}
 & \int_{\Omega} \boldsymbol{\sigma}(\mathbf{u}_h) : \nabla \delta \mathbf{u} \, d\Omega + \int_{\partial_I \Omega} \alpha \bar{\mathbf{t}}^-([\mathbf{u}]) \cdot [\delta \mathbf{u}] \, d\partial\Omega \\
 + & \int_{\partial_I \Omega} (1 - \alpha) [\delta \mathbf{u}] \cdot \langle \boldsymbol{\sigma} \rangle \cdot \mathbf{n}^- \, d\partial\Omega + \int_{\partial_I \Omega} (1 - \alpha) [\delta \mathbf{u}] \otimes \mathbf{n}^- : \langle \frac{\beta_s}{h_s} \mathbf{C}^e \rangle : [\mathbf{u}] \otimes \mathbf{n}^- \, d\partial\Omega \\
 & + \int_{\partial_I \Omega} (1 - \alpha) [\mathbf{u}] \cdot \langle \mathbf{C}^e : \nabla \delta \mathbf{u} \rangle \cdot \mathbf{n}^- \, d\partial\Omega = \int_{\partial_N \Omega} \bar{\mathbf{t}} \cdot \mathbf{n} \, d\partial\Omega
 \end{aligned}$$

- Transition from damage to crack
 - Critical damage D_T

- Combining with cohesive law

$$\begin{aligned}
 & \int_{\Omega} \boldsymbol{\sigma}(\mathbf{u}_h) : \nabla \delta \mathbf{u} \, d\Omega + \int_{\partial_I \Omega} \alpha \bar{\mathbf{t}}^- ([[\mathbf{u}]]) \cdot [[\delta \mathbf{u}]] \, d\partial\Omega \\
 + & \int_{\partial_I \Omega} (1 - \alpha) [[\delta \mathbf{u}]] \cdot \langle \boldsymbol{\sigma} \rangle \cdot \mathbf{n}^- \, d\partial\Omega + \int_{\partial_I \Omega} (1 - \alpha) [[\delta \mathbf{u}]] \otimes \mathbf{n}^- : \langle \frac{\beta_s}{h_s} \mathbf{C}^e \rangle : [[\mathbf{u}]] \otimes \mathbf{n}^- \, d\partial\Omega \\
 & + \int_{\partial_I \Omega} (1 - \alpha) [[\mathbf{u}]] \cdot \langle \mathbf{C}^e : \nabla \delta \mathbf{u} \rangle \cdot \mathbf{n}^- \, d\partial\Omega = \int_{\partial_N \Omega} \bar{\mathbf{t}} \cdot \mathbf{n} \, d\partial\Omega
 \end{aligned}$$

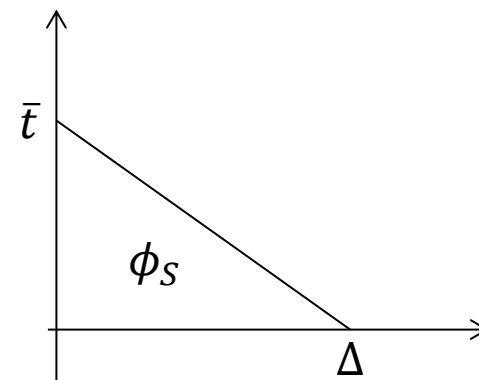
- Transition from damage to crack

- Critical damage D_T
- Effective stress

$$\sigma_c = \frac{\sigma}{(1 - D_T)}$$

- TSL Characterized by

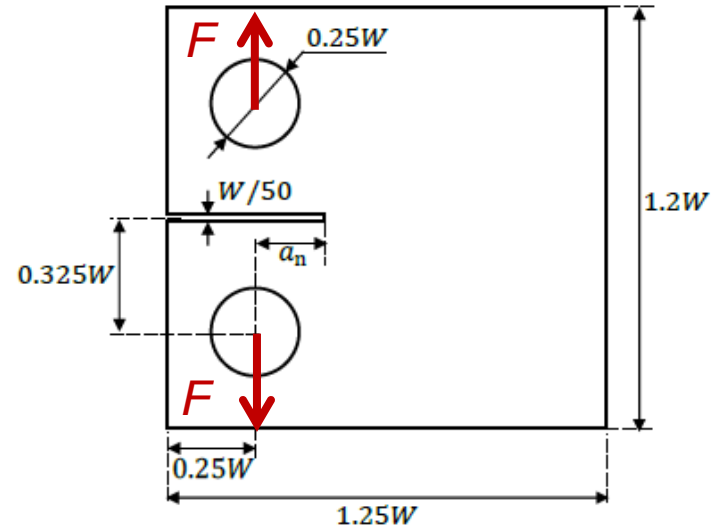
- Strength σ_c &
- Critical energy release rate ϕ_S



- Compact tension specimen [Geers et al. 1999, ...]

$W=50$ mm
 $a_n=10$ mm
Thickness: 3.8 mm

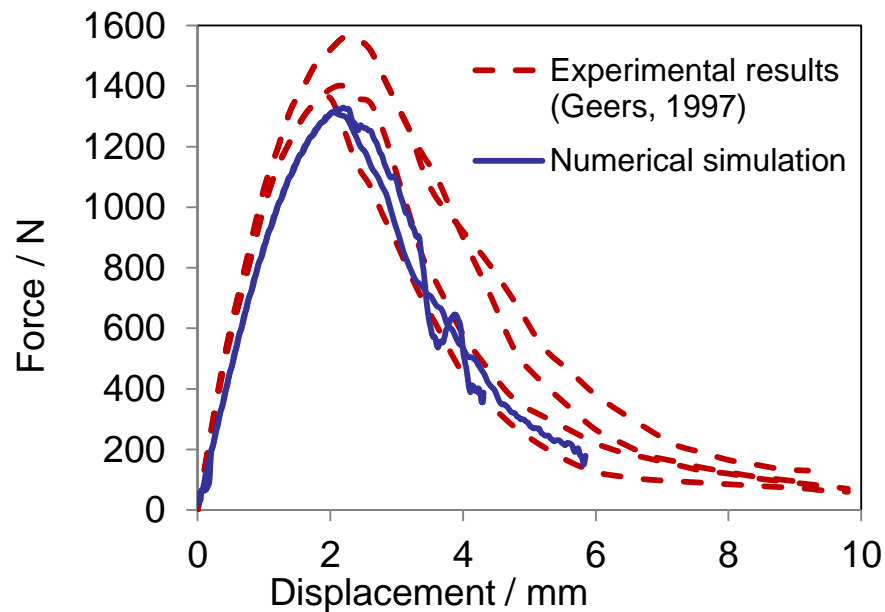
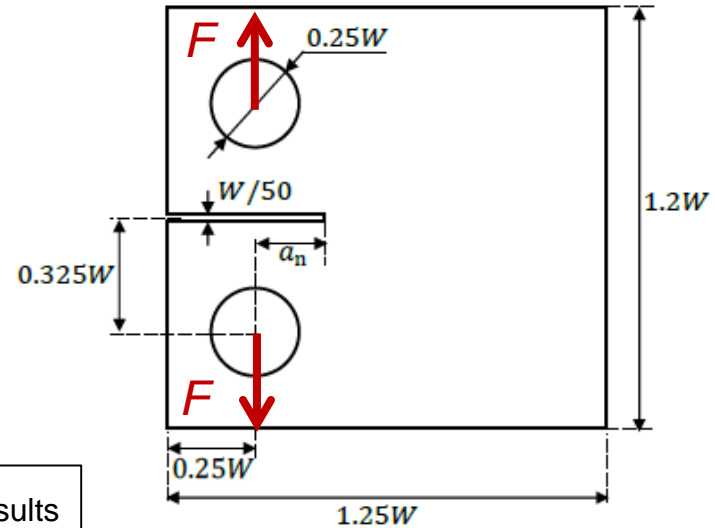
- 3D model
- Results



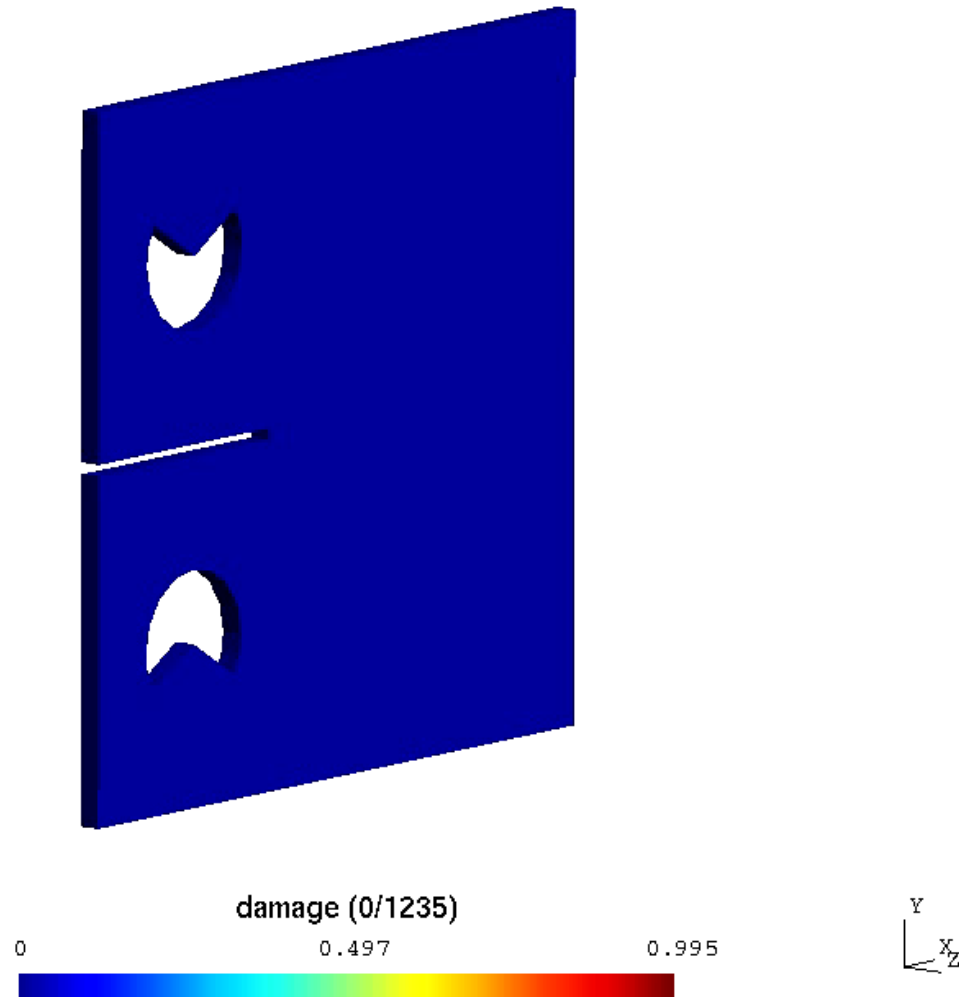
- Compact tension specimen [Geers et al. 1999, ...]

$W=50$ mm
 $a_n=10$ mm
Thickness: 3.8 mm

- 3D model
- Results



- Compact tension specimen
 - Results



- **Implicit gradient enhanced damage**
 - Easy implementation
 - Extra degree of freedom on nodes
- **Damage to crack**
 - Cohesive law needs to be constructed
 - High damage (approximation)
 - Low damage (numerical solution)
 - Transition criterion from the information of damage and stress
- **DG method**
 - Computationally efficient // method
 - Consistent
 - Extrinsic cohesive law