

MECHANICS AND CHARACTERISTICS OF TRANSITION TO TURBULENCE IN ELASTO-INERTIAL TURBULENCE

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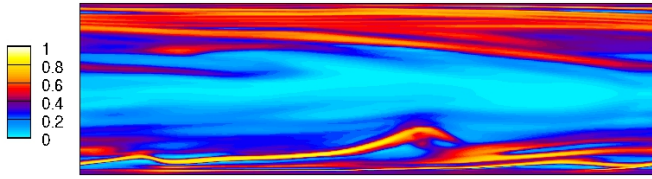
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Context and objectives

Polymer extension



$$\partial_t \mathbf{C} + (\mathbf{u} \cdot \nabla) \mathbf{C}$$

- Formation of sheets

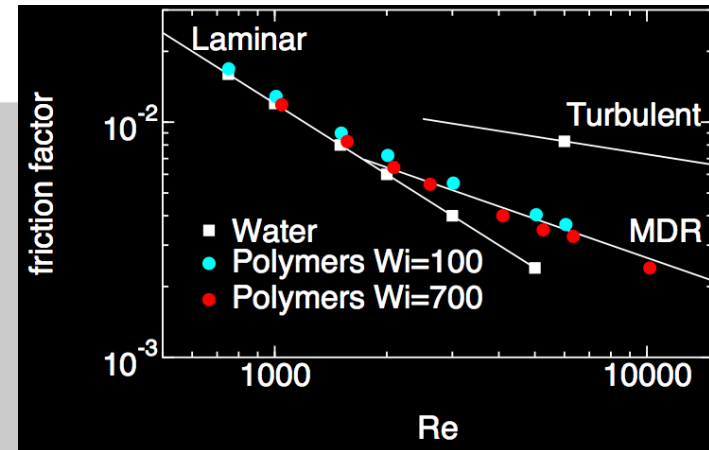
$$\nabla^2 p = 2Q_a - \frac{1-\beta}{Re} \nabla \cdot (\nabla \cdot \mathbf{T})$$

- Excitation of extensional sheet flow
- Elliptical pressure redistribution of energy

$$\mathbf{C}(\nabla \mathbf{u}) + (\nabla \mathbf{u})^T \mathbf{C} - \mathbf{T}$$

- Increase of extensional viscosity

Channel flow



Context and objectives

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- **Excitation of extensional sheet flow**
- Elliptical pressure redistribution of energy

- How do long-range interactions through pressure contribute to transition?
- What locations in the flow contribute most to instability excitation?
- What is the relative contribution of both terms in the Poisson equation?

Navier-Stokes for dilute polymer solutions

$$\partial_t \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\nabla p + \frac{\beta}{Re} \nabla^2 \mathbf{u} + \frac{1 - \beta}{Re} \nabla \cdot \mathbf{T}$$

Polymer stress – FENE-P model

$$\mathbf{T} = \frac{1}{Wi} \left(\frac{\mathbf{C}}{1 - \text{tr}(\mathbf{C})/L^2} - \mathbf{I} \right)$$

Polymer conformation tensor

$$\partial_t \mathbf{C} + (\mathbf{u} \cdot \nabla) \mathbf{C} = \mathbf{C}(\nabla \mathbf{u}) + (\nabla \mathbf{u})^T \mathbf{C} - \mathbf{T}$$

Equations

Navier-Stokes for dilute polymer solutions

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Polymer stress – FENE-P model

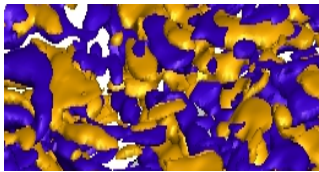
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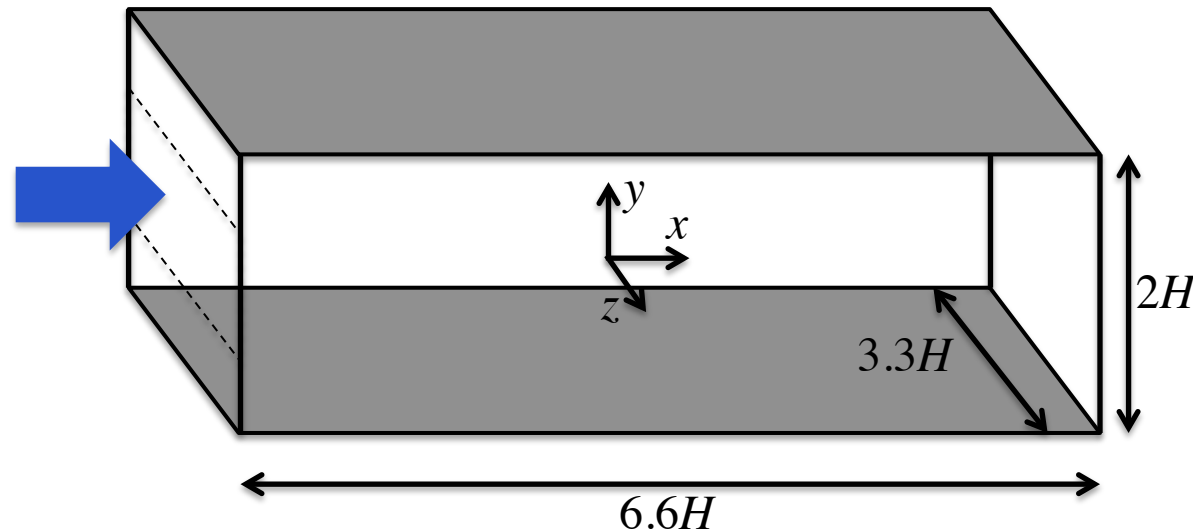
$$\partial_t \mathbf{C} + (\mathbf{u} \cdot \nabla) \mathbf{C} = \mathbf{C}(\nabla \mathbf{u}) + (\nabla \mathbf{u})^T \mathbf{C} - \mathbf{T}$$

Simulated by-pass transition

HIT



Periodic channel flow

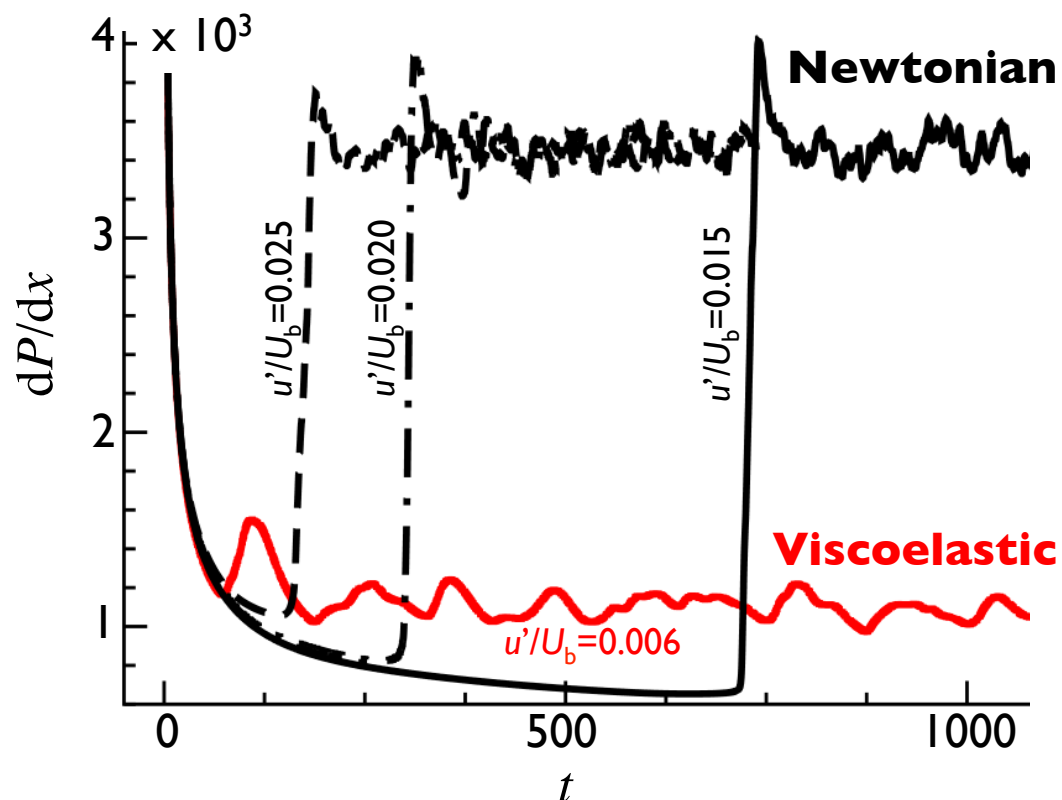


Parameters

- $Wi = 400$
- $L = 200$
- $Re = U_b H / \nu = 1000$
- $\beta = 0.9$

1. Plug flow with slip
2. Injection of homogeneous isotropic turbulence in channel center
3. No-slip at the wall

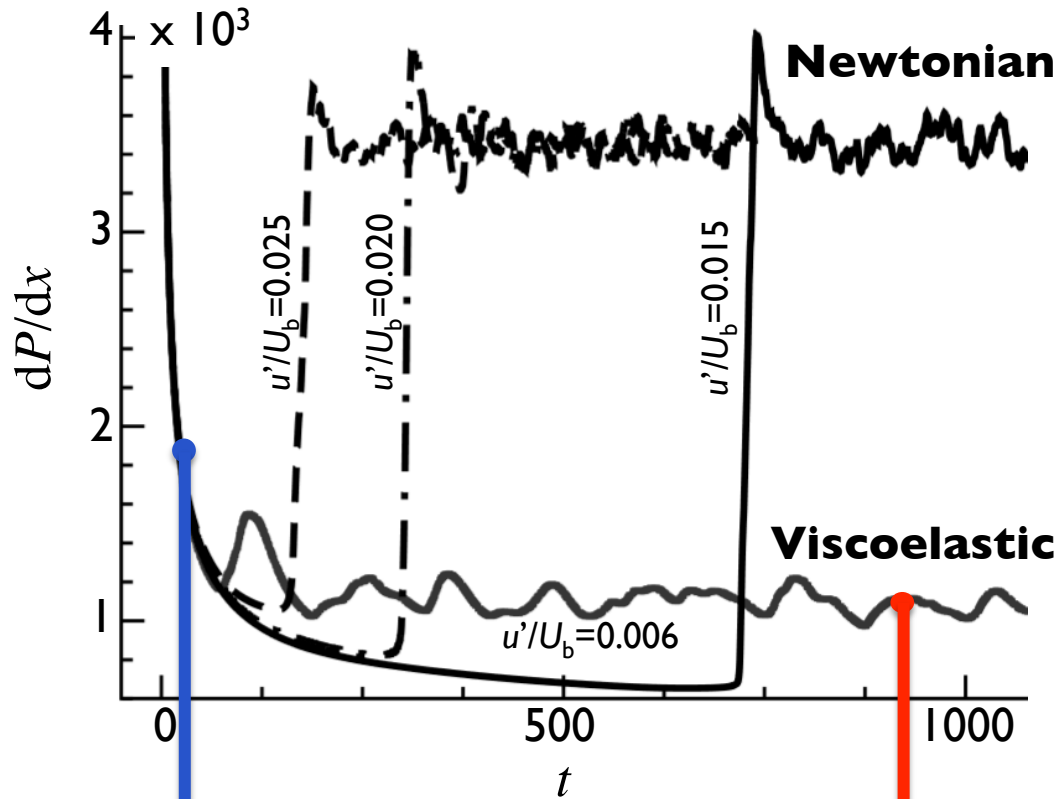
Evolution of wall friction



- Viscoelastic flow transitions with **weaker** perturbations
- Same perturbation level would lead to **laminar** Newtonian flow
- Viscoelastic flow transitions to **MDR** and stays at MDR

2 states of the evolution considered

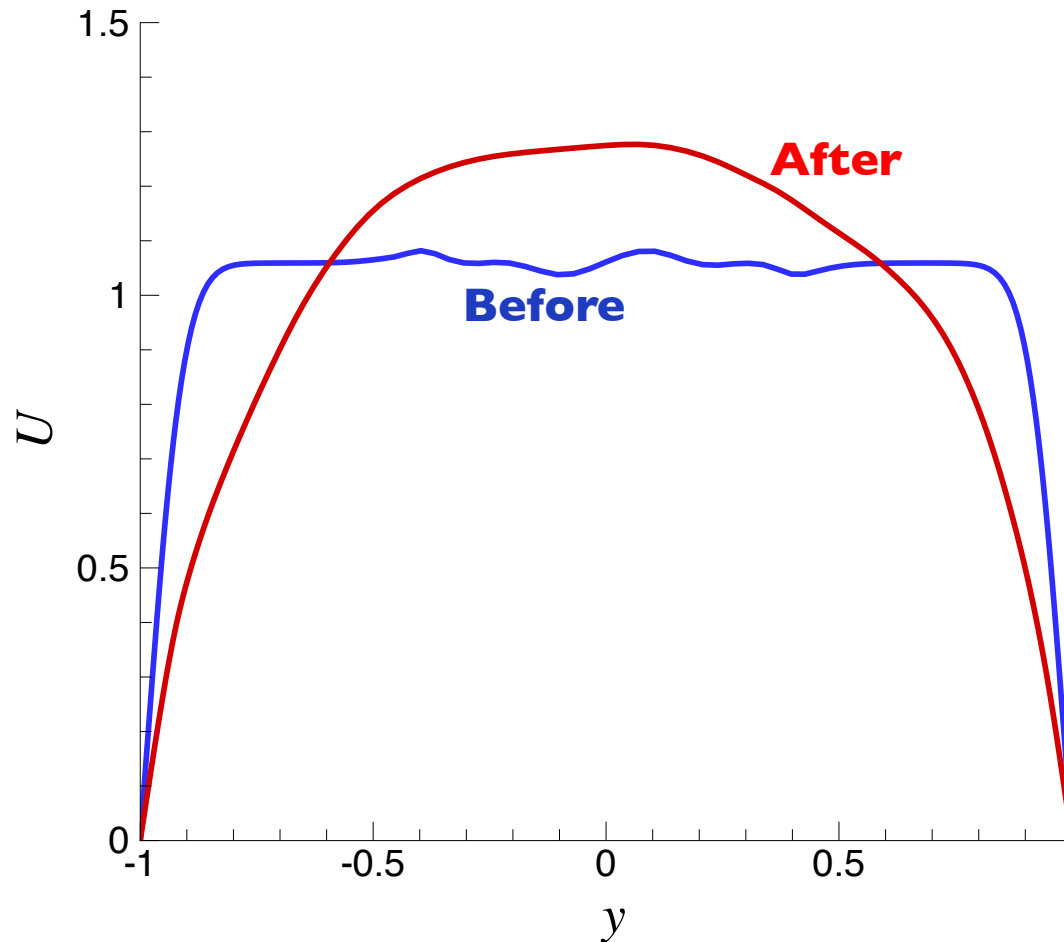
Evolution of wall friction



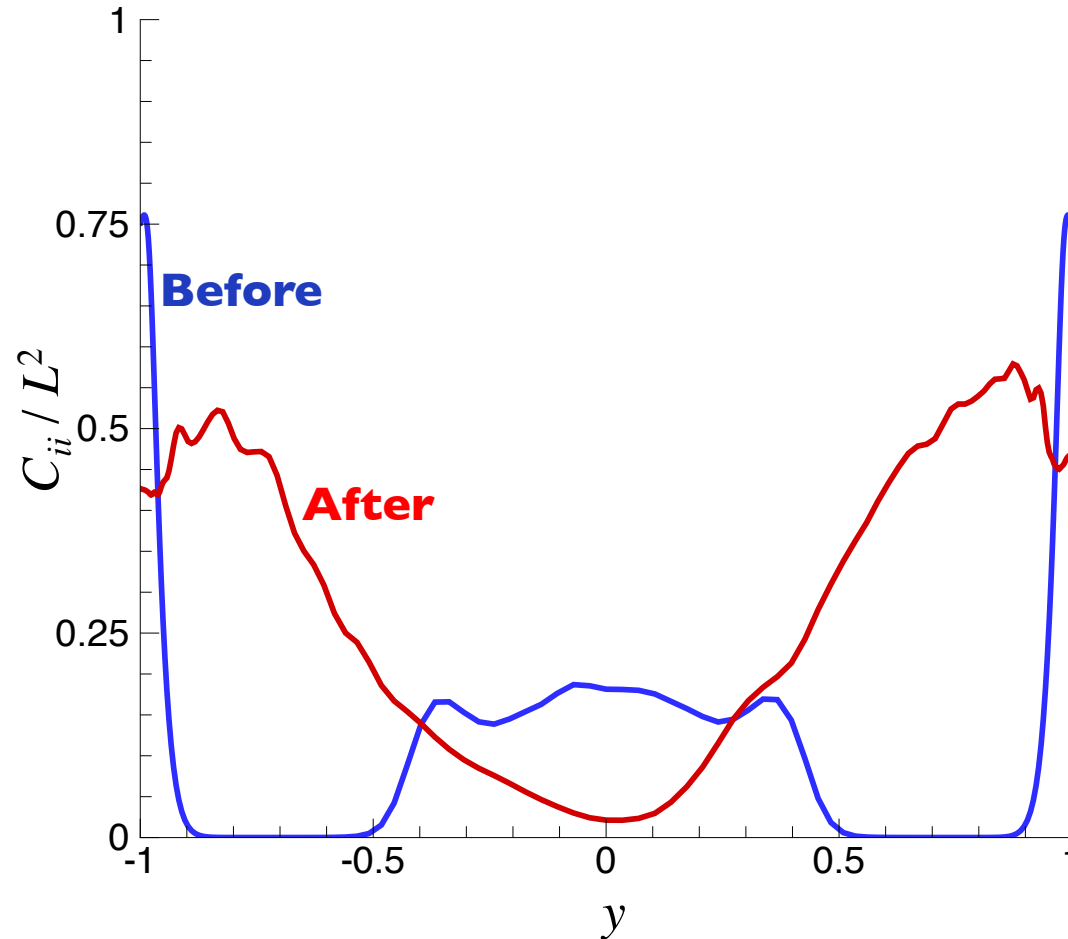
Before nonlinear
breakdown of instabilities

After nonlinear
breakdown of instabilities

Mean velocity profile

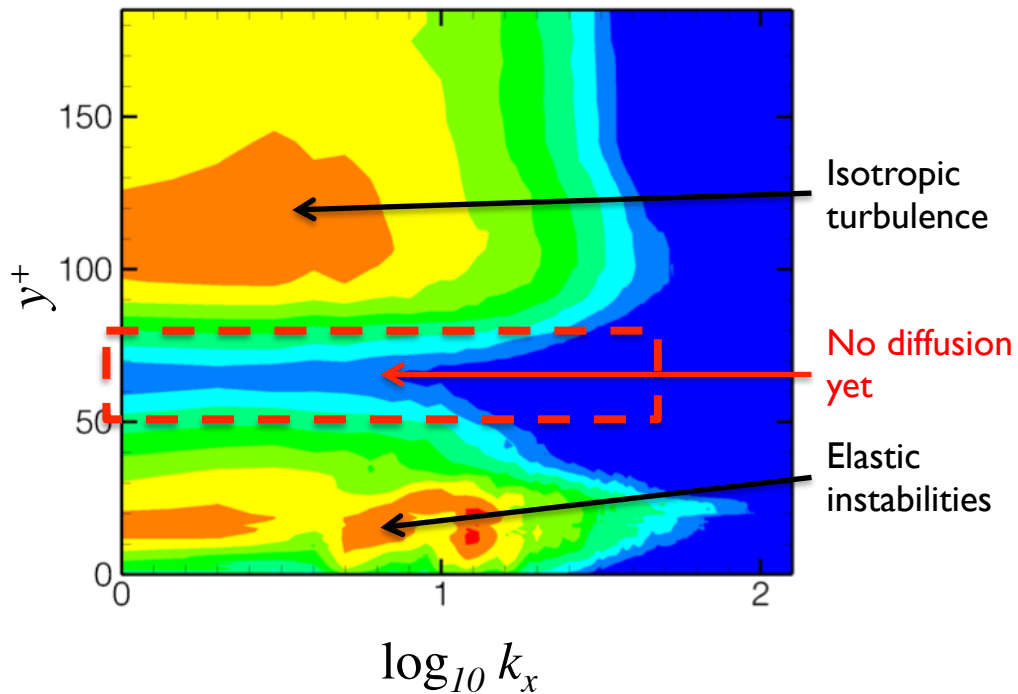


Mean polymer extension



Excitation of instabilities

Power spectrum of the elastic energy before nonlinear breakdown of instabilities



- Instabilities in near-wall regions not caused by diffusion of turbulence from channel center
- What triggers the instability?

Poisson equation for pressure

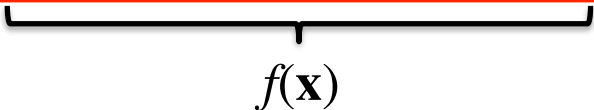
Extended Poisson equation

$$\nabla^2 p = \underbrace{2Q_a + \frac{1 - \beta}{Re} \nabla \cdot (\nabla \cdot \mathbf{T})}_{f(\mathbf{x})}$$

Poisson equation for pressure

Extended Poisson equation

$$\nabla^2 p = 2Q_a + \frac{1-\beta}{Re} \nabla \cdot (\nabla \cdot \mathbf{T})$$



 $f(\mathbf{x})$



Pressure kernel – Green function G

$$p(\boldsymbol{\xi}) = \int_V G(\boldsymbol{\xi}, \mathbf{x}) f(\mathbf{x}) d\mathbf{x} \equiv \int_V F(\boldsymbol{\xi}, \mathbf{x}) d\mathbf{x}$$

“Influence” function $F(\mathbf{x}, \boldsymbol{\xi})$ represents the contribution of point \mathbf{x} to the pressure at point $\boldsymbol{\xi}$

Poisson equation for pressure

Extended Poisson equation

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$\underbrace{\hspace{10em}}_{f(\mathbf{x})}$

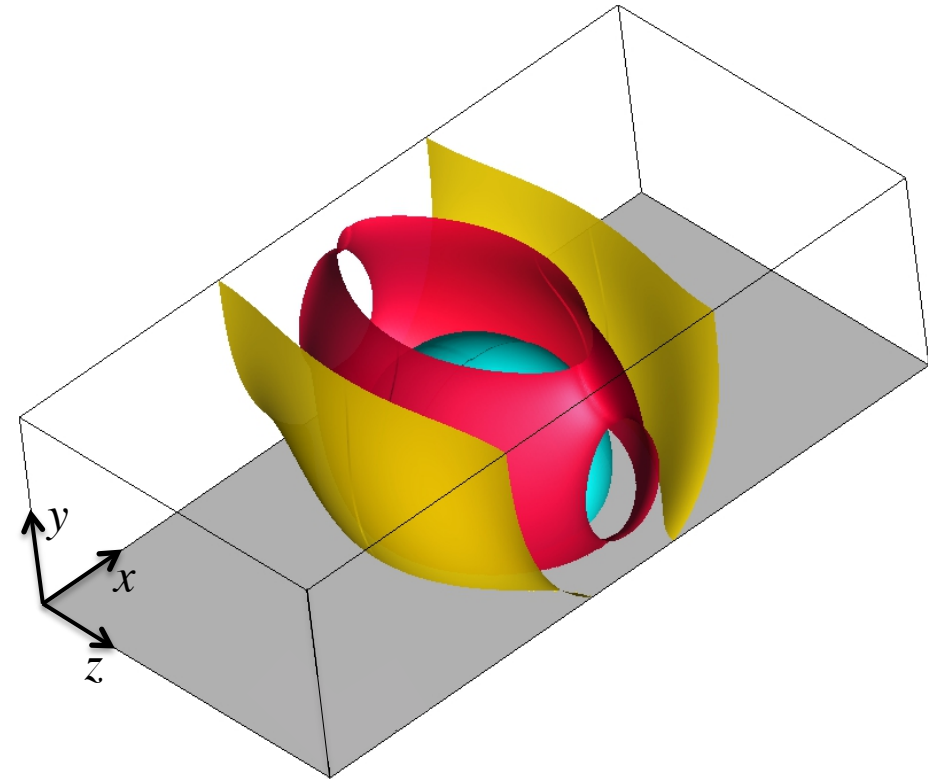


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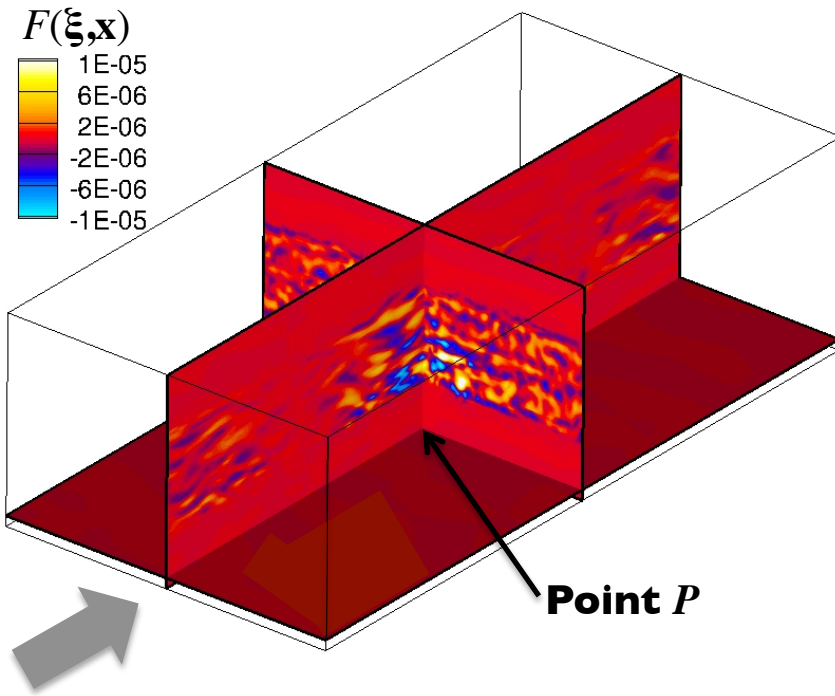
“Influence” function $F(\mathbf{x}, \xi)$ represents the contribution of point \mathbf{x} to the pressure at point ξ

Green function $G(0, -0.9H, 0; x, y, z)$



Influence function

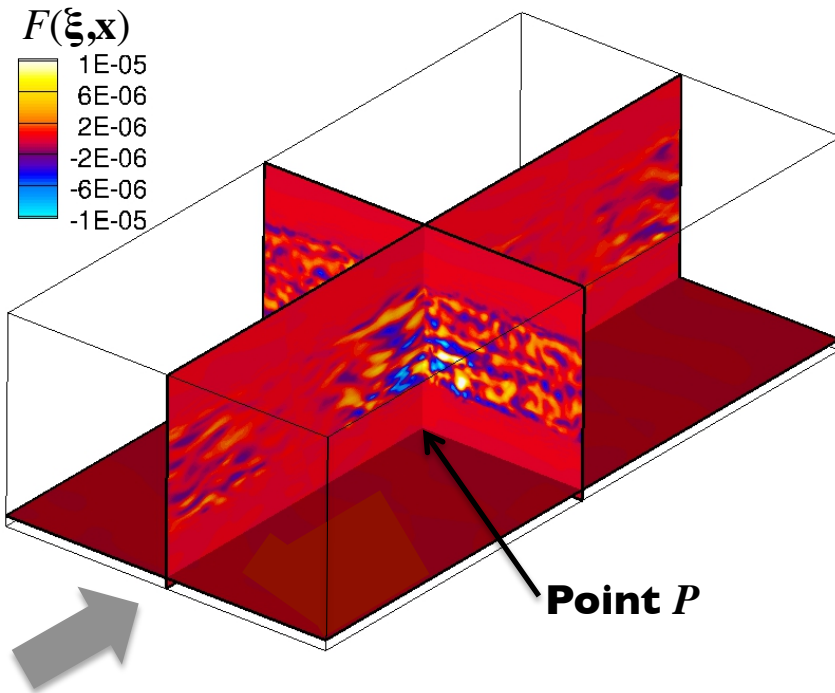
Before nonlinear breakdown of instabilities



Source of contribution to pressure at point P from relative “unorganized” free-stream turbulence in channel center

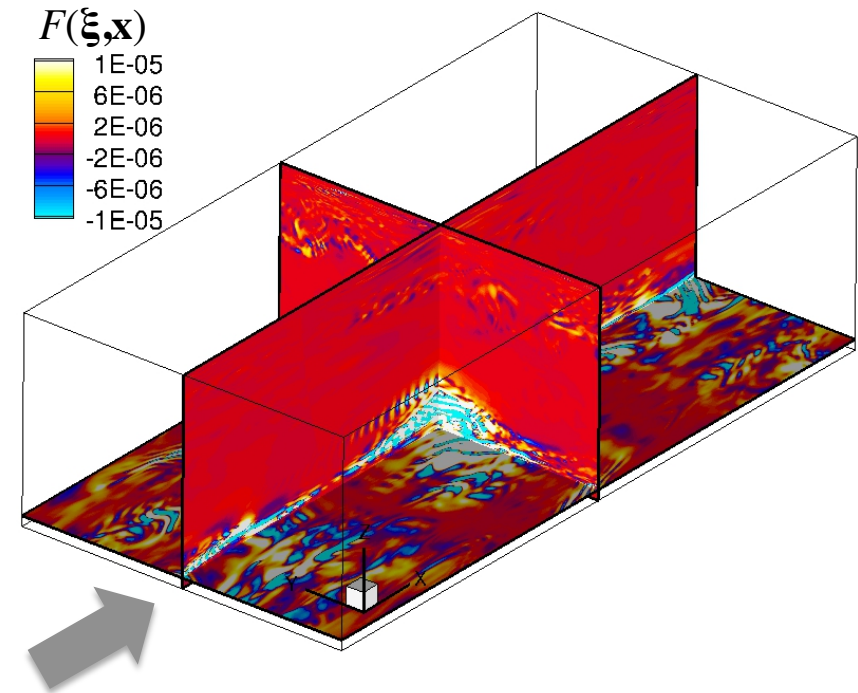
Influence function

Before nonlinear breakdown of instabilities



Source of contribution to pressure at point P from relative “unorganized” free-stream turbulence in channel center

After nonlinear breakdown of instabilities



Source of contribution to pressure at point P from elastically induced more “organized” structures in near-wall region

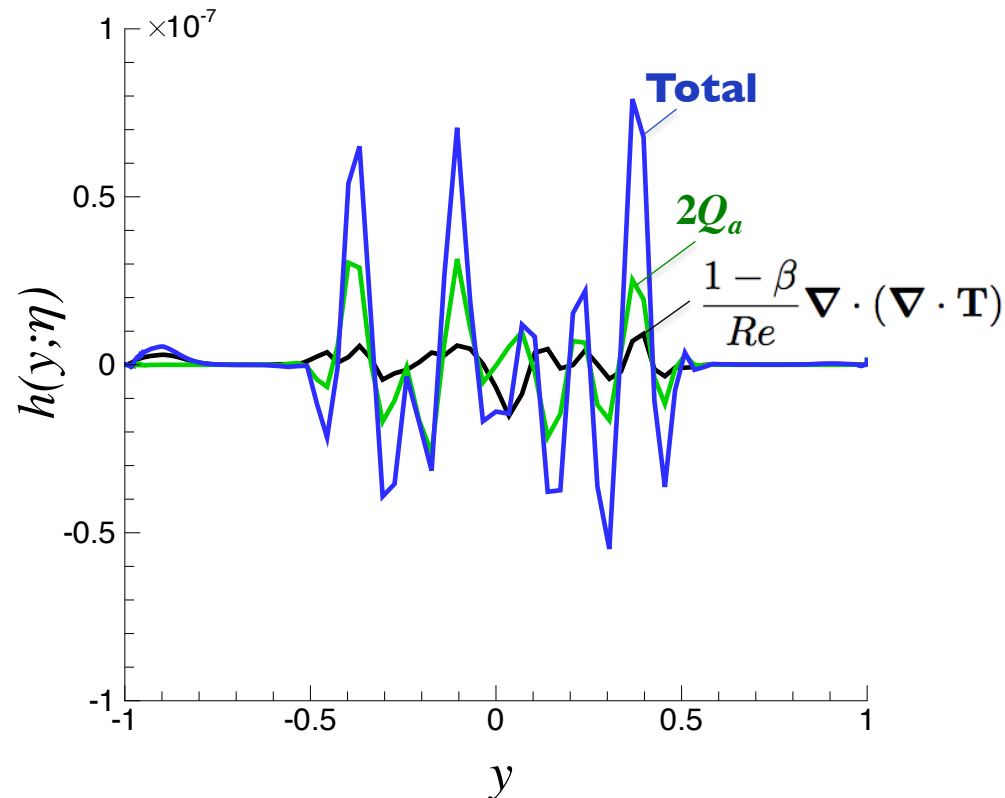
Plane-averaged pressure fluctuations

$$\nabla^2 p = 2Q_a - \frac{1-\beta}{Re} \nabla \cdot (\nabla \cdot \mathbf{T}) \quad \rightarrow \quad p(\boldsymbol{\xi}) = \int_V G(\boldsymbol{\xi}, \mathbf{x}) f(\mathbf{x}) d\mathbf{x} \quad \rightarrow \quad \overline{p^2}(\eta) = \int_{-H}^H h(y; \eta) dy$$

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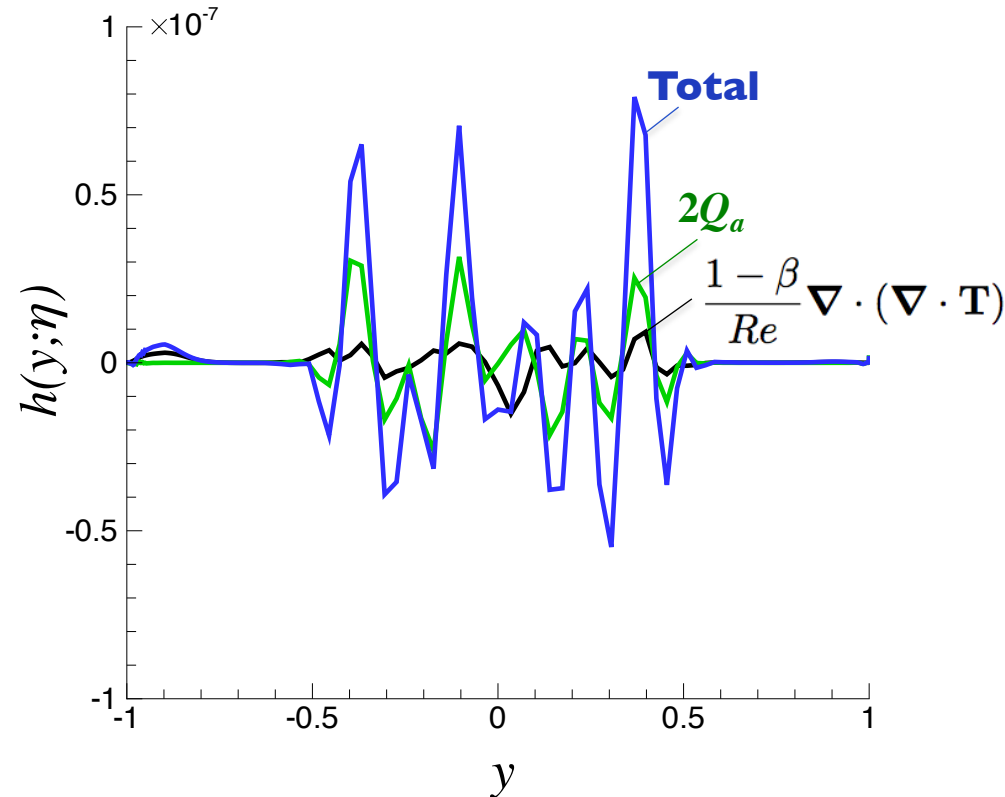
Before nonlinear breakdown



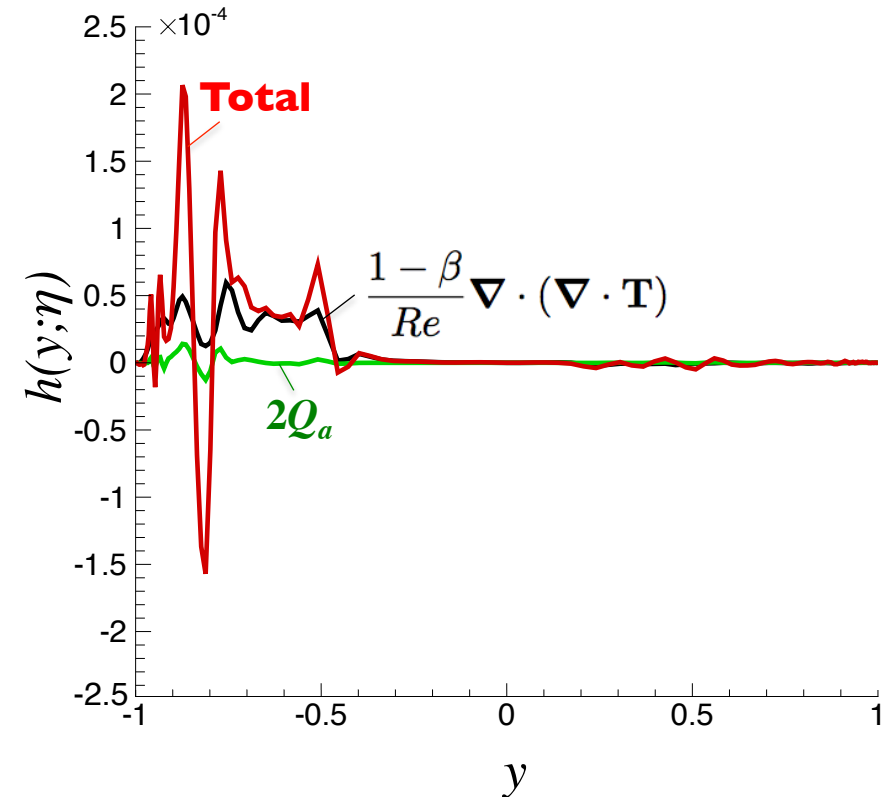
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Before nonlinear breakdown



After nonlinear breakdown



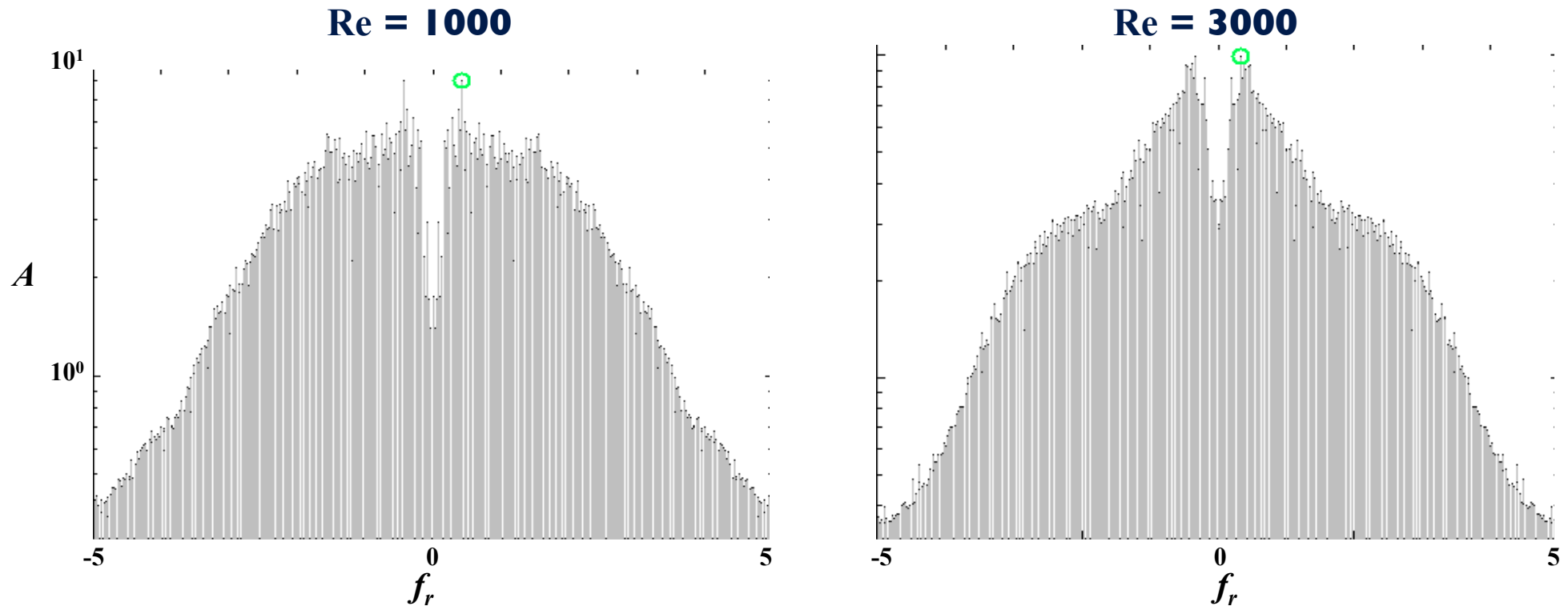
Current understanding of viscoelastic transition

- Long-range excitation of elastic instabilities through pressure
- Feeding of energy to elastic instabilities from mean flow
- Elastic instabilities then self-sustained
- Polymeric contribution in Poisson equation dominates kinematic contribution

Future work – DMD analysis

Mode amplitude as a function of frequency from DMD analysis

Q invariant (streamwise – wall-normal plane)

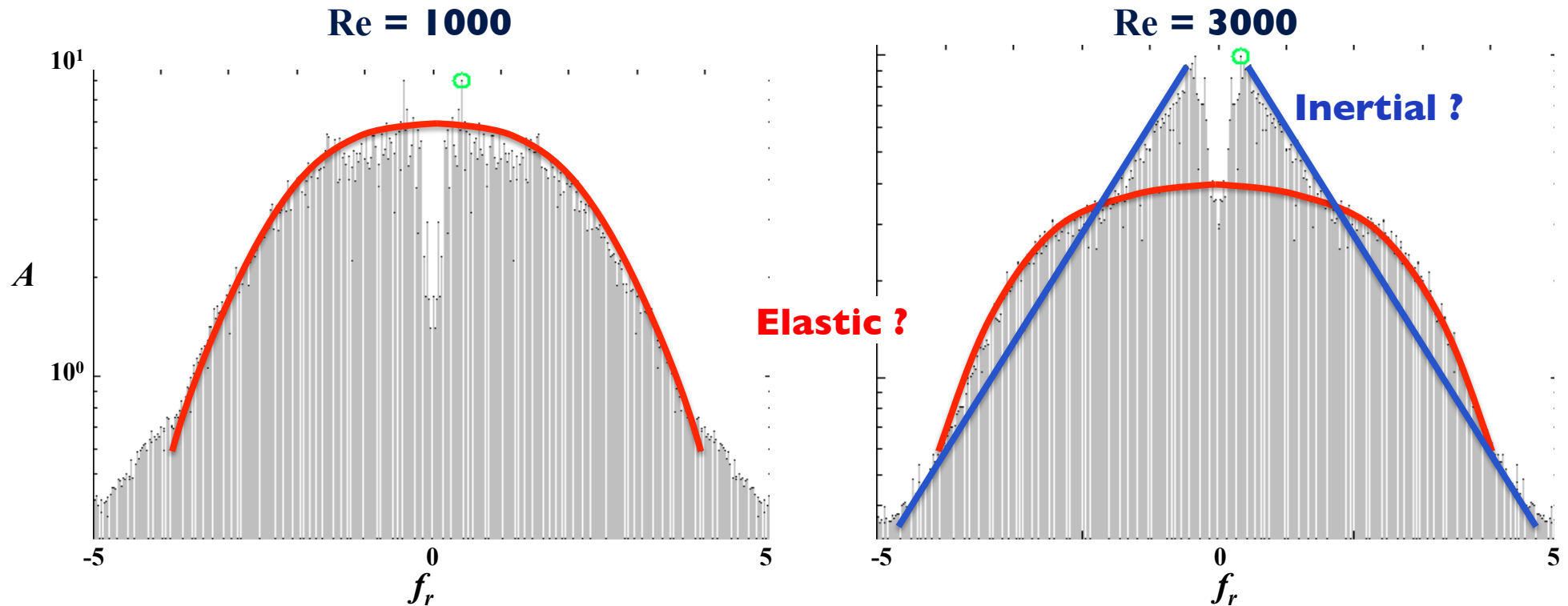


- Shape change with increasing Re
- At larger Re, two apparent contributions
- Hypothesis: elastic and inertial (to be verified)

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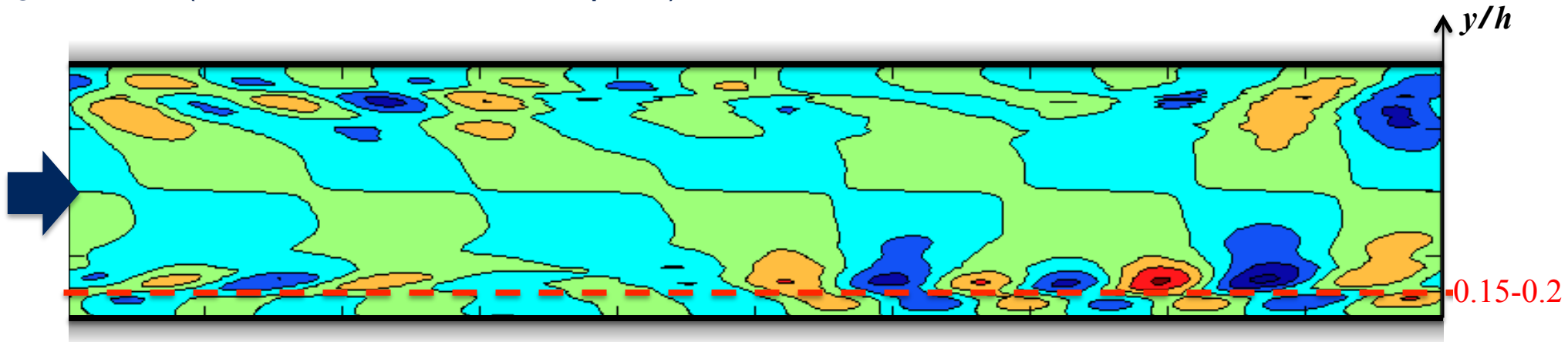


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Future work – DMD analysis

Most amplified mode from DMD analysis

Q invariant (streamwise – wall-normal plane) at $Re=1000$

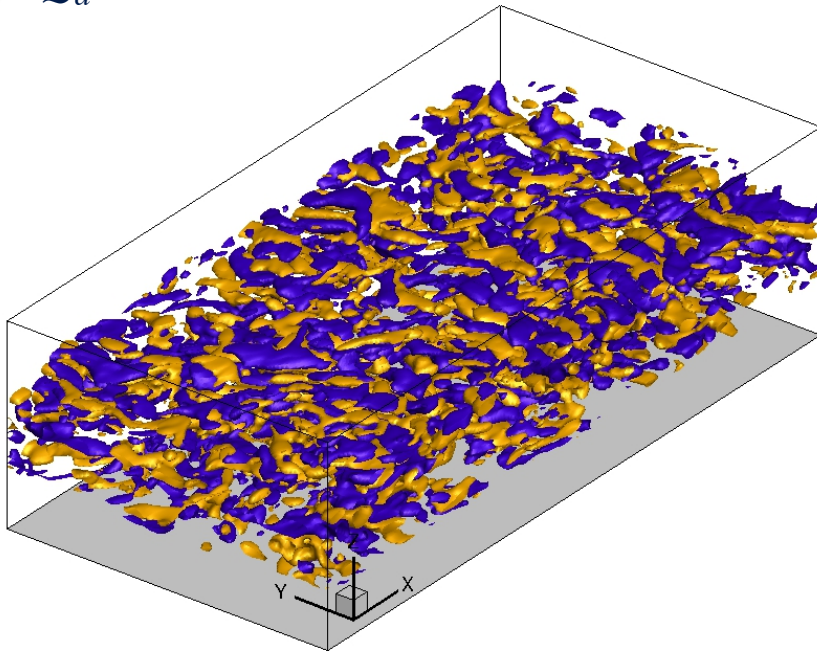


- Mostly two-dimensional structures
- Located in near-wall region
- Alternating pressure minima and maxima
- “Discontinuity” close to wall corresponding to location of extremum of mean polymer extension (critical layer?)

Vortices and extensional flow

Before nonlinear breakdown of instabilities

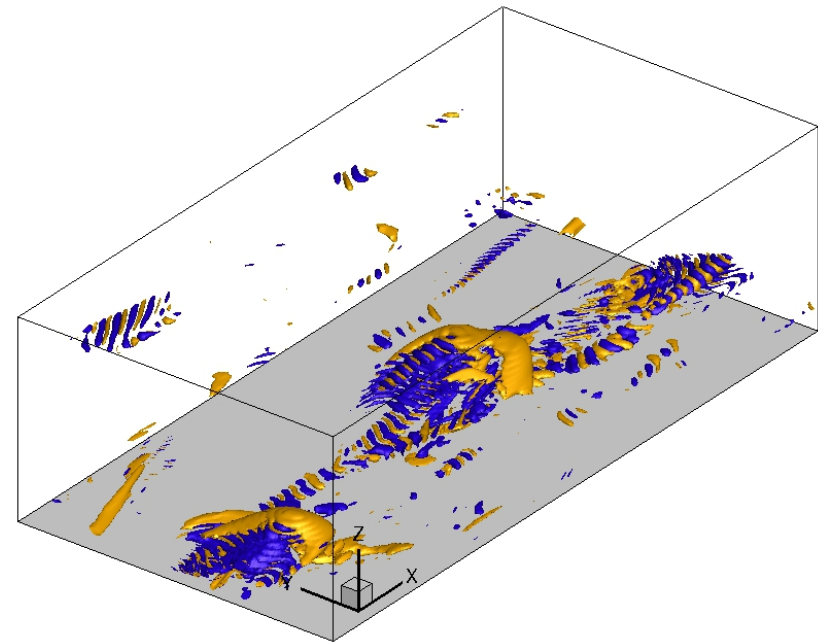
■ $Q_a = 0.02$
■ $Q_a = -0.02$



Weak homogeneous isotropic turbulence

After nonlinear breakdown of instabilities

■ $Q_a = 0.2$
■ $Q_a = -0.2$



Few hairpin-like vortices followed by train of alternating “rotational” and “straining” flow at very small scales