

# Modal identification of time-varying systems using simulated responses on wind turbines

Mathieu BERTHA

Jorge Patricio MAYORGA RIOS

Jean-Claude GOLINVAL

University of Liège

18 September, 2012

# Outline of the presentation

Description of the problem

Numerical model for simulations

Choice of an identification method

Encountered difficulties

Numerical results

# Problem statement

The considered wind turbine (NREL technical report, 2009)



Rating : 5 MW

Rotor diameter : 126 m

Hub height : 90 m

Wind speeds :

▶ Cut-in : 3 m/s

▶ Rated : 11.4 m/s

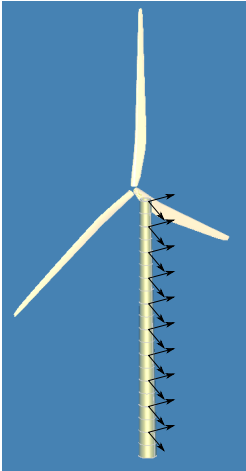
▶ Cut-out : 25 m/s

Rotor speeds :

▶ Cut-in : 6.9 r.p.m.

▶ Rated : 12.1 r.p.m.

# A numerical model is built to simulate structural response



**Beam** elements model the tower and blades

**Aero** elements compute aerodynamic loads on the blades

**Lumped masses** simulate the nacelle and the bedplate

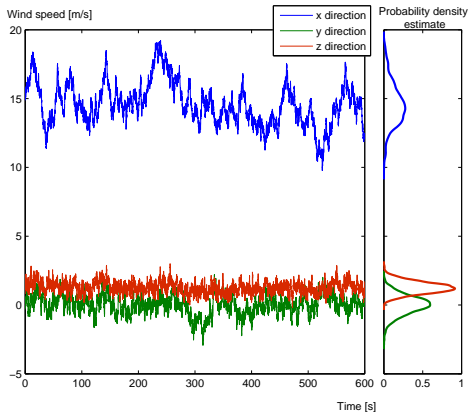
**Hinges** are used in the rotor and yaw mechanism

10 measurement points are considered along the tower

# The wind is simulated with the *TurbSim* simulator coupled with *S4WT*

The wind is generated based on the *Kaimal* model

A set of load cases is generated considering different mean wind speeds



# Operational analysis requires output-only identification method

Some techniques are suitable for output-only modal analysis :

- ▶ *(E)FDD*
- ▶ *p-LSCF (PolyMAX)*
- ▶ ***SSI***

# The working assumptions of the *SSI* methods are not completely fulfilled

Assumptions of :

- ▶ Linear time-invariant system
- ▶ Whiteness of the Gaussian process noise

Because of the dynamic properties of the system and the deviation from working assumptions, some difficulties appear

# The dynamic properties of the structure



The very low frequencies of the system require long time responses

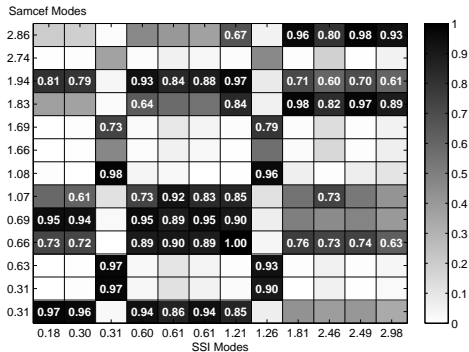
Due to high symmetry, the eigen modes are close in frequency



# The limited number of sensors causes high spatial aliasing

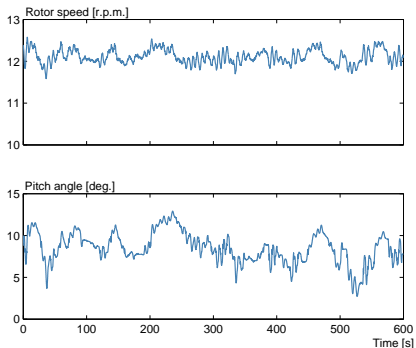
Tower bending modes are well identified

Blade modes are seen as tower bending modes



The method becomes sensible to the input parameters due to non constant operational conditions

The rotor speed and pitch angle slightly vary even under stationary winds



# One can use some tools to try to overcome these difficulties

Stabilisation with an automated clustering approach (Reynders et al., 2012)

Several simulations for different input parameters

Projection channels used as references (Jacobsen al., 2008)

# The automated stabilisation diagram does not require thresholds any more

The method in three steps :

- ▶ Separation between *possibly physical* and *certainly spurious* modes
- ▶ Grouping of similar modes
- ▶ Selection of a representative mode

# The number of criteria to distinguish modes is more substantial

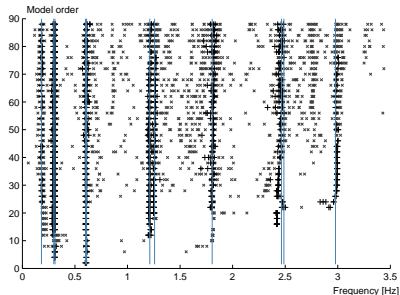
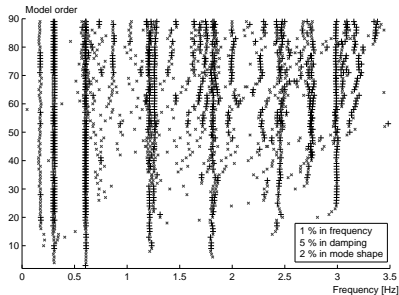
## Classical stabilisation :

- ▶ Frequency deflection
- ▶ Damping deflection
- ▶ Mode deflection

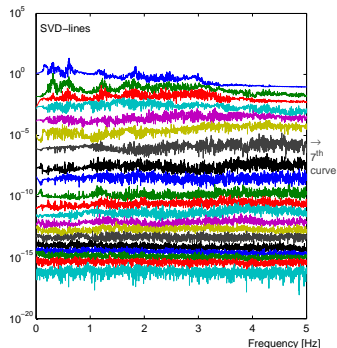
## Automated stabilisation :

- ▶ ...
- ▶ Pole deflection
- ▶ Mode shape complexity

# The automated method adaptively selects the physical modes



# The use of projection channels reduces the CPU time

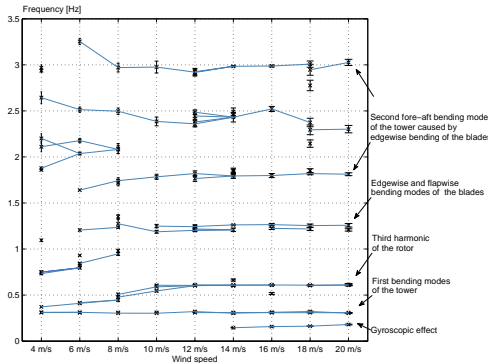


Reduction of the size of correlation  
blocks in the Hankel matrix

- ▶ Choice of the number of projection channels
- ▶ Selection of the first one
- ▶ Selection of the others

# Results

Mean wind speed [m/s]	Mean rotor speed [r.p.m.]
4	7.4336
6	8.2786
8	9.9039
10	11.8921
12	12.1079
14	12.1091
16	12.1161
18	12.1240
20	12.1314





# Conclusions

A series of load cases were generated and applied on a numerical model

Identifications were performed with the *SSI* method

Some difficulties were pointed out in such an application

Some tools were used to try to overcome these difficulties

One can conclude that the traditional *SSI* method is not accurately applicable to such an application

Thank you for your attention