

Assessing the environmental potential of carbon dioxide utilization: A graphical targeting approach

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Abstract

Carbon Capture and Utilization (CCU) has the potential to reduce both greenhouse gas emissions and fossil fuel use. However, the conversion of CO₂ is intrinsically difficult due to its low energetic state. Thus, a positive environmental effect of a CO₂-consuming reaction cannot be taken for granted. In this work, we therefore present a graphical method to identify promising reaction schemes using CO₂ as a feedstock. Reactant mixtures leading to minimal life-cycle greenhouse gas (GHG) emissions are determined. The optimal reaction schemes strongly depend on the reactants' global warming potential (GWP); in the case of CCU, the future GWP values of CO₂ and H₂ are particularly critical and subject to major uncertainty today. The graphical method therefore provides GWP targets for CO₂ capture and H₂ production technologies. The method is demonstrated for the production of methanol. Five optimal reaction schemes are identified depending on the GWP values of CO₂ and H₂. Thus, four threshold relations for the GWP of CO₂ and H₂ are derived showing directly under which conditions the utilization of CO₂ as a feedstock is environmentally preferential.

Keywords: Carbon Capture and Utilization, LCA, Methanol, CO₂ Conversion

1. Introduction

The utilization of captured CO₂ is drawing increasing attention [1]. With progress in capture technologies, high purity CO₂ can become abundantly available, e.g. from fossil fueled power plants. Using CO₂ as a feedstock for the production of chemicals and fuels might allow for a reduction of both greenhouse gas emissions and fossil fuel depletion. However, major challenges have to be overcome to implement CCU on a large scale: new products and pathways have to be identified and the reaction must be exergonic [2]. Systematic methods to identify promising candidate reactions are therefore desirable. Patel et al. [3] recently introduced a thermodynamic process design framework. The framework can directly be employed to identify promising CO₂-based reactions from a thermodynamic perspective. But the utilization of CCU is most often motivated environmentally. Therefore, we extend the framework from Patel et al. [3] by an optimization step based on ecological criteria such as the GWP. This extension enables the identification of the ecologically optimal composition of reactants and products. In a further step, the method can be used to determine GWP targets for CO₂ capture and H₂ production technologies.

In Section 2, the graphical method is introduced for the example of methanol production. In Section 3, results are presented before conclusions are given in Section 4.

2. Graphical Targeting Approach

After a short description of methanol production, the graphical design framework by Patel et al. [3] is briefly summarized and then extended for environmental analysis.

2.1. Methanol production from CO₂

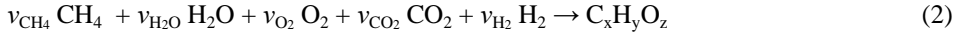
Methanol production from CO₂ has been evaluated both from a thermodynamic [4] and a simplified environmental [2] perspective, mostly for one particular reaction, namely:



Although reaction (1) is thermodynamically feasible, it might not be environmentally optimal. The following section will provide a graphical method to obtain an ecologically optimal scheme for the production of methanol. The approach is directly applicable to any other compound of the form C_xH_yO_z.

2.2. Obtaining an ecologically optimal reaction scheme

From a thermodynamic perspective, a reaction must fulfill the mass, energy and entropy (in terms of Gibbs energy) balances. Patel et al. [3] use these balance equations as constraints for a linear program (LP). We adopt the approach for the production of any compound of the form C_xH_yO_z at standard conditions (298K, 1 bar). The considered components (reactants or by-products) are limited to methane (CH₄), water (H₂O), oxygen (O₂), carbon dioxide (CO₂) and hydrogen (H₂):



The stoichiometric coefficient of the product C_xH_yO_z is always fixed to 1. The other components are reactants for negative and by-products for positive stoichiometric coefficients v_i . The mass, energy and entropy balances can be written as follows [3]:

$$0 = v_{\text{CH}_4} + v_{\text{CO}_2} + x \quad (3)$$

$$0 = 4 v_{\text{CH}_4} + 2 v_{\text{H}_2\text{O}} + 2 v_{\text{H}_2} + y \quad (4)$$

$$0 = v_{\text{H}_2\text{O}} + 2 v_{\text{O}_2} + 2 v_{\text{CO}_2} + z \quad (5)$$

$$\Delta h^{R,0} = \Delta h^{f,0}_{\text{C}_x\text{H}_y\text{O}_z} + \sum_i v_i \Delta h^{f,0}_i \leq 0 \quad (6)$$

$$\Delta g^{R,0} = \Delta g^{f,0}_{\text{C}_x\text{H}_y\text{O}_z} + \sum_i v_i \Delta g^{f,0}_i \leq 0 \quad (7)$$

In this work, a reaction with a minimal environmental impact is sought after. Since the focus of CCU is on greenhouse gas emissions, the method is exemplified using the GWP as an environmental impact category. Only the supply of the reactants is considered to contribute to the GWP of the reaction whereas no benefit, i.e. no avoided burden, is given to any of the by-products.

For the methanol example, the GWP values for CH₄, H₂O and O₂ are taken from the ecoinvent database [5] whereas those of CO₂ and H₂ are treated as variable. The resulting optimization problem can be formulated as follows:

$$\min \quad OF = - \sum_i v_i^R \text{GWP}_i \quad (8)$$

$$\text{s.t.} \quad (3) - (7) \quad \text{where} \quad v_i^R = \begin{cases} v_i, & \text{if } v_i < 0 \\ 0, & \text{if } v_i \geq 0 \end{cases} \quad (9)$$

Due to the discontinuity (9) of the objective function (OF), the problem is not an LP. A formulation as a mixed-integer linear program (MILP) is possible. However, it is insightful to decompose the solution space into regions with different, but continuous

OFs leading to several LPs. These regions are particularly conveniently determined by the graphical approach by Patel et al. [3] using so-called zero lines.

The procedure is demonstrated for the example of methanol synthesis where CO₂ and/or CH₄ act as potential carbon sources ($v_{\text{CH}_4} \leq 0$, $v_{\text{CO}_2} \leq 0$). Figure 1 shows the amount of H₂ produced or required as a function of the CO₂ amount used as feedstock. The zero lines represent stoichiometries with zero amounts of a certain compound ($v_i=0$), zero reaction enthalpy ($\Delta h^{R,0}=0$) or zero Gibbs energy ($\Delta g^{R,0}=0$). Here, the $\Delta h^{R,0}=0$ constraint (6) is dominated by the $\Delta g^{R,0} \leq 0$ constraint (7) due to a negative reaction entropy and is neglected for clarity in Figure 1.

The objective function OF_k is continuous within each region k bounded by the zero mass balance lines. In Figure 1, four reasonable regions ($k=1, \dots, 4$) exist, hence four LPs are solved. For example in region $k=3$, the following objective function is used:

$$OF_3 = - (v_{\text{CH}_4} \text{GWP}_{\text{CH}_4} + v_{\text{O}_2} \text{GWP}_{\text{O}_2} + v_{\text{CO}_2} \text{GWP}_{\text{CO}_2} + v_{\text{H}_2} \text{GWP}_{\text{H}_2}) \quad (11)$$

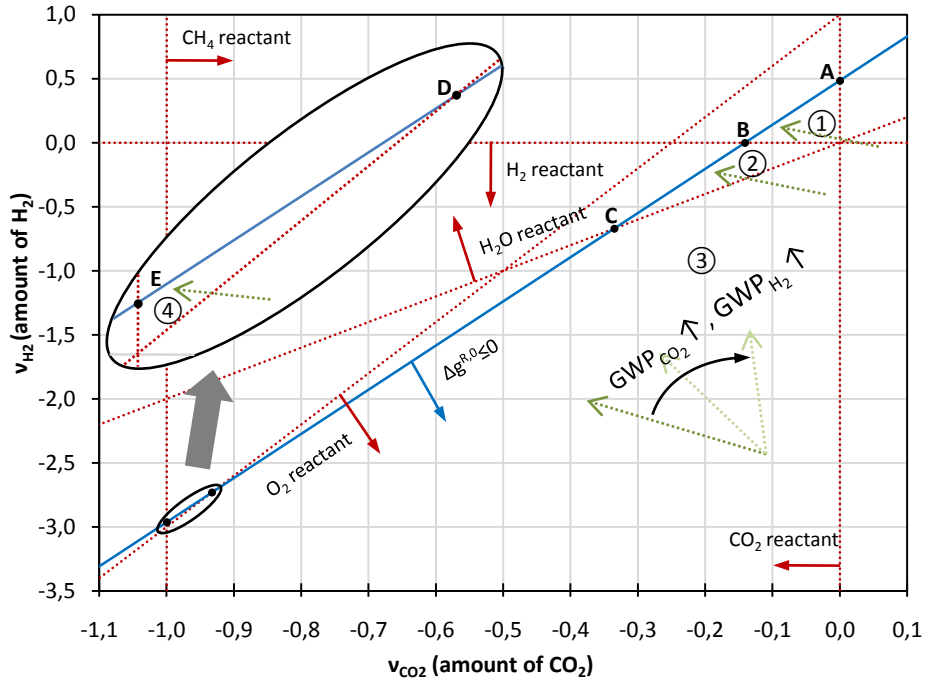


Figure 1: Solution space of (MI)LP for methanol synthesis with CO₂ as a potential feedstock. The (qualitative) dotted vectors pointing towards the regional optimal solution turn clockwise with increasing GWP values of CO₂ and H₂.

As for any LP, the optimal solution of every region is at a corner. A vector $\vec{n}_{OS,k}$ pointing towards the local (minimal) optimal solution (OS) can be defined as:

$$\vec{n}_{OS,k} = \begin{pmatrix} n_{OS,1,k} \\ n_{OS,2,k} \end{pmatrix} = \begin{pmatrix} -\partial OF / \partial v_{\text{CO}_2} \\ -\partial OF / \partial v_{\text{H}_2} \end{pmatrix} \quad (12)$$

For region 3, the vector $\vec{n}_{OS,3}$ is given by

$$\bar{n}_{OS,3} = \begin{pmatrix} \frac{\partial v_{CH_4}}{\partial v_{CO_2}} GWP_{CH_4} + \frac{\partial v_{O_2}}{\partial v_{CO_2}} GWP_{O_2} + GWP_{CO_2} \\ \frac{\partial v_{CH_4}}{\partial v_{H_2}} GWP_{CH_4} + \frac{\partial v_{O_2}}{\partial v_{H_2}} GWP_{O_2} + GWP_{H_2} \end{pmatrix} = \begin{pmatrix} -GWP_{CH_4} - 2GWP_{O_2} + GWP_{CO_2} \\ \frac{1}{2}GWP_{O_2} + GWP_{H_2} \end{pmatrix} \quad (13)$$

The global optimal solutions for given GWP values are obtained as follows: the vectors $\bar{n}_{OS,k}$ are plotted and the local optimal corners are identified. With the corners' reactant mixtures computed from (3) – (5), the objective function values OF_k (8) are compared to determine the global optimal solution.

2.3. Threshold values for the GWP of CO₂ and H₂

The GWP of CO₂ and H₂ are the critical factors in determining the environmental potential of a CCU scheme: How much additional CO₂ was produced in preparing the CO₂ feedstock? How was the – usually required – hydrogen produced? Most CCU proposals rely on projections about the future supply of the required feedstock. The presented graphical method allows for a convenient determination of GWP target values for future CO₂ capture and H₂ production technologies.

Eq. (13) shows, exemplary for k=3, that the vectors $\bar{n}_{OS,k}$ depend on the variable values GWP_{CO_2} and GWP_{H_2} . All vectors turn clockwise if GWP_{CO_2} or GWP_{H_2} increase. Only vector $\bar{n}_{OS,1}$ does not depend on GWP_{H_2} . This general behavior can be used to identify possible optimal corners. For example, the vector $\bar{n}_{OS,3}$ always points upwards in positive direction of v_{H_2} since $(\frac{1}{2} GWP_{O_2} + GWP_{H_2}) \geq 0$.

The optimal solution moves from its current to a neighboring corner if the vector $\bar{n}_{OS,k}$ is orthogonal to the zero-line connecting these corners. This condition is fulfilled if:

$$m_{zero-line} = -\frac{n_{OS,k,1}}{n_{OS,k,2}} = -\frac{\partial OF_k / \partial v_{CO_2}}{\partial OF_k / \partial v_{H_2}}, \quad (14)$$

where $m_{zero-line}$ denotes the slope of the zero line. The derivatives of the OF depend on the GWP_1 values. The GWP_1 values fulfilling Eq. (14) are called *local GWP threshold values* since values just below or above the threshold values result in different optimal solutions in a region k . For the two degrees of freedom (GWP_{CO_2} and GWP_{H_2}), it is convenient to compute threshold lines.

The procedure for obtaining global GWP threshold values is as follows: the potential local optimal corners are identified using (12) with variable values for GWP_{CO_2} and GWP_{H_2} . By applying (14) to the zero-lines that connect these corners, relations for the local GWP threshold values are derived. Whether these local values are also global threshold values can be checked in analogy to the procedure in 2.2.

3. Results

The proposed method is used to determine the global GWP threshold values for CH₃OH production. In this case, five global environmentally optimal solutions can be found in dependence of GWP_{CO_2} and GWP_{H_2} (corners A to E in Figure 1). Hence, four threshold lines can be computed, see Figure 2. If GWP_{CO_2} is above 0.276 kg CO₂eq./kg CO₂, the use of CO₂ as a feedstock for methanol synthesis is environmentally not advisable and methane should be employed as carbon source. If GWP_{CO_2} is below that value, it is always preferential to (partially) use CO₂ as a feedstock. How much CO₂ should be used, depends also on GWP_{H_2} , see Figure 2.

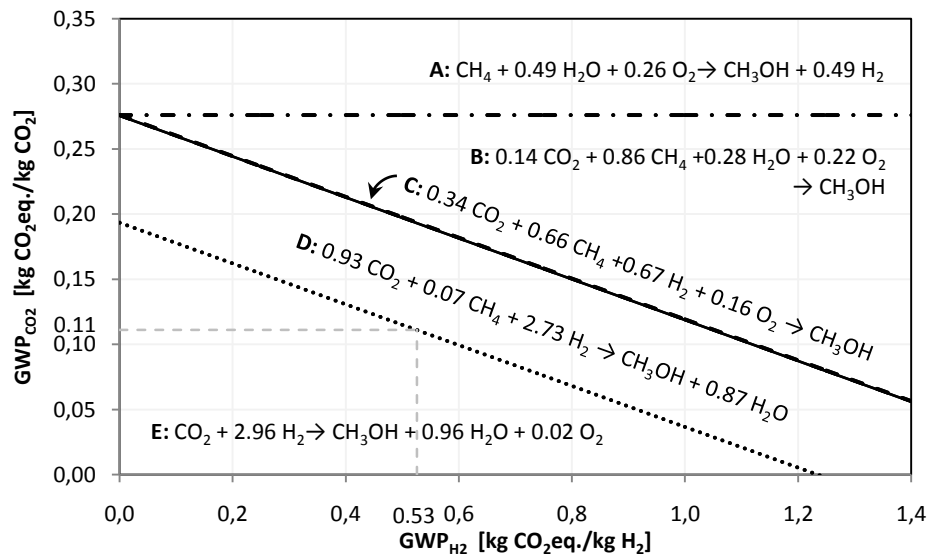


Figure 2: Environmentally optimal reactions as a function of the GWP of CO₂ and H₂.

Figure 2 can be used to define GWP targets for technologies. For example, in a power plant with a 90% CO₂ capture rate where all of the remaining 10% are allocated to the captured CO₂ stream, the GWP of CO₂ is 0.11 kg CO₂eq./kg CO₂ (=0.1/0.9). Please note that this allocation procedure provides a worst case value for GWP_{CO_2} . Still, with this worst case value, CO₂ should always be used as a feedstock. Moreover, CO₂ should be the only carbon source if GWP_{H_2} is below 0.53 kg CO₂eq./kg H₂.

4. Conclusions

Environmentally optimal reaction schemes for CCU can be obtained by introducing environmental impact coefficients into the process design framework by Patel et al. [3]. The resulting graphically-based targeting method gives further valuable insight into the process: threshold values for the GWP of CO₂ and H₂ can be derived that are tipping points between different reaction schemes. A worst case analysis shows that methanol production from CO₂ captured from power plants is a promising CCU scheme.

Acknowledgments

Niklas von der Assen and André Sternberg acknowledge financial support by the German Federal Ministry of Economics and Technology (ref. no.: 01RC1005B and 01RC1006B, respectively).

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