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# Structural and core parameters of the hot B subdwarf KPD 0629-0016 from CoRoT g-mode asteroseismology\*

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#### **ABSTRACT**

Context. The asteroseismic exploitation of long period, g-mode hot B subdwarf pulsators (sdBV<sub>s</sub>), undermined so far by limitations associated with ground-based observations, has now become possible, thanks to high quality data obtained from space such as those recently gathered with the CoRoT (COnvection, ROtation, and planetary Transits) satellite.

Aims. We propose a detailed seismic analysis of the  $sdBV_s$  star KPD 0629-0016, the first compact pulsator monitored with CoRoT, using the g-mode pulsations recently uncovered by that space-borne observatory during short run SRa03.

*Methods.* We use a forward modeling approach on the basis of our latest sdB models, which are now suitable for the accurate computation of the g-mode pulsation properties. The simultaneous match of the independent periods observed in KPD 0629-0016 with those of the models leads objectively to the identification of the pulsation modes and, more importantly, to the determination of the structural and core parameters of the star.

Results. The optimal model we found closely reproduces the 18 observed periods retained in our analysis at a 0.23% level on average. These are identified as low-degree ( $\ell=1$  and 2), intermediate-order (k=-9 through -74) g-modes. The structural and core parameters for KPD 0629-0016 are the following (formal fitting errors only):  $T_{\rm eff}=26\,290\pm530$  K,  $\log g=5.450\pm0.034$ ,  $M_*=0.471\pm0.002$   $M_{\odot}$ ,  $\log (M_{\rm env}/M_*)=-2.42\pm0.07$ ,  $\log (1-M_{\rm core}/M_*)=-0.27\pm0.01$ , and  $X_{\rm core}(C+O)=0.41\pm0.01$ . We additionally derive an age of  $42.6\pm1.0$  Myr after the zero-age extreme horizontal branch, the radius  $R=0.214\pm0.009$   $R_{\odot}$ , the luminosity  $L=19.7\pm3.2$   $L_{\odot}$ , the absolute magnitude  $M_V=4.23\pm0.13$ , the reddening index  $E(B-V)=0.128\pm0.023$ , and the distance  $d=1190\pm115$  pc.

Conclusions. The advent of high-precision time-series photometry from space with instruments like CoRoT now allows as demonstrated with KPD 0629-0016 the full exploitation of g-modes as deep probes of the internal structure of these stars, in particular for determining the mass of the convective core and its chemical composition.

Key words. stars: oscillations – stars: interiors – subdwarfs – stars: individual: KPD 0629-0016

### 1. Introduction

The asteroseismic exploitation of long period, g-mode hot B subdwarf pulsators (sdBV<sub>s</sub>) has been a long sought objective that was undermined, thus far, by the difficulty of obtaining sufficiently precise and continuous time-series data from the ground (see, e.g., Randall et al. 2006). Time-series photometry from space appears to be the only means for gathering well-constrained asteroseismic data for this type of star. The sdBV<sub>s</sub> stars are found in the cooler ( $T_{\rm eff} \lesssim 30\,000$  K) and less compact (log  $g \lesssim 5.6$ ) region in the effective temperature-surface gravity plane occupied by hot B subdwarfs. The latter cover the ranges of  $T_{\rm eff} = 20\,000$ –40 000 K and log g = 5.0–6.2, and are core-helium burning objects occupying the Extreme Horizontal Branch (EHB). Because the g-modes in hot B subdwarfs propagate mostly in the deep core (Charpinet et al. 2000), it has been hoped ever since their discovery (Green et al. 2003) that

the long-period pulsating B subdwarfs would reveal the internal structure of the deepest regions in stars of this type, including the thermonuclear furnace.

KPD 0629-0016 is one of the rare sdB stars identified in the CoRoT field with a confirmed pulsational nature (Koen & Green 2007). It was consequently selected as the primary target for the third short run in the Galactic anticenter direction (SRa03) scheduled in March 2010. The results of the ~24 day long outstanding CoRoT photometric observations are presented in Charpinet et al. (2010). A total of 17 gravity-type pulsations are clearly identified in the Fourier spectrum, with periods ranging from 2600 to 10 500 s and amplitudes between 0.25% and 0.024% of the mean star brightness (43.2 to 4.2 times the local noise level). In addition, seven possible peaks emerge with amplitudes in the range 0.020% and 0.024% (3.6–4.0 times the local noise). This CoRoT observation provides more modes than are typically detected for sdB stars from the ground and, more importantly, the frequencies of all uncovered q-modes are reliably measured. This paves the way for a detailed seismic analysis of KPD 0629-0016. In this article, we report on the results of such an analysis, only the second one exploiting g-modes in

<sup>\*</sup> The CoRoT space mission, launched on December 27th 2006, has been developed and is operated by CNES, with the contribution of Austria, Belgium, Brasil, ESA, Germany, and Spain.

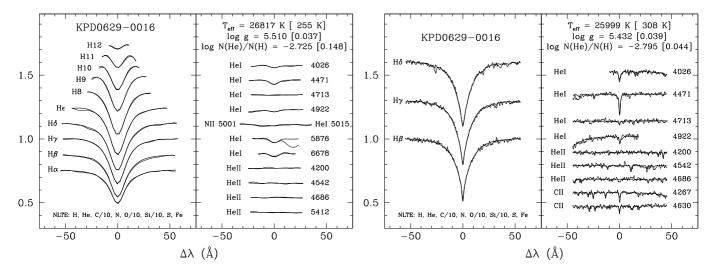


Fig. 1. Left panel: model fit (heavy curve) to all the hydrogen and strong helium lines (thin curve) available in our high S/N, low-resolution optical spectrum of KPD 0629-0016. The fit was done using a 3D grid of NLTE synthetic spectra ( $T_{\rm eff}$ , log g, log  $N({\rm He})/N({\rm H})$ ), in which the abundances of C, N, O, S, Si, and Fe were held fixed at amounts consistent with Blanchette et al. (2008). Right panel: similar, but for our intermediate-resolution MMT spectrum.

hot B subdwarfs after the very recent study of Van Grootel et al. (2010) on a similar object.

## 2. Atmospheric parameters from spectroscopy

Independent spectroscopic estimates for  $T_{\text{eff}}$  and  $\log g$  are essential constraints for lifting degeneracies encountered in seismic analyses of sdB pulsators (Charpinet et al. 2005). As part of a long-term program to characterize hot B subdwarfs in general, we had gathered a first spectrum of KPD 0629-0016 on 2002 September 26 using the Multiple Mirror Telescope on Mount Hopkins, Arizona. This spectrum, obtained with a total exposure time of 1000 s covers the wavelength range from ~4000 to ~5000 Å with a mean resolution of 1.05 Å and S/N~75. A mean spectrum was also built from eight low resolution (9.1 Å) spectra obtained with the Steward Observatory 2.3 m Bok Telescope from 2002 October 7 to 2003 November 30. This mean spectrum shows a high sensitivity  $(S/N \sim 310)$  and covers the spectral range from ~3600 to ~6900 Å. While the Bok mean spectrum is a true time-averaged measurement, this is not the case for the MMT data. Nevertheless, the amplitudes of the oscillations are so small (0.25% for the largest amplitude mode; Charpinet et al. 2010) that the MMT spectrum can still be considered as a useful indicator of the mean effective temperature and surface gravity.

We analyzed these two spectra with the help of new grids of NLTE model atmospheres and synthetic spectra developed for studying hot subdwarfs of the B and O types. These models were constructed with the public codes TLUSTY and SYNSPEC. In this application, we chose a representative heavy-element composition inspired from Blanchette et al. (2008). These authors used *FUSE* spectroscopy and suitable NLTE model spectra to determine the abundances of several astrophysically important elements in the atmospheres of five typical long-period pulsating sdB stars very similar to KPD 0629-0016. On the basis of their results, we assumed atmospheres containing C (1/10 solar), N (solar), O (1/10 solar), Si (1/10 solar), S (solar), and Fe (solar).

Figure 1 shows the best fits we have obtained. Weighted means of the two sets of atmospheric parameters according to

their formal errors lead to the following estimates for KPD 0629-0016:  $T_{\rm eff}=26\,484\pm196\,$  K, log  $g=5.473\pm0.027,$  and log  $N({\rm He})/N({\rm H})=-2.789\pm0.041.$  The quoted uncertainties are only formal errors of the fits and do not include systematic effects, which remain difficult to evaluate. These values of the atmospheric parameters have been used to guide the search for a seismic solution within a region of parameter space consistent with a  $3\sigma$  uncertainty range in effective temperature and surface gravity. To provide a measure of the effects of metals, we have refitted our two spectra using equivalent models with no metals. The weighted means now come out as  $T_{\rm eff}=26\,973\pm251\,$  K, log  $g=5.494\pm0.030,$  and log  $N({\rm He})/N({\rm H})=-2.758\pm0.044,$  indicating that the presence of metals (at least in the amounts assumed) is not a critical issue in the determination of the atmospheric parameters of KPD 0629-0016.

#### 3. Asteroseismic analysis

#### 3.1. Models and method

The forward modeling approach developed to perform objective asteroseismic studies of sdB pulsators has been described in detail in Charpinet et al. (2005, 2008). The basic principle is to fit simultaneously all observed pulsation periods with theoretical ones calculated from sdB models, in order to minimize in parameter space a merit function defined by

$$S^{2} = \sum_{i=1}^{N_{\text{obs}}} \left( P_{\text{obs}}^{i} - P_{\text{th}}^{i} \right)^{2}, \tag{1}$$

where  $N_{\rm obs}$  is the number of observed periods and  $\{P_{\rm obs}^i, P_{\rm th}^i\}$  are the associated pairs of observed/computed periods. Efficient optimization codes have been developed to explore the vast model parameter space and find the minima of the merit function  $S^2$ , which constitute the potential asteroseismic solutions. The results of this procedure are the mode identification and, more importantly, the structural parameters of the star.

In order to carry out quantitative seismology of g-mode pulsators, we developed "third-generation" (3G) models, suitable for the accurate evaluation of the g-mode pulsation periods.

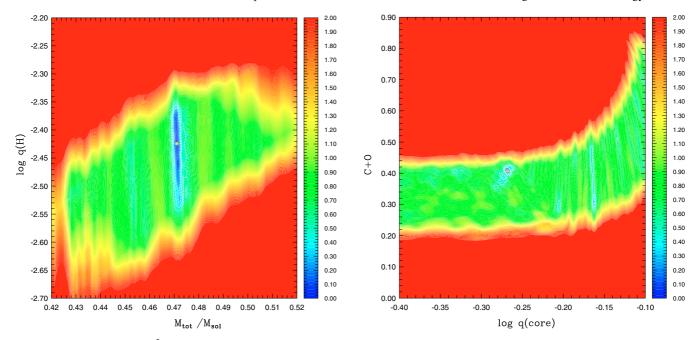


Fig. 2. Left panel: slice of the  $S^2$  function (in logarithmic units) along the  $M_*$ - log q(H) plane with the parameters log q(core) and  $X_{core}(C+O)$  set to the optimal values obtained for the best-fit seismic model. Right panel: slice of the  $S^2$  function (in log) along the log  $q(core) - X_{core}(C+O)$  plane with the parameters  $M_*$  and log q(H) set to their optimal values. White contours show regions where the period fits have  $S^2$  values within the  $1\sigma$ ,  $2\sigma$ , and  $3\sigma$  confidence level relative to the best-fit solution.

These are complete stellar structures in thermal equilibrium that include a detailed description of the central regions. Details about our 3G models are given in Brassard & Fontaine (2008, 2009). The input parameters needed to characterize a 3G model are (1) the total stellar mass  $M_*$ , (2) the fractional mass of the outer hydrogen-rich envelope  $\log (M_{\rm env}/M_*)$ , (3) the fractional mass of the mixed convective core  $\log (1 - M_{\rm core}/M_*)$ , and (4) the chemical composition of the core (under the constraint  $X({\rm He}) + X({\rm C}) + X({\rm O}) = 1$ ). These static parameterized structures offer much needed flexibility over evolutionary models for thoroughly exploring parameter space.

The effective temperature  $T_{\rm eff}$  and surface gravity  $\log g$  are computed a posteriori for a given 3G model. We then incorporate the atmospheric parameters determined by spectroscopy as external constraints in the optimization procedure for the search of a best-fit model. Only those models that have atmospheric parameter values within  $3\sigma$  of the spectroscopic estimates are considered acceptable, thus ensuring consistency with spectroscopy. In the specific case of KPD 0629-0016, acceptable solutions have to fall in the ranges of parameters defined by  $T_{\rm eff} = 26\,484 \pm 588\,{\rm K}$  and  $\log g = 5.473 \pm 0.123$ . Note that there is no guarantee, a priori, that a good period match exists within these constraints.

## 3.2. Search for the optimal model

The present seismic analysis is based on the frequencies uncovered by Charpinet et al. (2010) and presented in their Table 1. We selected the frequencies with amplitudes above or equal to 4 times the local noise level. Two out of these 20 pulsations, namely  $f_{10}$  and  $u_1$ , are very close to the higher amplitude peaks  $f_1$  and  $f_{16}$  and were consequently left aside. It is not clear at this stage if these close frequencies are associated with components of multiplets split by slow rotation (which is the usual case for single sdB stars) or with residual structure from the prewhitening of a dominant frequency whose amplitude and/or

phase experienced significant changes during the run. This is not critical for the present analysis and we decided to ignore them, leaving 18 pulsation modes that can be safely assumed to be independent, while still providing enough modes to tightly constrain the asteroseismic solution. Finally, the additional pulsation modes  $u_3$  to  $u_6$  (with amplitudes between 3.6 and 3.8 times the local noise) are neglected in the asteroseismic analysis that follows. We will discuss below how these additional frequencies may be interpreted and compared to the theoretical periods of the optimal model solution uncovered.

The search for best-fit solutions was carried out in a domain defined by  $0.30 \le M_*/M_\odot \le 0.70$ ,  $-5.0 \le \log q(\mathrm{H}) \equiv \log (M_{\mathrm{env}}/M_*) \le -1.8$ ,  $-0.45 \le \log q(\mathrm{core}) \equiv \log (1 - M_{\mathrm{core}}/M_*) \le -0.10$  and  $0 \le X_{\mathrm{core}}(\mathrm{C+O}) \le 0.99$ , where  $X_{\mathrm{core}}(\mathrm{C+O})$  is the fractional part (in mass) of carbon and oxygen in the convective core<sup>1</sup>. The ranges considered for  $\log q(\mathrm{H})$  and  $M_*$  rely on predictions from various hot subdwarf formation scenarios (see Han et al. 2002, 2003), whereas the limits on the size of the core are loosely inspired by horizontal branch stellar evolutionary calculations (Dorman et al. 1993). We considered all modes of degrees  $\ell = 1$  and 2 in the 2500 - 10 650 s period range in order to match the 18 pulsation periods retained for our analysis. These limits on the degree  $\ell$  correspond to the minimum value that can fully explain the observed mode density. No other assumption on the mode identification has been imposed.

The optimization code spotted one clear family of solutions with a minimum value of  $S^2$  corresponding to the following model:  $M_* = 0.4711~M_\odot$ ,  $\log q(\mathrm{H}) = -2.424$ ,  $\log q(\mathrm{core}) = -0.269$  and  $X_\mathrm{core}(\mathrm{C+O}) = 0.407$ . The computed atmospheric parameters for this model are  $T_\mathrm{eff} = 26\,290~\mathrm{K}$  and  $\log g = 5.450$ , in excellent agreement with the spectroscopic estimates, i.e, within the  $1\sigma$  averaged uncertainties (see Sect. 2). The maps shown in Fig. 2 illustrate the behavior of the  $S^2$  function in the vicinity of

<sup>&</sup>lt;sup>1</sup> The theoretical periods are not very sensitive to the exact core composition of C and O. In our experience, grouping (C+O) in one parameter facilitates and speeds up the optimization procedure.

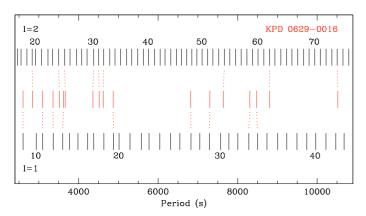
Table 1. Mode identification and details of the period fit obtained from the optimal model.

|  |    | k               | $ u_{ m obs}$ | $ u_{ m th}$ | $P_{ m obs}$ | $P_{th}$ | $\log E$ | $C_{kl}$ | $\Delta X/X$ | $\Delta P$ | Δν       | ID         |
|--|----|-----------------|---------------|--------------|--------------|----------|----------|----------|--------------|------------|----------|------------|
| 1  | Ü  | 10              |               |              |              |          |          | € KI     |              |            |          | ı          |
| 1 -10  | 1  | _9              |               |              |              |          |          | 0.4897   |              |            | •        | $f_7$      |
| 1  |    |                 |               |              |              |          |          |          |              |            |          | <i>J</i> / |
| 1       -12       298.009       297.466       3355.60       3361.72       45.256       0.4873       -0.18       -6.12       +0.543         1       -14        265.392        3768.02       45.650       0.4813       +0.32       +11.63       -0.893         1       -18        215.624        4637.71       44.275       0.4915            1       -19       205.289       205.204       4871.19       4873.20       43.685       0.4893       -0.04       -2.01       +0.085         1       -20        199.236        5019.17       43.792       0.4914            1       -26       1152.3791       152.704       16562.601       6548.64       43.783       0.4959       +0.211       [+13.96]       [-0.325]         1       -27       146.616       146.494       4820.56       8262.23       43.671       0.4959       -0.08       -5.68       +0.122         1       -29       136.966       137.201       730.08       728.85.6       43.659       0.4970       +0.17       +12.51       -0.235         1  |    |                 |               |              |              |          |          |          |              |            |          | $u_7$      |
| 1       -13       276.653       277.546       3614.64       3603.01       44.836       0.4835       +0.32       +11.63       -0.893         1       -14        265.392        3768.02       45.650       0.4818             1       -19       205.289       205.204       4871.19       4873.20       43.685       0.4893       -0.04       -2.01       +0.085         1       -20        199.236        5019.17       43.792       0.4914            1       -26       [152.379]       152.704       [6562.60]       6548.64       43.783       0.4959       [+0.21]       [+13.96]       [-0.325]         1       -26       [152.379]       152.704       [6562.60]       6548.64       43.786       0.4959       +0.21]       [+13.96]       [-0.325]         1       -27       146.616       146.494       6820.56       6826.23       43.671       0.4959       -0.08       -5.68       +0.122         1       -29       136.966       137.201       7301.08       7288.56       43.659       0.4970       +0.17       +12.51       -0.2  |    |                 |               |              |              |          |          |          |              |            |          | $f_5$      |
| 1       -14        265.392        3768.02       45.650       0.4818            1       -19       205.289       205.204       4871.19       4873.20       43.685       0.4893       -0.04       -2.01       +0.085         1       -20        199.236        5019.17       43.792       0.4914            1       -26       1152.3791       152.704       (6562.60)       6548.64       43.786       0.4959        -0.08       -5.68       +0.122         1       -26       1152.3791       152.704       (6562.60)       6548.64       43.786       0.4959        -0.08       -5.68       +0.122         1       -27       146.616       146.494       6820.56       6826.23       43.671       0.4959        -0.08       -5.68       +0.122         1       -29       136.966       137.201       7301.08       7288.56       43.659       0.4970       +0.17       +12.51       -0.235         1       -32        124.927        8004.68       43.381       0.4971       +0.17       +12.51       -0.235   |    |                 |               |              |              |          |          |          |              |            |          | $f_2$      |
| 1       -18        215.624        4637.71       44.275       0.4915  |    |                 |               |              |              |          |          |          |              |            |          | $J^2$      |
| 1       -19       205.289       205.204       4871.19       4873.20       43.685       0.4893       -0.04       -2.01       +0.085         1       -20        199.236        5019.17       43.792       0.4914            1       -25        158.446        6311.28       43.783       0.4954             1       -26       [152.379]       152.704       [6562.60]       6548.64       43.786       0.4959       [+0.21]       [+13.96]       [-0.325]         1       -27       146.616       146.494       6820.56       682.62.3       43.671       0.4959       -0.08       -5.68       +0.122         1       -29       136.966       137.201       7301.08       7288.56       43.659       0.4970       +0.17       +12.51       -0.235         1       -33       120.415       120.731       8304.59       8282.91       43.281       0.4971       +0.26       +21.68       -0.315         1       -33       120.415       120.731       8304.59       8282.91       43.281       0.4971       +0.26       421.68       -0.315  | •  | 11              | •••           | 203.372      | •••          | 3700.02  | 13.030   | 0.1010   | •••          | •••        | •••      |            |
| 1       -19       205.289       205.204       4871.19       4873.20       43.685       0.4893       -0.04       -2.01       +0.085         1       -20        199.236        5019.17       43.792       0.4914            1       -25        158.446        6311.28       43.783       0.4954             1       -26       [152.379]       152.704       [6562.60]       6548.64       43.786       0.4959       [+0.21]       [+13.96]       [-0.325]         1       -27       146.616       146.494       6820.56       682.62.3       43.671       0.4959       -0.08       -5.68       +0.122         1       -29       136.966       137.201       7301.08       7288.56       43.659       0.4970       +0.17       +12.51       -0.235         1       -33       120.415       120.731       8304.59       8282.91       43.281       0.4971       +0.26       +21.68       -0.315         1       -33       120.415       120.731       8304.59       8282.91       43.281       0.4971       +0.26       421.68       -0.315  | 1  | -18             |               | 215.624      |              | 4637.71  | 44.275   | 0.4915   |              |            |          |            |
| 1       -20        199.236        5019.17       43.792       0.4914            1       -25        158.446        6311.28       43.783       0.4954             1       -26       [152.379]       152.704       [6562.60]       6548.64       43.786       0.4959       [+0.21]       [+13.96]       [-0.325]         1       -27       146.616       146.494       6820.56       6826.23       43.671       0.4959       -0.08       -5.68       +0.122         1       -29       136.966       137.201       7301.08       7288.56       43.659       0.4970       +0.17       +12.51       -0.235         1       -32        124.927        8004.68       43.384       0.4971             1       -33       120.415       120.731       8304.59       8282.91       43.812       0.4971       +0.26       +21.68       -0.315         1       -34       177.966       177.599       847.01       8503.49       43.021       0.4959       -0.31       -21.68       +0.367 <td></td> <td><math>f_1</math></td>               |    |                 |               |              |              |          |          |          |              |            |          | $f_1$      |
| 1       -25        158.446        6311.28       43.783       0.4954            1       -26       [152.379]       152.704       [6562.60]       6548.64       43.786       0.4959       [+0.21]       [+13.96]       [-0.325]         1       -27       146.616       146.494       6820.56       6826.23       43.671       0.4959       -0.08       -5.68       +0.122         1       -29       136.966       137.201       7301.08       7288.56       43.659       0.4970       +0.17       +12.51       -0.235         1       -32        124.927        8004.68       43.384       0.4971            1       -33       120.415       120.731       8304.59       8282.91       43.281       0.4971       +0.26       +21.68       -0.315         1       -34       177.966       177.599       8477.01       8503.49       43.021       0.4959       -0.31       -26.48       +0.367         1       -35        114.420        8739.71       43.591       0.4972   |    |                 |               |              |              |          |          |          |              |            |          | JI         |
| 1       -26       [152.379]       152.704       [6562.60]       6548.64       43.786       0.4959       [+0.21]       [+13.96]       [-0.325]         1       -27       146.616       146.494       6820.53       6826.23       43.671       0.4959  | -  |                 |               | 177.200      |              | 0017117  | 2        | 0,1.     |              |            |          |            |
| 1       -26       [152.379]       152.704       [6562.60]       6548.64       43.786       0.4959       [+0.21]       [+13.96]       [-0.325]         1       -27       146.616       146.494       6820.56       6826.23       43.671       0.4959  | 1  | -25             |               | 158.446      |              | 6311.28  | 43.783   | 0.4954   |              |            |          |            |
| 1       -27       146.616       146.494       6820.56       6826.23       43.671       0.4959       -0.08       -5.68       +0.122         1       -28        141.851        7049.65       43.439       0.4950            1       -29       136.966       137.201       7301.08       7288.56       43.659       0.4970       +0.17       +12.51       -0.235         1       -32        124.927        8004.68       43.384       0.4971            1       -33       120.415       120.731       8304.59       8282.91       43.281       0.4971       +0.26       +21.68       -0.315         1       -34       177.966       177.599       8477.01       8503.49       43.021       0.4959       -0.31       -26.48       +0.367         1       -35        114.420        8739.71       43.191       0.4972            2       -17       [396.191]       391.954       [2524.04]       2551.32       43.976       0.1552       [-1.08]       [-27.28]       [+4.237]         2  |    |                 |               |              |              |          |          |          |              |            |          | $[u_4]$    |
| 1       -28        141.851        7049.65       43.439       0.4950          1       -29       136.966       137.201       7301.08       7288.56       43.659       0.4970       +0.17       +12.51       -0.235         1       -33       120.415       120.731       8304.59       8282.91       43.281       0.4971       +0.26       +21.68       -0.315         1       -34       177.966       177.599       8477.01       8503.49       43.021       0.4959       -0.31       -26.48       +0.367         1       -35        114.420        8739.71       43.191       0.4972 <td></td> <td><math>f_{15}</math></td>  |    |                 |               |              |              |          |          |          |              |            |          | $f_{15}$   |
| 1       -29       136.966       137.201       7301.08       7288.56       43.659       0.4970       +0.17       +12.51       -0.235         1       -32        124.927        8004.68       43.384       0.4971             1       -33       120.415       120.731       8304.59       8282.91       43.281       0.4971       +0.26       +21.68       -0.315         1       -34       177.966       177.599       8477.01       8503.49       43.021       0.4959       -0.31       -26.48       +0.367         1       -35        114.420        8739.71       43.191       0.4972 <td></td> <td>J 13</td>  |    |                 |               |              |              |          |          |          |              |            |          | J 13       |
| 1       -32        124.927        8004.68       43.384       0.4971            1       -33       120.415       120.731       8304.59       8282.91       43.281       0.4971       +0.26       +21.68       -0.315         1       -34       177.966       177.599       8477.01       8503.49       43.021       0.4959       -0.31       -26.48       +0.367         1       -35        114.420        8739.71       43.191       0.4972           2       -17       [396.191]       391.954       [2524.04]       2551.32       43.976       0.1552       [-1.08]       [-27.28]       [+4.237]         2       -18        370.111        2701.89       44.255       0.1583             2       -18        370.111        2701.89       44.255       0.1583             2       -23       [302.22]       299.272       [3308.82]       3341.45       43.822       0.1583       [-0.99]       [-32.62]       [+2.951]  |    |                 |               |              |              |          |          |          |              |            |          | $f_{13}$   |
| 1       -33       120.415       120.731       8304.59       8282.91       43.281       0.4971       +0.26       +21.68       -0.315         1       -34       177.966       177.599       8477.01       8503.49       43.021       0.4959       -0.31       -26.48       +0.367         1       -35        114.420        8739.71       43.191       0.4972            2       -17       [396.191]       391.954       [2524.04]       2551.32       43.976       0.1552       [-1.08]       [-27.28]       [+4.237]         2       -18        370.111        2701.89       44.255       0.1583           2       -19       352.292       353.294       2838.56       2830.51       43.665       0.1557       +0.28       +8.05       -1.002         2       -23       [302.222]       299.272       [3308.82]       3341.45       43.822       0.1583          1.2951]         2       -24       284.585       286.067       3513.89       3495.69       44.289       0.1622       +0.52       +18.20       -1.482   |    |                 |               |              |              |          |          |          |              |            |          | J 13       |
| 1       -34       177.966       177.599       8477.01       8503.49       43.021       0.4959       -0.31       -26.48       +0.367         1       -35        114.420        8739.71       43.191       0.4972            2       -17       [396.191]       391.954       [2524.04]       2551.32       43.976       0.1552       [-1.08]       [-27.28]       [+4.237]         2       -18        370.111        2701.89       44.255       0.1583             2       -19       352.292       353.294       2838.56       2830.51       43.665       0.1557       +0.28       +8.05       -1.002         2       -23       [302.222]       299.272       [3308.82]       3341.45       43.822       0.1583       [-0.99]       [-32.62]       [+2.951]         2       -24       284.585       286.067       3513.89       3495.69       44.289       0.1622       +0.52       +18.20       -1.482         2       -25       273.074       273.360        4213.19       43.653       0.1637   |    |                 |               |              |              |          |          |          |              |            |          | $f_{14}$   |
| 1       -35        114.420        8739.71       43.191       0.4972            2       -17       [396.191]       391.954       [2524.04]       2551.32       43.976       0.1552       [-1.08]       [-27.28]       [+4.237]         2       -18        370.111        2701.89       44.255       0.1583            2       -19       352.292       353.294       2838.56       2830.51       43.665       0.1557       +0.28       +8.05       -1.002         2       -23       [302.222]       299.272       [3308.82]       3341.45       43.822       0.1583       [-0.99]       [-32.62]       [+2.951]         2       -24       284.585       286.067       3513.89       3495.69       44.289       0.1622       +0.52       +18.20       -1.482         2       -25       273.074       273.962       3662.01       3650.14       43.901       0.1611       +0.32       +11.87       -0.888         2       -29        237.350        4213.19       43.653       0.1637 </td <td></td> <td><math>f_{16}</math></td> |    |                 |               |              |              |          |          |          |              |            |          | $f_{16}$   |
| 2       -17       [396.191]       391.954       [2524.04]       2551.32       43.976       0.1552       [-1.08]       [-27.28]       [+4.237]         2       -18        370.111        2701.89       44.255       0.1583            2       -19       352.292       353.294       2838.56       2830.51       43.665       0.1557       +0.28       +8.05       -1.002         2       -23       [302.222]       299.272       [3308.82]       3341.45       43.822       0.1583       [-0.99]       [-32.62]       [+2.951]         2       -24       284.585       286.067       3513.89       3495.69       44.289       0.1622       +0.52       +18.20       -1.482         2       -25       273.074       273.962       3662.01       3650.14       43.901       0.1611       +0.32       +11.87       -0.888         2       -29        237.350        4213.19       43.653       0.1637            2       -30       229.328       228.508       4360.57       4376.21       43.491       0.1635       -0.36       -15.64       +0.819   |    |                 |               |              |              |          |          |          |              |            |          | J 10       |
| 2       -18        370.111        2701.89       44.255       0.1583            2       -19       352.292       353.294       2838.56       2830.51       43.665       0.1557       +0.28       +8.05       -1.002         2       -23       [302.222]       299.272       [3308.82]       3341.45       43.822       0.1583       [-0.99]       [-32.62]       [+2.951]         2       -24       284.585       286.067       3513.89       3495.69       44.289       0.1622       +0.52       +18.20       -1.482         2       -25       273.074       273.962       3662.01       3650.14       43.901       0.1611       +0.32       +11.87       -0.888         2       -29        237.350        4213.19       43.653       0.1637            2       -30       229.328       228.508       4360.57       4376.21       43.491       0.1635       -0.36       -15.64       +0.819         2       -31       221.300       222.274       4518.74       4498.96       43.134       0.1616       +0.44       +19.78       -0.973   | -  |                 |               | 1120         |              | 0,0,1,1  | .0.171   | 0, 2     |              |            |          |            |
| 2       -18        370.111        2701.89       44.255       0.1583            2       -19       352.292       353.294       2838.56       2830.51       43.665       0.1557       +0.28       +8.05       -1.002         2       -23       [302.222]       299.272       [3308.82]       3341.45       43.822       0.1583       [-0.99]       [-32.62]       [+2.951]         2       -24       284.585       286.067       3513.89       3495.69       44.289       0.1622       +0.52       +18.20       -1.482         2       -25       273.074       273.962       3662.01       3650.14       43.901       0.1611       +0.32       +11.87       -0.888         2       -29        237.350        4213.19       43.653       0.1637            2       -30       229.328       228.508       4360.57       4376.21       43.491       0.1635       -0.36       -15.64       +0.819         2       -31       221.300       222.274       4518.74       4498.96       43.134       0.1616       +0.44       +19.78       -0.973   | 2  | -17             | [396.191]     | 391.954      | [2524.04]    | 2551.32  | 43.976   | 0.1552   | [-1.08]      | [-27.28]   | [+4.237] | $[u_3]$    |
| 2       -19       352.292       353.294       2838.56       2830.51       43.665       0.1557       +0.28       +8.05       -1.002         2       -23       [302.222]       299.272       [3308.82]       3341.45       43.822       0.1583       [-0.99]       [-32.62]       [+2.951]         2       -24       284.585       286.067       3513.89       3495.69       44.289       0.1622       +0.52       +18.20       -1.482         2       -25       273.074       273.962       3662.01       3650.14       43.901       0.1611       +0.32       +11.87       -0.888         2       -29        237.350        4213.19       43.653       0.1637            2       -30       229.328       228.508       4360.57       4376.21       43.491       0.1635       -0.36       -15.64       +0.819         2       -31       221.300       222.274       4518.74       4498.96       43.134       0.1616       +0.44       +19.78       -0.973         2       -32       216.529       216.145       4618.32       4626.53       43.376       0.1638          .   |    |                 |               |              |              |          |          |          |              |            |          | . 33       |
| 2       -23       [302.222]       299.272       [3308.82]       3341.45       43.822       0.1583       [-0.99]       [-32.62]       [+2.951]         2       -24       284.585       286.067       3513.89       3495.69       44.289       0.1622       +0.52       +18.20       -1.482         2       -25       273.074       273.962       3662.01       3650.14       43.901       0.1611       +0.32       +11.87       -0.888         2       -29        237.350        4213.19       43.653       0.1637             2       -30       229.328       228.508       4360.57       4376.21       43.491       0.1635       -0.36       -15.64       +0.819         2       -31       221.300       222.274       4518.74       4498.96       43.134       0.1616       +0.44       +19.78       -0.973         2       -32       216.529       216.145       4618.32       4626.53       43.376       0.1638       -0.18       -8.20       +0.384         2       -33        208.898        4787.04       43.288       0.1638   |    |                 |               |              |              |          |          |          |              |            |          | $f_3$      |
| 2       -24       284.585       286.067       3513.89       3495.69       44.289       0.1622       +0.52       +18.20       -1.482         2       -25       273.074       273.962       3662.01       3650.14       43.901       0.1611       +0.32       +11.87       -0.888         2       -29        237.350        4213.19       43.653       0.1637            2       -30       229.328       228.508       4360.57       4376.21       43.491       0.1635       -0.36       -15.64       +0.819         2       -31       221.300       222.274       4518.74       4498.96       43.134       0.1616       +0.44       +19.78       -0.973         2       -32       216.529       216.145       4618.32       4626.53       43.376       0.1638       -0.18       -8.20       +0.384         2       -33        208.898        4787.04       43.288       0.1638            2       -53        132.921        7523.27       42.928       0.1652            2 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><math>[u_6]</math></td></td<>        |    |                 |               |              |              |          |          |          |              |            |          | $[u_6]$    |
| 2       -25       273.074       273.962       3662.01       3650.14       43.901       0.1611       +0.32       +11.87       -0.888         2       -29        237.350        4213.19       43.653       0.1637            2       -30       229.328       228.508       4360.57       4376.21       43.491       0.1635       -0.36       -15.64       +0.819         2       -31       221.300       222.274       4518.74       4498.96       43.134       0.1616       +0.44       +19.78       -0.973         2       -32       216.529       216.145       4618.32       4626.53       43.376       0.1638       -0.18       -8.20       +0.384         2       -33        208.898        4787.04       43.288       0.1638            2       -34       [204.996]       203.452       [4878.15]       4915.16       43.021       0.1626            2       -53        132.921        7523.27       42.928       0.1652            2       -54   |    |                 |               |              |              |          |          |          |              |            |          | $f_9$      |
| 2       -29        237.350        4213.19       43.653       0.1637            2       -30       229.328       228.508       4360.57       4376.21       43.491       0.1635       -0.36       -15.64       +0.819         2       -31       221.300       222.274       4518.74       4498.96       43.134       0.1616       +0.44       +19.78       -0.973         2       -32       216.529       216.145       4618.32       4626.53       43.376       0.1638       -0.18       -8.20       +0.384         2       -33        208.898        4787.04       43.288       0.1638            2       -34       [204.996]       203.452       [4878.15]       4915.16       43.021       0.1626            2       -53        132.921        7523.27       42.928       0.1652            2       -54       130.879       130.472       7640.62       7664.49       42.851       0.1652       -0.31       -23.87       +0.408         2       -60   |    |                 |               |              |              |          |          |          |              |            |          | $f_6$      |
| 2       -30       229,328       228,508       4360,57       4376,21       43.491       0.1635       -0.36       -15.64       +0.819         2       -31       221,300       222,274       4518,74       4498,96       43.134       0.1616       +0.44       +19.78       -0.973         2       -32       216,529       216,145       4618,32       4626,53       43.376       0.1638       -0.18       -8.20       +0.384         2       -33        208,898        4787,04       43.288       0.1638             2       -34       [204,996]       203,452       [4878,15]       4915,16       43.021       0.1626             2       -53        132,921        7523,27       42,928       0.1652            2       -54       130,879       130,472       7640,62       7664,49       42,851       0.1652            2       -60       [117,219]       117,458       [8531,00]       8513,71       42,872       0.1656 <td></td> <td>30</td>   |    |                 |               |              |              |          |          |          |              |            |          | 30         |
| 2       -30       229,328       228,508       4360,57       4376,21       43.491       0.1635       -0.36       -15.64       +0.819         2       -31       221,300       222,274       4518,74       4498,96       43.134       0.1616       +0.44       +19.78       -0.973         2       -32       216,529       216,145       4618,32       4626,53       43.376       0.1638       -0.18       -8.20       +0.384         2       -33        208,898        4787,04       43.288       0.1638             2       -34       [204,996]       203,452       [4878,15]       4915,16       43.021       0.1626             2       -53        132,921        7523,27       42,928       0.1652            2       -54       130,879       130,472       7640,62       7664,49       42,851       0.1652            2       -60       [117,219]       117,458       [8531,00]       8513,71       42,872       0.1656 <td>2</td> <td>-29</td> <td></td> <td>237.350</td> <td></td> <td>4213.19</td> <td>43.653</td> <td>0.1637</td> <td></td> <td></td> <td></td> <td></td>   | 2  | -29             |               | 237.350      |              | 4213.19  | 43.653   | 0.1637   |              |            |          |            |
| 2       -31       221.300       222.274       4518.74       4498.96       43.134       0.1616       +0.44       +19.78       -0.973         2       -32       216.529       216.145       4618.32       4626.53       43.376       0.1638       -0.18       -8.20       +0.384         2       -33        208.898        4787.04       43.288       0.1638            2       -34       [204.996]       203.452       [4878.15]       4915.16       43.021       0.1626            2       -53        132.921        7523.27       42.928       0.1652            2       -54       130.879       130.472       7640.62       7664.49       42.851       0.1652       -0.31       -23.87       +0.408         2       -60       [117.219]       117.458       [8531.00]       8513.71       42.872       0.1656             2       -62       113.597       113.635       8803.02       8800.10       42.771       0.1655       +0.03       +2.92       -0.038   | 2  |                 |               |              | 4360.57      | 4376.21  |          |          |              |            |          | $f_8$      |
| 2       -32       216.529       216.145       4618.32       4626.53       43.376       0.1638       -0.18       -8.20       +0.384         2       -33        208.898        4787.04       43.288       0.1638             2       -34       [204.996]       203.452       [4878.15]       4915.16       43.021       0.1626             2       -53        132.921        7523.27       42.928       0.1652             2       -54       130.879       130.472       7640.62       7664.49       42.851       0.1652             2       -60       [117.219]       117.458       [8531.00]       8513.71       42.872       0.1656             2       -61        115.481        8659.42       42.858       0.1656             2       -62       113.597       113.635       8803.02       8800.10       42.771       0.1655       +0  |    |                 |               |              |              |          |          |          |              |            |          | $u_2$      |
| 2       -33        208.898        4787.04       43.288       0.1638  |    |                 | 216.529       |              |              |          |          |          |              |            |          | $f_4$      |
| 2     -34     [204.996]     203.452     [4878.15]     4915.16     43.021     0.1626          2     -53      132.921      7523.27     42.928     0.1652          2     -54     130.879     130.472     7640.62     7664.49     42.851     0.1652     -0.31     -23.87     +0.408       2     -60     [117.219]     117.458     [8531.00]     8513.71     42.872     0.1656          2     -61      115.481      8659.42     42.858     0.1656          2     -62     113.597     113.635     8803.02     8800.10     42.771     0.1655     +0.03     +2.92     -0.038       2     -73      96.431      10370.06     42.766     0.1659          2     -74     95.088     95.174     10516.56     10507.11     42.786     0.1659     +0.09     +9.45     -0.086       4     -44      288.089      3471.15     43.086     0.0482          4     -45     [  | 2  | -33             |               | 208.898      |              | 4787.04  | 43.288   |          |              |            |          |            |
| 2       -53        132.921        7523.27       42.928       0.1652            2       -54       130.879       130.472       7640.62       7664.49       42.851       0.1652       -0.31       -23.87       +0.408         2       -60       [117.219]       117.458       [8531.00]       8513.71       42.872       0.1656            2       -61        115.481        8659.42       42.858       0.1656             2       -62       113.597       113.635       8803.02       8800.10       42.771       0.1655       +0.03       +2.92       -0.038         2       -73        96.431        10370.06       42.766       0.1659            2       -74       95.088       95.174       10516.56       10507.11       42.786       0.1659       +0.09       +9.45       -0.086         4       -44        288.089        3471.15       43.086       0.0482            4       -  |    |                 | [204.996]     |              | [4878.15]    | 4915.16  |          |          |              |            |          | $[f_{10}]$ |
| 2     -54     130.879     130.472     7640.62     7664.49     42.851     0.1652     -0.31     -23.87     +0.408       2     -60     [117.219]     117.458     [8531.00]     8513.71     42.872     0.1656          2     -61      115.481      8659.42     42.858     0.1656          2     -62     113.597     113.635     8803.02     8800.10     42.771     0.1655     +0.03     +2.92     -0.038       2     -73      96.431      10370.06     42.766     0.1659          2     -74     95.088     95.174     10516.56     10507.11     42.786     0.1659     +0.09     +9.45     -0.086       4     -44      288.089      3471.15     43.086     0.0482          4     -45     [284.069]     281.688     [3520.27]     3550.02     42.964     0.0480  |    |                 |               |              |              |          |          |          |              |            |          |            |
| 2       -60       [117.219]       117.458       [8531.00]       8513.71       42.872       0.1656             2       -61        115.481        8659.42       42.858       0.1656             2       -62       113.597       113.635       8803.02       8800.10       42.771       0.1655       +0.03       +2.92       -0.038         2       -73        96.431        10370.06       42.766       0.1659            2       -74       95.088       95.174       10516.56       10507.11       42.786       0.1659       +0.09       +9.45       -0.086         4       -44        288.089        3471.15       43.086       0.0482            4       -45       [284.069]       281.688       [3520.27]       3550.02       42.964       0.0480  | 2  | -53             |               | 132.921      |              | 7523.27  | 42.928   | 0.1652   |              |            |          |            |
| 2       -60       [117.219]       117.458       [8531.00]       8513.71       42.872       0.1656             2       -61        115.481        8659.42       42.858       0.1656            2       -62       113.597       113.635       8803.02       8800.10       42.771       0.1655       +0.03       +2.92       -0.038         2       -73        96.431        10370.06       42.766       0.1659             2       -74       95.088       95.174       10516.56       10507.11       42.786       0.1659       +0.09       +9.45       -0.086         4       -44        288.089        3471.15       43.086       0.0482            4       -45       [284.069]       281.688       [3520.27]       3550.02       42.964       0.0480  | 2  | -54             | 130.879       | 130.472      | 7640.62      | 7664.49  | 42.851   | 0.1652   | -0.31        | -23.87     | +0.408   | $f_{11}$   |
| 2       -61        115.481        8659.42       42.858       0.1656  |    |                 |               |              |              |          |          |          |              |            |          |            |
| 2       -61        115.481        8659.42       42.858       0.1656             2       -62       113.597       113.635       8803.02       8800.10       42.771       0.1655       +0.03       +2.92       -0.038         2       -73        96.431        10370.06       42.766       0.1659             2       -74       95.088       95.174       10516.56       10507.11       42.786       0.1659       +0.09       +9.45       -0.086         4       -44        288.089        3471.15       43.086       0.0482            4       -45       [284.069]       281.688       [3520.27]       3550.02       42.964       0.0480   | 2  | -60             | [117.219]     | 117.458      | [8531.00]    | 8513.71  | 42.872   | 0.1656   |              |            |          | $[u_1]$    |
| 2     -62     113.597     113.635     8803.02     8800.10     42.771     0.1655     +0.03     +2.92     -0.038       2     -73      96.431      10370.06     42.766     0.1659          2     -74     95.088     95.174     10516.56     10507.11     42.786     0.1659     +0.09     +9.45     -0.086       4     -44      288.089      3471.15     43.086     0.0482          4     -45     [284.069]     281.688     [3520.27]     3550.02     42.964     0.0480  | 2  | -61             |               | 115.481      |              | 8659.42  | 42.858   | 0.1656   |              |            |          |            |
| 2     -73      96.431      10370.06     42.766     0.1659          2     -74     95.088     95.174     10516.56     10507.11     42.786     0.1659     +0.09     +9.45     -0.086       4     -44      288.089      3471.15     43.086     0.0482          4     -45     [284.069]     281.688     [3520.27]     3550.02     42.964     0.0480   |    | -62             | 113.597       |              | 8803.02      | 8800.10  |          |          |              |            | -0.038   | $f_{12}$   |
| 2 -74 95.088 95.174 10516.56 10507.11 42.786 0.1659 +0.09 +9.45 -0.086<br>4 -44 288.089 3471.15 43.086 0.0482<br>4 -45 [284.069] 281.688 [3520.27] 3550.02 42.964 0.0480   |    |                 |               |              |              |          |          |          |              |            |          |            |
| 2 -74 95.088 95.174 10516.56 10507.11 42.786 0.1659 +0.09 +9.45 -0.086<br>4 -44 288.089 3471.15 43.086 0.0482<br>4 -45 [284.069] 281.688 [3520.27] 3550.02 42.964 0.0480   | 2  | -73             |               | 96.431       |              | 10370.06 | 42.766   | 0.1659   |              |            |          |            |
| 4 -45 [284.069] 281.688 [3520.27] 3550.02 42.964 0.0480  |    | -74             | 95.088        | 95.174       | 10516.56     | 10507.11 | 42.786   | 0.1659   |              | +9.45      | -0.086   | $f_{17}$   |
| 4 -45 [284.069] 281.688 [3520.27] 3550.02 42.964 0.0480  |    |                 |               |              |              |          |          |          |              |            |          |            |
|  | 4  | -44             |               | 288.089      |              | 3471.15  | 43.086   | 0.0482   |              |            |          |            |
|  | 4  | -45             | [284.069]     | 281.688      | [3520.27]    | 3550.02  | 42.964   | 0.0480   |              |            |          | $[u_5]$    |
| 4 –46 276.149 3621.24 42.916 0.0479  | _4 | <del>-4</del> 6 |               | 276.149      |              | 3621.24  | 42.916   | 0.0479   |              |            |          |            |

the best-fit seismic solution. In both panels, the merit function  $S^2$  incorporates the spectroscopic constraints on atmospheric parameters, namely, an exponential correction factor multiplies the merit function if the model effective temperature and surface gravity are outside the averaged  $3\sigma$  spectroscopic uncertainties. This degrades in effect the  $S^2$  value of the model, and corresponds to regions in red in Fig. 2.

## 3.3. Period fit and mode identification

The details on the fit of the observed periods  $P_{\rm obs}$  to the theoretical values  $P_{\rm th}$  are given in Table 1. The table also lists along with the mode identification (degree  $\ell$  and radial order k) the logarithm of the kinetic energy  $\log E$  and the dimensionless Ledoux coefficient  $C_{\rm kl}$ . The optimal model isolated for KPD



**Fig. 3.** Distribution of the 18 observed periods of KPD 0629-0016 compared to the  $\ell=1$  and  $\ell=2$  g-mode theoretical pulsation spectrum of the optimal model. The radial order k of the computed modes is indicated for each series of degree  $\ell$ .

0629-0016 can account for the 18 observed pulsations to within 0.23%, which corresponds to an averaged absolute dispersion of  $\overline{\Delta P}=11.75$  s and  $\overline{\Delta \nu}=0.53~\mu{\rm Hz}$ . The standard deviations on these quantities are 7.67 s and 0.41  $\mu{\rm Hz}$  respectively. This excellent agreement, graphically represented in Fig. 3, is comparable to the best results obtained on  $p{\rm -mode}$  sdB pulsators, and is equivalent to the fit quality achieved for the  $g{\rm -mode}$  pulsator KPD 1943+4058 (Van Grootel et al. 2010). The 18 observed periods retained in our analysis are identified as low-degree ( $\ell=1$  and 2), intermediate-order (k=-9 through -74)  $g{\rm -modes}$ .

The presence of excited pulsation modes in sdB stars is understood by the action of a  $\kappa$ -effect associated with an opacity bump caused by partial ionization of heavy metals - especially iron - that are locally enhanced by radiative levitation at work in the envelope (Charpinet et al. 2001; Fontaine et al. 2003). Although our current models fairly well match the instability strip observed for the short-period p-mode pulsators, there is a well known discrepancy for the g-mode pulsators that remains to be solved (Charpinet et al. 2007). Beyond iron, the importance of nickel for the opacity profiles, as well as the opacity sources themselves (OPAL vs. OP), have been underlined by Jeffery & Saio (2006, 2007; see also Hu et al. 2009). It is likely that the radiative levitation of at least nickel, in addition to iron, has to be included in our next generation of sdB models (which we currently work on) in order to evaluate more accurately the stability of the modes and reconcile the theoretical and observed q-mode instability domain.

It is interesting to see how the additional frequencies may be compared to the theoretical periods of the seismic model. The pulsation modes  $u_3$ ,  $u_4$  and  $u_6$  (with amplitudes between 3.6 and 3.8 times the local noise) can find a corresponding mode in the  $\ell=1$  and  $\ell=2$  series without significantly degrading the fit (see details in Table 1). The left-aside  $f_{10}$ ,  $u_1$  and  $u_5$  frequencies could possibly be associated with the  $(\ell,k)=(2,-34),(2,-60)$  and (4,-45) modes respectively, but their origins are uncertain given their proximity to higher amplitude peaks. Better resolution data would definitely provide more information about them.

#### 3.4. Structural and core parameters

Table 2 summarizes the properties of KPD 0629-0016 inferred from the spectroscopic and seismic analyses. The quoted  $1\sigma$  uncertainties are the formal errors of the fit and do not include external and systematic errors. In particular, they assume perfect

Table 2. Structural and core parameters inferred for KPD 0629-0016.

| Quantity                        | Estimated Value       |
|---------------------------------|-----------------------|
| $T_{\rm eff}$ (K)               | $26484 \pm 196^{1}$   |
|                                 | $26290 \pm 530^2$     |
| $\log g$                        | $5.473 \pm 0.027^{1}$ |
|                                 | $5.450 \pm 0.034^2$   |
| $M_*/M_{\odot}$                 | $0.471 \pm 0.002$     |
| $\log(M_{\rm env}/M_*)$         | $-2.42 \pm 0.07$      |
| $\log(1-M_{\rm core}/M_*)$      | $-0.27 \pm 0.01$      |
| $M_{ m core}/M_{\odot}$         | $0.22 \pm 0.01$       |
| $X_{\rm core}({\rm C+O})$       | $0.41 \pm 0.01$       |
|                                 |                       |
| Age (Myr)                       | $42.6 \pm 1.0^3$      |
| $R/R_{\odot}$ $(M_*, g)$        | $0.214 \pm 0.009$     |
| $L/L_{\odot}$ $(T_{\rm eff},R)$ | $19.7 \pm 3.2$        |
| $M_V(g, T_{\rm eff}, M_*)$      | $4.23 \pm 0.13$       |
| E(B-V)                          | $0.128 \pm 0.023$     |
| $d(V, M_V)$ (pc)                | $1190 \pm 115$        |
|                                 |                       |

**Notes.** <sup>(1)</sup> From spectroscopy; <sup>(2)</sup> From asteroseismology <sup>(3)</sup> Since zeroage EHB.

input physics for the models. These uncertainties are represented in Fig. 2 by white dashed contours  $(1\sigma, 2\sigma \text{ and } 3\sigma \text{ limits, assuming that the } S^2 \text{ has a chi-squared distribution)}$  around the solution indicated by a yellow mark. The uncertainties on the derived atmospheric parameters  $T_{\text{eff}}$  and  $\log g$  are obtained from the uncertainties of the primary quantities. A set of secondary parameters (stellar radius R, luminosity L, absolute magnitude  $M_V$ , reddening index E(B-V), and distance from Earth d) is also derived on the basis of primary parameters.

The structural parameters inferred for KPD 0629-0016 indicate a "typical" sdB star, whose stellar mass and envelope thickness are close to the expected values for hot B subdwarfs (Dorman et al. 1993a; Han et al. 2002, 2003). The most interesting feature is the determination of the helium-burning core properties, including size and composition, thanks to the sensitivity of g-modes to the deep regions of the star. The mixed convective core (whose boundary is defined by the chemical transition He/C/O-He) includes 46% of the total mass of the star, after it has burned a little over 40% of its helium nuclear fuel. This size is slightly above the expectations based on evolutionary tracks with pure convective core defined by the Schwarzschild criterion (Dorman et al. 1993a). Van Grootel et al. (2010) also found the same in a different star. This may be an indication of the presence of overshooting and/or semi-convection, or any process that is able to carry out the (C+O) material beyond the convection zone itself. One of our long-term goals is to test the convection-related theories in hot B subdwarfs (Dorman et al. 1993b; Straniero et al. 2003). Finally, a comparison with an evolutionary sequence built on the same input physics for a star with similar structural and core parameters (including a moderate mechanical overshooting) indicates an age of  $42.6 \pm 1.0$  Myr after the zero-age extreme horizontal branch.

# 4. Conclusion

This article reported on the detailed asteroseismic analysis of the long-period, g-mode hot B subdwarf pulsator KPD 0629-0016. This has been made possible thanks to the outstanding light curve obtained by CoRoT in March 2010. For only the second time (see Van Grootel et al. 2010), a successful seismic analysis of a sdBV<sub>s</sub> star has been carried out. In both cases,

space observations have proven essential for the exploitation of *g*-mode seismology for this type of star. This new era in hot B subdwarfs seismology permits us the investigation of heliumburning cores – including their size and composition – along with the determination of structural parameters of the star. Our results suggest that overshooting and semiconvection are important processes that shape the helium-burning cores. Since all helium-burning cores share very similar characteristics, pulsating B subdwarfs are excellent probes of the interior properties of horizontal branch stars in general, an intermediate and underrated stage of stellar evolution.

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