

International Conference on Recent Advances in Nonlinear Models  
Structural Concrete Applications – CoRAN 2011

# **Structural behavior of concrete columns under natural fires including cooling down phase**

**T. GERNAY & M.S. DIMIA**

# Context

1. Context
2. Concrete Model
3. Column Analysis
4. Conclusion

## Collapse during the cooling phase

*Concrete structure subjected to natural fire*

*No failure at the time of temperature peak*

Is there a risk of **delayed collapse**?



Windsor Building – Madrid 2005

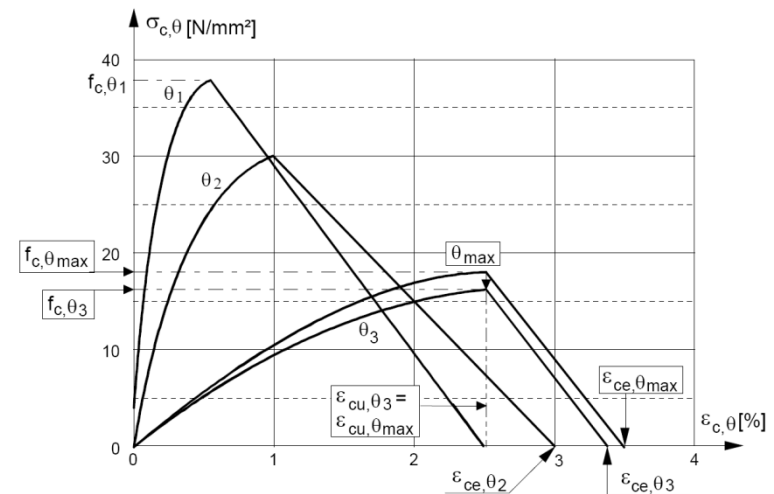
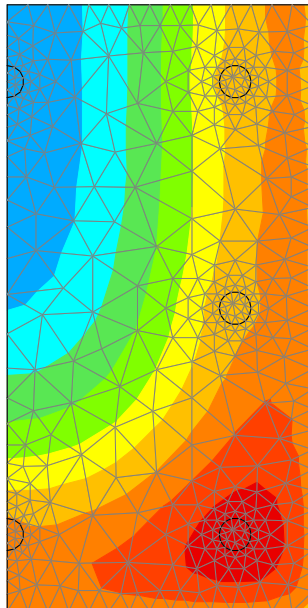
# Context

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## ➤ Possibility of occurrence

- ❑ The temperatures in the structure continue increasing thermal inertia → concrete

- ❑ Material behavior  
EN 1994-1-2 fig. C 2  
loss of strength → concrete



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## ➤ Possible consequence

- ☐ Collapse during the cooling phase: threat for the fire fighters
- ☐ Collapse after the cooling phase: time of first inspection!

⇒ There is a risk of delayed collapse for RC structures exposed to natural fire

# Context

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## Analysis on the risk of delayed collapse

- Performance-based analysis
  - ❑ Verification of the structural integrity at the time of maximum gas temperature does not guarantee against delayed collapse
- Insight into the concrete material law
  - ❑ Validation for the numerical analysis under natural fire
- Numerical analysis of concrete columns in natural fire
  - ❑ Conditions that lead to collapse during or after the cooling phase

# Material Models

1. Context
2. **Concrete Model**
3. Column Analysis
4. Conclusion

## Material models for the numerical analysis

- Steel and concrete
- Key for the validity of the numerical simulations
- Capture the material behavior during heating and cooling
- Thermal properties → EN 1994-1-2

# Material Models

1. Context
- 2. Concrete Model**
3. Column Analysis
4. Conclusion

## ➤ Mechanical properties for steel

- ☐ According to EN 1994-1-2
- ☐ Reversible properties (recovered during cooling)

## ➤ Mechanical properties for concrete

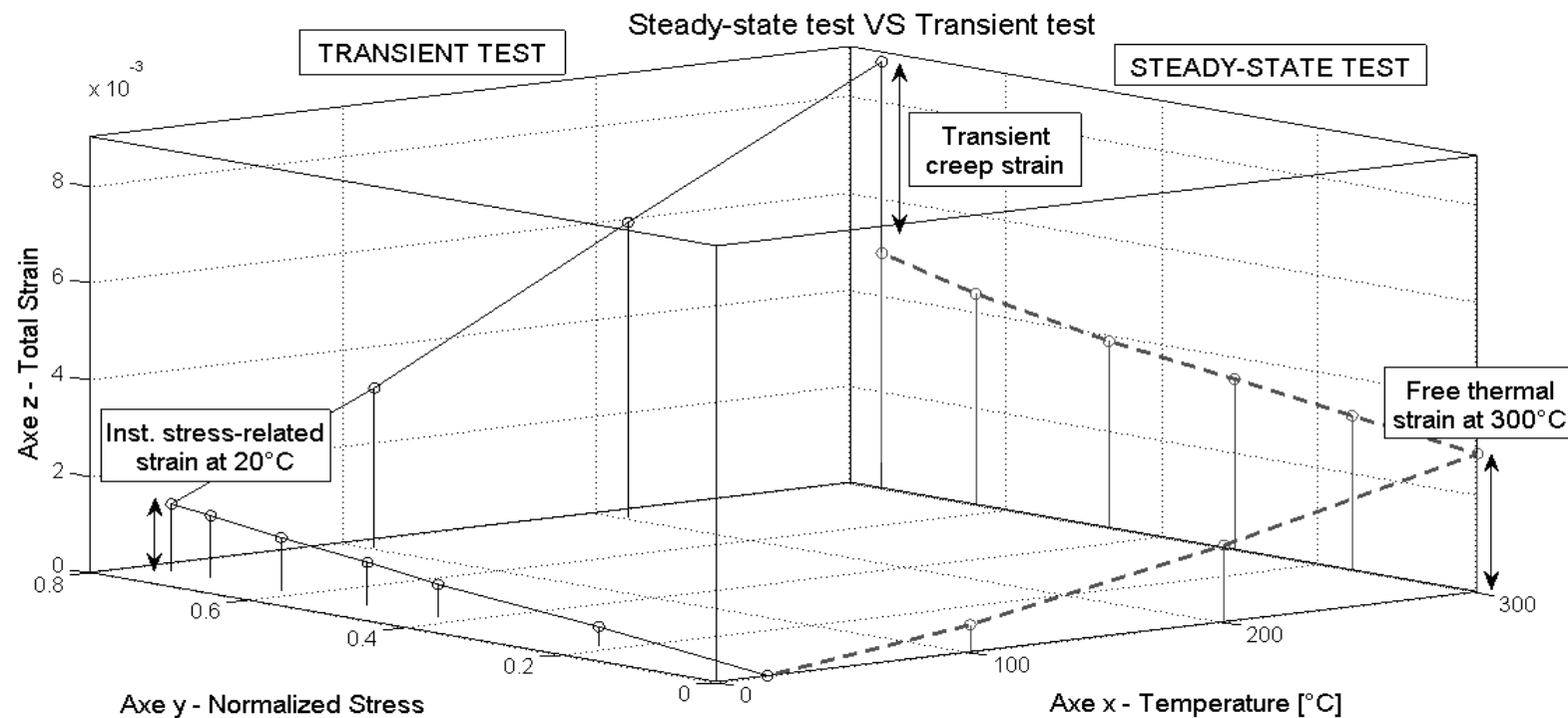
- ☐ Compressive strength of concrete not recovered during cooling  
Additional loss of 10% [EN 1994-1-2 ; Yi-Hai & Franssen 2011]
- ☐ Transient creep strain develops and is irrecoverable

# Concrete Model

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2. **Concrete Model**
3. Column Analysis
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## What is Transient Creep Strain?

- TCS develops in **concrete** that is (first-time) **heated under stress**





# Concrete Model

1. Context
- 2. Concrete Model**
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## 2 types of TCS model

Explicit models:  $\varepsilon_{tot} = \varepsilon_{th} + \varepsilon_{\sigma} + \varepsilon_{tr}$

TCS depends on the “history”

TCS = permanent strain

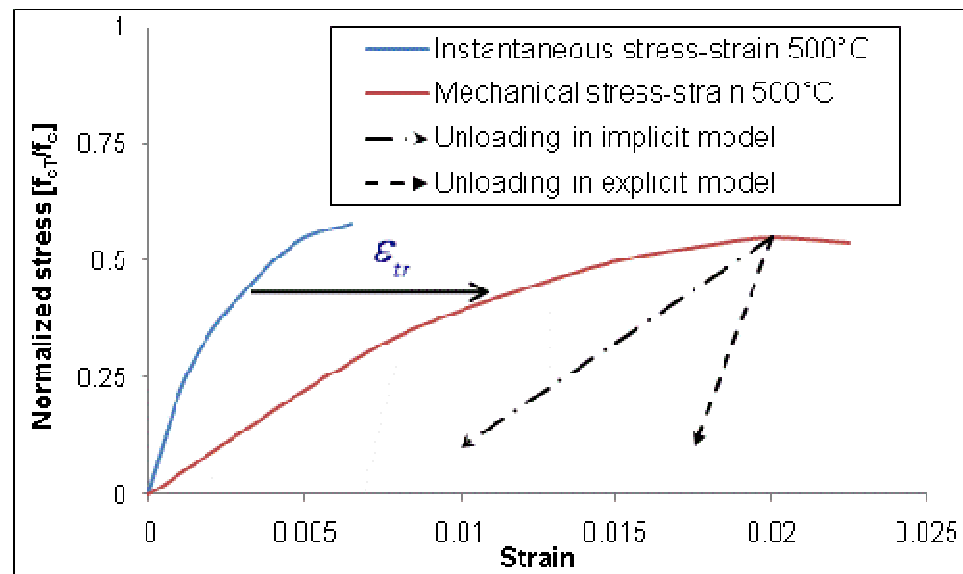
→ Actual unloading stiffness

Implicit models:  $\varepsilon_{tot} = \varepsilon_{th} + \varepsilon_m$

Univocal at given temperature

TCS, not known, is recovered

→ “Apparent” unloading stiffness



# Concrete Model

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- 2. Concrete Model**
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## ➤ Assets of the Eurocode 2 concrete model

- ☐ Generic model
- ☐ Proposed by experts, well accepted by authorities
- ☐ Widely used, good results for prescriptive design (ISO fire)

## ➤ Limitations of the EC2 model

- ☐ Implicit model for TCS → validity for performance-based analysis?

⇒ Reformulate the EC2 model with an explicit term for TCS

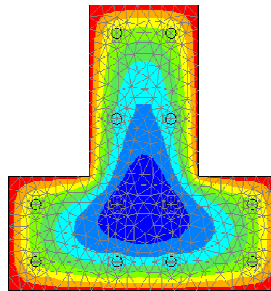
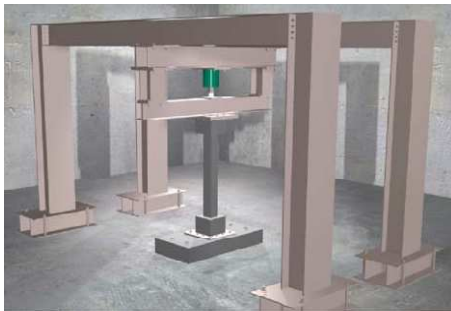
⇒ Explicit Transient Creep Model (ETC) developed and implemented in SAFIR

# Concrete Model

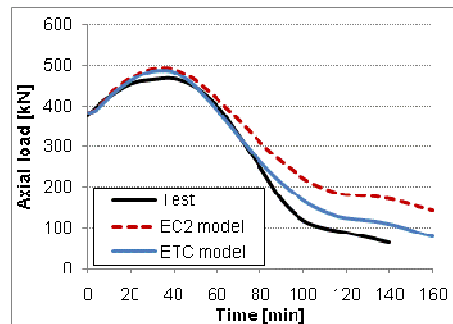
1. Context
2. **Concrete Model**
3. Column Analysis
4. Conclusion

## ➤ Experimental validation of ETC model

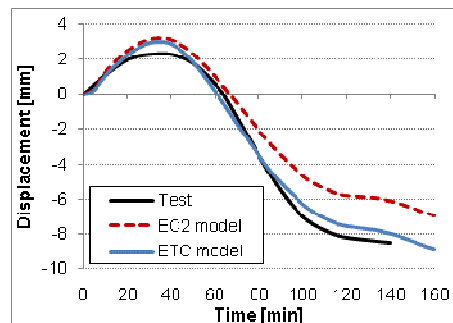
- ❑ RC columns subjected to heating and cooling [Wu et al., 2010]



**Axially restrained RC columns**  
**Load 375 kN (ratio 0.34)**  
**Axial restraint 34.5 MN/m**  
**Heating during 90 minutes**



**Axial load response**



**Deformation response**

## SAFIR analysis with EC2 and ETC

Difference in unloading stiffness

EC2 model → TCS is recovered

⇒ Explicit model of TCS needed for performance-based analysis

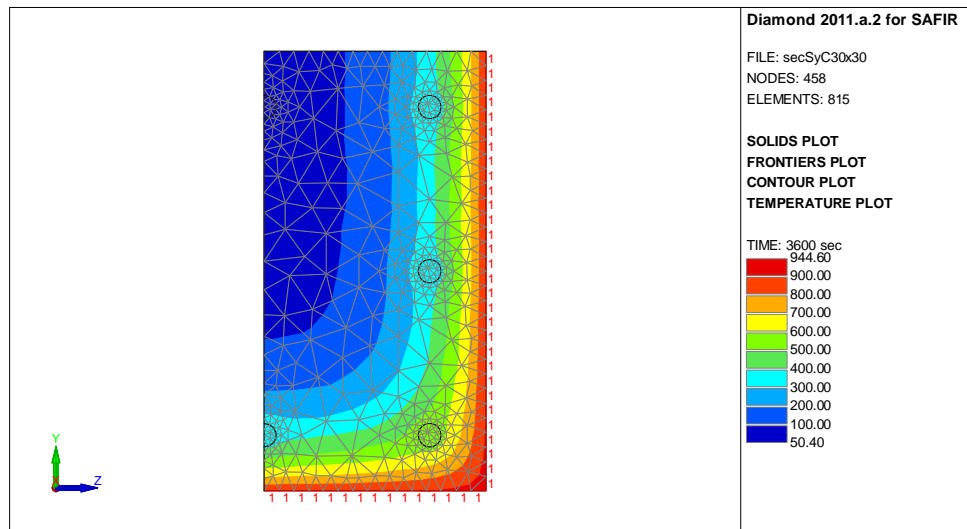
# Column Analysis

1. Context
2. Concrete Model
- 3. Column Analysis**
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## Delayed collapse: study case

### ➤ Structural concrete columns

- ❑ Section 300 x 300 mm<sup>2</sup> with 8  $\Phi$ 16 steel rebars
- ❑ Simply supported column of 4 m length
- ❑ Sinusoidal imperfection  $L/300$



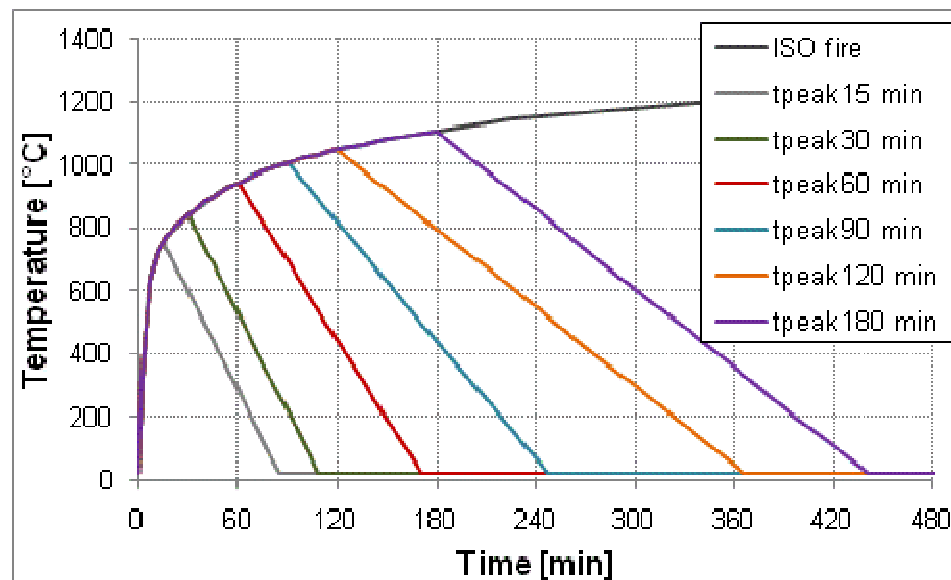
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## Delayed collapse: study case

### ➤ Natural fire curves

- ❑ Parametric fire model Annex A EN1991-1-2
- ❑ Factor  $\Gamma = 1$  for heating phase corresponding to ISO834

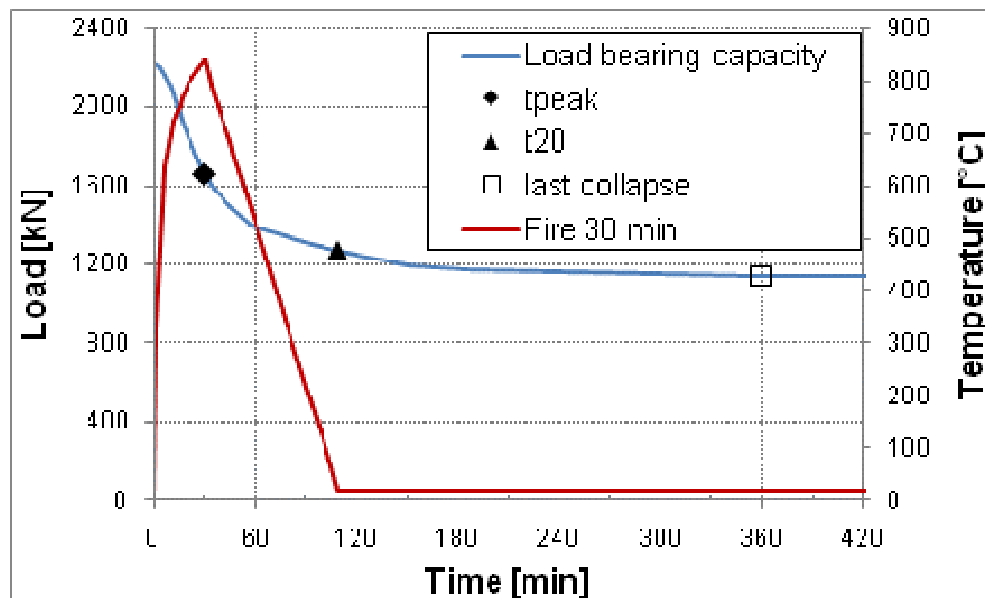


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1. Context
2. Concrete Model
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## Delayed collapse: numerical results

- Load bearing capacity of the column (fire 30 min)
  - ❑ Continue decreasing after the time of maximum gas temperature
  - ❑ Possibility of delayed collapse: + 4 hours after the end of the fire

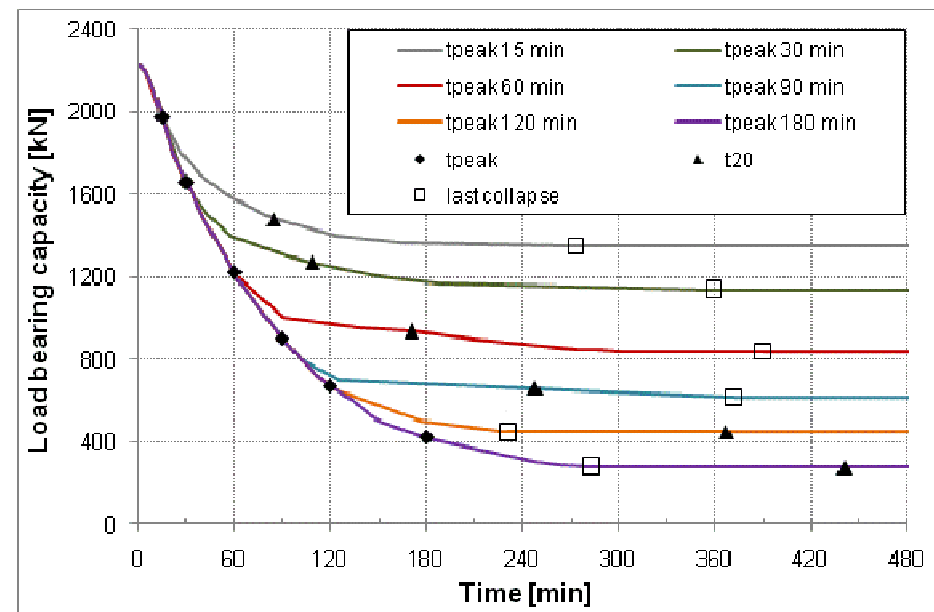
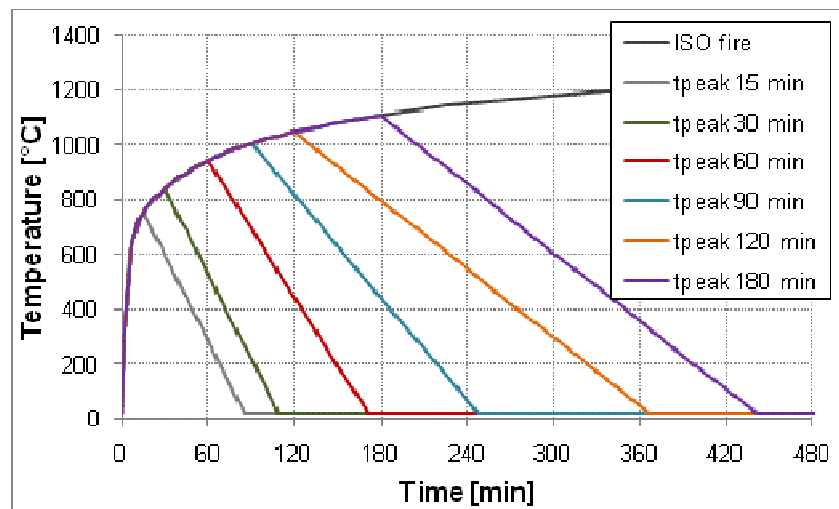


load 1200 kN  
→ collapse after 165 min

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4. Conclusion

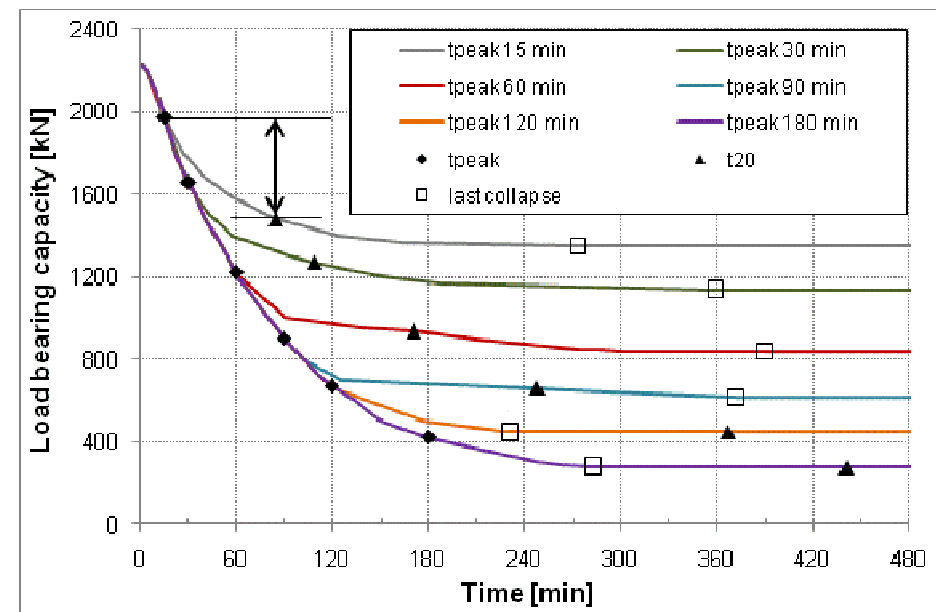
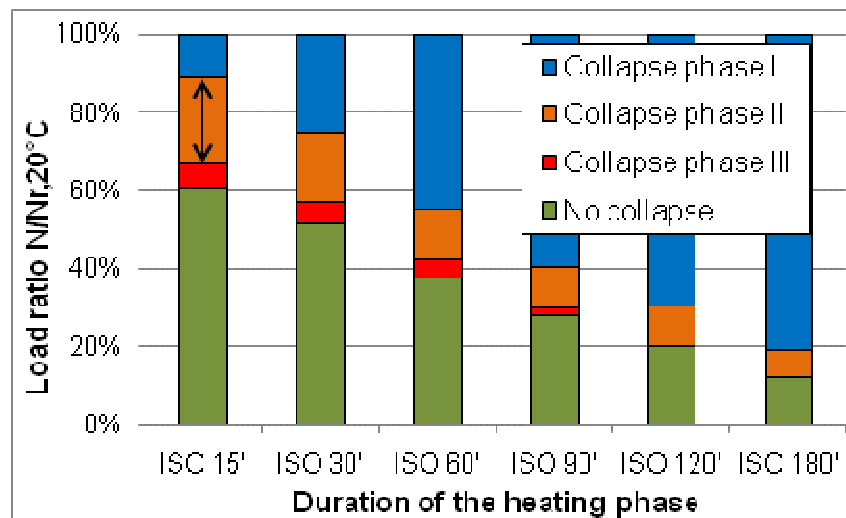
- Possibility of occurrence increases for shorter fire
  - ❑ Collapse during the cooling phase: observed for every fire duration
  - ❑ Collapse after the cooling phase: only for heating phase  $\leq 90$  min
  - ❑ Effect of thermal inertia of the section



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4. Conclusion

- Possibility of occurrence increases for shorter fire
  - ❑ Other presentation of the results
  - ❑ The relative range of loads that leads to delayed collapse decreases when the fire duration increases

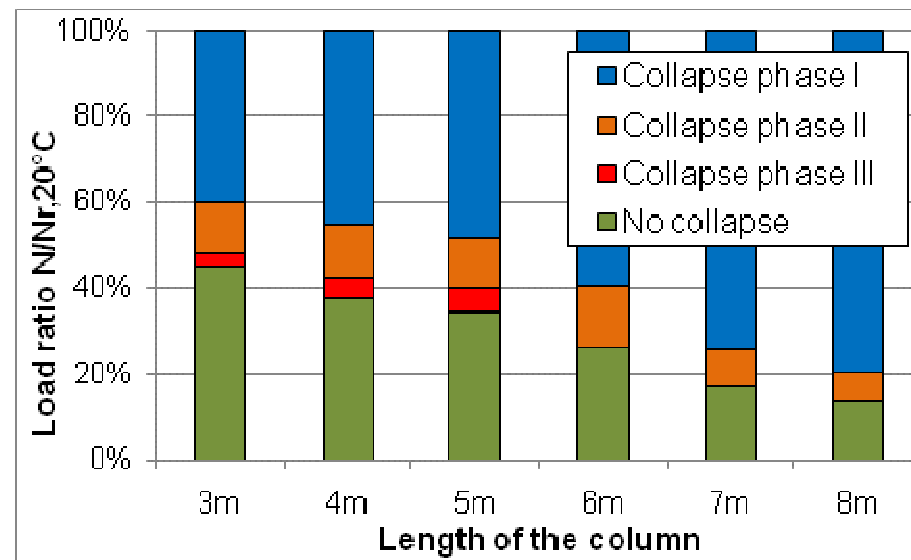




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2. Concrete Model
- 3. Column Analysis**
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- Possibility of occurrence increases for low slenderness
  - ❑ Columns with high slenderness: effect of thermal gradient exceeds effect of variation of neutral axis position  
During cooling: lateral displacement decreases
  - ❑ However, collapse during the cooling phase always observed

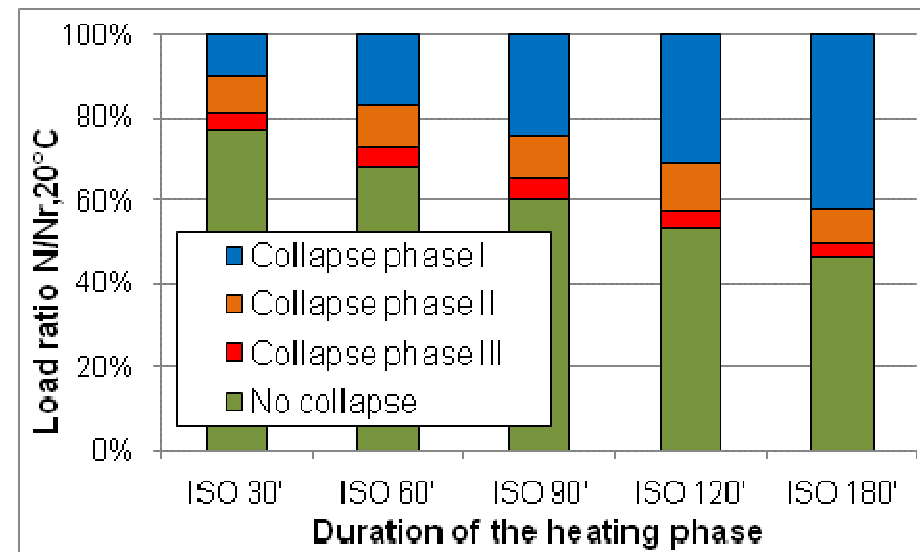
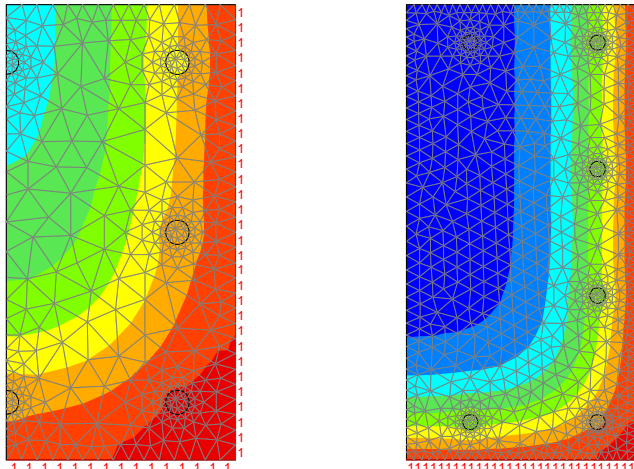


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1. Context
2. Concrete Model
- 3. Column Analysis**
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- Possibility of occurrence increases for wider section
  - ❑ Wider section = lower slenderness
  - ❑ Moreover, effect of thermal inertia increases for wider section

300x300 → 600x600

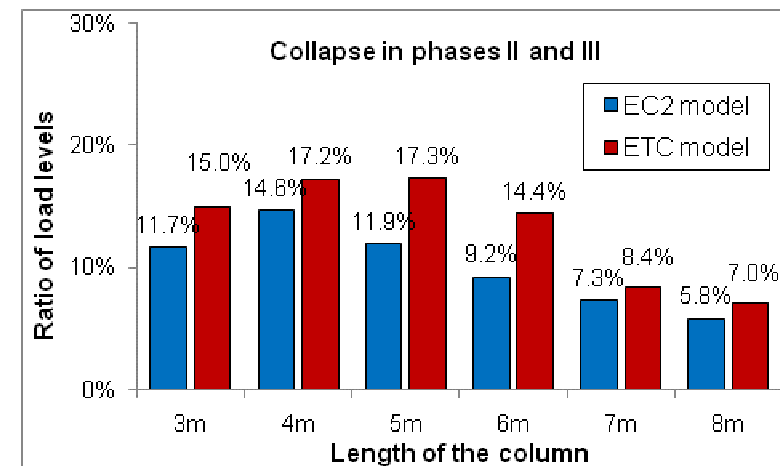
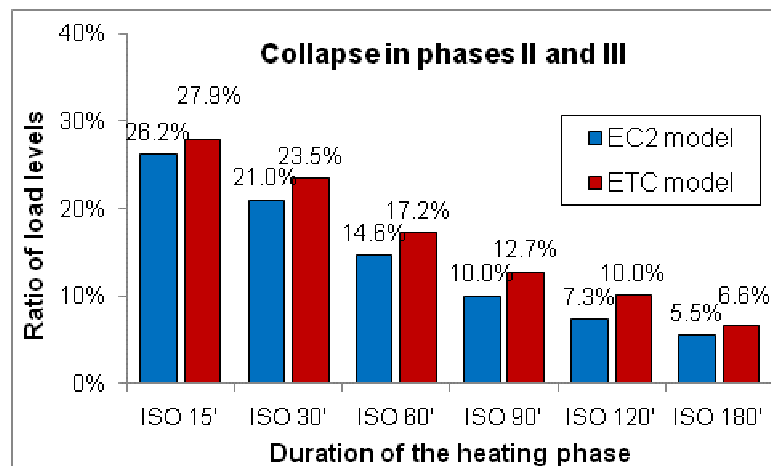


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## ➤ Effect of the concrete material model

- ❑ x % is the percentage of load ratio that leads to delayed collapse (sum of orange and red zones)



- ❑ Numerical analysis performed with ETC concrete model predict more occurrence of delayed collapse than with EC2 model

# Conclusion

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- Concrete constitutive law
  - ❑ Validated material models required (including for cooling)
  - ❑ Transient Creep Strain irrecoverable → explicit models
  - ❑ The ETC model has been developed and implemented in SAFIR
- Structural behavior of RC columns subjected to natural fire
  - ❑ Load bearing capacity continue decreasing during and after the cooling phase of the fire
  - ❑ Structural failure possible several hours after the end of the fire
  - ❑ Risk ↑ because consequence ↑↑↑

# Conclusion

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2. Concrete Model
3. Column Analysis
- 4. Conclusion**

- Occurrence of delayed collapse increases for:
  - ❑ Short fires
  - ❑ Columns with low slenderness (short length – massive section)
  - ❑ Predicted more often with the ETC concrete model than with EC2
- Futures works
  - ❑ Columns with axial and/or rotational restraint (frames)
  - ❑ Experimental basis

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**Thank you for your kind attention**

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